## Attachment A Air Quality Technical Documents

## A-1 CalEEMod Outputs

River Oaks Marketplace - Sacramento County, Annual

## River Oaks Marketplace

Sacramento County, Annual

### 1.0 Project Characteristics

### 1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Other Asphalt Surfaces | 3.24 | Acre | 3.24 | 141,134.40 | 0 |
| Parking Lot | 109.00 | Space | 0.98 | 43,600.00 | 0 |
| Fast Food Restaurant with Drive Thru | 4.50 | 1000sqft | 0.10 | 4,500.00 | 0 |
| Fast Food Restaurant with Drive Thru | 0.88 | 1000sqft | 0.02 | 880.00 | 0 |
| Convenience Market With Gas Pumps | 4.65 | 1000sqft | 0.11 | 4,650.00 | 0 |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 3.5 | Precipitation Freq (Days) |
| :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 6 |  | Operational Year |  |

### 1.3 User Entered Comments \& Non-Default Data

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| Project Characteristics - Assume power is SMUD |  |  |
| :---: | :---: | :---: |
| Land Use - based on RFI |  |  |
| Construction Phase - based on RFI |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - Arch coat only |  |  |
| Off-road Equipment - |  |  |
| Grading - acre graded based on entire site size |  |  |
| Trips and VMT - from RFI or default if unknown |  |  |
| Vehicle Trips - NO VMT complete because the project size is exempt from CEQA VMT analysis. Trips based on traffic memo |  |  |
| Construction Off-road Equipment Mitigation - No Haul trucks. BMPs require twice daily watering. Tier 4 Final ran, if applicable |  |  |
| Table Name Column Name | Default Value | New Value |
| tblConstEquipMitigation $\quad$ NumberOfEquipmentMitigated | 0.00 | 1.00 |
| tbIConstEquipMitigation :- NumberOfEquipmentMitigated | 0.00 | 4.00 |
|  | 0.00 | 1.00 |
| tbIConstEquipMitigation | 0.00 | 3.00 |
|  | 0.00 | 1.00 |
| tbIConstEquipMitigation : NumberOfEquipmentMitigated | 0.00 | 2.00 |
|  | 0.00 | 4.00 |
| tbIConstEquipMitigation | 0.00 | 4.00 |
|  | 0.00 | 12.00 |
|  | 0.00 | 1.00 |
|  | 0.00 | 1.00 |
| tblConstEquipMitigation | 0.00 | 4.00 |

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| tblConstEquipMitigation | NumberOfEquipmentMitigated | 0.00 | 1.00 |
| :---: | :---: | :---: | :---: |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No-Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstructionPhase | NumDays | 18.00 | 34.00 |
| tbiConstructionPhase | NumDays | 230.00 | 102.00 |
| tbiConstructionPhase | NumDays | 5.00 | 48.00 |
| tbiConstructionPhase | NumDays | 18.00 | 47.00 |
| tbiConstructionPhase | NumDays | 8.00 | 48.00 |
| tbiConstructionPhase | PhaseEndDate | 6/7/2022 | 6/1/2022 |
| tbiConstructionPhase | PhaseEndDate | 4/18/2022 | 3/23/2022 |
| tbiconstructionPhase | PhaseEndDate | 5/12/2021 | 6/21/2021 |
| tbiConstructionPhase | PhaseEndDate | 5/31/2021 | 11/1/2021 |
| tbiConstructionPhase | PhaseEndDate | 5/12/2022 | 4/15/2022 |
| tblConstructionPhase | PhaseEndDate | 5/19/2021 | 8/26/2021 |
| tbiconstructionPhase | PhaseStartDate | 5/13/2022 | -7/15/2022 |
| tbiConstructionPhase | PhaseStartDate | 6/1/2021 | 11/2/2021 |

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| tblConstructionPhase | PhaseStartDate | 5/20/2021 | 8/27/2021 |
| :---: | :---: | :---: | :---: |
| tbiConstructionPhase | PhaseStartDate | -4/19/2022 | 3/23/2022 |
| tbiconstructionPhase | PhaseStartDate | 5/13/2021 | 6/22/2021 |
| tblarading | AcresOfGrading | 24.00 | 5.23 |
| tbiTripsAndVMT | WorkerTripNumber | 18.00 | 40.00 |
| tbiTripsAndVMT | WorkerTripNumber | 15.00 | 40.00 |
| tbiTripsAndVMT | WorkerTripNumber | 20.00 | 40.00 |
| tbiTripsAndVMT | WorkerTripNumber | 81.00 | 80.00 |
| tblVehicleTrips | ST_TR | 1,448.33 | 914.62 |
| tbiVehicleTrips | ST_TR | 722.03 | 727.14 |
| tbiVehicleTrips | SÜ_TR | 1,182.08 | 914.62 |
| tblVehicleTrips | SU_TR | 542.72 | 727.14 |
| tbiVehicleTrips | WD_TR | 845.60 | 914.62 |
| tbiVehicleTrips | WD_TR | 496.12 | 727.14 |

### 2.0 Emissions Summary

### 2.1 Overall Construction

## Unmitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2021 | 0.2396 | 2.2863 | 1.6772 | $\begin{gathered} 3.1500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6189 | 0.1120 | 0.7310 | 0.3283 | 0.1035 | 0.4318 | 0.0000 | 277.7651 | 277.7651 | 0.0723 | 0.0000 | 279.5717 |
| 2022 | 0.1574 | 0.7233 | 0.7868 | $\begin{aligned} & 1.5400 \mathrm{e} \\ & 003 \end{aligned}$ | 0.0260 | 0.0329 | 0.0589 | $\begin{gathered} 7.0400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0308 | 0.0379 | 0.0000 | 135.9149 | 135.9149 | 0.0266 | 0.0000 | 136.5804 |
| Maximum | 0.2396 | 2.2863 | 1.6772 | $\begin{gathered} 3.1500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6189 | 0.1120 | 0.7310 | 0.3283 | 0.1035 | 0.4318 | 0.0000 | 277.7651 | 277.7651 | 0.0723 | 0.0000 | 279.5717 |

## Mitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2021 | 0.0560 | 0.2402 | 1.7652 | $3.1500 \mathrm{e}-$ 003 | 0.2995 | $4.6700 \mathrm{e}-$ 003 | 0.3041 | 0.1534 | $4.6500 \mathrm{e}-$ 003 | 0.1580 | 0.0000 | ${ }^{\prime} 277.7648$ | 1277.7648 | 0.0723 | 0.0000 | 279.5714 |
| 2022 | 0.1030 | 0.1780 | 0.8415 | 1.5400 e 003 | 0.0260 | 2.0900 e 003 | 0.0281 | $7.0400 \mathrm{e}-$ 003 | $2.0700 \mathrm{e}-$ 003 | $9.1100 \mathrm{e}-$ 003 | 0.0000 | ,135.9148 | -135.9148 | 0.0266 | 0.0000 | 136.5803 |
| Maximum | 0.1030 | 0.2402 | 1.7652 | $\begin{gathered} 3.1500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.2995 | $\begin{gathered} 4.6700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3041 | 0.1534 | $\begin{gathered} 4.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1580 | 0.0000 | 277.7648 | 277.7648 | 0.0723 | 0.0000 | 279.5714 |
|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
| Percent Reduction | 59.95 | 86.11 | -5.79 | 0.00 | 49.54 | 95.33 | 57.94 | 52.17 | 95.00 | 64.42 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 |

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| Quarter | Start Date | End Date | Maximum Unmitigated ROG + NOX (tons/quarter) | Maximum Mitigated ROG + NOX (tons/quarter) |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{4 - 1 5 - 2 0 2 1}$ | $\mathbf{7 - 1 4 - 2 0 2 1}$ |  | 0.3084 |
| $\mathbf{2}$ | $\mathbf{7 - 1 5 - 2 0 2 1}$ | $\mathbf{1 0 - 1 4 - 2 0 2 1}$ | 0.6360 | 0.0623 |
| $\mathbf{3}$ | $\mathbf{1 0 - 1 5 - 2 0 2 1}$ | $\mathbf{1 - 1 4 - 2 0 2 2}$ | 0.6819 | 0.1796 |
| $\mathbf{4}$ | $\mathbf{1 - 1 5 - 2 0 2 2}$ | $\mathbf{4 - 1 4 - 2 0 2 2}$ | 0.5893 | 0.2189 |
| $\mathbf{5}$ | $\mathbf{4 - 1 5 - 2 0 2 2}$ | $\mathbf{7 - 1 4 - 2 0 2 2}$ | 0.1909 | 0.03 |
|  | Highest | 1.3078 |  |  |

### 2.2 Overall Operational

 Unmitigated Operational|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Area | 0.0585 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.5600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 |  | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.0300 \mathrm{e}-\mathrm{a} \\ 003 \end{gathered}$ | $\begin{gathered} 3.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{aligned} & 3.2300 \mathrm{e}- \\ & 003 \end{aligned}$ |
| Energy | $\begin{gathered} 5.2900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0481 | 0.0404 | $\begin{gathered} 2.9000 \mathrm{e} \\ 004 \end{gathered}$ |  | $\begin{gathered} 3.6600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.6600 \mathrm{e} \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.6600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.6600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 130.9391 | 130.9391 | $\begin{gathered} 4.8600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 1.7600 \mathrm{e}- \\ 003 \end{gathered}$ | 131.5848 |
| Mobile | 1.7178 | 5.7905 | 11.1571 | 0.0231 | 1.6370 | 0.0248 | 1.6618 | 0.4389 | 0.0231 | 0.4620 | 0.0000 | ${ }_{6}^{2,123.839}$ | 2,123.839 | 0.1478 | 0.0000 | $\begin{gathered} 2,127.534 \\ 3 \end{gathered}$ |
| Waste |  |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 15.4151 | 0.0000 | 15.4151 | 0.9110 | 0.0000 | 38.1903 |
| Water |  |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.6996 | 2.9337 | 3.6334 | $\begin{aligned} & 2.5500 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.5500 e- \\ 003 \end{gathered}$ | 4.1594 |
| Total | 1.7816 | 5.8386 | 11.1991 | 0.0234 | 1.6370 | 0.0284 | 1.6654 | 0.4389 | 0.0268 | 0.4657 | 16.1148 | $\begin{array}{\|c\|} \hline 2,257.715 \\ 4 \end{array}$ | $\begin{array}{\|c} \hline 2,273.830 \\ 2 \end{array}$ | 1.0662 | $\begin{gathered} 3.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{array}{\|c} 2,301.472 \\ 1 \end{array}$ |

### 2.2 Overall Operational

Mitigated Operational


### 3.0 Construction Detail

## Construction Phase

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| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Period 1a | :Site Preparation | 14/15/2021 | 16/21/2021 | 5 | 48 |  |
| 2 | Period 1b | Grading | -6/22/2021 | 18/26/2021 | 5 | 48 |  |
| 3 | Period 1 c | ------ | -8/27/2021 | 111/1/2021 | 5 | 47 |  |
| 4 | Period 2 C | Building Construction | 11/2/2021 | 3/23/2022 | 5 | 102 |  |
| 5 | Period 2b | Architectural Coating | 3/23/2022 | 14/15/2022 | 5 | 18 |  |
| 6 | Period 3 | Paving | :4/15/2022 | :6/1/2022 | 5 | 34 |  |

## Acres of Grading (Site Preparation Phase): 0

## Acres of Grading (Grading Phase): 0

## Acres of Paving: 4.22

Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 15,045; Non-Residential Outdoor: 5,015; Striped Parking Area: 11,084 (Architectural Coating - sqft)

OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period 3 | Air Compressors | 0 | 0.00 | 78' | 0.48 |
| Period 2b | Cement and Mortar Mixers | 0 | 0.00 | 91 | 0.56 |
| Period 1a | Concrete/Industrial Saws | 0 |  | 81' | 0.73 |
| Period 1a | Excavators | 0 |  | 158' | 0.38 |
| Period 2a | Cranes | 1 | 7.00 | 231' | 0.29 |
| Period 2a | Forklifts | 3 | 8.00 | 891 | 0.20 |
| Period 1c | Excavators | 0 | 0.00 | 158' | 0.38 |
| Period 2b | Pavers | 0 | 0.00 | 130 | 0.42 |
| Period 2b | Rollers | 0 | 0.00 | 80' | 0.38 |
| Period 1a | Rubber Tired Dozers | 3 | 8.00 | 247: | 0.40 |

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| Period 1c | :Rubber Tired Dozers | $0:$ | 0.00 | 247: | 0.40 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period 2a | :Tractors/Loaders/Backhoes | 3 | 7.00 | 97 | 0.37 |
| Period 2 a | :Generator Sets | 1 | 8.00 | 84! | 0.74 |
| Period 1c | :Tractors/Loaders/Backhoes | 1 | 8.00 | 97 | 0.37 |
| Period 2b | :Tractors/Loaders/Backhoes | 0 | 0.00 | 971 | 0.37 |
| Period 1b | :Tractors/Loaders/Backhoes | 3 | 8.00 | 971, | 0.37 |
| Period 1c | :Graders | 0 | 0.00 | 187: | 0.41 |
| Period 2 b | Paving Equipment | 0 | 0.00 | 132: | 0.36 |
| Period 1b | :Rubber Tired Dozers | 1 | 8.00 | 247: | 0.40 |
| Period 2 a | :Welders | 1 | 8.00 | 46! | 0.75 |
| Period 2 b | Air Compressors | 1 | 6.00 | 78: | 0.48 |
| Period 1c | :Cement and Mortar Mixers | 2 | 6.00 | 9 | 0.56 |
| Period 3 | :Cement and Mortar Mixers | 2 | 6.00 | 91 | 0.56 |
| Period 1b | Excavators | 1 | 8.00 | 158 | 0.38 |
| Period 1b | ;Graders | 1 | 8.00 | 187: | 0.41 |
| Period 1 c | PPavers | 1 | 8.00 | 130: | 0.42 |
| Period 3 | : Pavers | 1 | 8.00 | 130! | 0.42 |
| Period 1c | Paving Equipment | 2 | 6.00 | 132 | 0.36 |
| Period 3 | :Paving Equipment | 2 | 6.00 | 132: | 0.36 |
| Period 1c | :Rollers | 2 | 6.00 | 80 | 0.38 |
| Period 3 | :Rollers | 2 | 6.00 | 80 | 0.38 |
| Period 3 | Tractors/Loaders/Backhoes | 1 | 8.00 | 97 | 0.37 |
| Period 1a | :Tractors/Loaders/Backhoes | 4: | 8.00 | 97: | 0.37 |

Trips and VMT

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| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period 1a | 7 | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | [HDT_Mix | HHDT |
| Period 1b | 6 | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Period 1 c |  | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | THDT |
| Period 2a |  | 80.00 | 32.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Period 2 b | 1 | 16.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | THDT |
| Period 3 | 8 | 20.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | ;HDT_Mix | :HHDT |

### 3.1 Mitigation Measures Construction

Use Cleaner Engines for Construction Equipment
Water Exposed Area

### 3.2 Period 1a-2021

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.4336 | 0.0000 | 0.4336 | 0.2383 | 0.0000 | 0.2383 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0933 | 0.9719 | 0.5077 | $9.1000 \mathrm{e}-$ 004 |  | 0.0491 | 0.0491 |  | 0.0451 | 0.0451 | 0.0000 | 80.2457 | 80.2457 | 0.0260 | 0.0000 | 80.8946 |
| Total | 0.0933 | 0.9719 | 0.5077 | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.4336 | 0.0491 | 0.4827 | 0.2383 | 0.0451 | 0.2835 | 0.0000 | 80.2457 | 80.2457 | 0.0260 | 0.0000 | 80.8946 |

### 3.2 Period 1a-2021

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 3.3200e- | 2.1700e- | 0.0243 | 7.0000e- | 7.0500e- | 5.0000e- | 7.1000e- | 1.8800e- | 5.0000e- | $1.9200 \mathrm{e}-$ | 0.0000 | 6.0344 | 6.0344 | 1.6000e- | 0.0000 | 6.0383 |
| Total | $\begin{gathered} 3.3200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.1700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0243 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.0500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.1000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.8800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 6.0344 | 6.0344 | $\begin{aligned} & 1.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 6.0383 |

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.1951 | 0.0000 | 0.1951 | 0.1073 | 0.0000 | 0.1073 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0112 | 0.0484 | 0.5009 | $\begin{aligned} & 9.1000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 1.4900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.4900 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{aligned} & 1.4900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 1.4900 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 80.2456 | 80.2456 | 0.0260 | 0.0000 | 80.8945 |
| Total | 0.0112 | 0.0484 | 0.5009 | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.1951 | $\begin{gathered} 1.4900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1966 | 0.1073 | $\begin{gathered} 1.4900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1087 | 0.0000 | 80.2456 | 80.2456 | 0.0260 | 0.0000 | 80.8945 |

### 3.2 Period 1a-2021

## Mitigated Construction Off-Site

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 3.3200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.1700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0243 | $7.0000 \mathrm{e}-$ | $\begin{gathered} 7.0500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.1000 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{aligned} & 1.8800 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 5.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 1.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 6.0344 | 6.0344 | $1.6000 \mathrm{e}-$ $004$ | 0.0000 | 6.0383 |
| Total | $\begin{gathered} 3.3200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.1700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0243 | $\begin{aligned} & 7.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{gathered} 7.0500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.1000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.8800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 6.0344 | 6.0344 | $\begin{aligned} & 1.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 6.0383 |

### 3.3 Period 1b-2021

Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.1473 | 0.0000 | 0.1473 | 0.0797 | 0.0000 | 0.0797 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0550 | 0.5937 | 0.3806 | $\begin{aligned} & 7.1000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | 0.0278 | 0.0278 |  | 0.0256 | 0.0256 | 0.0000 | 62.5289 | 62.5289 | 0.0202 | 0.0000 | 63.0345 |
| Total | 0.0550 | 0.5937 | 0.3806 | $\begin{aligned} & \hline 7.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.1473 | 0.0278 | 0.1751 | 0.0797 | 0.0256 | 0.1054 | 0.0000 | 62.5289 | 62.5289 | 0.0202 | 0.0000 | 63.0345 |

### 3.3 Period 1b-2021

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $3.3200 \mathrm{e}-$ | 2.1700e- | 0.0243 | 7.0000e- | 7.0500e- | 5.0000e- | 7.1000e- | 1.8800e- | 5.0000e- | $1.9200 \mathrm{e}-$ | 0.0000 | 6.0344 | 6.0344 | 1.6000e- | 0.0000 | 6.0383 |
| Total | $\begin{gathered} 3.3200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.1700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0243 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.0500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.1000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.8800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 6.0344 | 6.0344 | $\begin{aligned} & 1.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 6.0383 |

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.0663 | 0.0000 | 0.0663 | 0.0359 | 0.0000 | 0.0359 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | $\begin{gathered} 8.7200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0378 | 0.4261 | $\begin{aligned} & 7.1000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 1.1600 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 62.5288 | 62.5288 | 0.0202 | 0.0000 | 63.0344 |
| Total | $\begin{gathered} 8.7200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0378 | 0.4261 | $\begin{gathered} 7.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0663 | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0675 | 0.0359 | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0371 | 0.0000 | 62.5288 | 62.5288 | 0.0202 | 0.0000 | 63.0344 |

### 3.3 Period 1b-2021

Mitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 3.3200 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 2.1700 \mathrm{e} \\ 003 \end{gathered}$ | 0.0243 | $\begin{gathered} 7.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 7.0500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.1000 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 1.8800 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 1.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 6.0344 | 6.0344 | $1.6000 \mathrm{e}-$ <br> 004 | 0.0000 | 6.0383 |
| Total | $\begin{gathered} 3.3200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.1700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0243 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.0500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 7.1000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.8800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.9200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 6.0344 | 6.0344 | $\begin{aligned} & 1.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 6.0383 |

### 3.4 Period 1c-2021

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.0257 | 0.2547 | 0.2881 | $\begin{aligned} & 4.4000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | 0.0136 | 0.0136 |  | 0.0126 | 0.0126 | 0.0000 | 38.4710 | 38.4710 | 0.0121 | 0.0000 | 38.7732 |
| Paving | $\begin{gathered} 5.5300 \mathrm{e}- \\ 003 \end{gathered}$ |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | 0.0312 | 0.2547 | 0.2881 | $\begin{gathered} 4.4000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 0.0136 | 0.0136 |  | 0.0126 | 0.0126 | 0.0000 | 38.4710 | 38.4710 | 0.0121 | 0.0000 | 38.7732 |

### 3.4 Period 1c-2021

## Unmitigated Construction Off-Site

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 3.2500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.1300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0238 | $7.0000 \mathrm{e}-$ | $\begin{gathered} -9.9000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 6.9500 \mathrm{e} \\ 003 \end{gathered}$ | $1.8400 \mathrm{e}-$ $003$ | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 1.8800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 5.9086 | 5.9086 | $1.6000 \mathrm{e}-$ | 0.0000 | 5.9125 |
| Total | $\begin{gathered} 3.2500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.1300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0238 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 6.9000 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 6.9500 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.8400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.8800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 5.9086 | 5.9086 | $\begin{gathered} 1.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 5.9125 |

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | $5.1600 \mathrm{e}-$ 003 | 0.0224 | 0.3180 | $4.4000 \mathrm{e}-$ 004 |  | $6.9000 \mathrm{e}-$ 004 | $6.9000 \mathrm{e}-1$ 004 |  | $6.9000 \mathrm{e}-$ 004 | $6.9000 \mathrm{e}-$ 004 | 0.0000 | 38.4709 | 38.4709 | 0.0121 | 0.0000 | 38.7731 |
| Paving | $5.5300 \mathrm{e}-$ 003 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | -0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | -0.0000 |
| Total | 0.0107 | 0.0224 | 0.3180 | $\begin{aligned} & \hline 4.4000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{gathered} 6.9000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 6.9000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 6.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 6.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 38.4709 | 38.4709 | 0.0121 | 0.0000 | 38.7731 |

### 3.4 Period 1c-2021

Mitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $3.2500 \mathrm{e}-$ | $2.1300 \mathrm{e}-$ | 0.0238 | $7.0000 \mathrm{e}-$ | 6.9000e- | $5.0000 \mathrm{e}-$ | $6.9500 \mathrm{e}-$ | 1.8400e- | $4.0000 \mathrm{e}-$ | $1.8800 \mathrm{e}-$ | 0.0000 | 5.9086 | 5.9086 | $1.6000 \mathrm{e}-$ | 0.0000 | 5.9125 |
| Total | $\begin{gathered} 3.2500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.1300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0238 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 6.9000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 6.9500 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.8400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.8800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 5.9086 | 5.9086 | $\begin{aligned} & 1.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 5.9125 |

### 3.5 Period 2a-2021

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.0418 | 0.3835 | 0.3647 | $\begin{gathered} 5.9000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 0.0211 | 0.0211 |  | 0.0198 | 0.0198 | 0.0000 | 50.9602 | 50.9602 | 0.0123 | 0.0000 | 51.2676 |
| Total | 0.0418 | 0.3835 | 0.3647 | $\begin{gathered} 5.9000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 0.0211 | 0.0211 |  | 0.0198 | 0.0198 | 0.0000 | 50.9602 | 50.9602 | 0.0123 | 0.0000 | 51.2676 |

### 3.5 Period 2a-2021

## Unmitigated Construction Off-Site

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | $2.21000-$ 003 | 0.0720 | 0.0193 | $\begin{gathered} 1.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 4.1200 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 2.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 4.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 1.1900 \mathrm{e} \\ & 003 \end{aligned}$ | $\begin{aligned} & 1.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 1.3800 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 16.5190 | 16.5190 | $\begin{aligned} & 9.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 16.5426 |
| Worker | $\begin{aligned} & \overline{6} .09000 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 3.9800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0446 | $\begin{gathered} 1.2000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0129 | $\begin{gathered} 9.0000 \mathrm{e} \\ 005 \end{gathered}$ | 0.0130 | $\begin{aligned} & 3.4400 \mathrm{e} \\ & 003 \end{aligned}$ | $\begin{gathered} 8.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 3.5200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 11.0630 | 11.0630 | $\begin{gathered} 2.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 11.0703 |
| Total | $\begin{gathered} 8.3000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0760 | 0.0638 | $\begin{aligned} & 2.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0171 | $\begin{gathered} 2.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0173 | $\begin{gathered} 4.6300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 27.5820 | 27.5820 | $\begin{gathered} 1.2300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 27.6128 |

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | $7.2100 \mathrm{e}-$ 003 | 0.0492 | 0.3841 | $5.9000 \mathrm{e}-$ 004 |  | $9.0000 \mathrm{e}-$ 004 | $9.0000 \mathrm{e}-$ 004 |  | $\begin{aligned} & 9.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | $9.0000 \mathrm{e}-$ 004 | 0.0000 | 50.9601 | 50.9601 | 0.0123 | 0.0000 | 51.2675 |
| Total | $\begin{gathered} 7.2100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0492 | 0.3841 | $\begin{aligned} & 5.9000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 9.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 9.0000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{aligned} & 9.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 9.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 50.9601 | 50.9601 | 0.0123 | 0.0000 | 51.2675 |

### 3.5 Period 2a-2021

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | $\begin{aligned} & 0.0000 \\ & \hline----\quad . \end{aligned}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | $\begin{gathered} 2.2100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0720 | 0.0193 | $\begin{gathered} 1.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.1200 \mathrm{e}- \\ 003 \end{gathered}$ | $2.0000 \mathrm{e}-$ 004 | $\begin{aligned} & 4.3100 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 1.1900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.9000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 1.3800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 16.5190 | 16.5190 | $9.4000 \mathrm{e}-\mathrm{C}$ 004 | 0.0000 | -16.5426 |
| Worker | $6.0900 \mathrm{e}-$ 003 | $3.9800 \mathrm{e}-$ 003 | 0.0446 | 1.2000 e 004 | 0.0129 | $9.0000 \mathrm{e}-$ 005 | 0.0130 | $3.4400 \mathrm{e}-$ 003 | 8.0000 e 005 | $3.5200 \mathrm{e}-$ 003 | 0.0000 | 11.0630 | 11.0630 | $2.9000 \mathrm{e}-$ 004 | 0.0000 | 11.0703 |
| Total | $\begin{aligned} & 8.3000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0760 | 0.0638 | $\begin{aligned} & 2.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0171 | $\begin{aligned} & 2.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0173 | $\begin{gathered} 4.6300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.9000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 27.5820 | 27.5820 | $\begin{gathered} 1.2300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 27.6128 |

3.5 Period 2a-2022

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N 2 O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.0495 | 0.4529 | 0.4745 | $7.8000 \mathrm{e}-$ 004 |  | 0.0235 | 0.0235 |  | 0.0221 | 0.0221 | 0.0000 | 67.2003 | 67.2003 | 0.0161 | 0.0000 | 67.6028 |
| Total | 0.0495 | 0.4529 | 0.4745 | $\begin{gathered} 7.8000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 0.0235 | 0.0235 |  | 0.0221 | 0.0221 | 0.0000 | 67.2003 | 67.2003 | 0.0161 | 0.0000 | 67.6028 |

### 3.5 Period 2a-2022

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | ${ }^{2.71000} 00$ | 0.0901 | 0.0234 | $\begin{aligned} & 2.2000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 5.4200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 2.3000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 5.6600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 1.5700 \mathrm{e} \\ & 003 \end{aligned}$ | $\begin{aligned} & 2.2000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.7900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 21.5836 | 21.5836 | $\begin{aligned} & 1.2100 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 21.6139 |
| Worker | $\begin{gathered} 7.5100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.7200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0540 | $\begin{aligned} & 1.6000 \mathrm{e} \\ & 004 \end{aligned}$ | 0.0170 | $\begin{gathered} 1.2000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0172 | $\begin{gathered} 4.5300 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 1.1000 \mathrm{e} \\ 004 \end{gathered}$ | $4.6400 \mathrm{e}-$ $003$ | 0.0000 | 14.0607 | 14.0607 | $\begin{aligned} & 3.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 14.0693 |
| Total | 0.0102 | 0.0949 | 0.0774 | $\begin{aligned} & 3.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0225 | $\begin{aligned} & 3.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0228 | $\begin{aligned} & 6.1000 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 3.3000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 6.4300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 35.6443 | 35.6443 | $\begin{gathered} 1.5500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 35.6831 |

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | $9.5100 \mathrm{e}-$ 003 | 0.0648 | 0.5064 | 7.8000e- 004 |  | $1.1800 \mathrm{e}-$ 003 | $1.1800 \mathrm{e}-$ 003 |  | $\begin{gathered} 1.1800 \mathrm{e}- \\ 003 \end{gathered}$ | $1.1800 \mathrm{e}-$ 003 | 0.0000 | 67.2002 | 67.2002 | 0.0161 | 0.0000 | 67.6027 |
| Total | $\begin{gathered} 9.5100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0648 | 0.5064 | $\begin{aligned} & \hline 7.8000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{gathered} 1.1800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.1800 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 1.1800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 1.1800 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 67.2002 | 67.2002 | 0.0161 | 0.0000 | 67.6027 |

### 3.5 Period 2a-2022

Mitigated Construction Off-Site

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | $2.7100 \mathrm{e}-$ 003 | 0.0901 | 0.0234 | $\begin{gathered} 2.2000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 5.4200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 2.3000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 5.6600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 1.5700 \mathrm{e} \\ & 003 \end{aligned}$ | $\begin{aligned} & 2.2000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.7900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 21.5836 | 21.5836 | $\begin{gathered} 1.2100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 21.6139 |
| Worker | $\begin{gathered} 7.5100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.7200 \mathrm{e} \\ 003 \end{gathered}$ | 0.0540 | $\begin{gathered} 1.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0170 | $\begin{gathered} 1.2000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0172 | $\begin{gathered} 4.5300 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.6400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 14.0607 | 14.0607 | $\begin{aligned} & 3.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 14.0693 |
| Total | 0.0102 | 0.0949 | 0.0774 | $\begin{aligned} & 3.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0225 | $\begin{aligned} & 3.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0228 | $\begin{gathered} 6.1000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.3000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 6.4300 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 35.6443 | 35.6443 | $\begin{gathered} 1.5500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 35.6831 |

3.6 Period 2b-2022

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Archit. Coating | 0.0722 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | $\begin{gathered} 1.8400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0127 | 0.0163 | $\begin{aligned} & 3.00000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 7.4000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{gathered} 7.4000-- \\ 004 \end{gathered}$ | $\begin{gathered} 7.4000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 2.2979 | 2.2979 | $\begin{aligned} & 1.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 2.3017 |
| Total | 0.0740 | 0.0127 | 0.0163 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{gathered} 7.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 2.2979 | 2.2979 | $\begin{aligned} & 1.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 2.3017 |

### 3.6 Period 2b-2022

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $4.7000 \mathrm{e}-$ 004 | $\begin{gathered} 2.9000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 3.3500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 2.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.8727 | 0.8727 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.8733 |
| Total | $\begin{gathered} 4.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 2.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 3.3500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 2.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 2.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.8727 | 0.8727 | $\begin{aligned} & 2.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | 0.0000 | 0.8733 |

## Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Archit. Coating | 0.0722 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | $\begin{gathered} 2.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0165 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 2.2979 | 2.2979 | $\begin{aligned} & 1.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 2.3017 |
| Total | 0.0725 | $\begin{aligned} & 1.1600 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0165 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 2.2979 | 2.2979 | $\begin{aligned} & 1.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 2.3017 |

### 3.6 Period 2b-2022

Mitigated Construction Off-Site


### 3.7 Period 3-2022

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.0166 | 0.1619 | 0.2073 | $\begin{gathered} 3.2000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{aligned} & 8.2900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 8.2900 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 7.6600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 7.6600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 27.8390 | 27.8390 | $\begin{gathered} 8.7500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 28.0576 |
| Paving | $5.53000-$ 003 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | 0.0221 | 0.1619 | 0.2073 | $\begin{gathered} 3.2000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{gathered} 8.2900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 8.2900 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 7.6600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 7.6600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 27.8390 | 27.8390 | $\begin{gathered} 8.7500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 28.0576 |

### 3.7 Period 3-2022

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 1.1000 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{aligned} & 6.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 7.9100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 6.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 2.0606 | 2.0606 | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 2.0619 |
| Total | $\begin{gathered} 1.1000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 6.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 7.9100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 6.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 2.0606 | 2.0606 | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 2.0619 |

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | $3.7300 \mathrm{e}-$ 003 | 0.0162 | 0.2301 | $3.2000 \mathrm{e}-$ 004 |  | $5.0000 \mathrm{e}-1$ 004 | $5.0000 \mathrm{e}-$ 004 |  | $5.0000 \mathrm{e}-$ 004 | $5.0000 \mathrm{e}-$ 004 | 0.0000 | 27.8389 | 27.8389 | $8.7500 \mathrm{e}-$ 003 | 0.0000 | 28.0576 |
| Paving | $\begin{gathered} 5.5300 \mathrm{e}- \\ 003 \end{gathered}$ |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | $\begin{gathered} 9.2600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0162 | 0.2301 | $\begin{aligned} & 3.2000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 5.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 5.0000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{gathered} 5.0000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 5.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 27.8389 | 27.8389 | $\begin{aligned} & 8.7500 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 28.0576 |

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### 3.7 Period 3-2022

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 1.1000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.9000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 7.9100 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 6.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 2.0606 | 2.0606 | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 2.0619 |
| Total | $\begin{gathered} 1.1000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.9000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 7.9100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.5100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 6.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 2.0606 | 2.0606 | $\begin{gathered} 5.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 2.0619 |

### 4.0 Operational Detail - Mobile

4.1 Mitigation Measures Mobile

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Mitigated | $1.7178$ |  |  |  |  |  | 1.6618 |  |  |  | 0.0000 |  | $\begin{gathered} 2,123.839 \\ 6 \end{gathered}$ | $0.1478$ | $0.0000$ | $\begin{gathered} 2,127.534 \\ 3 \end{gathered}$ |
| Unmitigated | $1.7178$ | 5.7905 | 11.1571 | 0.0231 |  |  |  |  | 0.0231 | 0.4620 | 0.0000 | : | 2,123.839 | 0.1478 | 0.0000 | $\underset{3}{2,127.534}$ |

### 4.2 Trip Summary Information

|  | Average Daily Trip Rate |  |  | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Convenience Market With Gas Pumps | 4,252.98 | 4,252.98 | 4252.98 | 1,687,510 | 1,687,510 |
| Fast Food Restaurant with Drive Thru | 3,272.13 | 3,272.13 | 3272.13 | 2,260,370 | 2,260,370 |
| Fast Food Restaurant with Drive Thru | 639.88 | 639.88 | 639.88 | 442,028 | 442,028 |
| - - - Other Asphalt Surfaces | 0.00 | 0.00 | 0.00 |  |  |
| Parking Lot | 0.00 | 0.00 | 0.00 |  |  |
| Total | 8,165.00 | 8,165.00 | 8,165.00 | 4,389,908 | 4,389,908 |

### 4.3 Trip Type Information

|  | Miles |  |  | Trip \% |  |  | Trip Purpose \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted | Pass-by |
| Convenience Market With Gas | 10.00 | 5.00 | 6.50 | 0.80 | 80.20 | 19.00 | 14 | 21 | 65 |
| Fast Food Restaurant with Drive | 10.00 | 5.00 | 6.50 | 2.20 | 78.80 | 19.00 | 29 | 21 | 50 |
| Fast Food Restaurant with Drive | 10.00 | 5.00 | 6.50 | 2.20 | 78.80 | 19.00 | 29 | 21 | 50 |
| - - Other Asphalt Surfaces | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |
| Parking Lot | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

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### 4.4 Fleet Mix

| Land Use | LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Convenience Market With Gas Pumps | 0.55952 | 0.038733: | 0.206173: | 0.118029 | 0.019040: | 0.005245 | 0.018552 | 0.023249 | 0.002031: | 0.002054: | 0.005884 | 0.000619! | 0.000865 |
| Fast Food Restaurant with Drive Thru | 0.55952 | 0.038733 | 0.206173 | 0.118029 | 0.019040 | 0.005245 | 0.018552 | 0.023249 | 0.002031 | 0.002054 | 0.005884 | 0.000619: | 0.000865 |
| Other Asphalt Surfaces | 0.55952 | 0.038733 | 0.206173 | 0.118029 | 0.019040 | 0.005245 | 0.018552 | 0.023249 | 0.002031 | 0.002054 | 0.005884 | 0.000619 | 0.000865 |
| Parking Lot | 0.55952 | 0.038733 | 0.206173: | 0.118029! | 0.019040: | 0.005245 | 0.018552 | 0.023249 | 0.002031: | 0.002054 | 0.005884: | 0.000619: | 0.000865 |

### 5.0 Energy Detail

Historical Energy Use: N

### 5.1 Mitigation Measures Energy

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Electricity Mitigated |  |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 78.5770 | 78.5770 | $3.8600 \mathrm{e}-$ 003 | $8.0000 \mathrm{e}-$ 004 | 78.9115 |
| Electricity Unmitigated |  |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 78.5770 | 78.5770 | $3.8600 \mathrm{e}-$ 003 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 78.9115 |
| NaturalGas Mitigated | $5.2900 \mathrm{e}-$ 003 | 0.0481 | 0.0404 | $\begin{gathered} 2.9000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $3.6600 \mathrm{e}-$ 003 | $\begin{gathered} 3.6600 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.6600 \mathrm{e}- \\ 003 \end{gathered}$ | 3.6600 e 003 | 0.0000 | 52.3621 | 52.3621 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 9.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 52.6733 |
| NaturalGas Unmitigated | $5.2900 \mathrm{e}-$ 003 | 0.0481 | 0.0404 | $\begin{gathered} 2.9000 \mathrm{e}- \\ 004 \end{gathered}$ |  | 3.6600 e 003 | $3.6600 \mathrm{e}-$ 003 |  | $3.6600 \mathrm{e}-$ 003 | $3.6600 \mathrm{e}-$ 003 | 0.0000 | 52.3621 | 52.3621 | $1.0000 \mathrm{e}-$ 003 | $\begin{gathered} 9.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 52.6733 |

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### 5.2 Energy by Land Use - NaturalGas

## Unmitigated

|  | NaturalGa s Use | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Convenience Market With Gas Pumps | 25203 | $1.4000 \mathrm{e}-$ 004 | $\begin{gathered} 1.2400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $9.0000 \mathrm{e}-$ 005 | $9.0000 \mathrm{e}-$ 005 |  | $9.0000 \mathrm{e}-$ 005 | $9.0000 \mathrm{e}-$ 005 | 0.0000 | 1.3449 | 1.3449 | $3.0000 \mathrm{e}-$ 005 | $2.0000 \mathrm{e}-$ 005 | 1.3529 |
| Fast Food Restaurant with Drive Thru | 156376 | $8.4000 \mathrm{e}-$ 004 | $\begin{gathered} 7.6700 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 6.4400-- \\ 003 \end{gathered}$ | $\begin{gathered} 5.0000 \mathrm{e} \\ 005 \end{gathered}$ |  | $\begin{gathered} 5.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 5.8000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{gathered} 5.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 5.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 8.3448 | 8.3448 | $\begin{gathered} 1.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.5000 \mathrm{e} \\ 004 \end{gathered}$ | 8.3944 |
| Fast Food Restaurant with Drive Thru | 799650 | ${ }^{4.3100 e-}$ | 0.0392 | 0.0329 | ${ }^{2.40000-}$ |  | ${ }^{2.98000} 0$ | ${ }^{2.98000-}$ |  | ${ }^{2.98000} 0$ | ${ }^{2.98000} 00$ | 0.0000 | 42.6724 | 42.6724 | $8.2000 e-$ 004 | $\begin{aligned} & 7.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | 42.9260 |
| Other Asphalt Surfaces |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  | $\begin{gathered} 5.2900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0481 | 0.0404 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{gathered} 3.6500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.6500 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.6500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 52.3621 | 52.3621 | $\begin{gathered} 1.0100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 9.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 52.6733 |

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### 5.2 Energy by Land Use - NaturalGas

## Mitigated

|  | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Convenience Market With Gas Pumps | , 25203 | $1.4000 \mathrm{e}-$ 004 | $1.2400 \mathrm{e}-$ 003 | $\begin{gathered} 1.0400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $9.0000 \mathrm{e}-$ 005 |  | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $9.0000 \mathrm{e}-$ 005 | 0.0000 | 1.3449 | 1.3449 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 1.3529 |
| Fast Food Restaurant with Drive Thru | 799650 | $4.3100 \mathrm{e}-$ 003 | 0.0392 | 0.0329 | $2.4000 \mathrm{e}-$ 004 |  | $2.9800 \mathrm{e}-$ 003 | $2.9800 \mathrm{e}-$ 003 |  | $2.9800 \mathrm{e}-$ 003 | $2.9800 \mathrm{e}-$ 003 | 0.0000 | 42.6724 | 42.6724 | $8.2000 \mathrm{e}-$ 004 | $7.8000 \mathrm{e}-$ 004 | 42.9260 |
| Fast Food Restaurant with Drive Thru | 156376 | $8.4000 \mathrm{e}-$ 004 | 7.6700 e 003 | $6.4400 \mathrm{e}-$ 003 | 5.0000 e 005 |  | $5.8000 \mathrm{e}-$ 004 | $5.8000 \mathrm{e}-$ 004 |  | $5.8000 \mathrm{e}-$ 004 | $5.8000 \mathrm{e}-$ 004 | 0.0000 | 8.3448 | 8.3448 | $1.6000 \mathrm{e}-$ 004 | $1.5000 \mathrm{e}-$ 004 | 8.3944 |
| Other Asphalt Surfaces | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  | $\begin{gathered} 5.2900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0481 | 0.0404 | $\begin{aligned} & 3.0000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{gathered} 3.6500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.6500 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.6500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 52.3621 | 52.3621 | $\begin{aligned} & 1.0100 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 9.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 52.6733 |

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### 5.3 Energy by Land Use - Electricity

## Unmitigated

|  | $\begin{aligned} & \text { Electricity } \\ & \text { Use } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kWh/yr | MT/yr |  |  |  |
| Convenience Market With Gas Pumps | 53800.5 | 14.4056 | $\begin{gathered} 7.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 14.4670 |
| Fast Food Restaurant with Drive Thru | 187695 | 50.2572 | $\begin{gathered} 2.4700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 5.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 50.4712 |
| $\begin{aligned} & \text { Fast Food } \\ & \text { Restaurant with } \\ & \text { Drive Thru } \end{aligned}$ | 36704.8 | 9.8281 | $4.8000 \mathrm{e}-$ 004 | ${ }^{1.00000 e-}$ | 9.8699 |
| Other Asphalt Surfaces |  | $0.0000$ | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | 15260 | $4.0860$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 4.1034 |
| Total |  | 78.5770 | $\begin{gathered} 3.8600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 8.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 78.9115 |

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### 5.3 Energy by Land Use - Electricity

Mitigated

|  | $\begin{array}{\|c} \hline \text { Electricity } \\ \text { Use } \end{array}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kWh/yr | MT/yr |  |  |  |
| Convenience Market With Gas Pumps | 53800.5 | 14.4056 | $\begin{gathered} 7.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 14.4670 |
| Fast Food Restaurant with Drive Thru | 187695 | 50.2572 | $\begin{gathered} 2.4700 \mathrm{e} \\ 003 \end{gathered}$ | $5.10000-$ 004 | 50.4712 |
| Fast Food Restaurant with Drive Thru | 36704.8 | 9.8281 | $\begin{aligned} & 4.8000 \mathrm{e} \\ & 004 \end{aligned}$ | $1.00000-$ 004 | -9.8699 |
| Other Asphalt Surfaces |  | 0.0000 | 0.0000 | 0.0000 | -0.0000 |
| Parking Lot | $-\overline{15260}$ | $4.0860$ | $\begin{gathered} 2.0000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | 4.1034 |
| Total |  | 78.5770 | $\begin{gathered} 3.8600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 78.9115 |

### 6.0 Area Detail

6.1 Mitigation Measures Area

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|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Mitigated | 0.0585 | $1.0000 \mathrm{e}-$ 005 | $1.5600 \mathrm{e}-$ 003 | 0.0000 |  | $1.0000 \mathrm{e}-$ 005 | $1.0000 \mathrm{e}-$ 005 |  | $1.0000 \mathrm{e}-$ 005 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | 0.0000 | $\begin{gathered} 3.2300 \mathrm{e}- \\ 003 \end{gathered}$ |
| Unmitigated | 0.0585 | $1.0000 \mathrm{e}-$ 005 | $1.5600 \mathrm{e}-$ 003 | 0.0000 |  | $1.0000 \mathrm{e}-$ 005 | $1.0000 \mathrm{e}-$ 005 |  | $1.0000 \mathrm{e}-$ 005 | $1.0000 \mathrm{e}-$ 005 | 0.0000 | : $\begin{gathered}3.0300 \mathrm{e}- \\ \\ \\ \end{gathered}$ | $3.0300 \mathrm{e}-$ 003 | $1.0000 \mathrm{e}-$ 005 | 0.0000 | $3.2300 \mathrm{e}-$ 003 |

### 6.2 Area by SubCategory

## Unmitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Architectural Coating | $\begin{gathered} 7.2200 \mathrm{e}- \\ 003 \end{gathered}$ |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Consumer Products | 0.0511 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | $\begin{gathered} 1.5000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.5600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 |  | $\begin{gathered} 1.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{gathered} 1.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 3.0300 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.0000-- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.2300 \mathrm{e}- \\ 003 \end{gathered}$ |
| Total | 0.0585 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.5600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 |  | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} \hline 3.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} \hline 3.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{aligned} & \hline 3.2300 \mathrm{e}- \\ & 003 \end{aligned}$ |

### 6.2 Area by SubCategory

## Mitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Architectural Coating | $\begin{gathered} 7.2200 \mathrm{e}- \\ 003 \end{gathered}$ |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Consumer Products | 0.0511 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | $1.5000 \mathrm{e}-$ 004 | $1.0000 \mathrm{e}-$ 005 | $1.5600 \mathrm{e}-\mathrm{-}$ 003 | 0.0000 |  | 1.0000 e 005 | $1.0000 \mathrm{e}-$ 005 |  | 1.0000 e 005 | $1.0000 \mathrm{e}-$ 005 | 0.0000 | (3.0300e- | $3.0300 \mathrm{e}-$ 003 | $1.0000 \mathrm{e}-$ 005 | 0.0000 | $3.2300 \mathrm{e}-$ 003 |
| Total | 0.0585 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.5600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 |  | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.2300 \mathrm{e}- \\ 003 \end{gathered}$ |

### 7.0 Water Detail

7.1 Mitigation Measures Water

River Oaks Marketplace - Sacramento County, Annual

|  | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: |
| Category | MT/yr |  |  |  |
| Mitigated | 3.6334 | $2.5500 \mathrm{e}-$ 003 | $1.5500 \mathrm{e}-$ 003 | 4.1594 |
| Unmitigated | $3.6334$ | $\begin{gathered} 2.5500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.5500 \mathrm{e}- \\ 003 \end{gathered}$ | 4.1594 |

### 7.2 Water by Land Use

## Unmitigated

|  | Indoor/Out door Use | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Mgal | MT/yr |  |  |  |
| Convenience Market With Gas Pumps | $\begin{aligned} & 0.344437 /: \\ & 0.211107 \\ & \hline \end{aligned}$ | 0.7792 | $\begin{gathered} 4.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.8715 |
| Fast Food Restaurant with Drive Thru | 石 $1.63301 /$ | 2.8541 | 2.1000e- 003 | 1.-2800e- 003 | 3.2879 |
| Other Asphalt Surfaces |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | $0 / 0$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  | 3.6333 | $\begin{gathered} 2.5500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.5500 \mathrm{e}- \\ 003 \end{gathered}$ | 4.1594 |

River Oaks Marketplace - Sacramento County, Annual

### 7.2 Water by Land Use

## Mitigated

|  | $\begin{array}{\|l\|} \hline \text { Indoor/Out } \\ \text { door Use } \end{array}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Mgal | MT/yr |  |  |  |
| Convenience Market With Gas Pumps | $\begin{aligned} & \hline 0.344437 / \\ & 10.211107 \end{aligned}$ | 0.7792 | $\begin{gathered} 4.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.8715 |
| Fast Food Restaurant with Drive Thru | $\begin{aligned} & -1.63301 / \\ & 10.104235 \\ & \hline \end{aligned}$ | 2.8541 | $2.1000 \mathrm{e}-$ 003 | $1.28000-$ 003 | 3.2879 |
| Other Asphalt Surfaces | 0/0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | 0/0 | $0.0000$ | 0.0000 | 0.0000 | 0.0000 |
| Total |  | 3.6333 | $\begin{gathered} 2.5500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.5500 \mathrm{e}- \\ 003 \end{gathered}$ | 4.1594 |

### 8.0 Waste Detail

8.1 Mitigation Measures Waste

River Oaks Marketplace - Sacramento County, Annual

## Category/Year

|  | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: |
|  | MT/yr |  |  |  |
| Mitigated | 15.4151 | 0.9110 | 0.0000 | 38.1903 |
| Unmitigated | 15.4151 | 0.9110 | 0.0000 | 38.1903 |

### 8.2 Waste by Land Use

## Unmitigated

|  | Waste Disposed | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | tons | MT/yr |  |  |  |
| Convenience Market With Gas Pumps | 13.97 | 2.8358 | 0.1676 | 0.0000 | 7.0255 |
| Fast Food Restaurant with Drive Thru | 61.97 | $12.5794$ | 0.7434 | 0.0000 | 31.1648 |
| Other Asphalt Surfaces |  | - 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | 0 | $0.0000$ | 0.0000 | 0.0000 | 0.0000 |
| Total |  | 15.4151 | 0.9110 | 0.0000 | 38.1903 |

River Oaks Marketplace - Sacramento County, Annual

### 8.2 Waste by Land Use

Mitigated

|  | Waste Disposed | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | tons | MT/yr |  |  |  |
| Convenience Market With Gas Pumps | 13.97 | 2.8358 | 0.1676 | 0.0000 | 7.0255 |
| Fast Food Restaurant with Drive Thru | 61.97 | 12.5794 | 0.7434 | 0.0000 | 31.1648 |
| Other Asphalt Surfaces | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  | 15.4151 | 0.9110 | 0.0000 | 38.1903 |

### 9.0 Operational Offroad

| Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

### 10.0 Stationary Equipment

Fire Pumps and Emergency Generators

| Equipment Type | Number | Hours/Day | Hours/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## Boilers

| Equipment Type | Number | Heat Input/Day | Heat Input/Year | Boiler Rating | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: |

User Defined Equipment

## River Oaks Marketplace - Sacramento County, Annual

$\square$
11.0 Vegetation

River Oaks Marketplace - Sacramento County, Summer

## River Oaks Marketplace

## Sacramento County, Summer

### 1.0 Project Characteristics

### 1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Other Asphalt Surfaces | 3.24 | Acre | 3.24 | 141,134.40 | 0 |
| Parking Lot | 109.00 | Space | 0.98 | 43,600.00 | 0 |
| Fast Food Restaurant with Drive Thru | 4.50 | 1000sqft | 0.10 | 4,500.00 | 0 |
| Fast Food Restaurant with Drive Thru | 0.88 | 1000sqft | 0.02 | 880.00 | 0 |
| Convenience Market With Gas Pumps | 4.65 | 1000sqft | 0.11 | 4,650.00 | 0 |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 3.5 | Precipitation Freq (Days) |
| :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 6 |  | Operational Year |  |

### 1.3 User Entered Comments \& Non-Default Data

## River Oaks Marketplace - Sacramento County, Summer

| Project Characteristics - Assume power is SMUD |  |  |
| :---: | :---: | :---: |
| Land Use - based on RFI |  |  |
| Construction Phase - based on RFI |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - Arch coat only |  |  |
| Off-road Equipment - |  |  |
| Grading - acre graded based on entire site size |  |  |
| Trips and VMT - from RFI or default if unknown |  |  |
| Vehicle Trips - NO VMT complete because the project size is exempt from CEQA VMT analysis. Trips based on traffic memo |  |  |
| Construction Off-road Equipment Mitigation - No Haul trucks. BMPs require twice daily watering. Tier 4 Final ran, if applicable |  |  |
| Table Name ${ }^{\text {a }}$ Column Name | Default Value | New Value |
| tblConstEquipMitigation | 0.00 | 1.00 |
|  | 0.00 | 4.00 |
|  | 0.00 | 1.00 |
| tbIConstEquipMitigation --- | 0.00 | 3.00 |
|  | 0.00 | 1.00 |
|  | 0.00 | 2.00 |
|  | 0.00 | 4.00 |
|  | 0.00 | 4.00 |
|  | 0.00 | 12.00 |
|  | 0.00 | 1.00 |
|  | 0.00 | 1.00 |
| tbiConstEquipMitigation | 0.00 | 4.00 |

River Oaks Marketplace - Sacramento County, Summer

| tblConstEquipMitigation | NumberOfEquipmentMitigated | 0.00 | 1.00 |
| :---: | :---: | :---: | :---: |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| -tblConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbIConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | -Tier 4 Final |
| - tbiConstEquipMitigation | Tier | No Change | Tier 4-Final |
| tblConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| - tbiConstEquipMitigation | Tier | No Change | Tier 4-Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4Final |
| tbiConstructionPhase | NumDays | 18.00 | 34.00 |
| tbiConstructionPhase | NumDays | 230.00 | 102.00 |
| tblConstructionPhase | NumDays | 5.00 | 48.00 |
| tbiConstructionPhase | NumDays | 18.00 | 47.00 |
| tbiConstructionPhase | NumDays | 8.00 | 48.00 |
| tbiConstructionPhase | PhaseEndDate | 6/7/2022 | 6/1/2022 |
| tbiConstructionPhase | PhaseEndDate | 4/18/2022 | 3/23/2022 |
| tbiConstructionPhase | PhaseEndDate | 5/12/2021 | 6/21/2021 |
| tbiConstructionPhase | PhaseEndDate | 5/31/2021 | 11/1/2021 |
| tbiConstructionPhase | PhaseEndDate | 5/12/2022 | 4/15/2022 |
| tbiConstructionPhase | PhaseEndDate | 5/19/2021 | 8/26/2021 |
| tbiconstructionPhase | PhaseStartDate | 5/13/2022 | -7/15/2022 |
| tbiConstructionPhase | PhaseStartDate | 6/1/2021 | 11/2/2021 |

River Oaks Marketplace - Sacramento County, Summer

| tblConstructionPhase | PhaseStartDate | 5/20/2021 | 8/27/2021 |
| :---: | :---: | :---: | :---: |
| tbiConstructionPhase | PhaseStartDate | 4/19/2022 | 3/23/2022 |
| tbiConstructionPhase | PhaseStartDate | 5/13/2021 | 6/22/2021 |
| tblGrading | AcresOfGrading | 24.00 | 5.23 |
| tbiTripsÄdVMT | WorkerTripNumber | 18.00 | 40.00 |
| tbiTripsAndVMT | WorkerTripNumber | 15.00 | 40.00 |
| tbiTripsÄndVMT | WorkerTripNumber | 20.00 | 40.00 |
| tbiTripsAndVMT | WorkerTripNumber | 81.00 | 80.00 |
| tbiVehicleTrips | ST"-TR | 1,448.33 | 914.62 |
| tbiVehicleTrips | ST_TR | 722.03 | 727.14 |
| tbiVehicleTrips | SU_TR | 1,182.08 | 914.62 |
| tbiVehicleTrips | SU_TR | 542.72 | 727.14 |
| tbiVehicleTrips | WD_TR | 845.60 | 914.62 |
| tbIVehicleTrips | WD_TR | 496.12 | 727.14 |

### 2.0 Emissions Summary

### 2.1 Overall Construction (Maximum Daily Emission) Unmitigated Construction

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| 2021 |  |  |  |  |  |  | 20.4171 | 10.0114 | 1.8828 | 11.8942 | 0.0000 | 4,003.276 | 4,003.276 | 1.2002 | 0.0000 | $\begin{gathered} 4,022.252 \\ 9 \end{gathered}$ |
| 2022 | 10.3813 | 20.2570 | 21.5780 | 0.0449 | 0.9228 | 0.9033 | 1.8261 | 0.2491 | 0.8547 | 1.1038 | 0.0000 | $4,374.643$ <br> 7 | $\begin{gathered} 4,374.643 \\ 7 \end{gathered}$ | 0.6923 | 0.0000 | $\begin{gathered} 4,391.950 \\ 7 \end{gathered}$ |
| Maximum | 10.3813 | 40.5792 | 22.3509 | 0.0449 | 18.3705 | 2.0465 | 20.4171 | 10.0114 | 1.8828 | 11.8942 | 0.0000 | $4,374.643$ <br> 7 | $4,374.643$ 7 | 1.2002 | 0.0000 | $\begin{array}{\|c} 4,391.950 \\ 7 \end{array}$ |

## Mitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| 2021 | 0.7473 | 5.6129 | 22.0656 | 0.0411 | 8.4341 | 0.0641 | 8.4982 | 4.5495 | 0.0640 | 4.6135 | 0.0000 | : $4,003.276$ | 4,003.276 | 1.2002 | 0.0000 | $4,022.252$ 9 |
| 2022 | 8.8280 | 5.5963 | 22.6936 | 0.0449 | 0.9228 | 0.0573 | 0.9801 | 0.2491 | 0.0566 | 0.3057 | - 0.0000 | : $4,374.643$ | (4,374.643 | 0.6923 | 0.000 | $\begin{gathered} 7,391.950 \\ 7 \end{gathered}$ |
| Maximum | 8.8280 | 5.6129 | 22.6936 | 0.0449 | 8.4341 | 0.0641 | 8.4982 | 4.5495 | 0.0640 | 4.6135 | 0.0000 | $\begin{gathered} 4,374.643 \\ 7 \end{gathered}$ | $\begin{gathered} 4,374.643 \\ 7 \end{gathered}$ | 1.2002 | 0.0000 | $\begin{array}{\|c} \hline 4,391.950 \\ 7 \end{array}$ |
|  | ROG | NOx | CO | SO2 | Fugitive <br> PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
| Percent Reduction | 33.64 | 81.57 | -1.89 | 0.00 | 51.50 | 95.88 | 57.39 | 53.23 | 95.60 | 62.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

### 2.2 Overall Operational

## Unmitigated Operational

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{gathered} \hline \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Area | 0.3208 | $\begin{aligned} & 1.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0285 |
| Energy | 0.0290 | 0.2636 | 0.2214 | $\begin{aligned} & 1.5800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | $\begin{gathered} 6.0600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 5.8000 \mathrm{e}- \\ & 003 \end{aligned}$ | 318.1499 |
| Mobile | 12.6792 | 31.4431 | 60.5521 | 0.1361 | 9.3112 | 0.1337 | 9.4449 | 2.4891 | 0.1248 | 2.6139 |  | $: \begin{gathered} 13,804.48 \\ : \end{gathered}$ | $\begin{aligned} & 13,804.48 \\ & 70 \end{aligned}$ | 0.8704 |  | $\begin{gathered} 13,826.24 \\ 59 \end{gathered}$ |
| Total | 13.0289 | 31.7068 | 60.7859 | 0.1377 | 9.3112 | 0.1537 | 9.4650 | 2.4891 | 0.1449 | 2.6340 |  | $\begin{gathered} 14,120.78 \\ 42 \end{gathered}$ | $\begin{array}{\|c\|} \hline 14,120.78 \\ 42 \end{array}$ | 0.8765 | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{array}{\|c} \hline 14,144.42 \\ 43 \end{array}$ |

## Mitigated Operational

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Area | 0.3208 | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0285 |
| Energy | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | ${ }^{316.2704}$ | 316.2704 | $\begin{gathered} 6.0600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | 318.1499 |
| Mobile | 12.6792 | 31.4431 | 60.5521 | 0.1361 | 9.3112 | 0.1337 | 9.4449 | 2.4891 | 0.1248 | 2.6139 |  | : | 13,804.48 | 0.8704 |  | $\begin{gathered} 13,826.24 \\ 59 \end{gathered}$ |
| Total | 13.0289 | 31.7068 | 60.7859 | 0.1377 | 9.3112 | 0.1537 | 9.4650 | 2.4891 | 0.1449 | 2.6340 |  | $\begin{array}{\|c\|} \hline 14,120.78 \\ 42 \end{array}$ | $\begin{array}{\|c\|} \hline 14,120.78 \\ \hline 2 \end{array}$ | 0.8765 | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 14,144.42 \\ 43 \end{gathered}$ |

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|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{array}{r} \hline \text { PM2.5 } \\ \text { Total } \end{array}$ | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Percent } \\ \text { Reduction } \end{gathered}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

### 3.0 Construction Detail

## Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Period 1a | Site Preparation | 14/15/2021 | 16/21/2021 |  | 481 |  |
| 2 | Period 1b | :Grading | 16/22/2021 | 18/26/2021 |  | 48! |  |
| 3 | Period 1c | Paving | 18/27/2021 | 11/1/2021 | 15 | 47! |  |
| 4 | Period 2a | Building Construction | 11/2/2021 | 3/23/2022 | 5 | 102 |  |
| 5 | Period 2b | Architectural Coating | 3/23/2022 | 14/15/2022 | ) 5 | 18! |  |
| 6 | Period 3 | :Paving | :4/15/2022 | :6/1/2022 | 5 | 34' |  |

## Acres of Grading (Site Preparation Phase): 0

## Acres of Grading (Grading Phase): 0

## Acres of Paving: 4.22

Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 15,045; Non-Residential Outdoor: 5,015; Striped Parking Area: 11,084 (Architectural Coating - sqft)

OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period 3 | Air Compressors | 0 | 0.00 | 78' | 0.48 |
| Period 2b | Cement and Mortar Mixers | 0 | 0.00 | 9 | 0.56 |
| Period 1a | Concrete/Industrial Saws | 0 |  | 811 | 0.73 |
| Period 1a | Excavators | 0 |  | 158: | 0.38 |

River Oaks Marketplace - Sacramento County, Summer

| Period 2a | Cranes | $1:$ | 7.00! | 231: | 0.29 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period 2a | :Forklifts | 3 | 8.00 | 89, | 0.20 |
| Period 1c | -Excavators | 0 | 0.00 | 158' | 0.38 |
| Period 2b | PPavers | 0 | 0.00 | 130 | 0.42 |
| Period 2b | :Rollers | 0 | 0.00 | 801 | 0.38 |
| Period 1a | Rubber Tired Dozers | 3 | 8.00 | 247! | 0.40 |
| Period 1c | :Rubber Tired Dozers | 0 | 0.00 | 247, | 0.40 |
| Period 2a | :Tractors/Loaders/Backhoes | 3 | 7.00 | 971 | 0.37 |
| Period 2a | :Generator Sets | 1 | 8.00 | 84' | 0.74 |
| Period 1c | :Tractors/Loaders/Backhoes | 1 | 8.00 | 97' | 0.37 |
| Period 2b | :Tractors/Loaders/Backhoes | 0 | 0.00 | 97' | 0.37 |
| Period 1b | :Tractors/Loaders/Backhoes | 3 | 8.00 | 97, | 0.37 |
| Period 1c | :Graders | 0 | 0.00 | 187! | 0.41 |
| Period 2b | Paving Equipment | 0 | 0.00 | 132 | 0.36 |
| Period 1b | :Rubber Tired Dozers | 1 | 8.00 | 247 | 0.40 |
| Period 2a | Welders | 1 | 8.00 | 46' | 0.45 |
| Period 2b | -Air Compressors | 1 | 6.00 | 781 | 0.48 |
| Period 1c | :Cement and Mortar Mixers | 2 | 6.00 | 91 | 0.56 |
| Period 3 | :Cement and Mortar Mixers | 2 | 6.00 | 91 | 0.56 |
| Period 1b | :Excavators | 1 | 8.00 | 158' | 0.38 |
| Period 1b | :Graders | 1 | 8.00 | 187 | 0.41 |
| Period 1c | Pavers | 1 | 8.00 | 130' | 0.42 |
| Period 3 | Pavers | 1 | 8.00 | 130 | 0.42 |
| Period 1c | Paving Equipment | 2 | 6.00 | 132 | 0.36 |
| Period 3 | :Paving Equipment | 2 | 6.00 | 132 | 0.36 |
| Period 1c | Rollers | 2 | 6.00 | 80, | 0.38 |
| Period 3 | :Rollers | 2 | 6.00! | 80: | 0.38 |

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| Period 3 | :Tractors/Loaders/Backhoes | $1:$ | 8.00 | 97: | 0.37 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period 1a | :Tractors/Loaders/Backhoes | 4 ! | 8.00! | 97: | 0.37 |

## Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period 1a | 7 | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Period 1b | 6 | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Period 1c |  | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_M ${ }^{\text {- }}$ | HHDT |
| Period 2 a |  | 80.00 | 32.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Period 2 b |  | 16.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_M ${ }^{\text {- }}$ | HHDT |
| Period 3 | 8 | 20.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |

### 3.1 Mitigation Measures Construction

Use Cleaner Engines for Construction Equipment
Water Exposed Area

### 3.2 Period 1a-2021

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 18.0663 | 0.0000 | 18.0663 | 9.9307 | 0.0000 | 9.9307 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 3.8882 | 40.4971 | 21.1543 | 0.0380 |  | 2.0445 | 2.0445 |  | 1.8809 | 1.8809 |  | ${ }_{9}^{3,685.656}$ | 3,685.656 | 1.1920 |  | $\begin{gathered} 3,715.457 \\ 3 \end{gathered}$ |
| Total | 3.8882 | 40.4971 | 21.1543 | 0.0380 | 18.0663 | 2.0445 | 20.1107 | 9.9307 | 1.8809 | 11.8116 |  | $\underset{9}{3,685.656}$ | $\begin{array}{\|c\|} \hline 3,685.656 \\ 9 \end{array}$ | 1.1920 |  | $\underset{3}{3,715.457}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{aligned} & 8.1600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 306.7956 |
| Total | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{aligned} & 8.1600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 306.7956 |

### 3.2 Period 1a-2021

## Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dus |  |  |  |  | 8.1298 | 0.0000 | 8.1298 | 4.4688 | 0.0000 | 4.4688 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 0.4656 | 2.0175 | 20.8690 | 0.0380 |  | 0.0621 | 0.0621 |  | 0.0621 | 0.0621 | 0.0000 | ${ }_{9}^{3,685.656}$ | ${ }_{9}^{3,685.656}$ | 1.1920 |  | ${ }_{3}^{3,715.457}$ |
| Total | 0.4656 | 2.0175 | 20.8690 | 0.0380 | 8.1298 | 0.0621 | 8.1919 | 4.4688 | 0.0621 | 4.5309 | 0.0000 | $\underset{9}{3,685.656}$ | ${ }_{9}^{3,685.656}$ | 1.1920 |  | $3,715.457$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e} \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{aligned} & 8.1600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 306.7956 |
| Total | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{aligned} & 8.1600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 306.7956 |

### 3.3 Period 1b-2021

## Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Tota | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 6.1376 | 0.0000 | 6.1376 | 3.3227 | 0.0000 | 3.3227 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 2.2903 | 24.7367 | 15.8575 | 0.0296 |  | 1.1599 | 1.1599 |  | 1.0671 | 1.0671 |  | $\left.\right\|_{5} ^{2,871.928}$ | $\begin{gathered} 2,871.928 \\ 5 \end{gathered}$ | 0.9288 |  | $\begin{gathered} 2,895.149 \\ 5 \end{gathered}$ |
| Total | 2.2903 | 24.7367 | 15.8575 | 0.0296 | 6.1376 | 1.1599 | 7.2976 | 3.3227 | 1.0671 | 4.3898 |  | $2,871.928$ <br> 5 | $\begin{gathered} 2,871.928 \\ 5 \end{gathered}$ | 0.9288 |  | $\underset{5}{2,895.149}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendo | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Work | 0.1603 | 0.0821 | 1.1966 | $\begin{aligned} & 3.0800 \mathrm{e}-\mathrm{-} \\ & 003 \end{aligned}$ | 0.3043 | $2.0500 \mathrm{e}-$ 003 | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{aligned} & 8.1600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 306.7956 |
| Total | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{aligned} & 2.0500 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{aligned} & 8.1600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 306.7956 |

### 3.3 Period 1b-2021

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 2.7619 | 0.0000 | 2.7619 | 1.4952 | 0.0000 | 1.4952 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road |  | 1.5737 | 17.7527 | 0.0296 |  | 0.0484 | 0.0484 |  | 0.0484 | 0.0484 | 0.0000 | ${ }_{5}^{2,871.928}$ | 2,871.928 | 0.9288 |  | $2,895.149$ |
| Total | 0.3632 | 1.5737 | 17.7527 | 0.0296 | 2.7619 | 0.0484 | 2.8104 | 1.4952 | 0.0484 | 1.5436 | 0.0000 | $\underset{5}{2,871.928}$ | $\begin{array}{\|c\|} \hline 2,871.928 \\ 5 \end{array}$ | 0.9288 |  | $\begin{array}{\|c} \hline 2,895.149 \\ 5 \end{array}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e} \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{aligned} & 8.1600 \mathrm{e}-\mathrm{-} \\ & 003 \end{aligned}$ |  | 306.7956 |
| Total | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{aligned} & 8.1600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 306.7956 |

### 3.4 Period 1c-2021

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 1.0940 | 10.8399 | 12.2603 | 0.0189 |  | 0.5788 | 0.5788 |  | 0.5342 | 0.5342 |  | ${ }^{1,804.552}$ | $\begin{gathered} 1,804.552 \\ 3 \end{gathered}$ | 0.5670 |  | ${ }_{\substack{1,818.727 \\ 0}}$ |
| Paving | 0.2352 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Total | 1.3292 | 10.8399 | 12.2603 | 0.0189 |  | 0.5788 | 0.5788 |  | 0.5342 | 0.5342 |  | $\begin{array}{\|c\|} \hline 1,804.552 \\ 3 \end{array}$ | $\begin{array}{\|c\|} \hline 1,804.552 \\ 3 \end{array}$ | 0.5670 |  | $\begin{array}{\|c} 1,818.727 \\ 0 \end{array}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1603 | 0.0821 | 1.1966 | $\begin{aligned} & 3.0800 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e} \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{gathered} 8.1600 \mathrm{e}- \\ 003 \end{gathered}$ |  | 306.7956 |
| Total | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{gathered} 8.1600 \mathrm{e}- \\ 003 \end{gathered}$ |  | 306.7956 |

### 3.4 Period 1c-2021

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 0.2194 | 0.9509 | 13.5323 | 0.0189 |  | 0.0293 | 0.0293 |  | 0.0293 | 0.0293 | 0.0000 | ${ }_{3}^{1,804.552}$ | ${ }_{3}^{1,804.552}$ | 0.5670 |  | 1,818.727 0 |
| Paving | 0.2352 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Total | 0.4547 | 0.9509 | 13.5323 | 0.0189 |  | 0.0293 | 0.0293 |  | 0.0293 | 0.0293 | 0.0000 | $\begin{array}{\|c\|} \hline 1,804.552 \\ 3 \end{array}$ | $\begin{array}{\|c\|} \hline 1,804.552 \\ 3 \end{array}$ | 0.5670 |  | $\begin{array}{\|c} 1,818.727 \\ 0 \end{array}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e} \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e} \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{aligned} & 1.8900 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{gathered} 8.1600 \mathrm{e}- \\ 003 \end{gathered}$ |  | 306.7956 |
| Total | 0.1603 | 0.0821 | 1.1966 | $\begin{gathered} 3.0800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 306.5916 | 306.5916 | $\begin{gathered} 8.1600 \mathrm{e}- \\ 003 \end{gathered}$ |  | 306.7956 |

### 3.5 Period 2a-2021

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 1.9009 | 17.4321 | 16.5752 | 0.0269 |  | 0.9586 | 0.9586 |  | 0.9013 | 0.9013 |  | $: \begin{gathered} 2,553.363 \\ \vdots \end{gathered}$ | 2,553.363 | 0.6160 |  | $\begin{gathered} 2,568.764 \\ 3 \end{gathered}$ |
| Total | 1.9009 | 17.4321 | 16.5752 | 0.0269 |  | 0.9586 | 0.9586 |  | 0.9013 | 0.9013 |  | $\left.\begin{array}{\|c\|} \hline 2,553.363 \\ 9 \end{array} \right\rvert\,$ | $\begin{array}{\|c\|} \hline 2,553.363 \\ 9 \end{array}$ | 0.6160 |  | $\underset{3}{2,568.764}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0989 | 3.2141 | 0.8207 | $\begin{gathered} 7.9000 \mathrm{e} \\ 003 \end{gathered}$ | 0.1926 | $\begin{gathered} 8.8200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.2014 | 0.0554 | $\begin{gathered} 8.4300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0638 |  | 836.7293 | 836.7293 | 0.0457 |  | 837.8726 |
| Worker |  | 0.1641 | 2.3932 | $\begin{gathered} 6.1600 \mathrm{e} \\ 003 \end{gathered}$ | 0.6086 | $\begin{gathered} 4.1100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6127 | 0.1614 | $\begin{gathered} 3.7900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1652 |  | 613.1832 | 613.1832 | 0.0163 |  | 613.5911 |
| Total | 0.4195 | 3.3782 | 3.2140 | 0.0141 | 0.8011 | 0.0129 | 0.8140 | 0.2168 | 0.0122 | 0.2291 |  | $\begin{array}{\|c\|} \hline 1,449.912 \\ 5 \end{array}$ | $\begin{gathered} 1,449.912 \\ 5 \end{gathered}$ | 0.0621 |  | $\begin{gathered} 1,451.463 \\ 7 \end{gathered}$ |

### 3.5 Period 2a-2021

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 0.3278 | 2.2347 | 17.4603 | 0.0269 |  | 0.0408 | 0.0408 |  | 0.0408 | 0.0408 | 0.0000 | $\begin{gathered} 2,553.363 \\ \vdots \\ \hline \end{gathered}$ | $\begin{gathered} 2,553.363 \\ 9 \end{gathered}$ | 0.6160 |  | $\underset{3}{2,568.764}$ |
| Total | 0.3278 | 2.2347 | 17.4603 | 0.0269 |  | 0.0408 | 0.0408 |  | 0.0408 | 0.0408 | 0.0000 | $\left.\begin{array}{\|c\|} \hline 2,553.363 \\ 9 \end{array} \right\rvert\,$ | $\begin{array}{\|c\|} \hline 2,553.363 \\ 9 \end{array}$ | 0.6160 |  | $\begin{array}{\|c} 2,568.764 \\ 3 \end{array}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0989 | 3.2141 | 0.8207 | $\begin{aligned} & 7.9000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.1926 | $\begin{gathered} 8.8200 \mathrm{e}- \\ 003 \end{gathered}$ | 0.2014 | 0.0554 | $\begin{aligned} & 8.4300 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0638 |  | 836.7293 | 836.7293 | 0.0457 |  | 837.8726 |
| Worker |  | 0.1641 | 2.3932 | $\begin{gathered} -7.1600 \mathrm{e} \\ 003 \end{gathered}$ | 0.6086 | $\begin{gathered} 4.1100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6127 | 0.1614 | $\begin{gathered} 3.7900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1652 |  | 613.1832 | 613.1832 | 0.0163 |  | 613.5911 |
| Total | 0.4195 | 3.3782 | 3.2140 | 0.0141 | 0.8011 | 0.0129 | 0.8140 | 0.2168 | 0.0122 | 0.2291 |  | $\begin{array}{\|c\|} \hline 1,449.912 \\ 5 \end{array}$ | $\begin{array}{\|c} 1,449.912 \\ 5 \end{array}$ | 0.0621 |  | $\underset{7}{1,451.463}$ |

### 3.5 Period 2a-2022

## Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO 2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road |  | 15.6156 | 16.3634 | 0.0269 |  | 0.8090 | 0.8090 |  | 0.7612 | 0.7612 |  | $2,554.333$ <br> 6 | 2,554.333 | 0.6120 |  | $\underset{2}{2,569.632}$ |
| Total | 1.7062 | 15.6156 | 16.3634 | 0.0269 |  | 0.8090 | 0.8090 |  | 0.7612 | 0.7612 |  | $\begin{array}{\|c\|} \hline 2,554.333 \\ 6 \end{array}$ | $\begin{array}{\|c\|} \hline 2,554.333 \\ 6 \end{array}$ | 0.6120 |  | $\underset{2}{2,569.632}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  |  |
| Vendor | 0.0918 | 3.0557 | 0.7562 | $7.82000-$ 003 | 0.1925 | 7.7200e- 003 | 0.2003 | 0.0554 | $7.3900 \mathrm{e}-$ 003 | 0.0628 |  | 829.4304 | 829.4304 | 0.0444 |  | 830.5407 |
| Worker |  | 0.1476 | 2.2040 | $\begin{gathered} 5.9400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6086 | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.6126 | 0.1614 | $\begin{gathered} 3.6900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1651 |  | 591.1930 | 591.1930 | 0.0147 |  | 591.5597 |
| Total | 0.3910 | 3.2033 | 2.9602 | 0.0138 | 0.8011 | 0.0117 | 0.8128 | 0.2168 | 0.0111 | 0.2279 |  | $1,420.623$ <br> 4 | $\begin{array}{\|c} \hline 1,420.623 \\ 4 \end{array}$ | 0.0591 |  | $\begin{aligned} & 1,422.100 \\ & \hline \end{aligned}$ |

### 3.5 Period 2a-2022

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO 2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 0.3278 | 2.2347 | 17.4603 | 0.0269 |  | 0.0408 | 0.0408 |  | 0.0408 | 0.0408 | 0.0000 | 2,554.333 | 2,554.333 | 0.6120 |  | $\begin{gathered} 2,569.632 \\ 2 \end{gathered}$ |
| Total | 0.3278 | 2.2347 | 17.4603 | 0.0269 |  | 0.0408 | 0.0408 |  | 0.0408 | 0.0408 | 0.0000 | $\begin{array}{\|c} \hline 2,554.333 \\ 6 \end{array}$ | $\begin{array}{\|c\|} \hline 2,554.333 \\ 6 \end{array}$ | 0.6120 |  | $\begin{gathered} 2,569.632 \\ 2 \end{gathered}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0918 | 3.0557 | 0.7562 | $\begin{gathered} 7.8200 \mathrm{e} \\ 003 \end{gathered}$ | 0.1925 | $\begin{gathered} 7.7200 \mathrm{e} \\ 003 \end{gathered}$ | 0.2003 | 0.0554 | $\begin{gathered} 7.3900 e- \\ 003 \end{gathered}$ | 0.0628 |  | 829.4304 | 829.4304 | 0.0444 |  | 830.5407 |
| Worker | 0.2993 | 0.1476 | 2.2040 | $\begin{gathered} -7.9400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6086 | $\begin{gathered} -\quad-0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6126 | 0.1614 | $\begin{gathered} 3 .-9900-- \\ 003 \end{gathered}$ | 0.1651 |  | 591.1930 | 591.1930 | 0.0147 |  | 591.5597 |
| Total | 0.3910 | 3.2033 | 2.9602 | 0.0138 | 0.8011 | 0.0117 | 0.8128 | 0.2168 | 0.0111 | 0.2279 |  | $\begin{array}{\|c\|} \hline 1,420.623 \\ 4 \end{array}$ | $\begin{gathered} 1,420.623 \\ 4 \end{gathered}$ | 0.0591 |  | $\underset{4}{1,422.100}$ |

### 3.6 Period 2b-2022

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Archit. Coating | 8.0196 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 0.2045 | 1.4085 | 1.8136 | $2.9700 \mathrm{e}-$ |  | 0.0817 | 0.0817 |  | 0.0817 | 0.0817 |  | 281.4481 | 281.4481 | 0.0183 |  | 281.9062 |
| Total | 8.2241 | 1.4085 | 1.8136 | $\begin{gathered} 2.9700 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0817 | 0.0817 |  | 0.0817 | 0.0817 |  | 281.4481 | 281.4481 | 0.0183 |  | 281.9062 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Work | 0.0599 | 0.0295 | 0.4408 | $1.1900 \mathrm{e}-$ | 0.1217 | $8.0000 \mathrm{e}-$ | 0.1225 | 0.0323 | $7.4000 \mathrm{e}-$ | 0.0330 |  | 118.2386 | 118.2386 | $2.9300 \mathrm{e}-$ |  | 118.3119 |
| Total | 0.0599 | 0.0295 | 0.4408 | $\begin{gathered} 1.1900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1217 | $8.0000 \mathrm{e}-$ | 0.1225 | 0.0323 | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0330 |  | 118.2386 | 118.2386 | $2.9300 \mathrm{e}-$ |  | 118.3119 |

### 3.6 Period 2b-2022

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Archit. Coating | 8.0196 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 0.0297 | 0.1288 | 1.8324 | $\begin{gathered} 2.9700 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.9600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 3.9600- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.9600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 3.9600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 281.4481 | 281.4481 | 0.0183 |  | 281.9062 |
| Total | 8.0493 | 0.1288 | 1.8324 | $\begin{gathered} 2.9700 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.9600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 3.9600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | $\begin{gathered} 3.9600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.9600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 281.4481 | 281.4481 | 0.0183 |  | 281.9062 |

## Mitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | $0.0000^{-1}$ |
| Worker |  | 0.0295 | 0.4408 | $1.1900 \mathrm{e}-$ | 0.1217 | $8.0000 \mathrm{e}-$ | 0.1225 | 0.0323 | $7.4000 \mathrm{e}-$ | 0.0330 |  | 118.2386 | 118.2386 | $2.9300 \mathrm{e}-$ |  | 118.3119 |
| Total | 0.0599 | 0.0295 | 0.4408 | $\begin{gathered} 1.1900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1217 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.1225 | 0.0323 | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0330 |  | 118.2386 | 118.2386 | $\begin{gathered} 2.9300 \mathrm{e}- \\ 003 \end{gathered}$ |  | 118.3119 |

### 3.7 Period 3-2022

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 0.9765 |  | 12.1940 | 0.0189 |  |  | 0.4877 |  | 0.4504 | 0.4504 |  | $\underset{7}{1,805.129}$ | ${ }^{1,805.129}$ | 0.5672 |  | $\begin{gathered} \hline 1,819.309 \\ 1 \end{gathered}$ |
| Paving | 0.3252 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Total | 1.3017 | 9.5221 | 12.1940 | 0.0189 |  | 0.4877 | 0.4877 |  | 0.4504 | 0.4504 |  | $1,805.129$ <br> 7 | $\begin{gathered} 1,805.129 \\ 7 \end{gathered}$ | 0.5672 |  | $1,819.309$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.0748 | 0.0369 | 0.5510 | $\begin{gathered} 1.4800 \mathrm{e} \\ 003 \end{gathered}$ | 0.1521 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1531 | 0.0404 | $\begin{gathered} 9.2000-- \\ 004 \end{gathered}$ | 0.0413 |  | 147.7983 | 147.7983 | $\begin{gathered} 3.6700 e- \\ 003 \end{gathered}$ |  | 147.8899 |
| Total | 0.0748 | 0.0369 | 0.5510 | $\begin{gathered} 1.4800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1521 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1531 | 0.0404 | $\begin{gathered} 9.2000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0413 |  | 147.7983 | 147.7983 | $\begin{gathered} 3.6700 \mathrm{e}- \\ 003 \end{gathered}$ |  | 147.8899 |

### 3.7 Period 3-2022

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2. 5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road |  | 0.9509 | 13.5323 | 0.0189 |  |  | 0.0293 |  |  |  | 0.0000 | ${ }_{1}^{1,805.129}$ | $\frac{1,805.129}{7}$ | 0.5672 |  | $\begin{gathered} 1,819.309 \\ 1 \end{gathered}$ |
| Paving | 0.3252 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Total | 0.5446 | 0.9509 | 13.5323 | 0.0189 |  | 0.0293 | 0.0293 |  | 0.0293 | 0.0293 | 0.0000 | $\begin{array}{\|c\|} \hline 1,805.129 \\ 7 \end{array}$ | $\begin{array}{\|c\|} \hline 1,805.129 \\ 7 \end{array}$ | 0.5672 |  | $1,819.309$ 1 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.0748 | 0.0369 | 0.5510 | $\begin{aligned} & 1.4800 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.1521 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.1531 | 0.0404 | $\begin{gathered} 9.2000 e- \\ 004 \end{gathered}$ | 0.0413 |  | 147.7983 | 147.7983 | $\begin{gathered} 3.6700 \mathrm{e}- \\ 003 \end{gathered}$ |  | 147.8899 |
| Total | 0.0748 | 0.0369 | 0.5510 | $\begin{aligned} & 1.4800 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.1521 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1531 | 0.0404 | $\begin{gathered} 9.2000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0413 |  | 147.7983 | 147.7983 | $\begin{gathered} 3.6700 \mathrm{e}- \\ 003 \end{gathered}$ |  | 147.8899 |

### 4.0 Operational Detail - Mobile

### 4.1 Mitigation Measures Mobile

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{array}{r} \text { PM2.5 } \\ \text { Total } \end{array}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Mitigated |  |  |  |  |  |  |  |  |  |  |  | ${ }^{13,804.48}$ | $\begin{gathered} 13,804.48 \\ 70 \end{gathered}$ | $0.8704$ |  | $\begin{gathered} 13,826.24 \\ 59 \end{gathered}$ |
| Unmitigated | 12.6792 |  |  | 0.1361 |  |  |  | 2.4891 | 0.1248 | 2.6139 |  | : | $\begin{gathered} 13,804.48 \\ 70 \end{gathered}$ | $0.8704$ |  | $\begin{aligned} & 13,826.24 \\ & 59 \end{aligned}$ |

### 4.2 Trip Summary Information

|  | Average Daily Trip Rate |  |  | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Convenience Market With Gas Pumps | 4,252.98 | 4,252.98 | 4252.98 | 1,687,510 | 1,687,510 |
| - ' Fast Food Restaurant with Drive Thru | 3,272.13 | 3,272.13 | 3272.13 | 2,260,370 | 2,260,370 |
| - - - Fast Food Restaurant with Drive Thru | 639.88 | 639.88 | 639.88 | - 442,028 | 442,028 |
| - - - - - - - - Other Asphalt Surfaces - - | $0.00$ | 0.00 | -0.00 |  |  |
| Parking Lot | 0.00 | 0.00 | 0.00 |  |  |
| Total | 8,165.00 | 8,165.00 | 8,165.00 | 4,389,908 | 4,389,908 |

### 4.3 Trip Type Information

River Oaks Marketplace - Sacramento County, Summer

|  | Miles |  |  | Trip \% |  |  | Trip Purpose \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted | Pass-by |
| Convenience Market With Gas | 10.00 | 5.00 | 6.50 | 0.80 | 80.20 | 19.00 | 14 | 21 | 65 |
| Fast Food Restaurant with Drive | 10.00 | 5.00 | 6.50 | 2.20 | 78.80 | 19.00 | 29 | 21 | 50 |
| Fast Food Restaurant with Drive | 10.00 | 5.00 | 6.50 | 2.20 | 78.80 | 19.00 | 29 | 21 | 50 |
| - "OBther Asphalt Surfaces | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |
| - 'Parking Lot | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

### 4.4 Fleet Mix

| Land Use | LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Convenience Market With Gas Pumps | 0.559527: | 0.038733: | 0.206173: | 0.118029: | 0.019040 | 0.005245 | 0.018552; | 0.023249: | 0.002031! | 0.002054 | 0.005884 | 0.000619 | 0.000865 |
| Fast Food Restaurant with Drive Thru | 0.559527: | 0.038733 | 0.206173 | 0.118029: | 0.019040 | 0.005245 | 0.018552 | 0.023249 | 0.002031 | 0.002054 | 0.005884 | 0.000619 | 0.000865 |
| Other Asphalt Surfaces | 0.559527 | 0.038733 | 0.206173 | 0.118029 | 0.019040 | 0.005245 | 0.018552 | 0.023249 | 0.002031 | 0.002054 | 0.005884 | 0.000619 | 0.000865 |
| Parking Lot | 0.559527 | 0.038733 | 0.206173: | 0.118029: | 0.019040 | 0.005245: | 0.018552 | 0.023249 | 0.002031: | 0.002054 | 0.005884: | 0.000619: | 0.000865 |

### 5.0 Energy Detail

Historical Energy Use: N
5.1 Mitigation Measures Energy

## River Oaks Marketplace - Sacramento County, Summer

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| NaturalGas Mitigated | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | 6.0600e- | $5.8000 \mathrm{e}-1$ 003 | 318.1499 |
| NaturalGas Unmitigated |  | 0.2636 | 0.2214 | ${ }^{1.58000-}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 |  | 6.0600e- | 5.8000e- | 318.1499 |

River Oaks Marketplace - Sacramento County, Summer

### 5.2 Energy by Land Use - NaturalGas

## Unmitigated

|  | NaturalGa s Use | ROG | NOx | CO | SO2 | $\begin{aligned} & \text { Fugitive } \\ & \text { PM10 } \end{aligned}$ | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Convenience Market With Gas Pumps | 69.0493 | 7.4000e- | $\begin{gathered} 6.7700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.6900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $5.1000 \mathrm{e}-$ 004 | $\begin{gathered} 5.1000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $5.1000 \mathrm{e}-$ 004 | 5.1000e- |  | 8.1235 | 8.1235 | $1.6000 \mathrm{e}-$ 004 | $1.5000 \mathrm{e}-$ 004 | 8.1717 |
| Fast Food Restaurant with Drive Thru | 2190.82 | 0.0236 | 0.2148 | 0.1804 | $1.29000-$ 003 |  | 0.0163 | 0.0163 |  | 0.0163 | 0.0163 |  | 257.7438 | 257.7438 | ${ }^{4.94000-}$ | $\begin{gathered} 4.7300-- \\ 003 \end{gathered}$ | 259.2754 |
| Fast Food Restaurant with Drive Thru | 428.427 | ${ }^{4.62000} 0$ | 0.0420 | 0.0353 | 2.5000e- |  | ${ }^{3.1900 e-}$ | ${ }^{3.19000 e-}$ |  | ${ }^{3.19000-}$ | 3.19000 003 |  | 50.4032 | 50.4032 | ${ }^{9} 904000 \mathrm{e}-$ | $\begin{gathered} 9.2000-- \\ 004 \end{gathered}$ | 50.7027 |
| Other Asphalt Surfaces |  |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | $\begin{gathered} 6.0700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | 318.1499 |

River Oaks Marketplace - Sacramento County, Summer

### 5.2 Energy by Land Use - NaturalGas

## Mitigated

|  | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Convenience Market With Gas Pumps | 0.0690493 | $\begin{gathered} 7.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 6.7700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.6900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $5.1000 \mathrm{e}-$ 004 | $\begin{gathered} 5.1000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{gathered} 5.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $5.1000 \mathrm{e}-$ 004 |  | 8.1235 | 8.1235 | $1.6000 \mathrm{e}-$ 004 | $\begin{gathered} 1.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 8.1717 |
| Fast Food Restaurant with Drive Thru | , 0.428427 | 4.6200 e 003 | 0.0420 | 0.0353 | $2.5000 \mathrm{e}-$ 004 |  | 3.1900 e 003 | $3.1900 \mathrm{e}-$ 003 |  | $3.1900 \mathrm{e}-$ 003 | $3.1900 \mathrm{e}-$ 003 |  | 50.4032 | 50.4032 | $9.7000 \mathrm{e}-$ 004 | $9.2000 \mathrm{e}-$ 004 | 50.7027 |
| Fast Food Restaurant with Drive Thru | -2.19082 | 0.0236 | 0.2148 | 0.1804 | $1.2900 \mathrm{e}-$ 003 |  | 0.0163 | 0.0163 |  | 0.0163 | 0.0163 |  | 257.7438 | 257.7438 | $4.9400 \mathrm{e}-\mathrm{-}$ 003 | 4.7-------- 003 | 259.2754 |
| Other Asphalt Surfaces | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | $\overline{0}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | $\begin{gathered} 6.0700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | 318.1499 |

### 6.0 Area Detail

### 6.1 Mitigation Measures Area

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Mitigated | 0.3208 | $1.1000 \mathrm{e}-$ 004 | 0.0125 | 0.0000 |  | $4.0000 \mathrm{e}-$ 005 | $4.0000 \mathrm{e}-$ 005 |  | 4.0000e- 005 | $4.0000 \mathrm{e}-$ 005 |  | 0.0268 | 0.0268 | $7.0000 \mathrm{e}-$ 005 |  | 0.0285 |
| Unmitigated | 0.3208 | $\begin{gathered} -1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} -0.000-- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ |  | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | $0.0268$ | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0285 |

### 6.2 Area by SubCategory

## Unmitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Architectural Coating | 0.0396 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Consumer Products | 0.2801 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Landscaping | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.1000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000-- \\ 005 \end{gathered}$ |  | 0.0285 |
| Total | 0.3208 | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & \hline 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000 e- \\ 005 \end{gathered}$ |  | 0.0285 |

### 6.2 Area by SubCategory

Mitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 <br> Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Architectural Coating | 0.0396 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Consumer Products | 0.2801 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Landscaping | $1.1600 \mathrm{e}-$ 003 | $1.1000 \mathrm{e}-$ 004 | 0.0125 | 0.0000 |  | 4.0000 e 005 | 4.0000 e 005 |  | $4.0000 \mathrm{e}-\mathrm{-}$ 005 | 4.0000 e 005 |  | 0.0268 | 0.0268 | $7.0000 \mathrm{e}-\mathrm{C}$ 005 |  | 0.0285 |
| Total | 0.3208 | $\begin{aligned} & 1.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{aligned} & \hline 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0285 |

### 7.0 Water Detail

7.1 Mitigation Measures Water

### 8.0 Waste Detail

### 8.1 Mitigation Measures Waste

### 9.0 Operational Offroad

| Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

### 10.0 Stationary Equipment

Fire Pumps and Emergency Generators

River Oaks Marketplace - Sacramento County, Summer

| Equipment Type | Number | Hours/Day | Hours/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Boilers |  |  |  |  |  |  |
| Equipment Type | Number | Heat Input/Day | Heat InputYear | Boiler Rating | Fuel Type |  |
| User Defined Equipment |  |  |  |  |  |  |
| Equipment Type | Number |  |  |  |  |  |

### 11.0 Vegetation

River Oaks Marketplace - Sacramento County, Winter

## River Oaks Marketplace

Sacramento County, Winter

### 1.0 Project Characteristics

### 1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Other Asphalt Surfaces | 3.24 | Acre | 3.24 | 141,134.40 | 0 |
| Parking Lot | 109.00 | Space | 0.98 | 43,600.00 | 0 |
| Fast Food Restaurant with Drive Thru | 4.50 | 1000sqft | 0.10 | 4,500.00 | 0 |
| Fast Food Restaurant with Drive Thru | 0.88 | 1000sqft | 0.02 | 880.00 | 0 |
| Convenience Market With Gas Pumps | 4.65 | 1000sqft | 0.11 | 4,650.00 | 0 |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 3.5 | Precipitation Freq (Days) |
| :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 6 |  | Operational Year |  |

### 1.3 User Entered Comments \& Non-Default Data

## River Oaks Marketplace - Sacramento County, Winter

| Project Characteristics - Assume power is SMUD |  |  |
| :---: | :---: | :---: |
| Land Use - based on RFI |  |  |
| Construction Phase - based on RFI |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - |  |  |
| Off-road Equipment - Arch coat only |  |  |
| Off-road Equipment - |  |  |
| Grading - acre graded based on entire site size |  |  |
| Trips and VMT - from RFI or default if unknown |  |  |
| Vehicle Trips - NO VMT complete because the project size is exempt from CEQA VMT analysis. Trips based on traffic memo |  |  |
| Construction Off-road Equipment Mitigation - No Haul trucks. BMPs require twice daily watering. Tier 4 Final ran, if applicable |  |  |
| Table Name Column Name | Default Value | New Value |
| tblConstEquipMitigation $\quad$ NumberOfEquipmentMitigated | 0.00 | 1.00 |
| tbIConstEquipMitigation :- NumberOfEquipmentMitigated | 0.00 | 4.00 |
|  | 0.00 | 1.00 |
| tbIConstEquipMitigation | 0.00 | 3.00 |
|  | 0.00 | 1.00 |
| tbIConstEquipMitigation : NumberOfEquipmentMitigated | 0.00 | 2.00 |
|  | 0.00 | 4.00 |
| tbIConstEquipMitigation | 0.00 | 4.00 |
|  | 0.00 | 12.00 |
|  | 0.00 | 1.00 |
|  | 0.00 | 1.00 |
| tblConstEquipMitigation | 0.00 | 4.00 |

River Oaks Marketplace - Sacramento County, Winter

| tblConstEquipMitigation | NumberOfEquipmentMitigated | 0.00 | 1.00 |
| :---: | :---: | :---: | :---: |
| tbIConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbIConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbIConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiconstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| - tbiConstEquipMitigation | Tier | No Change | Tier 4 Final |
| tbiConstructionPhase | NumDays | 18.00 | 34.00 |
| tbiconstructionPhase | NumDays | 230.00 | 102.00 |
| tbiConstructionPhase | NumDays | 5.00 | 48.00 |
| tbiConstructionPhase | NumDays | 18.00 | 47.00 |
| tbiConstructionPhase | NumDays | 8.00 | 48.00 |
| tbiConstructionPhase | PhaseEndDate | 6/7/2022 | 6/1/2022 |
| tbiConstructionPhase | PhaseEndDate | 4/18/2022 | 3/23/2022 |
| tbiconstructionPhase | PhaseEndDate | 5/12/2021 | 6/21/2021 |
| tbiConstructionPhase | PhaseEndDate | 5/31/2021 | 11/1/2021 |
| tbiConstructionPhase | PhaseEndDate | 5/12/2022 | 4/15/2022 |
| tbiConstructionPhase | PhaseEndDate | 5/19/2021 | 8/26/2021 |
| tbiconstructionPhase | PhaseStartDate | 5/13/2022 | 4/15/2022 |
| tbiConstructionPhase | PhaseStartDate | 6/1/2021 | 11/2/2021 |

River Oaks Marketplace - Sacramento County, Winter

| tblConstructionPhase | PhaseStartDate | 5/20/2021 | 8/27/2021 |
| :---: | :---: | :---: | :---: |
| tblConstructionPhase | PhaseStartDate | 4/19/2022 | 3/23/2022 |
| tbiconstructionPhase | PhaseStartDate | 5/13/2021 | 6/22/2021 |
| tbiGrading | AcresOfGrading | 24.00 | 5.23 |
| tbiTripsAndVMT | WorkerTripNumber | 18.00 | 40.00 |
| tblTripsAndVMT | WorkerTripNumber | 15.00 | 40.00 |
| tbiTripsAndVMT | WorkerTripNumber | 20.00 | 40.00 |
| tbiTripsAndVMT | WorkerTripNumber | 81.00 | 80.00 |
| tbiVehicleTrips | ST_TR | 1,448.33 | 914.62 |
| tblVehicleTrips | ST_TR | 722.03 | 727.14 |
| tbiVehicleTrips | SU̇-TR | 1,182.08 | 914.62 |
| tblVehicleTrips | SU_TR | 542.72 | 727.14 |
| tbiVehicleTrips | WD_TR | 845.60 | 914.62 |
| tbiVehicleTrips | WD_TR | 496.12 | 727.14 |

### 2.0 Emissions Summary

### 2.1 Overall Construction (Maximum Daily Emission) Unmitigated Construction

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| 2021 |  |  | 22.1749 |  |  | 2.0465 | 20.4171 | 10.0114 | 1.8828 | 11.8942 | 0.0000 | \%,954.922 | 3,954.922 | 1.1992 | 0.0000 | $\begin{gathered} 3,984.902 \\ 4 \end{gathered}$ |
| 2022 | 10.3589 | 20.3433 | 21.3011 | 0.0438 | 0.9228 | 0.9038 | 1.8266 | 0.2491 | 0.8552 | 1.1043 | 0.0000 | ${ }_{9}^{4,266.843}$ | $\begin{gathered} 4,266.843 \\ 9 \end{gathered}$ | 0.6938 | 0.0000 | $\begin{gathered} 4,284.189 \\ 7 \end{gathered}$ |
| Maximum | 10.3589 | 40.5985 | 22.1749 | 0.0438 | 18.3705 | 2.0465 | 20.4171 | 10.0114 | 1.8828 | 11.8942 | 0.0000 | $\begin{array}{\|c\|} \hline 4,266.843 \\ 9 \end{array}$ | $\begin{gathered} 4,266.843 \\ 9 \end{gathered}$ | 1.1992 | 0.0000 | $\begin{gathered} 4,284.189 \\ 7 \end{gathered}$ |

## Mitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| 2021 | 0.7279 | 5.7044 | 21.8896 | 0.0407 | 8.4341 | 0.0641 | 8.4982 | 4.5495 | 0.0640 | 4.6135 | 0.0000 | : $3,954.922$ | : $3,954.922$ | 1.1992 | 0.0000 | $3,984.902$ 4 |
| 2022 | 8.8057 | 5.6827 | 22.4168 | 0.0438 | 0.9228 | 0.0578 | 0.9806 | 0.2491 | 0.0570 | 0.3062 | 0.0000 | :$4,266.843$ <br>  | :4,266.843 <br>  | 0.6938 | 0.0000 | $4,284.189$ |
| Maximum | 8.8057 | 5.7044 | 22.4168 | 0.0438 | 8.4341 | 0.0641 | 8.4982 | 4.5495 | 0.0640 | 4.6135 | 0.0000 | $\begin{gathered} 4,266.843 \\ 9 \end{gathered}$ | $\begin{gathered} 4,266.843 \\ 9 \end{gathered}$ | 1.1992 | 0.0000 | $\begin{gathered} 4,284.189 \\ 7 \end{gathered}$ |
|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
| Percent Reduction | 33.77 | 81.31 | -1.91 | 0.00 | 51.50 | 95.87 | 57.39 | 53.23 | 95.58 | 62.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

### 2.2 Overall Operational

## Unmitigated Operational

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Area | 0.3208 | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | 0.0268 | $\begin{aligned} & 7.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | 0.0285 |
| Energy | 0.0290 | 0.2636 | 0.2214 | $\begin{aligned} & 1.5800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | $\begin{gathered} 6.0600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | 318.1499 |
| Mobile | 8.7172 | 32.1067 | 69.2273 | 0.1235 | 9.3112 | 0.1396 | 9.4508 | 2.4891 | 0.1305 | 2.6196 |  | :12,511.368 | 12,511.368 | 0.9522 |  | $\begin{gathered} 12,535.17 \\ 43 \end{gathered}$ |
| Total | 9.0669 | 32.3704 | 69.4612 | 0.1251 | 9.3112 | 0.1597 | 9.4709 | 2.4891 | 0.1505 | 2.6397 |  | $\begin{gathered} 12,827.66 \\ 53 \end{gathered}$ | $\begin{array}{\|c} \hline 12,827.66 \\ 53 \end{array}$ | 0.9584 | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{array}{\|c} \hline 12,853.35 \\ 26 \end{array}$ |

## Mitigated Operational

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | 1b/day |  |  |  |  |  |
| Area | 0.3208 | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0285 |
| Energy | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | $\begin{gathered} -0 .-00-0 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 5.8000 \mathrm{e} \\ 003 \end{gathered}$ | 318.1499 |
| Mobile | 8.7172 | 32.1067 | 69.2273 | 0.1235 | 9.3112 | 0.1396 | 9.4508 | 2.4891 | 0.1305 | 2.6196 |  |  | 12,511.368: | 0.9522 |  | $\begin{gathered} 12,535.17 \\ 43 \end{gathered}$ |
| Total | 9.0669 | 32.3704 | 69.4612 | 0.1251 | 9.3112 | 0.1597 | 9.4709 | 2.4891 | 0.1505 | 2.6397 |  | $\begin{array}{\|c\|} \hline 12,827.66 \\ 53 \end{array}$ | $\begin{array}{\|c\|} \hline 12,827.66 \\ 53 \end{array}$ | 0.9584 | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 12,853.35 \\ 26 \end{gathered}$ |

River Oaks Marketplace - Sacramento County, Winter

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | $\begin{array}{r} \text { PM2.5 } \\ \text { Total } \end{array}$ | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percent Reduction | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

### 3.0 Construction Detail

## Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Period 1a | :Site Preparation | 4/15/2021 | 16/21/2021 |  | 48' |  |
| 2 | Period 1b | :Grading | 16/22/2021 | 18/26/2021 | 5 | 48! |  |
| 3 | Period 1c | Paving | 18/27/2021 | 111/1/2021 | 5 | 471 |  |
| 4 | Period 2a | Building Construction | 11/2/2021 | 3/23/2022 | 5 | 102 |  |
| 5 | Period 2b | Architectural Coating | 3/23/2022 | 14/15/2022 | 5 | 18! |  |
| 6 | Period 3 | PPaving | ;4/15/2022 | :6/1/2022 |  | 34; |  |

## Acres of Grading (Site Preparation Phase): 0

## Acres of Grading (Grading Phase): 0

## Acres of Paving: 4.22

Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 15,045; Non-Residential Outdoor: 5,015; Striped Parking Area: 11,084 (Architectural Coating - sqft)

OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period 3 | Air Compressors | 0 | 0.00 | 78' | 0.48 |
| Period 2b | Cement and Mortar Mixers | 0 | 0.00 | 9 | 0.56 |
| Period 1a | Concrete/Industrial Saws | 0 |  | 811 | 0.73 |
| Period 1a | Excavators | 0 |  | 158: | 0.38 |

River Oaks Marketplace - Sacramento County, Winter

| Period 2a | Cranes | $1:$ | 7.00! | 231: | 0.29 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period 2a | :Forklifts | 3 | 8.00 | 89' | 0.20 |
| Period 1c | Excavators | 0 | 0.001 | 158' | 0.38 |
| Period 2b | PPavers | 0 | 0.00 | 130 | 0.42 |
| Period 2b | :Rollers | 0 | 0.00 | 801 | 0.38 |
| Period 1a | Rubber Tired Dozers | 3 | 8.00 | 2471, | 0.40 |
| Period 1c | :Rubber Tired Dozers | 0 | 0.00 | 247! | 0.40 |
| Period 2a | Tractors/Loaders/Backhoes | 3 | 7.00 | 971 | 0.37 |
| Period 2a | :Generator Sets | 1 | 8.00 | 84' | 0.74 |
| Period 1c | Tractors/Loaders/Backhoes | 1 | 8.00 | 97' | 0.37 |
| Period 2b | :Tractors/Loaders/Backhoes | 0 | 0.00 | 971 | 0.37 |
| Period 1b | :Tractors/Loaders/Backhoes | 3 | 8.00 | 97, | 0.37 |
| Period 1c | :Graders | 0 | 0.00 | 187! | 0.41 |
| Period 2b | :Paving Equipment | 0 | 0.00 | 132' | 0.36 |
| Period 1b | :Rubber Tired Dozers | 1 | 8.00 | 247, | 0.40 |
| Period 2a | Welders | 1 | 8.00 | 46' | 0.45 |
| Period 2b | :Air Compressors | 1 | 6.00 | 78' | 0.48 |
| Period 1c | Cement and Mortar Mixers | 2 | 6.00 | 91 | 0.56 |
| Period 3 | Cement and Mortar Mixers | 2 | 6.00 | 91 | 0.56 |
| Period 1b | Excavators | 1 | 8.00 | 158'-1 | 0.38 |
| Period 1b | :Graders | 1 | 8.00 | 187 | 0.41 |
| Period 1c | Pavers | 1 | 8.00 | 130 | 0.42 |
| Period 3 | Pavers | 1 | 8.00 | 130 | 0.42 |
| Period 1c | Paving Equipment | 2 | 6.00 | 132' | 0.36 |
| Period 3 | Paving Equipment | 2 | 6.001 | 132 | 0.36 |
| Period 1c | Rollers | 2 | 6.00 | 80' | 0.38 |
| Period 3 | :Rollers | 2 | 6.00! | 80! | 0.38 |

River Oaks Marketplace - Sacramento County, Winter

| Period 3 | :Tractors/Loaders/Backhoes | $1:$ | 8.00 | 97: | 0.37 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period 1a | Tractors/Loaders/Backhoes | 4 | 8.00: | 97: | 0.37 |

## Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period 1a | 7 | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Period 1b | 6 | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Period 1c |  | 40.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_M ${ }^{\text {- }}$ | HHDT |
| Period 2 a |  | 80.00 | 32.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Period 2 b |  | 16.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_M ${ }^{\text {- }}$ | HHDT |
| Period 3 | 8 | 20.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | D_Mix | HDT_Mix | HHDT |

### 3.1 Mitigation Measures Construction

Use Cleaner Engines for Construction Equipment
Water Exposed Area

### 3.2 Period 1a-2021

## Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 18.0663 | 0.0000 | 18.0663 | 9.9307 | 0.0000 | 9.9307 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 3.8882 | 40.4971 | 21.1543 | 0.0380 |  | 2.0445 | 2.0445 |  | 1.8809 | 1.8809 |  | ${ }_{9}^{3,685.656}$ | $\begin{gathered} 9,685.656 \\ \hline \end{gathered}$ | 1.1920 |  | $\begin{gathered} 3,715.457 \\ \hline \end{gathered}$ |
| Total | 3.8882 | 40.4971 | 21.1543 | 0.0380 | 18.0663 | 2.0445 | 20.1107 | 9.9307 | 1.8809 | 11.8116 |  | $\underset{9}{3,685.656}$ | $\begin{gathered} 3,685.656 \\ 9 \end{gathered}$ | 1.1920 |  | $\underset{3}{3,715.457}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendo | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Work | 0.1476 | 0.1014 | 1.0207 | $2.7000 \mathrm{e}-$ 003 | 0.3043 | $2.0500 \mathrm{e}-$ 003 | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{aligned} & 7.1800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 269.4451 |
| Total | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{aligned} & 2.0500 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{aligned} & 7.1800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 269.4451 |

### 3.2 Period 1a-2021

## Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | 1b/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 8.1298 | 0.0000 | 8.1298 | 4.4688 | 0.0000 | 4.4688 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 0.4656 | 2.0175 | 20.8690 | 0.0380 |  | 0.0621 | 0.0621 |  | 0.0621 | 0.0621 | 0.0000 | $:$ | $\begin{array}{\|c} 3,685.656 \\ 9 \end{array}$ | 1.1920 |  | $\begin{gathered} 3,715.457 \\ 3 \end{gathered}$ |
| Total | 0.4656 | 2.0175 | 20.8690 | 0.0380 | 8.1298 | 0.0621 | 8.1919 | 4.4688 | 0.0621 | 4.5309 | 0.0000 | ($3,685.656$ | $\begin{array}{\|c} 3,685.656 \\ 9 \end{array}$ | 1.1920 |  | $\begin{array}{\|c} \hline 3,715.457 \\ 3 \end{array}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e} \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | , 269.2657 | 269.2657 | $\begin{aligned} & 7.1800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 269.4451 |
| Total | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{gathered} 7.1800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 269.4451 |

### 3.3 Period 1b-2021

## Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Tota | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 6.1376 | 0.0000 | 6.1376 | 3.3227 | 0.0000 | 3.3227 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 2.2903 | 24.7367 | 15.8575 | 0.0296 |  | 1.1599 | 1.1599 |  | 1.0671 | 1.0671 |  | $\left.\right\|_{5} ^{2,871.928}$ | $\begin{gathered} 2,871.928 \\ 5 \end{gathered}$ | 0.9288 |  | $\begin{gathered} 2,895.149 \\ 5 \end{gathered}$ |
| Total | 2.2903 | 24.7367 | 15.8575 | 0.0296 | 6.1376 | 1.1599 | 7.2976 | 3.3227 | 1.0671 | 4.3898 |  | $2,871.928$ <br> 5 | $\begin{gathered} 2,871.928 \\ 5 \end{gathered}$ | 0.9288 |  | $\underset{5}{2,895.149}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendo | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Work | 0.1476 | 0.1014 | 1.0207 | $2.7000 \mathrm{e}-$ 003 | 0.3043 | $2.0500 \mathrm{e}-$ 003 | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{aligned} & 7.1800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 269.4451 |
| Total | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{aligned} & 2.0500 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{aligned} & 7.1800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 269.4451 |

### 3.3 Period 1b-2021

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | 1b/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 2.7619 | 0.0000 | 2.7619 | 1.4952 | 0.0000 | 1.4952 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 0.3632 | 1.5737 | 17.7527 | 0.0296 |  | 0.0484 | 0.0484 |  | 0.0484 | 0.0484 | 0.0000 | ${ }^{2} 8$ | $\begin{gathered} 2,871.928 \\ 5 \end{gathered}$ | 0.9288 |  | $\begin{gathered} 2,895.149 \\ 5 \end{gathered}$ |
| Total | 0.3632 | 1.5737 | 17.7527 | 0.0296 | 2.7619 | 0.0484 | 2.8104 | 1.4952 | 0.0484 | 1.5436 | 0.0000 | $\begin{array}{\|c\|} \hline 2,871.928 \\ 5 \end{array}$ | $\begin{array}{\|c\|} \hline 2,871.928 \\ 5 \end{array}$ | 0.9288 |  | $\begin{gathered} 2,895.149 \\ 5 \end{gathered}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e} \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | , 269.2657 | 269.2657 | $\begin{aligned} & 7.1800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 269.4451 |
| Total | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{gathered} 7.1800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 269.4451 |

### 3.4 Period 1c-2021

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 1.0940 | 10.8399 | 12.2603 | 0.0189 |  | 0.5788 | 0.5788 |  | 0.5342 | 0.5342 |  | ${ }^{1,804.552}$ | $\begin{gathered} 1,804.552 \\ 3 \end{gathered}$ | 0.5670 |  | ${ }_{\substack{1,818.727 \\ 0}}$ |
| Paving | 0.2352 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Total | 1.3292 | 10.8399 | 12.2603 | 0.0189 |  | 0.5788 | 0.5788 |  | 0.5342 | 0.5342 |  | $\begin{array}{\|c\|} \hline 1,804.552 \\ 3 \end{array}$ | $\begin{array}{\|c\|} \hline 1,804.552 \\ 3 \end{array}$ | 0.5670 |  | $\begin{array}{\|c} 1,818.727 \\ 0 \end{array}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e} \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e} \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{aligned} & 7.1800 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 269.4451 |
| Total | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{gathered} \hline 7.1800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 269.4451 |

### 3.4 Period 1c-2021

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 0.2194 | 0.9509 | 13.5323 | 0.0189 |  | 0.0293 | 0.0293 |  | 0.0293 | 0.0293 | 0.0000 | ${ }_{3}^{1,804.552}$ | ${ }_{3}^{1,804.552}$ | 0.5670 |  | 1,818.727 0 |
| Paving | 0.2352 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Total | 0.4547 | 0.9509 | 13.5323 | 0.0189 |  | 0.0293 | 0.0293 |  | 0.0293 | 0.0293 | 0.0000 | $\begin{array}{\|c\|} \hline 1,804.552 \\ 3 \end{array}$ | $\begin{array}{\|c\|} \hline 1,804.552 \\ 3 \end{array}$ | 0.5670 |  | $\begin{array}{\|c} 1,818.727 \\ 0 \end{array}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} --7 .--\overline{-7} 000 \mathrm{e} \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900-- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{gathered} 7.1800- \\ 003 \end{gathered}$ |  | 269.4451 |
| Total | 0.1476 | 0.1014 | 1.0207 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3043 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.3063 | 0.0807 | $\begin{gathered} 1.8900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0826 |  | 269.2657 | 269.2657 | $\begin{gathered} 7.1800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 269.4451 |

### 3.5 Period 2a-2021

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 1.9009 | 17.4321 | 16.5752 | 0.0269 |  | 0.9586 | 0.9586 |  | 0.9013 | 0.9013 |  | ${ }_{9}^{2,553.363}$ | $\begin{gathered} 2,553.363 \\ 9 \end{gathered}$ | 0.6160 |  | $\begin{gathered} 2,568.764 \\ 3 \end{gathered}$ |
| Total | 1.9009 | 17.4321 | 16.5752 | 0.0269 |  | 0.9586 | 0.9586 |  | 0.9013 | 0.9013 |  | $\begin{array}{\|c\|} \hline 2,553.363 \\ 9 \end{array}$ | $\begin{array}{\|c\|} \hline 2,553.363 \\ 9 \end{array}$ | 0.6160 |  | $\underset{3}{2,568.764}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  |  |
| Vendor | 0.1048 | 3.2670 | 0.9519 | 7.7000 e 003 | 0.1926 | $9.3600 e-$ 003 | 0.2019 | 0.0554 | $8.9600 e-$ 003 | 0.0644 |  | 815.2066 | 815.2066 | 0.0495 |  | 816.4447 |
| Worker |  | 0.2027 | 2.0413 | $\begin{gathered} 5.4100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6086 | $\begin{gathered} 4.1100-\mathrm{e} \\ 003 \end{gathered}$ | 0.6127 | 0.1614 | $\begin{gathered} 3.7900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1652 |  | 538.5314 | 538.5314 | 0.0144 |  | 538.8902 |
| Total | 0.4000 | 3.4697 | 2.9932 | 0.0131 | 0.8011 | 0.0135 | 0.8146 | 0.2168 | 0.0128 | 0.2296 |  | $\begin{array}{\|c\|} \hline 1,353.738 \\ 0 \end{array}$ | $\begin{array}{\|c\|} \hline 1,353.738 \\ 0 \end{array}$ | 0.0639 |  | $\begin{gathered} 1,355.334 \\ 9 \end{gathered}$ |

### 3.5 Period 2a-2021

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | 1b/day |  |  |  |  |  |
| Off-Road | 0.3278 | 2.2347 | 17.4603 | 0.0269 |  | 0.0408 | 0.0408 |  | 0.0408 | 0.0408 | 0.0000 | ${ }_{9}^{2,553.363}$ | $\text { i, } 253.363$ | 0.6160 |  | $\begin{gathered} 2,568.764 \\ 3 \end{gathered}$ |
| Total | 0.3278 | 2.2347 | 17.4603 | 0.0269 |  | 0.0408 | 0.0408 |  | 0.0408 | 0.0408 | 0.0000 | $\begin{array}{\|c\|} \hline 2,553.363 \\ 9 \end{array}$ | $\begin{array}{\|c\|} \hline 2,553.363 \\ 9 \end{array}$ | 0.6160 |  | $\underset{3}{2,568.764}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  |  |
| Vendor | 0.1048 | 3.2670 | 0.9519 | 7.7000 e 003 | 0.1926 | $9.3600 e-$ 003 | 0.2019 | 0.0554 | $8.9600 e-$ 003 | 0.0644 |  | 815.2066 | 815.2066 | 0.0495 |  | 816.4447 |
| Worker |  | 0.2027 | 2.0413 | $\begin{gathered} 5.4100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6086 | $\begin{gathered} 4.1100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6127 | 0.1614 | $\begin{gathered} 3.7900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1652 |  | 538.5314 | 538.5314 | 0.0144 |  | 538.8902 |
| Total | 0.4000 | 3.4697 | 2.9932 | 0.0131 | 0.8011 | 0.0135 | 0.8146 | 0.2168 | 0.0128 | 0.2296 |  | $\begin{array}{\|c\|} \hline 1,353.738 \\ 0 \end{array}$ | $\begin{array}{\|c\|} \hline 1,353.738 \\ 0 \end{array}$ | 0.0639 |  | $\begin{gathered} 1,355.334 \\ 9 \end{gathered}$ |

### 3.5 Period 2a-2022

## Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2. 5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 1.7062 | 15.6156 | 16.3634 | 0.0269 |  | 0.8090 | 0.8090 |  | 0.7612 |  |  | $\underset{\substack{2,554.333 \\ 6}}{ }$ | 2,554.333 | 0.6120 |  | $\begin{gathered} 2,569.632 \\ 2 \end{gathered}$ |
| Total | 1.7062 | 15.6156 | 16.3634 | 0.0269 |  | 0.8090 | 0.8090 |  | 0.7612 | 0.7612 |  | $\left.\begin{array}{\|c\|} \hline 2,554.333 \\ 6 \end{array} \right\rvert\,$ | $\begin{array}{\|c\|} \hline 2,554.333 \\ 6 \end{array}$ | 0.6120 |  | $\underset{2}{2,569.632}$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{array}{r} \text { PM2.5 } \\ \text { Total } \end{array}$ | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  |  |
| Vendor | 0.0972 | 3.1005 | 0.8779 | $7.62000-$ 003 | 0.1925 | $8.2300 \mathrm{e}-$ 003 | 0.2008 | 0.0554 | $7.8700 \mathrm{e}-$ 003 | 0.0633 |  | 807.9632 | 807.9632 | 0.0481 |  | 809.1661 |
| Worker |  | 0.1822 | 1.8719 | $\begin{gathered} 5.2100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6086 | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.6126 | 0.1614 | $\begin{gathered} 3.6900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1651 |  | 519.2493 | 519.2493 | 0.0129 |  | 519.5710 |
| Total | 0.3734 | 3.2828 | 2.7497 | 0.0128 | 0.8011 | 0.0122 | 0.8133 | 0.2168 | 0.0116 | 0.2284 |  | $\begin{array}{\|c\|} \hline 1,327.212 \\ 4 \end{array}$ | $\begin{array}{\|c\|} \hline 1,327.212 \\ 4 \end{array}$ | 0.0610 |  | $\begin{gathered} 1,328.737 \\ \hline \end{gathered}$ |

### 3.5 Period 2a-2022

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 0.3278 | 2.2347 | 17.4603 | 0.0269 |  | 0.0408 | 0.0408 |  | 0.0408 | 0.0408 | 0.0000 | : ${ }^{2,554.333}$ | $\begin{gathered} 2,554.333 \\ 6 \end{gathered}$ | 0.6120 |  | $\begin{gathered} 2,569.632 \\ 2 \end{gathered}$ |
| Total | 0.3278 | 2.2347 | 17.4603 | 0.0269 |  | 0.0408 | 0.0408 |  | 0.0408 | 0.0408 | 0.0000 | $\begin{array}{\|c\|} \hline 2,554.333 \\ 6 \end{array}$ | $\begin{gathered} 2,554.333 \\ 6 \end{gathered}$ | 0.6120 |  | $\begin{gathered} 2,569.632 \\ 2 \end{gathered}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | 1b/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0972 | 3.1005 | 0.8779 | $\begin{gathered} 7.6200 \mathrm{e} \\ 003 \end{gathered}$ | 0.1925 | $\begin{gathered} 8.2300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.2008 | 0.0554 | $\begin{gathered} 7.8700 e- \\ 003 \end{gathered}$ | 0.0633 |  | 807.9632 | 807.9632 | 0.0481 |  | 809.1661 |
| Worker | 0.2761 | 0.1822 | 1.8719 | $\begin{gathered} 5.2100 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6086 | $\begin{gathered} -\quad-0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.6126 | 0.1614 | $\begin{gathered} 3 .-9900-- \\ 003 \end{gathered}$ | 0.1651 |  | 519.2493 | 519.2493 | 0.0129 |  | 519.5710 |
| Total | 0.3734 | 3.2828 | 2.7497 | 0.0128 | 0.8011 | 0.0122 | 0.8133 | 0.2168 | 0.0116 | 0.2284 |  | $\begin{array}{\|c\|} \hline 1,327.212 \\ 4 \end{array}$ | $\begin{array}{\|c\|} \hline 1,327.212 \\ 4 \end{array}$ | 0.0610 |  | $\underset{2}{1,328.737}$ |

### 3.6 Period 2b-2022

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Archit. Coating | 8.0196 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 0.2045 | 1.4085 | 1.8136 | $2.9700 \mathrm{e}-$ 003 |  | 0.0817 | 0.0817 |  | 0.0817 | 0.0817 |  | 281.4481 | 281.4481 | 0.0183 |  | 281.9062 |
| Total | 8.2241 | 1.4085 | 1.8136 | $\begin{gathered} 2.9700 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0817 | 0.0817 |  | 0.0817 | 0.0817 |  | 281.4481 | 281.4481 | 0.0183 |  | 281.9062 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | $\begin{gathered} \text { Fugitive } \\ \text { PM10 } \end{gathered}$ | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | $0.0000^{-1}$ |
| Worker |  | 0.0365 | 0.3744 | $1.0400 \mathrm{e}-$ | 0.1217 | $8.0000 \mathrm{e}-$ | 0.1225 | 0.0323 | $7.4000 \mathrm{e}-$ | 0.0330 |  | 103.8499 | 103.8499 | $2.5700 \mathrm{e}-$ |  | 103.9142 |
| Total | 0.0552 | 0.0365 | 0.3744 | $\begin{gathered} 1.0400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1217 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.1225 | 0.0323 | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0330 |  | 103.8499 | 103.8499 | $\begin{gathered} 2.5700 \mathrm{e}- \\ 003 \end{gathered}$ |  | 103.9142 |

### 3.6 Period 2b-2022

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Archit. Coating | 8.0196 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Off-Road | 0.0297 | 0.1288 | 1.8324 | $\begin{gathered} 2.9700 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.9600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 3.9600- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.9600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 3.9600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 281.4481 | 281.4481 | 0.0183 |  | 281.9062 |
| Total | 8.0493 | 0.1288 | 1.8324 | $\begin{gathered} 2.9700 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.9600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 3.9600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | $\begin{gathered} 3.9600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.9600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 281.4481 | 281.4481 | 0.0183 |  | 281.9062 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | $\begin{gathered} \text { Fugitive } \\ \text { PM10 } \end{gathered}$ | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | $0.0000^{-1}$ |
| Worker |  | 0.0365 | 0.3744 | $1.0400 \mathrm{e}-$ | 0.1217 | $8.0000 \mathrm{e}-$ | 0.1225 | 0.0323 | $7.4000 \mathrm{e}-$ | 0.0330 |  | 103.8499 | 103.8499 | $2.5700 \mathrm{e}-$ |  | 103.9142 |
| Total | 0.0552 | 0.0365 | 0.3744 | $\begin{gathered} 1.0400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1217 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.1225 | 0.0323 | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0330 |  | 103.8499 | 103.8499 | $\begin{gathered} 2.5700 \mathrm{e}- \\ 003 \end{gathered}$ |  | 103.9142 |

### 3.7 Period 3-2022

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 0.9765 |  | 12.1940 | 0.0189 |  |  | 0.4877 |  | 0.4504 | 0.4504 |  | $\underset{7}{1,805.129}$ | ${ }^{1,805.129}$ | 0.5672 |  | $\begin{gathered} \hline 1,819.309 \\ 1 \end{gathered}$ |
| Paving | 0.3252 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Total | 1.3017 | 9.5221 | 12.1940 | 0.0189 |  | 0.4877 | 0.4877 |  | 0.4504 | 0.4504 |  | $1,805.129$ <br> 7 | $\begin{gathered} 1,805.129 \\ 7 \end{gathered}$ | 0.5672 |  | $1,819.309$ |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | $\begin{gathered} \text { Fugitive } \\ \text { PM2.5 } \end{gathered}$ | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker |  | 0.0456 | 0.4680 | $\begin{gathered} 1.3000 \mathrm{e} \\ 003 \end{gathered}$ | 0.1521 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.1531 | 0.0404 | $\begin{gathered} 9.2000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0413 |  | 129.8123 | 129.8123 | $\begin{gathered} 3.2200 \mathrm{e} \\ 003 \end{gathered}$ |  | 129.8928 |
| Total | 0.0690 | 0.0456 | 0.4680 | $\begin{gathered} 1.3000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1521 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1531 | 0.0404 | $\begin{gathered} 9.2000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0413 |  | 129.8123 | 129.8123 | $\begin{aligned} & 3.2200 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 129.8928 |

### 3.7 Period 3-2022

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Tota | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road |  | 0.9509 | 13.5323 | 0.0189 |  |  |  |  | 0.0293 | 0.0293 | 0.0000 | ${ }_{7}^{1,805.129}$ | ${ }_{7}^{1,805.129}$ | 0.5672 |  | $\begin{gathered} 1,819.309 \\ 1 \end{gathered}$ |
| Paving | 0.3252 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Total | 0.5446 | 0.9509 | 13.5323 | 0.0189 |  | 0.0293 | 0.0293 |  | 0.0293 | 0.0293 | 0.0000 | $\begin{array}{\|c\|} \hline 1,805.129 \\ 7 \end{array}$ | $\begin{gathered} 1,805.129 \\ 7 \end{gathered}$ | 0.5672 |  | $\begin{gathered} 1,819.309 \\ \hline \end{gathered}$ |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 |
| Worker | 0.0690 | 0.0456 | 0.4680 | $\begin{gathered} 1.3000- \\ 003 \end{gathered}$ | 0.1521 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1531 | 0.0404 | $\begin{gathered} 9 .--000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0413 |  | 129.8123 | 129.8123 | $\begin{gathered} 3.2200 \mathrm{e} \\ 003 \end{gathered}$ |  | 129.8928 |
| Total | 0.0690 | 0.0456 | 0.4680 | $\begin{gathered} 1.3000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1521 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.1531 | 0.0404 | $\begin{gathered} 9.2000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0413 |  | 129.8123 | 129.8123 | $\begin{gathered} 3.2200 \mathrm{e}- \\ 003 \end{gathered}$ |  | 129.8928 |

### 4.0 Operational Detail - Mobile

### 4.1 Mitigation Measures Mobile

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Mitigated | 8.7172 |  |  |  |  |  |  |  |  |  |  | :12,511.368 | 12,511.368 | 0.9522 |  | ${ }_{43}^{12,535.17}$ |
| Unmitigated | $-8.7172$ |  | -99.2273 | 0.1235 |  |  | 9.4508 |  | 0.1305 |  |  |  | $\begin{gathered} 12,511.368 \\ 1 \end{gathered}$ |  |  | $\begin{gathered} 12,535.17 \\ 43 \end{gathered}$ |

### 4.2 Trip Summary Information

|  | Average Daily Trip Rate |  |  | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Convenience Market With Gas Pumps | 4,252.98 | 4,252.98 | 4252.98 | 1,687,510 | 1,687,510 |
| - ' Fast 'rood Restaurant with Drive Thru | 3,272.13 | 3,272.13 | 3272.13 | 2,260,370 | 2,260,370 |
| - - - Fast Food Restaurant with Drive Thru | 639.88 | 639.88 | 639.88 | - 442,028 | 442,028 |
| - - - - - - - - Other Asphalt Surfaces - - | $0.00$ | 0.00 | -0.00 |  |  |
| Parking Lot | 0.00 | 0.00 | 0.00 |  |  |
| Total | 8,165.00 | 8,165.00 | 8,165.00 | 4,389,908 | 4,389,908 |

### 4.3 Trip Type Information

River Oaks Marketplace - Sacramento County, Winter

|  | Miles |  |  | Trip \% |  |  | Trip Purpose \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted | Pass-by |
| Convenience Market With Gas | 10.00 | 5.00 | 6.50 | 0.80 | 80.20 | 19.00 | 14 | 21 | 65 |
| Fast Food Restaurant with Drive: | 10.00 | 5.00 | 6.50 | 2.20 | 78.80 | 19.00 | 29 | 21 | 50 |
| Fast Food Restaurant with Drive: | 10.00 | 5.00 | 6.50 | 2.20 | 78.80 | 19.00 | 29 | 21 | 50 |
|  | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |
|  | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

### 4.4 Fleet Mix

| Land Use | LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Convenience Market With Gas Pumps | 0.559527: | 0.038733: | 0.206173: | 0.118029: | 0.019040 | 0.005245 | 0.018552; | 0.023249: | 0.002031! | 0.002054 | 0.005884 | 0.000619 | 0.000865 |
| Fast Food Restaurant with Drive Thru | 0.559527: | 0.038733 | 0.206173 | 0.118029: | 0.019040 | 0.005245 | 0.018552 | 0.023249 | 0.002031 | 0.002054 | 0.005884 | 0.000619 | 0.000865 |
| Other Asphalt Surfaces | 0.559527 | 0.038733 | 0.206173 | 0.118029 | 0.019040 | 0.005245 | 0.018552 | 0.023249 | 0.002031 | 0.002054 | 0.005884 | 0.000619 | 0.000865 |
| Parking Lot | 0.559527 | 0.038733: | 0.206173: | 0.118029 | 0.019040 | 0.005245: | 0.018552 | 0.023249 | 0.002031: | 0.002054 | 0.005884? | 0.000619: | 0.000865 |

### 5.0 Energy Detail

Historical Energy Use: N
5.1 Mitigation Measures Energy

## River Oaks Marketplace - Sacramento County, Winter

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | Exhaust PM2 5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| NaturalGas Mitigated | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | $\begin{gathered} 6.0600 \mathrm{e}- \\ 003 \end{gathered}$ | $5.8000 \mathrm{e}-1$ 003 | 318.1499 |
| NaturalGas Unmitigated | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | -716.2704 | - -216.2704 | $\begin{gathered} -0600 \mathrm{e} \\ 603 \end{gathered}$ | $\begin{gathered} 5.8000- \\ 003 \end{gathered}$ | 318.1499 |

River Oaks Marketplace - Sacramento County, Winter

### 5.2 Energy by Land Use - NaturalGas

## Unmitigated

|  | NaturalGa s Use | ROG | NOX | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Convenience Market With Gas Pumps | 69.0493 | 7.4000e- 004 | $\begin{gathered} 6.7700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.6900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $5.1000 \mathrm{e}-$ 004 | $\begin{aligned} & 5.1000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $5.1000 \mathrm{e}-$ 004 | $5.1000 \mathrm{e}-$ 004 |  | 8.1235 | 8.1235 | $1.6000 \mathrm{e}-$ 004 | $1.5000 \mathrm{e}-$ 004 | 8.1717 |
| Fast Food Restaurant with Drive Thru | 2190.82 | 0.0236 | 0.2148 | 0.1804 | $\begin{gathered} 1.2900 \mathrm{e} \\ 003 \end{gathered}$ |  | 0.0163 | 0.0163 |  | 0.0163 | 0.0163 |  | 257.7438 | 257.7438 | ${ }_{0}^{4.9400 e^{-}}$ | $\begin{gathered} 4.7300-- \\ 003 \end{gathered}$ | 259.2754 |
| Fast Food Restaurant with Drive Thru | 428.427 | ${ }^{4.62000-}$ | 0.0420 | 0.0353 | $2.50000-$ 004 |  | $3.19000-$ 003 | $3.19000-$ 003 |  | $3.19000-$ 003 | 3.1900 e 003 |  | 50.4032 | 50.4032 | $9.70000-$ 004 | 9.2000e- | 50.7027 |
| Other Asphalt Surfaces |  |  | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | $\begin{gathered} 6.0700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | 318.1499 |

### 5.2 Energy by Land Use - NaturalGas

## Mitigated

|  | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Convenience Market With Gas Pumps | 0.0690493 | $\begin{gathered} 7.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 6.7700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.6900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $5.1000 \mathrm{e}-$ 004 | $\begin{gathered} 5.1000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{gathered} 5.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $5.1000 \mathrm{e}-$ 004 |  | 8.1235 | 8.1235 | $1.6000 \mathrm{e}-$ 004 | $\begin{gathered} 1.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 8.1717 |
| Fast Food Restaurant with Drive Thru | -2.19082 | 0.0236 | 0.2148 | 0.1804 | $1.2900-\mathrm{e}-\mathrm{-}$ 003 |  | 0.0163 | 0.0163 |  | 0.0163 | 0.0163 |  | 257.7438 | 257.7438 | $4.9400 \mathrm{e}-\mathrm{-}$ 003 | $\begin{gathered} 4.7300 \mathrm{e}- \\ 003 \end{gathered}$ | 259.2754 |
| Fast Food Restaurant with Drive Thru | -0.428427 | 4.6200 e 003 | 0.0420 | 0.0353 | $2.5000 \mathrm{e}-1$ 004 |  | 3.1900 e 003 | $3.1900 \mathrm{e}-$ 003 |  | $3.1900 \mathrm{e}-1$ 003 | $3.1900 \mathrm{e}-$ 003 |  | 50.4032 | 50.4032 | $9.7000 \mathrm{e}-\mathrm{-}$ 004 | $9.2000-$ 004 | 50.7027 |
| Other Asphalt Surfaces | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Parking Lot | $\square$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  | 0.0290 | 0.2636 | 0.2214 | $\begin{gathered} 1.5800 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0200 | 0.0200 |  | 0.0200 | 0.0200 |  | 316.2704 | 316.2704 | $\begin{gathered} 6.0700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.8000 \mathrm{e}- \\ 003 \end{gathered}$ | 318.1499 |

### 6.0 Area Detail

### 6.1 Mitigation Measures Area

River Oaks Marketplace - Sacramento County, Winter

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Mitigated | 0.3208 | $1.1000 \mathrm{e}-$ 004 | 0.0125 | 0.0000 |  | $4.0000 \mathrm{e}-$ 005 | $4.0000 \mathrm{e}-$ 005 |  | $4.0000 \mathrm{e}-$ 005 | $4.0000 \mathrm{e}-$ 005 |  | 0.0268 | 0.0268 | $7.0000 \mathrm{e}-$ 005 |  | 0.0285 |
| Unmitigated | $0.3208$ | $\begin{gathered} -1.0000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} -0.000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | $0.0268$ | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0285 |

### 6.2 Area by SubCategory

## Unmitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Architectural Coating | 0.0396 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Consumer Products | 0.2801 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Landscaping | $\begin{gathered} 1.1600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.1000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000-- \\ 005 \end{gathered}$ |  | 0.0285 |
| Total | 0.3208 | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & \hline 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000 e- \\ 005 \end{gathered}$ |  | 0.0285 |

### 6.2 Area by SubCategory

Mitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 <br> Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Architectural Coating | 0.0396 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Consumer Products | 0.2801 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 |  |  | 0.0000 |  |  | 0.0000 |
| Landscaping | $1.1600 \mathrm{e}-$ 003 | $1.1000 \mathrm{e}-$ 004 | 0.0125 | 0.0000 |  | 4.0000 e 005 | 4.0000 e 005 |  | $4.0000 \mathrm{e}-\mathrm{-}$ 005 | 4.0000 e 005 |  | 0.0268 | 0.0268 | $7.0000 \mathrm{e}-\mathrm{C}$ 005 |  | 0.0285 |
| Total | 0.3208 | $\begin{aligned} & 1.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0125 | 0.0000 |  | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{aligned} & \hline 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0268 | 0.0268 | $\begin{gathered} 7.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | 0.0285 |

### 7.0 Water Detail

7.1 Mitigation Measures Water

### 8.0 Waste Detail

### 8.1 Mitigation Measures Waste

### 9.0 Operational Offroad

| Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

### 10.0 Stationary Equipment

Fire Pumps and Emergency Generators

River Oaks Marketplace - Sacramento County, Winter


### 11.0 Vegetation

## A-2 AERSCREEN Output

## RiverOaksMarketplace

```
AERSCREEN 16216 / AERMOD 18081
09/25/20
15:30:13
```

TITLE: RiverOaksMarketplace


BUILDING DOWNWASH NOT USED FOR NON-POINT SOURCES

```
*************************** FLOW SECTOR ANALYSIS ***************************
    25 meter receptor spacing: 1. meters - 5000. meters
```

MAXIMUM IMPACT RECEPTOR

| Zo | SURFACE | 1-HR CONC | RADIAL | DIST | TEMPORAL |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SECTOR | ROUGHNESS | (ug/m3) | (deg) | (m) | PERIOD |
| 1* | 0.050 | 2640. | 0 | 125.0 | AUT |

```
********************* MAKEMET METEOROLOGY PARAMETERS ********************
MIN/MAX TEMPERATURE: 250.0 / 310.0 (K)
MINIMUM WIND SPEED: }0.5\textrm{m}/\textrm{s
ANEMOMETER HEIGHT: 10.000 meters
SURFACE CHARACTERISTICS INPUT: AERMET SEASONAL TABLES
DOMINANT SURFACE PROFILE: Cultivated Land
DOMINANT CLIMATE TYPE: Average Moisture
DOMINANT SEASON: Autumn
ALBEDO: 0.18
BOWEN RATIO: 0.70
ROUGHNESS LENGTH: 0.050 (meters)
SURFACE FRICTION VELOCITY (U*) ADJUSTED
```

METEOROLOGY CONDITIONS USED TO PREDICT OVERALL MAXIMUM IMPACT
YR MO DY JDY HR
-- -- -- --- --
$100107 \quad 701$

HT REF TA HT
$10.0 \quad 250.0 \quad 2.0$
************************* AERSCREEN AUTOMATED DISTANCES $* * * * * * * * * * * * * * * * * * * * * ~$
OVERALL MAXIMUM CONCENTRATIONS BY DISTANCE

|  | RiverOaksMarketplace |  |  |
| :---: | :---: | :---: | :---: |
|  | MAXIMUM |  | MAXIMUM |
| DIST | 1-HR CONC | DIST | 1-HR CONC |
| (m) | (ug/m3) | (m) | (ug/m3) |
| 1.00 | 1261. | 2525.00 | 261.0 |
| 25.00 | 1565. | 2550.00 | 257.7 |
| 50.00 | 1841. | 2575.00 | 254.5 |
| 75.00 | 2155. | 2600.00 | 251.4 |
| 100.00 | 2476. | 2625.00 | 248.4 |
| 125.00 | 2640. | 2650.00 | 245.4 |
| 150.00 | 2634. | 2675.00 | 242.5 |
| 175.00 | 2595. | 2700.00 | 240.6 |
| 200.00 | 2506. | 2725.00 | 239.0 |
| 225.00 | 2420. | 2750.00 | 237.5 |
| 250.00 | 2374. | 2775.00 | 236.0 |
| 275.00 | 2308. | 2800.00 | 234.5 |
| 300.00 | 2231. | 2825.00 | 233.1 |
| 325.00 | 2148. | 2850.00 | 231.6 |
| 350.00 | 2064. | 2875.00 | 230.2 |
| 375.00 | 1980. | 2900.00 | 228.8 |
| 400.00 | 1896. | 2925.00 | 227.5 |
| 425.00 | 1818. | 2950.00 | 226.1 |
| 450.00 | 1741. | 2975.00 | 224.8 |
| 475.00 | 1668. | 3000.00 | 223.5 |
| 500.00 | 1599. | 3025.00 | 222.2 |
| 525.00 | 1535. | 3050.00 | 220.9 |
| 550.00 | 1473. | 3075.00 | 219.6 |
| 575.00 | 1415. | 3100.00 | 218.4 |
| 600.00 | 1360. | 3125.00 | 217.2 |
| 625.00 | 1310. | 3150.00 | 215.9 |
| 650.00 | 1261. | 3174.99 | 214.8 |
| 675.00 | 1215. | 3200.00 | 213.6 |
| 700.00 | 1171. | 3225.00 | 212.4 |
| 725.00 | 1131. | 3250.00 | 211.3 |
| 750.00 | 1093. | 3275.00 | 210.1 |
| 775.00 | 1056. | 3300.00 | 209.0 |
| 800.00 | 1021. | 3325.00 | 207.9 |
| 825.00 | 988.6 | 3350.00 | 206.8 |
| 850.00 | 957.4 | 3375.00 | 205.8 |
| 875.00 | 928.0 | 3400.00 | 204.7 |
| 900.00 | 900.1 | 3425.00 | 203.6 |
| 925.00 | 873.6 | 3450.00 | 202.6 |
| 950.00 | 848.1 | 3475.00 | 201.6 |
| 975.00 | 823.8 | 3500.00 | 200.6 |
| 1000.00 | 800.8 | 3525.00 | 199.6 |
| 1025.00 | 778.9 | 3550.00 | 198.6 |
| 1050.00 | 758.1 | 3575.00 | 197.6 |
| 1075.00 | 738.1 | 3600.00 | 196.7 |
|  |  |  |  |


| 1100.00 | 718.9 |
| :---: | :---: |
| 1125.00 | 700.6 |
| 1150.00 | 683.1 |
| 1175.00 | 666.4 |
| 1200.00 | 650.1 |
| 1225.00 | 634.5 |
| 1250.00 | 619.6 |
| 1275.00 | 605.3 |
| 1300.00 | 591.7 |
| 1325.00 | 578.4 |
| 1350.00 | 565.7 |
| 1375.00 | 553.5 |
| 1400.00 | 541.8 |
| 1425.00 | 530.5 |
| 1450.00 | 519.6 |
| 1475.00 | 509.1 |
| 1500.00 | 498.9 |
| 1525.00 | 489.1 |
| 1550.00 | 479.5 |
| 1575.00 | 470.3 |
| 1600.00 | 461.4 |
| 1625.00 | 452.7 |
| 1650.00 | 444.2 |
| 1675.00 | 436.1 |
| 1700.00 | 428.2 |
| 1725.00 | 420.5 |
| 1750.00 | 413.1 |
| 1775.00 | 406.0 |
| 1800.00 | 399.0 |
| 1825.00 | 392.2 |
| 1850.00 | 385.7 |
| 1875.01 | 379.3 |
| 1900.00 | 373.1 |
| 1924.99 | 367.1 |
| 1950.00 | 361.3 |
| 1975.00 | 355.6 |
| 2000.00 | 350.0 |
| 2025.00 | 344.6 |
| 2050.00 | 339.4 |
| 2075.00 | 334.3 |
| 2100.00 | 329.3 |
| 2125.00 | 324.5 |
| 2150.00 | 319.8 |
| 2175.00 | 315.2 |
| 2200.00 | 310.7 |
| 2225.00 | 306.4 |
| 2250.00 | 302.1 |
| 2275.00 | 297.9 |

1100.00 1150.00 1175.00 1200.00 1225.00 1250.00 1275.00 1300.00 1325.00 1350.00 1375.00 1425.00 530.5 519.6 1475.00 1500.00 1525.00 489.1 479.5 470.3 461.4 452.7 444.2 436.1 428.2 420.5 413.1 406.0 399.0 392.2 385.7 379.3 373.1 367.1 361.3 355.6 350.0 344.6 339.4 334.3 329.3 324.5 319.8 315.2 310.7 306.4 297.9

RiverOaksMarketplace

| 3625.00 | 195.7 |
| :--- | :--- |
| 3650.00 | 194.8 |
| 3675.00 | 193.8 |
| 3700.00 | 192.9 |

$3725.00 \quad 192.0$
3750.00191 .1
$3775.00 \quad 190.2$
$3800.00 \quad 189.4$
$3825.00 \quad 188.5$
$3850.00 \quad 187.6$
$3875.00 \quad 186.8$
$3900.00 \quad 185.9$
$3925.00 \quad 185.1$
$3950.00 \quad 184.3$
$3975.00 \quad 183.5$
$4000.00 \quad 182.7$
$4025.00 \quad 181.9$
$4050.00 \quad 181.1$
$4075.00 \quad 180.3$
$4100.00 \quad 179.5$
$4125.00 \quad 178.8$
$4150.00 \quad 178.0$
$4175.00 \quad 177.3$
$4200.00 \quad 176.5$
$4225.00 \quad 175.8$
$4250.00 \quad 175.1$
$4275.00 \quad 174.4$
$4300.00 \quad 173.6$
$4325.00 \quad 172.9$
$4350.00 \quad 172.2$
$4375.00 \quad 171.6$
$4400.00 \quad 170.9$
$4425.00 \quad 170.2$
$4450.00 \quad 169.5$
$4475.00 \quad 168.9$
$4500.00 \quad 168.2$
$4525.00 \quad 167.6$
$4550.00 \quad 166.9$
$4575.00 \quad 166.3$
$4600.00 \quad 165.6$
$4625.00 \quad 165.0$
$4650.00 \quad 164.4$
$4675.00 \quad 163.8$
$4700.00 \quad 163.2$
$4725.00 \quad 162.6$
$4750.00 \quad 162.0$
$4775.00 \quad 161.4$
$4800.00 \quad 160.8$
Page 4

| 2300.00 | 293.9 |
| :--- | :--- |
| 2325.00 | 289.9 |
| 2350.00 | 286.0 |
| 2375.00 | 282.2 |
| 2400.00 | 278.4 |
| 2425.00 | 274.8 |
| 2450.00 | 271.2 |
| 2475.00 | 267.7 |
| 2500.00 | 264.3 |

RiverOaksMarketplace
4825.00160 .2
$4850.00 \quad 159.6$
$4875.00 \quad 159.0$
$4899.99 \quad 158.5$
$4925.00 \quad 157.9$
$4950.00 \quad 157.3$
$4975.00 \quad 156.8$
$5000.00 \quad 156.2$
********************** AERSCREEN MAXIMUM IMPACT SUMMARY $* * * * * * * * * * * * * * * * * * * * *$

3-hour, 8-hour, and 24-hour scaled
concentrations are equal to the 1-hour concentration as referenced in
SCREENING PROCEDURES FOR ESTIMATING THE AIR QUALITY
IMPACT OF STATIONARY SOURCES, REVISED (Section 4.5.4)
Report number EPA-454/R-92-019
http://www.epa.gov/scram001/guidance_permit.htm
under Screening Guidance

|  | MAXIMUM | SCALED | SCALED | SCALED | SCALED |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1-HOUR | 3-HOUR | 8-HOUR | 24-HOUR | ANNUAL |
| CALCULATION | CONC | CONC | CONC | CONC | CONC |
| PROCEDURE | (ug/m3) | (ug/m3) | (ug/m3) | (ug/m3) | (ug/m3) |
| FLAT TERRAIN | 2656. | 2656. | 2656. | 2656. | N/A |
| DISTANCE FROM |  | 00 meter |  |  |  |

IMPACT AT THE
AMBIENT BOUNDARY 1261. 1261. 1261. 1261. N/A

DISTANCE FROM SOURCE 1.00 meters

## A-3 Health Risk Assessment Calculations

## River Oaks Marketplace - Construction HRA

For Nearby Resident

## MEISR

|  | Distance from Source Center | AERSCREEN OUT <br> $\left[\mathrm{ug} / \mathrm{m}^{3}\right] /[\mathrm{g} / \mathrm{s}]$ |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $(\mathrm{ft})$ | $(\mathrm{m})$ | $\max$ | annual |
| Resident | 376 | 115 | 2656.0 | 265.6 |


|  | PM $_{10}$ Exhaust (tons) |  | Start Date | End Date | Duration |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | Unmitigated | Mitigated |  |  |  |
| Construction | 0.1441 | 0.0060 | $4 / 15 / 2021$ | $6 / 1 / 2022$ | 412 |


|  | DPM Exhaust (g/s) |  |
| :--- | :---: | :---: |
|  | Unmitigated | Mitigated |
| Construction | 0.0037 | 0.0002 |

Cancer Risk $=$ Dose inhalation $\times$ Inhalation $C P F \times A S F \times E D / A T \times F A H$
(Equation 8.2.4 A)
Where
Cancer Risk $=$ residential inhalation cancer risk
Dose inhalation (mg/kg-day) $=\mathrm{C}_{\mathrm{AIR}} \times \mathrm{DBR} \times \mathrm{A} \times \mathrm{EF} \times 10^{-6}$
(Equation 5.4.1.1)
Inhalation CPF = inhalation cancer potency factor ( $[\mathrm{mg} / \mathrm{kg} / \text { day }]^{-1}$ )
ASF = age sensitivity factor for a specified age group (unitless)
$E D=$ exposure duration for a specified age group (years)
AT = averaging time period over which exposure is averaged in days (years)
FAH = fraction of time at home (unitless)
Where:
$\mathrm{C}_{\text {AIR }}=$ concentration of compound in air in micrograms per cubic meter ( $\mu \mathrm{g} / \mathrm{m}^{3}$ )
DBR = daily breathing rate in liter per kilogram of body weight per day (L/kg-body weight/day)
$A=$ inhalation absorption factor (1 for DPM, unitless)
$E F=$ exposure frequency in days per year (unitless, days/365 days)
$10^{-6}=$ micrograms to milligrams conversion, liters to cubic meters conversion
Hazard Quotient $=\mathrm{C}_{\text {air }} /$ REL
(Section 8.3.1)
Where:
Hazard Quotient = chronic non-cancer hazard
$\mathrm{C}_{\text {AIR }}=$ concentration of compound in air in micrograms per cubic meter ( $\mu \mathrm{g} / \mathrm{m}^{3}$ )
REL = Chronic non-cancer Reference Exposure Level for substance ( $\mu \mathrm{g} / \mathrm{m}^{3}$ )

| Dose Inhalation Inputs |  |  | Unmitigated | Mitigated |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Receptor Type | Exposure <br> Scenario | Receptor Group Age | $\begin{gathered} \mathrm{C}_{\mathrm{AIR}} \\ \left(\mu \mathrm{~g} / \mathrm{m}^{3}\right) \end{gathered}$ |  | DBR (L/kg-day) | $\begin{gathered} A \\ \text { (unitless) } \end{gathered}$ | EF <br> (days/yea <br> r) <br> 0.96 |
| Off-Site Child Resident | Construction | 3rd Trimester | 9.76E-01 | 4.03E-02 | 361 | 1 | 0.96 |
|  |  | Age 0<2 | $9.76 \mathrm{E}-01$ | $4.03 \mathrm{E}-02$ | 1090 | 1 | 0.96 |


| Dose Inhalation Outputs |  |  | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: |
| Receptor <br> Type | Exposure <br> Scenario | Receptor <br> Group Age | Dose inhalation (mg/kg-day) |  |
| Off-Site Child Resident | Construction | 3rd Trimester | $3.38 \mathrm{E}-04$ | $1.40 \mathrm{E}-05$ |
|  |  | Age 0<2 | $1.02 \mathrm{E}-03$ | $4.22 \mathrm{E}-05$ |

Risk Inputs

| Receptor Type | Exposure Scenario | Receptor <br> Group Age | $\begin{gathered} \text { CPF } \\ \left(\mathrm{mg} / \mathrm{kg}^{-d a y}{ }^{-1}\right) \end{gathered}$ | ASF (unitless) | $\begin{gathered} \hline \text { ED } \\ \text { (years) } \end{gathered}$ | $\begin{gathered} \mathrm{AT} \\ \text { (years) } \end{gathered}$ | FAH (unitless) | $\begin{gathered} \text { MAF } \\ \text { (unitless) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Off-Site Child Resident | Construction | 3rd Trimester | 1.1 | 10 | 0.25 | 70.00 | 1 | 1 |
|  |  | Age 0<2 | 1.1 | 10 | 0.88 | 70.00 | 1 | 1 |


| Risk Outputs |  |  | Unmitigated | Mitigated | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Receptor Type | Exposure <br> Scenario | Receptor <br> Group Age | Cancer Risk |  | Hazard Risk |  |
| Off-Site Child Resident | Construction | 3rd Trimester | $1.33 \mathrm{E}-05$ | 5.49E-07 | 0.20 | 0.01 |
|  |  | Age 0<2 | $1.41 \mathrm{E}-04$ | 5.83E-06 |  |  |
|  | Total Cancer Risk (per million) |  | 154.24 | 6.38 |  |  |

SOURCE: Office of Environmental Health Hazard Assessment, 2015. Air Toxics Hot Spots Program Guidance Manual for the Preparation of Health Risk Assessments . Daily breathing rate for school receptor is based on the OEHHA 95th percentile 8-hour moderate intensity breathing rates (Table 5.8).
Fraction of time at home is set to 1 for residential since the nearest school unmitigated cancer risk is $>1$ per million, per OEHHA Table 8.4.
Inhalation cancer potency factor from Table 7.1

## Attachment B Biological Resources

Query Summary
Quad IS (Grays Bend (3812166) OR Taylor Monument (3812165) OR Rio Linda (3812164) OR Davis (3812156) OR Sacramento East (3812154) OR Sacramento West (3812155) OR Saxon (3812146) OR Clarksburg (3812145) OR Florin (3812144))

## Print Close

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Scientific Name | Common Name | Taxonomic Group | Element Code | Total Occs | Returned Occs | Federal Status | State Status | Global Rank | State Rank | CA Rare Plant Rank | Other Status | Habitats |
| Accipiter cooperii | Cooper's hawk | Birds | ABNKC12040 | 118 | 3 | None | None | G5 | S4 | null | CDFW_WL-Watch List, IUCN_LCLeast Concern | Cismontane woodland, <br> Riparian forest, Riparian woodland, Upper montane coniferous forest |
| Agelaius tricolor | tricolored blackbird | Birds | ABPBXB0020 | 955 | 22 | None | Threatened | G2G3 | S1S2 | null | BLM_S-Sensitive, CDFW_SSC- <br> Species of Special Concern, <br> IUCN_EN- <br> Endangered, <br> NABCI_RWL-Red <br> Watch List, <br> USFWS_BCC-Birds of Conservation Concern | Freshwater marsh, Marsh \& swamp, Swamp, Wetland |
| Ammodramus savannarum | grasshopper sparrow | Birds | ABPBXA0020 | 27 | 2 | None | None | G5 | S3 | null | CDFW_SSC- <br> Species of Special Concern, IUCN_LCLeast Concern | Valley \& foothill grassland |
| Antrozous pallidus | pallid bat | Mammals | AMACC10010 | 420 | 1 | None | None | G5 | S3 | null | BLM_S-Sensitive, CDFW_SSCSpecies of Special Concern, IUCN_LCLeast Concern, USFS_S-Sensitive, WBWG_H-High Priority | Chaparral, <br> Coastal scrub, <br> Desert wash, <br> Great Basin grassland, Great Basin scrub, Mojavean desert scrub, Riparian woodland, Sonoran desert scrub, Upper montane coniferous forest, Valley \& foothill grassland |
| Archoplites interruptus | Sacramento perch | Fish | AFCQB07010 | 5 | 1 | None | None | G2G3 | S1 | null | AFS_TH- <br> Threatened, CDFW_SSCSpecies of Special Concern | Aquatic, <br> Sacramento/San <br> Joaquin flowing waters, <br> Sacramento/San Joaquin standing waters |
| Ardea alba | great egret | Birds | ABNGA04040 | 43 | 6 | None | None | G5 | S4 | null | CDF_S-Sensitive, IUCN_LC-Least Concern | Brackish marsh, Estuary, Freshwater marsh, Marsh \& swamp, Riparian forest, Wetland |
| Ardea herodias | great blue heron | Birds | ABNGA04010 | 156 | 7 | None | None | G5 | S4 | null | CDF_S-Sensitive, IUCN_LC-Least Concern | Brackish marsh, Estuary, Freshwater marsh, Marsh \& swamp, Riparian forest, Wetland |
| Astragalus tener var. ferrisiae | Ferris' milkvetch | Dicots | PDFAB0F8R3 | 18 | 4 | None | None | G2T1 | S1 | 1B. 1 | null | Meadow \& seep, Valley \& foothill grassland, Wetland |
| Astragalus tener var. tener | alkali milkvetch | Dicots | PDFAB0F8R1 | 65 | 10 | None | None | G2T1 | S1 | 1B. 2 | null | Alkali playa, Valley \& foothill grassland, Vernal pool, Wetland |
|  | burrowing owl | Birds | ABNSB10010 | 1989 | 87 | None | None | G4 | S3 | null |  |  |


| Athene cunicularia |  |  |  |  |  |  |  |  |  |  | $\begin{array}{\|l} \text { BLM_S-Sensitive, } \\ \text { CDFW_SSC- } \\ \text { Species of Special } \\ \text { Concern, IUCN_LC- } \\ \text { Least Concern, } \\ \text { USFWS_BCC-Birds } \\ \text { of Conservation } \\ \text { Concern } \end{array}$ | Coastal prairie Coastal scrub, Great Basin grassland, Great Basin scrub, Mojavean desert scrub, Sonoran desert scrub, Valley \& foothill grassland |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Atriplex cordulata var. cordulata | heartscale | Dicots | PDCHE040B0 | 66 | 1 | None | None | G3T2 | S2 | 1B. 2 | BLM_S-Sensitive | Chenopod scrub, Meadow \& seep, Valley \& foothill grassland |
| Atriplex depressa | brittlescale | Dicots | PDCHE042L0 | 60 | 5 | None | None | G2 | S2 | 1B. 2 | null | Alkali playa, Chenopod scrub, Meadow \& seep, Valley \& foothill grassland, Vernal pool, Wetland |
| Bombus crotchii | Crotch bumble bee | Insects | IIHYM24480 | 276 | 1 | None | Candidate Endangered | G3G4 | S1S2 | null | null | null |
| Bombus occidentalis | western bumble bee | Insects | IIHYM24250 | 281 | 1 | None | Candidate Endangered | G2G3 | S1 | null | USFS_S-Sensitive | null |
| Branchinecta conservatio | Conservancy fairy shrimp | Crustaceans | ICBRA03010 | 47 | 1 | Endangered | None | G2 | S2 | null | IUCN_ENEndangered | Valley \& foothill grassland, Vernal pool, Wetland |
| Branchinecta lynchi | vernal pool fairy shrimp | Crustaceans | ICBRA03030 | 791 | 39 | Threatened | None | G3 | S3 | null | IUCN_VU- <br> Vulnerable | Valley \& foothill grassland, Vernal pool, Wetland |
| Branchinecta mesovallensis | midvalley fairy shrimp | Crustaceans | ICBRA03150 | 144 | 8 | None | None | G2 | S2S3 | null | null | Vernal pool, Wetland |
| Buteo regalis | ferruginous hawk | Birds | ABNKC19120 | 107 | 2 | None | None | G4 | S3S4 | null | CDFW_WL-Watch List, IUCN_LCLeast Concern, USFWS_BCC-Birds of Conservation Concern | Great Basin grassland, Great Basin scrub, Pinon \& juniper woodlands, Valley \& foothill grassland |
| Buteo swainsoni | Swainson's hawk | Birds | ABNKC19070 | 2535 | 313 | None | Threatened | G5 | S3 | null | BLM_S-Sensitive, IUCN_LC-Least Concern, USFWS_BCC-Birds of Conservation Concern | Great Basin grassland, Riparian forest, Riparian woodland, Valley \& foothill grassland |
| Carex comosa | bristly sedge | Monocots | PMCYP032Y0 | 29 | 1 | None | None | G5 | S2 | 2B. 1 | null | Coastal prairie, Freshwater marsh, Marsh \& swamp, Valley \& foothill grassland, Wetland |
| Centromadia parryi ssp. parryi | pappose tarplant | Dicots | PDAST4R0P2 | 39 | 2 | None | None | G3T2 | S2 | 1B. 2 | BLM_S-Sensitive | Chaparral, Coastal prairie, Marsh \& swamp, Meadow \& seep, Valley \& foothill grassland |
| Charadrius alexandrinus nivosus | western snowy plover | Birds | ABNNB03031 | 138 | 2 | Threatened | None | G3T3 | S2S3 | null | CDFW_SSCSpecies of Special Concern, NABCI_RWL-Red Watch List, USFWS_BCC-Birds of Conservation Concern | Great Basin standing waters, Sand shore, Wetland |
| Charadrius montanus | mountain plover | Birds | ABNNB03100 | 90 | 4 | None | None | G3 | S2S3 | null | BLM_S-Sensitive, CDFW_SSCSpecies of Special Concern, IUCN_NT-Near Threatened, NABCI_RWL-Red Watch List, USFWS_BCC-Birds of Conservation Concern | Chenopod scrub, Valley \& foothill grassland |
| Chloropyron palmatum |  | Dicots | PDSCR0JOJO | 25 | 3 | Endangered | Endangered | G1 | S1 | 1B. 1 | SB_CaIBG/RSABGCalifornia/Rancho | Chenopod scrub, Meadow |


|  | \|palmatebracted bird's-beak |  |  |  |  |  |  |  |  |  | \|Santa Ana Botanic Garden | \& seep, Valley \& foothill grassland, Wetland |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cicindela hirticollis abrupta | Sacramento Valley tiger beetle | Insects | IICOL02106 | 6 | 2 | None | None | G5TH | SH | null | null | Sand shore |
| Coccyzus americanus occidentalis | western yellow-billed cuckoo | Birds | ABNRB02022 | 165 | 2 | Threatened | Endangered | G5T2T3 | S1 | null | BLM_S-Sensitive, NABCI_RWL-Red Watch List, USFS_S-Sensitive, USFWS_BCC-Birds of Conservation Concern | Riparian forest |
| Cuscuta obtusiflora var. glandulosa | Peruvian dodder | Dicots | PDCUS01111 | 6 | 1 | None | None | G5T4? | SH | 2B. 2 | null | Marsh \& swamp, Wetland |
| Desmocerus californicus dimorphus | valley elderberry longhorn beetle | Insects | IICOL48011 | 271 | 24 | Threatened | None | G3T2 | S2 | null | null | Riparian scrub |
| Downingia pusilla | dwarf downingia | Dicots | PDCAM060C0 | 132 | 6 | None | None | GU | S2 | 2B. 2 | null | Valley \& foothill grassland, Vernal pool, Wetland |
| Egretta thula | snowy egret | Birds | ABNGA06030 | 20 | 1 | None | None | G5 | S4 | null | IUCN_LC-Least Concern | Marsh \& swamp, Meadow \& seep, Riparian forest, Riparian woodland, Wetland |
| Elanus leucurus | white-tailed kite | Birds | ABNKC06010 | 180 | 18 | None | None | G5 | S3S4 | null | BLM_S-Sensitive, CDFW_FP-Fully Protected, IUCN_LC-Least Concern | Cismontane woodland, Marsh \& swamp, Riparian woodland, Valley \& foothill grassland, Wetland |
| Elderberry Savanna | Elderberry <br> Savanna | Riparian | CTT63440CA | 4 | 3 | None | None | G2 | S2. 1 | null | null | Riparian scrub |
| Emys marmorata | western pond turtle | Reptiles | ARAAD02030 | 1398 | 7 | None | None | G3G4 | S3 | null | BLM_S-Sensitive, CDFW_SSC- <br> Species of Special Concern, IUCN_VUVulnerable, USFS_S-Sensitive | Aquatic, Artificial flowing waters, Klamath/North coast flowing waters, Klamath/North coast standing waters, Marsh \& swamp, <br> Sacramento/San Joaquin flowing waters, Sacramento/San Joaquin standing waters, South coast flowing waters, South coast standing waters, Wetland |
| Eryngium jepsonii | Jepson's coyote-thistle | Dicots | PDAPIOZ130 | 19 | 2 | None | None | G2 | S2 | 1B. 2 | null | Valley \& foothill grassland, Vernal pool |
| Extriplex joaquinana | San Joaquin spearscale | Dicots | PDCHE041F3 | 127 | 9 | None | None | G2 | S2 | 1B. 2 | BLM_S-Sensitive, SB_CalBG/RSABGCalifornia/Rancho Santa Ana Botanic Garden | Alkali playa, Chenopod scrub, Meadow \& seep, Valley \& foothill grassland |
| Falco columbarius | merlin | Birds | ABNKD06030 | 37 | 6 | None | None | G5 | S3S4 | null | CDFW_WL-Watch List, IUCN_LCLeast Concern | Estuary, Great Basin grassland, Valley \& foothill grassland |
| Fritillaria agrestis | stinkbells | Monocots | PMLIL0V010 | 32 | 2 | None | None | G3 | S3 | 4.2 | null | Chaparral, Cismontane woodland, Pinon \& juniper woodlands, Ultramafic, Valley \& foothill grassland |
| Gonidea angulata | western ridged mussel | Mollusks | IMBIV19010 | 143 | 1 | None | None | G3 | S1S2 | null | null | Aquatic |
|  |  |  |  |  |  |  |  |  |  |  |  |  |


| Gratiola heterosepala | Boggs Lake hedgehyssop | Dicots | \|PDSCR0R060 | 199 | 1 | None | \|Endangered | G2 | \|S2 | 1B. 2 | \|BLM_S-Sensitive | \|Freshwater marsh, Marsh \& swamp, Vernal pool, Wetland |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Great Valley Cottonwood Riparian Forest | Great Valley Cottonwood Riparian Forest | Riparian | CTT61410CA | 56 | 1 | None | None | G2 | S2.1 | null | null | Riparian forest |
| Hibiscus lasiocarpos var. occidentalis | woolly rosemallow | Dicots | PDMALOH0R3 | 173 | 10 | None | None | G5T3 | S3 | 1B. 2 | SB_CaIBG/RSABGCalifornia/Rancho Santa Ana Botanic Garden, SB_UCBG-UC Botanical Garden at Berkeley | Freshwater marsh, Marsh \& swamp, Wetland |
| Lasionycteris noctivagans | silver-haired bat | Mammals | AMACC02010 | 139 | 1 | None | None | G5 | S3S4 | null | IUCN_LC-Least Concern, WBWG_M-Medium Priority | Lower montane coniferous forest, Oldgrowth, Riparian forest |
| Lasiurus cinereus | hoary bat | Mammals | AMACC05030 | 238 | 2 | None | None | G5 | S4 | null | IUCN_LC-Least Concern, WBWG_M-Medium Priority | Broadleaved upland forest, Cismontane woodland, Lower montane coniferous forest, North coast coniferous forest |
| Lasthenia chrysantha | alkali-sink goldfields | Dicots | PDAST5L030 | 55 | 1 | None | None | G2 | S2 | 1B. 1 | null | Vernal pool |
| Laterallus jamaicensis coturniculus | California black rail | Birds | ABNME03041 | 303 | 1 | None | Threatened | G3G4T1 | S1 | null | BLM_S-Sensitive, CDFW_FP-Fully Protected, IUCN_NT-Near Threatened, NABCI_RWL-Red Watch List, USFWS_BCC-Birds of Conservation Concern | Brackish marsh, Freshwater marsh, Marsh \& swamp, Salt marsh, Wetland |
| Legenere limosa | legenere | Dicots | PDCAM0C010 | 83 | 7 | None | None | G2 | S2 | 1B. 1 | BLM_S-Sensitive, SB_UCBG-UC Botanical Garden at Berkeley | Vernal pool, Wetland |
| Lepidium latipes var. heckardii | Heckard's pepper-grass | Dicots | PDBRA1M0K1 | 14 | 7 | None | None | G4T1 | S1 | 1B. 2 | null | Valley \& foothill grassland, Vernal pool |
| Lepidurus packardi | vernal pool tadpole shrimp | Crustaceans | ICBRA10010 | 324 | 26 | Endangered | None | G4 | S3S4 | null | IUCN_EN- <br> Endangered | Valley \& foothill grassland, Vernal pool, Wetland |
| Lilaeopsis masonii | Mason's lilaeopsis | Dicots | PDAPI19030 | 198 | 1 | None | Rare | G2 | S2 | 1B. 1 | null | Freshwater marsh, Marsh \& swamp, Riparian scrub, Wetland |
| Linderiella occidentalis | California linderiella | Crustaceans | ICBRA06010 | 508 | 42 | None | None | G2G3 | S2S3 | null | IUCN_NT-Near Threatened | Vernal pool |
| Melospiza melodia | song sparrow ("Modesto" population) | Birds | ABPBXA3010 | 92 | 10 | None | None | G5 | S3? | null | CDFW_SSCSpecies of Special Concern | null |
| Myrmosula pacifica | Antioch multilid wasp | Insects | IIHYM15010 | 3 | 1 | None | None | GH | SH | null | null | Interior dunes |
| Navarretia leucocephala ssp. bakeri | Baker's navarretia | Dicots | PDPLM0C0E1 | 64 | 2 | None | None | G4T2 | S2 | 1B. 1 | null | Cismontane woodland, Lower montane coniferous forest, Meadow \& seep, Valley \& foothill grassland, Vernal pool, Wetland |
| Neostapfia colusana | Colusa grass | Monocots | PMPOA4C010 | 66 | 3 | Threatened | Endangered | G1 | S1 | 1B. 1 | null | Vernal pool, Wetland |
| Northern Claypan Vernal Pool | Northern Claypan Vernal Pool | Herbaceous | CTT44120CA | 21 | 1 | None | None | G1 | S1.1 | null | null | Vernal pool, Wetland |
| Northern <br> Hardpan Vernal Pool | Northern Hardpan Vernal Pool | Herbaceous | CTT44110CA | 126 | 8 | None | None | G3 | S3.1 | null | null | Vernal pool, Wetland |
| Nycticorax nycticorax |  | Birds | ABNGA11010 | 37 | 4 | None | None | G5 | S4 | null | IUCN_LC-Least Concern | Marsh \& swamp, Riparian forest, |


|  | blackcrowned night heron |  |  |  |  |  |  |  |  |  |  | \|Riparian woodland, Wetland |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Oncorhynchus mykiss irideus pop. 11 | steelhead Central Valley DPS | Fish | AFCHA0209K | 31 | 5 | Threatened | None | G5T2Q | S2 | null | AFS_TH- <br> Threatened | Aquatic, Sacramento/San Joaquin flowing waters |
| Oncorhynchus tshawytscha pop. 6 | chinook salmon Central Valley spring-run ESU | Fish | AFCHA0205A | 13 | 1 | Threatened | Threatened | G5 | S2 | null | AFS_TH- <br> Threatened | Aquatic, Sacramento/San Joaquin flowing waters |
| Oncorhynchus tshawytscha pop. 7 | chinook salmon Sacramento River winterrun ESU | Fish | AFCHA0205B | 2 | 1 | Endangered | Endangered | G5 | S1 | null | AFS_ENEndangered | Aquatic, Sacramento/San Joaquin flowing waters |
| Phalacrocorax auritus | doublecrested cormorant | Birds | ABNFD01020 | 39 | 3 | None | None | G5 | S4 | null | CDFW_WL-Watch List, IUCN_LCLeast Concern | Riparian forest, Riparian scrub, Riparian woodland |
| Plagiobothrys hystriculus | bearded popcornflower | Dicots | PDBOROVOHO | 15 | 1 | None | None | G2 | S2 | 1B. 1 | null | Valley \& foothill grassland, Vernal pool, Wetland |
| Plegadis chihi | white-faced ibis | Birds | ABNGE02020 | 20 | 1 | None | None | G5 | S3S4 | null | CDFW_WL-Watch List, IUCN_LCLeast Concern | Marsh \& swamp, Wetland |
| Pogonichthys macrolepidotus | Sacramento splittail | Fish | AFCJB34020 | 15 | 1 | None | None | GNR | S3 | null | AFS_VUVulnerable, CDFW_SSCSpecies of Special Concern, IUCN_ENEndangered | Aquatic, Estuary, Freshwater marsh, Sacramento/San Joaquin flowing waters |
| Progne subis | purple martin | Birds | ABPAU01010 | 71 | 10 | None | None | G5 | S3 | null | CDFW_SSCSpecies of Special Concern, IUCN_LCLeast Concern | Broadleaved upland forest, Lower montane coniferous forest |
| Puccinellia simplex | California alkali grass | Monocots | PMPOA53110 | 80 | 8 | None | None | G3 | S2 | 1 B .2 | BLM_S-Sensitive | Chenopod scrub, Meadow \& seep, Valley \& foothill grassland, Vernal pool |
| Riparia riparia | bank swallow | Birds | ABPAU08010 | 298 | 1 | None | Threatened | G5 | S2 | null | BLM_S-Sensitive, IUCN_LC-Least Concern | Riparian scrub, Riparian woodland |
| Sagittaria sanfordii | Sanford's arrowhead | Monocots | PMALI040Q0 | 126 | 25 | None | None | G3 | S3 | 1B. 2 | BLM_S-Sensitive | Marsh \& swamp, Wetland |
| Sidalcea keckii | Keck's checkerbloom | Dicots | PDMAL110D0 | 50 | 2 | Endangered | None | G2 | S2 | 1B. 1 | SB CaIBG/RSABGCalifornia/Rancho Santa Ana Botanic Garden | Cismontane woodland, Ultramafic, Valley \& foothill grassland |
| Spirinchus thaleichthys | Iongfin smelt | Fish | AFCHB03010 | 46 | 1 | Candidate | Threatened | G5 | S1 | null | null | Aquatic, Estuary |
| Symphyotrichum lentum | Suisun Marsh aster | Dicots | PDASTE8470 | 175 | 1 | None | None | G2 | S2 | 1 B .2 | SB_CaIBG/RSABGCalifornia/Rancho Santa Ana Botanic Garden, SB_USDAUS Dept of Agriculture | Brackish marsh, Freshwater marsh, Marsh \& swamp, Wetland |
| Taxidea taxus | American badger | Mammals | AMAJF04010 | 594 | 3 | None | None | G5 | S3 | null | CDFW_SSCSpecies of Special Concern, IUCN_LCLeast Concern | Alkali marsh, Alkali playa, Alpine, Alpine dwarf scrub, Bog \& fen, Brackish marsh, Broadleaved upland forest, Chaparral, Chenopod scrub, Cismontane woodland, Closed-cone coniferous forest, Coastal bluff scrub, Coastal dunes, Coastal prairie, Coastal scrub, Desert dunes, |


|  |  |  |  |  |  |  |  |  |  |  |  | \|Desert wash, Freshwater marsh, Great Basin grassland, Great Basin scrub, Interior dunes, Ione formation, Joshua tree woodland, Limestone, Lower montane coniferous forest, Marsh \& swamp, <br> Meadow \& seep, Mojavean desert scrub, Montane dwarf scrub, North coast coniferous forest, Oldgrowth, Pavement plain, Redwood, Riparian forest, Riparian scrub, Riparian woodland, Salt marsh, Sonoran desert scrub, Sonoran thorn woodland, Ultramafic, Upper montane coniferous forest, Upper Sonoran scrub, Valley \& foothill grassland |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thamnophis gigas | giant gartersnake | Reptiles | ARADB36150 | 366 | 87 | Threatened | Threatened | G2 | S2 | null | IUCN_VUVulnerable | Marsh \& swamp, Riparian scrub, Wetland |
| Trifolium hydrophilum | saline clover | Dicots | PDFAB400R5 | 56 | 8 | None | None | G2 | S2 | 1B. 2 | null | Marsh \& swamp, Valley \& foothill grassland, Vernal pool, Wetland |
| Tuctoria mucronata | Crampton's tuctoria or Solano grass | Monocots | PMPOA6N020 | 4 | 2 | Endangered | Endangered | G1 | S1 | 1B. 1 | SB_CaIBG/RSABGCalifornia/Rancho Santa Ana Botanic Garden | Valley \& foothill grassland, Vernal pool, Wetland |
| Vireo bellii pusillus | least Bell's vireo | Birds | ABPBW01114 | 503 | 2 | Endangered | Endangered | G5T2 | S2 | null | IUCN_NT-Near Threatened, NABCI_YWLYellow Watch List | Riparian forest, Riparian scrub, Riparian woodland |
| Xanthocephalus xanthocephalus | yellowheaded blackbird | Birds | ABPBXB3010 | 13 | 1 | None | None | G5 | S3 | null | CDFW_SSC- <br> Species of Special Concern, IUCN_LCLeast Concern | Marsh \& swamp, Wetland |

##  construction. View updates and changes made since May 2019 here.

## Plant List

31 matches found. Click on scientific name for details

## Search Criteria

Found in Quads 3812166, 3812165, 3812164, 3812156, 3812155, 3812154, 38121463812145 and 3812144;

## Q Modify Search Criteria Export to Excel $\cap$ Modify Columns $\mathbb{Z}^{*}$ Modify Sort DisplayPhotos

| Scientific Name | Common Name | Family | Lifeform | Blooming Period | CA Rare Plant Rank | State Rank | Global Rank |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Astragalus pauperculus | depauperate milk-vetch | Fabaceae | annual herb | Mar-Jun | 4.3 | S4 | G4 |
| Astragalus tener var. ferrisiae | Ferris' milk-vetch | Fabaceae | annual herb | Apr-May | 1B. 1 | S1 | G2T1 |
| Astragalus tener var. tener | alkali milk-vetch | Fabaceae | annual herb | Mar-Jun | 1B. 2 | S1 | G2T1 |
| Atriplex cordulata var. cordulata | heartscale | Chenopodiaceae | annual herb | Apr-Oct | 1B. 2 | S2 | G3T2 |
| Atriplex depressa | brittlescale | Chenopodiaceae | annual herb | Apr-Oct | 1B. 2 | S2 | G2 |
| Brodiaea rosea ssp. vallicola | valley brodiaea | Themidaceae | perennial bulbiferous herb | Apr- <br> May(Jun) | 4.2 | S3 | G5T3 |
| Carex comosa | bristly sedge | Cyperaceae | perennial rhizomatous herb | May-Sep | 2B. 1 | S2 | G5 |
| Centromadia parryi ssp. parryi | pappose tarplant | Asteraceae | annual herb | May-Nov | 1B. 2 | S2 | G3T2 |
| Centromadia parryi ssp. rudis | Parry's rough tarplant | Asteraceae | annual herb | May-Oct | 4.2 | S3 | G3T3 |
| Chloropyron palmatum | palmate-bracted bird'sbeak | Orobanchaceae | annual herb (hemiparasitic) | May-Oct | 1B. 1 | S1 | G1 |
| Cuscuta obtusiflora var. glandulosa | Peruvian dodder | Convolvulaceae | annual vine (parasitic) | Jul-Oct | 2B. 2 | SH | G5T4? |
| Downingia pusilla | dwarf downingia | Campanulaceae | annual herb | Mar-May | 2B. 2 | S2 | GU |
| Eryngium jepsonii | Jepson's coyote thistle | Apiaceae | perennial herb | Apr-Aug | 1B. 2 | S2? | G2? |
| Extriplex joaquinana | San Joaquin spearscale | Chenopodiaceae | annual herb | Apr-Oct | 1B. 2 | S2 | G2 |
| Fritillaria agrestis | stinkbells | Liliaceae | perennial bulbiferous herb | Mar-Jun | 4.2 | S3 | G3 |
| Gratiola heterosepala | Boggs Lake hedgehyssop | Plantaginaceae | annual herb | Apr-Aug | 1B. 2 | S2 | G2 |
| Hesperevax caulescens | hogwallow starfish | Asteraceae | annual herb | Mar-Jun | 4.2 | S3 | G3 |


| Hibiscus lasiocarpos var. occidentalis | woolly rose-mallow | Malvaceae | perennial rhizomatous herb (emergent) | Jun-Sep | 1B. 2 | S3 | G5T3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Juglans hindsii | Northern California black walnut | Juglandaceae | perennial deciduous tree | Apr-May | 1B. 1 | S1 | G1 |
| Legenere limosa | legenere | Campanulaceae | annual herb | Apr-Jun | 1B. 1 | S2 | G2 |
| Lepidium latipes var. heckardii | Heckard's peppergrass | Brassicaceae | annual herb | Mar-May | 1B. 2 | S1 | G4T1 |
| Lilaeopsis masonii | Mason's lilaeopsis | Apiaceae | perennial rhizomatous herb | Apr-Nov | 1B. 1 | S2 | G2 |
| Myosurus minimus ssp. apus | little mousetail | Ranunculaceae | annual herb | Mar-Jun | 3.1 | S2 | G5T2Q |
| Navarretia leucocephala ssp. bakeri | Baker's navarretia | Polemoniaceae | annual herb | Apr-Jul | 1B. 1 | S2 | G4T2 |
| Neostapfia colusana | Colusa grass | Poaceae | annual herb | May-Aug | 1B. 1 | S1 | G1 |
| Plagiobothrys hystriculus | bearded popcornflower | Boraginaceae | annual herb | Apr-May | 1B. 1 | S2 | G2 |
| Puccinellia simplex | California alkali grass | Poaceae | annual herb | Mar-May | 1B. 2 | S2 | G3 |
| Sagittaria sanfordii | Sanford's arrowhead | Alismataceae | perennial rhizomatous herb (emergent) | May- <br> Oct(Nov) | 1B. 2 | S3 | G3 |
| Symphyotrichum lentum | Suisun Marsh aster | Asteraceae | perennial rhizomatous herb | (Apr)MayNov | 1B. 2 | S2 | G2 |
| Trifolium hydrophilum | saline clover | Fabaceae | annual herb | Apr-Jun | 1B. 2 | S2 | G2 |
| Tuctoria mucronata | Crampton's tuctoria or Solano grass | Poaceae | annual herb | Apr-Aug | 1B. 1 | S1 | G1 |

## Suggested Citation

California Native Plant Society, Rare Plant Program. 2020. Inventory of Rare and Endangered Plants of California (online edition, v8-03 0.39). Website http://www.rareplants.cnps.org [accessed 23 September 2020].
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## Questions and Comments

rareplants@cnps.org
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# United States Department of the Interior 

FISH AND WILDLIFE SERVICE<br>Sacramento Fish And Wildlife Office<br>Federal Building<br>2800 Cottage Way, Room W-2605<br>Sacramento, CA 95825-1846<br>Phone: (916) 414-6600 Fax: (916) 414-6713



In Reply Refer To:
September 23, 2020
Consultation Code: 08ESMF00-2020-SLI-2957
Event Code: 08ESMF00-2020-E-09157
Project Name: River Oaks Marketplace
Subject: List of threatened and endangered species that may occur in your proposed project location, and/or may be affected by your proposed project

## To Whom It May Concern:

The enclosed species list identifies threatened, endangered, proposed and candidate species, as well as proposed and final designated critical habitat, under the jurisdiction of the U.S. Fish and Wildlife Service (Service) that may occur within the boundary of your proposed project and/or may be affected by your proposed project. The species list fulfills the requirements of the Service under section 7(c) of the Endangered Species Act (Act) of 1973, as amended (16 U.S.C. 1531 et seq.).

Please follow the link below to see if your proposed project has the potential to affect other species or their habitats under the jurisdiction of the National Marine Fisheries Service:
http://www.nwr.noaa.gov/protected_species/species_list/species_lists.html
New information based on updated surveys, changes in the abundance and distribution of species, changed habitat conditions, or other factors could change this list. Please feel free to contact us if you need more current information or assistance regarding the potential impacts to federally proposed, listed, and candidate species and federally designated and proposed critical habitat. Please note that under 50 CFR 402.12(e) of the regulations implementing section 7 of the Act, the accuracy of this species list should be verified after 90 days. This verification can be completed formally or informally as desired. The Service recommends that verification be completed by visiting the ECOS-IPaC website at regular intervals during project planning and implementation for updates to species lists and information. An updated list may be requested through the ECOS-IPaC system by completing the same process used to receive the enclosed list.

The purpose of the Act is to provide a means whereby threatened and endangered species and the ecosystems upon which they depend may be conserved. Under sections 7(a)(1) and 7(a)(2) of the Act and its implementing regulations ( 50 CFR 402 et seq.), Federal agencies are required to utilize their authorities to carry out programs for the conservation of threatened and endangered species and to determine whether projects may affect threatened and endangered species and/or designated critical habitat.

A Biological Assessment is required for construction projects (or other undertakings having similar physical impacts) that are major Federal actions significantly affecting the quality of the human environment as defined in the National Environmental Policy Act (42 U.S.C. 4332(2) (c)). For projects other than major construction activities, the Service suggests that a biological evaluation similar to a Biological Assessment be prepared to determine whether the project may affect listed or proposed species and/or designated or proposed critical habitat. Recommended contents of a Biological Assessment are described at 50 CFR 402.12.

If a Federal agency determines, based on the Biological Assessment or biological evaluation, that listed species and/or designated critical habitat may be affected by the proposed project, the agency is required to consult with the Service pursuant to 50 CFR 402. In addition, the Service recommends that candidate species, proposed species and proposed critical habitat be addressed within the consultation. More information on the regulations and procedures for section 7 consultation, including the role of permit or license applicants, can be found in the "Endangered Species Consultation Handbook" at:
http://www.fws.gov/endangered/esa-library/pdf/TOC-GLOS.PDF
Please be aware that bald and golden eagles are protected under the Bald and Golden Eagle Protection Act (16 U.S.C. 668 et seq.), and projects affecting these species may require development of an eagle conservation plan (http://www.fws.gov/windenergy/ eagle_guidance.html). Additionally, wind energy projects should follow the wind energy guidelines (http://www.fws.gov/windenergy/) for minimizing impacts to migratory birds and bats.

Guidance for minimizing impacts to migratory birds for projects including communications towers (e.g., cellular, digital television, radio, and emergency broadcast) can be found at: http:// www.fws.gov/migratorybirds/CurrentBirdIssues/Hazards/towers/towers.htm; http:// www.towerkill.com; and http://www.fws.gov/migratorybirds/CurrentBirdIssues/Hazards/towers/ comtow.html.

We appreciate your concern for threatened and endangered species. The Service encourages Federal agencies to include conservation of threatened and endangered species into their project planning to further the purposes of the Act. Please include the Consultation Tracking Number in the header of this letter with any request for consultation or correspondence about your project that you submit to our office.

Attachment(s):

- Official Species List


## Official Species List

This list is provided pursuant to Section 7 of the Endangered Species Act, and fulfills the requirement for Federal agencies to "request of the Secretary of the Interior information whether any species which is listed or proposed to be listed may be present in the area of a proposed action".

This species list is provided by:

## Sacramento Fish And Wildlife Office

Federal Building

2800 Cottage Way, Room W-2605
Sacramento, CA 95825-1846
(916) 414-6600

## Project Summary

Consultation Code: 08ESMF00-2020-SLI-2957
Event Code: 08ESMF00-2020-E-09157
Project Name: River Oaks Marketplace
Project Type: DEVELOPMENT
Project Description: Development
Project Location:
Approximate location of the project can be viewed in Google Maps: https:// www.google.com/maps/place/38.61581420214891N121.53180859451444W


Counties: Sacramento, CA

## Endangered Species Act Species

There is a total of 8 threatened, endangered, or candidate species on this species list.
Species on this list should be considered in an effects analysis for your project and could include species that exist in another geographic area. For example, certain fish may appear on the species list because a project could affect downstream species.

IPaC does not display listed species or critical habitats under the sole jurisdiction of NOAA Fisheries ${ }^{1}$, as USFWS does not have the authority to speak on behalf of NOAA and the Department of Commerce.

See the "Critical habitats" section below for those critical habitats that lie wholly or partially within your project area under this office's jurisdiction. Please contact the designated FWS office if you have questions.

1. NOAA Fisheries, also known as the National Marine Fisheries Service (NMFS), is an office of the National Oceanic and Atmospheric Administration within the Department of Commerce.

## Birds

| NAME | STATUS |
| :--- | :--- |
| Least Bell's Vireo Vireo bellii pusillus | Endangered |
| There is final critical habitat for this species. Your location is outside the critical habitat. |  |
| Species profile: https://ecos.fws.gov/ecp/species/5945 |  |

## Reptiles

## NAME <br> STATUS

## Giant Garter Snake Thamnophis gigas

Threatened
No critical habitat has been designated for this species.
Species profile: https://ecos.fws.gov/ecp/species/4482

## Amphibians

| NAME | STATUS |
| :---: | :---: |
| California Red-legged Frog Rana draytonii | Threatened |
| There is final critical habitat for this species. Your location is outside the critical habitat. Species profile: https://ecos.fws.gov/ecp/species/2891 |  |
| Species survey guidelines: <br> https://ecos.fws.gov/ipac/guideline/survey/population/205/office/11420.pdf |  |
| California Tiger Salamander Ambystoma californiense <br> Population: U.S.A. (Central CA DPS) <br> There is final critical habitat for this species. Your location is outside the critical habitat. <br> Species profile: https://ecos.fws.gov/ecp/species/2076 | Threatened |

## Fishes

NAME STATUS

Delta Smelt Hypomesus transpacificus
There is final critical habitat for this species. Your location is outside the critical habitat.
Species profile: https://ecos.fws.gov/ecp/species/321

## Insects

| NAME | STATUS |
| :--- | :--- |
| Valley Elderberry Longhorn Beetle Desmocerus californicus dimorphus | Threatened |
| There is final critical habitat for this species. Your location is outside the critical habitat. |  |
| Species profile: https://ecos.fws.gov/ecp/species/7850 |  |
| Habitat assessment guidelines: |  |
| https://ecos.fws.gov/ipac/guideline/assessment/population/436/office/11420.pdf |  |

## Crustaceans

| NAME | STATUS |
| :---: | :---: |
| Vernal Pool Fairy Shrimp Branchinecta lynchi There is final critical habitat for this species. Your location is outside the critical habitat. Species profile: https://ecos.fws.gov/ecp/species/498 | Threatened |
| Vernal Pool Tadpole Shrimp Lepidurus packardi There is final critical habitat for this species. Your location is outside the critical habitat. Species profile: https://ecos.fws.gov/ecp/species/2246 | Endangered |

## Critical habitats

THERE ARE NO CRITICAL HABITATS WITHIN YOUR PROJECT AREA UNDER THIS OFFICE'S JURISDICTION.

## Attachment C

 Transportation Analysis
## RIVER OAKS MARKETPLACE

## CIRCULATION AND ACCESS ANALYSIS

DRAFT REPORT

AUGUST 27, 2020

PREPARED FOR:

CITY OF SACRAMENTO

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## INTRODUCTI ON

This transportation analysis addresses circulation and access conditions associated with the proposed River Oaks Marketplace in the City of Sacramento. The analysis focuses on the project's relationship to the City street system, including nearby intersections, the proposed access points, and on-site circulation. The analysis includes consideration of motorized vehicle traffic, transit service, bicyclists, and pedestrians. Quantitative transportation analyses have been conducted for the following scenarios:

- Existing Conditions (2020)
- Baseline Conditions
- Baseline Plus Project Conditions


## PROJ ECT DESCRIPTION

As illustrated in Figure 1, the 5.23-acre project site is located on the northwest corner of West El Camino Avenue and Orchard Lane in the City of Sacramento. The River Oaks Marketplace project consists of 13,657 square feet of commercial space. The project plan shows uses that include a 7-Eleven (comprised of a Community Market, Restaurant, and Fuel Station), a McDonald's Restaurant with Drive-Through, a Dutch Brothers Coffee Shop with Drive-Through, and a Car Wash. Adjacent properties include The Cove residential development across Orchard Lane to the east (currently under construction and partially occupied), The Core Natomas apartments under construction to the north across Orchard Court, and a vacant parcel to the west.

Figure 2 shows the project site plan. Access is proposed to West El Camino Avenue (right-in / right-out), Orchard Lane (full access), and Orchard Court at two locations (full access).

## ENVIRONMENTAL SETTING

The roadway, transit, bicycle, and pedestrian transportation systems within the study area are described below.

## ROADWAY SYSTEM

The roadway system near the proposed project is described below.
El Camino Avenue is an east-west arterial roadway, extending from El Centro Road to the west to Fair Oaks Boulevard to the east. It accommodates two to four through lanes. In the project vicinity, it is known as West El Camino Avenue and has two through Ianes in each direction. To the west, it provides access to I-80 via a full interchange immediately west of the site. To the east, it provides access to I-5 via a partial interchange (northbound exit, southbound entrance) about 1.0 miles east of the site. West El Camino Avenue has signalized intersections with the I-80 ramps, Orchard Lane, West River Drive / North Cove Drive, and Gateway Oaks Drive.


FIGURE 1. STUDY AREA


FIGURE 2. SITE PLAN

El Centro Road is a two- to four-lane north-south arterial roadway at the western terminus of West El Camino Avenue. To the south, it terminates at a cul-de-sac at I-80. To the north, it extends north of Del Paso Road, and becomes Bayou Way as it curves to the west to parallel I-5. The intersection of El Centro Road and West El Camino Avenue is controlled by stop-signs on the westbound and northbound approaches.

Orchard Lane is a two-lane north-south minor collector that begins at Garden Highway to the south. As part of ongoing construction associated with adjacent development projects, it has recently been completed to a roundabout approximately 700 feet north of West El Camino Avenue. Orchard Lane intersects with Lone Silo Avenue and a driveway to The Core project.

Orchard Court is a local street under construction extending approximately 570 feet west from Orchard Lane to a cul-de-sac.

Lone Silo Avenue is a local residential street that extends easterly from the roundabout at Orchard Lane for about 600 feet to a T-intersection at Bathford Street.

West River Drive is a two-lane local street that begins at West El Camino Avenue. It proceeds southerly for about 0.2 miles, and then turns westerly and crosses Orchard Lane. West River Drive continues westerly through a residential area to its terminus at Wheelhouse Avenue.

North of West El Camino Avenue, West River Drive becomes North Cove Drive, a local residential street that extends northerly for about 600 feet to a T-intersection with Endsley Avenue. As part of The Cove development, a traffic signal was recently installed at the intersection of West El Camino Avenue, West River Drive, and North Cove Drive.

Unity Park Street is a two-lane local street that begins at West El Camino Avenue. It proceeds southerly for about 0.1 miles to its terminus at Unity Pointe Avenue. At West El Camino Avenue, turning movements are limited to right-in / right-out at a stop-sign controlled intersection.

North of West El Camino Avenue, Unity Park Street will extend northerly as a future street into The Cove. It is referred to as "P" Street in this analysis. At West El Camino Avenue, turning movements will be limited to right-in / right-out at a stop-sign controlled intersection.

Gateway Oaks Drive is a north-south minor collector located about 0.7 miles east of the site. The roadway generally has one travel lane in each direction north of its signalized intersection with West El Camino Avenue, and two travel lanes in each direction to the south. Gateway Oaks Drive serves residential development on its west side and office development on its east side. To the south, it extends to Garden Highway. To the north, it extends to the Natomas Main Drainage Canal.

## EXISTING PEDESTRIAN SYSTEM

The pedestrian system in the site vicinity consists of sidewalks on some, but not all, sides of the study area street system.

Adjacent to the site, sidewalks are provided along the north side of West El Camino Avenue. These sidewalks extend through the I-80 interchange to El Centro Road to the west, and beyond the I-5 interchange to the east. On the south side of West El Camino Avenue, sidewalks begin about 250 feet west of Orchard Lane (along the Arco / AM-PM store) and continue to the east. Marked crosswalks are provided on all legs of the signalized West El Camino Avenue / Orchard Lane intersection.

Sidewalks have recently been constructed along the east side of Orchard Lane north of West El Camino Avenue. Sidewalks along the west side of Orchard Lane north of West El Camino Avenue will be constructed as adjacent development occurs. Similarly, sidewalks will be constructed on both sides of Orchard Court.

Continuous sidewalks are provided on both sides of West River Drive, Gateway Oaks Drive and Unity Park Street. Continuous sidewalks are provided on Orchard Lane south of West El Camino Avenue. On El Centro Road in the site vicinity, sidewalks are provided on the east side of the roadway from the I-80 cul-de-sac to about 600 feet north of West El Camino Avenue.

## EXISTING BICYCLE SYSTEM

Figure 3 illustrates the existing bicycle system in the site vicinity. On-street bikeways currently exist on:

- West El Camino Avenue from El Centro Road to the I-5 interchange.
- Orchard Lane from Lone Silo Avenue to Garden Highway (recently constructed north of West El Camino Avenue.
- Gateway Oaks Drive from the Natomas Main Drainage Canal to Garden Highway.
- Garden Highway from Orchard Lane to Gateway Oaks Drive.
- Barandas Drive from Orchard Lane to West River Drive.
- West River Drive from Orchard Lane to west of Barandas Drive.

Off-street bikeways currently include:

- An east-west path from Orchard Lane to West River Drive, extending approximately from Barandas Drive to West River Drive.
- A north-south path on the east side of the Natomas Main Drainage Canal. To the south, it continues to Garden Highway and Natomas Oaks Park. To the north, it crosses I-80 into North Natomas.



## FIGURE 3. BIKEWAYS

Source: City of Sacramento Bikeway User Map, Bicycle master Plan amended on Aug 14, 2018.

## TRANSIT SYSTEM

Regional Transit (RT) service in the site vicinity is illustrated in Figure 4. The closest bus route is Route 88 (West El Camino), which operates along West El Camino Avenue, Gateway Oaks Drive, and Garden Highway. To the east Route 88 extends along West El Camino Avenue to the Arden / Del Paso light rail station. To the south Route 88 extends along Gateway Oaks Drive, Garden Highway, and I-5 to Downtown Sacramento. Route 88 provides weekday, Saturday, and Sunday service.

## STUDY AREA

The following intersections are included in the study area and shown in Figure 1:

1. West El Camino Avenue \& I-80 Westbound Ramps
2. West El Camino Avenue \& I-80 Eastbound Ramps
3. West El Camino Avenue \& Orchard Lane
4. West El Camino Avenue \& West River Drive / North Cove Drive
5. West El Camino Avenue \& Unity Park Street / "P" Street
6. West El Camino Avenue \& Gateway Oaks Drive
7. Orchard Court \& Orchard Lane (under construction)
8. Lone Silo Avenue \& Orchard Lane (under construction)

## EXISTING I NTERSECTION GEOMETRY

Existing intersection geometry (number of approach lanes and traffic control) is illustrated in Figure 5.

## DATA COLLECTION

Peak period intersection turning movement counts were conducted for the AM weekday peak period (7:00 to 9:00 AM) and the PM weekday peak period (4:00 to 6:00 PM) on Thursday, February 6, 2020 at intersections 1 and 2 (freeway ramps). These counts were conducted on behalf of the City as part of the interchange monitoring program.

Due to the economic and travel disruptions of the COVID-19 pandemic, it was not feasible to conduct traffic counts at the other intersections. Earlier counts for intersections 1 through 6 conducted on Thursday, November 16, 2017, were available.


FIGURE 4. REGIONAL TRANSIT MAP
Source: Sacramento Regional Transit Bus \& Light Rail System Map


FIGURE 5. EXISTING INTERSECTION LANE CONFIGURATION

Estimates of intersection turning movement traffic volumes on Tuesday through Thursday February 2020 weekdays were obtained from StreetLight for intersections 1 through 6. StreetLight uses anonymous cell phone traveler data and proprietary algorithms to estimate hourly traffic volumes.

The 2017 counts, 2020 counts, and StreetLight estimates were evaluated and compared:

- At intersections 1 and 2, the AM peak hour counts from 2020 were 2 to 8 percent higher than 2017. They were 0 to 2 percent higher in the PM peak hour.
- The StreetLight estimates included volumes on the north legs of intersections 3 and 4 associated with Cove residents and construction traffic.
- Compared to 2017 data, the StreetLight estimates were generally lower, except at the freeway interchange.

Based upon this comparison, estimated 2020 "existing" traffic volumes were computed as follows:

- At intersections 1 and 2, the 2020 counts were utilized.
- At intersections 3 through 6 , the 2017 counts were utilized, and adjusted as follows:
- At intersections 3 and 4, traffic volumes entering and exiting the north legs were derived from the StreetLight estimates.
- At intersections 3 through 6, eastbound and westbound volumes were increased based upon the difference between 2017 and 2020 counts west of Orchard Lane. These differences were 108 and 131 vehicles per hour eastbound and westbound, respectively in the AM peak hour. During the PM peak hour, the differences were 9 and 0 vehicles per hour eastbound and westbound, respectively.

Figure 6 illustrates the existing 2020 peak hour traffic volumes used in the analysis. Detailed traffic count data are included in the appendix.


FIGURE 6. EXISTING 2020 AM AND PM PEAK HOUR VOLUMES

## REGULATORY SETTING

The site of the project, along with the site of the Core Natomas apartments and the vacant property to the west, were previously reviewed as part of the Park El Camino PUD (adopted by City Council on September 13, 2005). Accordingly, this circulation and access analysis reviews both LOS and VMT. The prior LOS review specified the installation of traffic signals at intersections 1 and 2 (freeway ramps) under baseline plus project conditions. These traffic signals have been installed.

## CITY OF SACRAMENTO

The Mobility Element of the Sacramento 2035 General Plan outlines goals and policies that coordinate the transportation and circulation system with planned land uses. The following level of service policy has been used in this study, as amended on January 23, 2018:

Policy M 1.2.2 Level of Service (LOS) Standard. The City shall implement a flexible context sensitive Level of Service (LOS) standard, and will measure traffic operations against the vehicle LOS thresholds established in this policy. The City will measure Vehicle LOS based on the methodology contained in the latest version of the Highway Capacity Manual (HCM) published by the Transportation Research Board. The City's specific vehicle LOS thresholds have been defined based on community values with respect to modal priorities, land use context, economic development, and environmental resources and constraints. As such, the City has established variable LOS thresholds appropriate for the unique characteristics of the City's diverse neighborhoods and communities. The City will strive to operate the roadway network at LOS D or better for vehicles during typical weekday conditions, including AM and PM peak hour with the following exceptions described below and mapped on Figure M-1 (Figure 7):
A. Core Area (Central City Community Plan Area) - LOS F allowed
B. Priority Investment Areas - LOS F allowed
C. LOS E Roadways - LOS E is allowed for the following roadways because expansion of the roadways would cause undesirable impacts or conflict with other community values.

- 65th Street: Elvas Avenue to 14th Avenue
- Arden Way: Royal Oaks Drive to I-80 Business
- Broadway: Stockton Boulevard to 65th Street
- College Town Drive: Hornet Drive to La Rivera Drive
- El Camino Avenue: I-80 Business to Howe Avenue
- Elder Creek Road: Stockton Boulevard to Florin Perkins Road
- Elder Creek Road: South Watt Avenue to Hedge Avenue
- Fruitridge Road: Franklin Boulevard to SR 99
- Fruitridge Road: SR 99 to 44th Street


FIGURE 7. VEHICLE LEVEL OF SERVICE EXCEPTION AREAS

- Howe Avenue: El Camino Avenue to Auburn Boulevard
- Sutterville Road: Riverside Boulevard to Freeport Boulevard

LOS E is also allowed on all roadway segments and associated intersections located within $1 / 2$ mile walking distance of light rail stations.
D. Other LOS F Roadways - LOS F is allowed for the following roadways because expansion of the roadways would cause undesirable impacts or conflict with other community values.

- 47th Avenue: State Route 99 to Stockton Boulevard
- Arcade Boulevard: Marysville Boulevard to Roseville Road
- Carlson Drive: Moddison Avenue to H Street
- Duckhorn Drive: Arena Boulevard to San Juan Road
- El Camino Avenue: Grove Avenue to Del Paso Boulevard
- Elvas Avenue: J Street to Folsom Boulevard
- Elvas Avenue/56th Street: 52nd Street to H Street
- Florin Road: Havenside Drive to Interstate 5
- Florin Road: Freeport Boulevard to Franklin Boulevard
- Florin Road: Interstate 5 to Freeport Boulevard
- Folsom Boulevard: 47th Street to 65th Street
- Folsom Boulevard: Howe Avenue to Jackson Highway
- Folsom Boulevard: US 50 to Howe Avenue
- Freeport Boulevard: Sutterville Road (North) to Sutterville Road (South)
- Freeport Boulevard: 21st Street to Sutterville Road (North)
- Freeport Boulevard: Broadway to 21st Street
- Garden Highway: Truxel Road to Northgate Boulevard
- H Street: Alhambra Boulevard to 45th Street
- H Street 45th: Street to Carlson Drive
- Hornet Drive: US 50 Westbound On-ramp to Folsom Boulevard
- Howe Avenue: US 50 to Fair Oaks Boulevard
- Howe Avenue: US 50 to 14th Avenue
- Raley Boulevard: Bell Avenue to Interstate 80
- San Juan Road: Duckhorn Drive to Truxel Road
- South Watt Avenue: US 50 to Kiefer Boulevard
- West El Camino Avenue: Northgate Boulevard to Grove Avenue
E. If maintaining the above LOS standards would, in the City's judgment be infeasible and/or conflict with the achievement of other goals, LOS E or F conditions may be accepted provided that provisions are made to improve the overall system, promote non vehicular
transportation, and/or implement vehicle trip reduction measures as part of a development project or a city-initiated project. Additionally, the City shall not expand the physical capacity of the planned roadway network to accommodate a project beyond that identified in Figure M4 and M4a (2035 General Plan Roadway Classification and Lanes).


## LEVEL OF SERVICE AND QUEUE LENGTH ANALYSIS AND METHODOLOGY

Intersection analyses were conducted using a methodology outlined in the Transportation Research Board's Special Report 209, Highway Capacity Manual 6 ${ }^{\text {th }}$ Edition (HCM 6). The methodology utilized is known as "operational analysis." This procedure calculates an average control delay per vehicle at an intersection and assigns a level of service designation based upon the delay. Table 1 presents the level of service criteria for intersections in accordance with the HCM 6 methodology. In accordance with City of Sacramento policy, at unsignalized intersection, the intersection average delay / LOS is used to determine conformity with City policies.

TABLE 1. INTERSECTION LEVEL OF SERVICE

|  | I NTERSECTI ON LEVEL OF SERVICE CRITERIA |  |
| :---: | :---: | :---: |
| LEVEL OF SERVI CE (LOS) | TOTAL DELAY PER VEHI CLE (SECONDS) |  |
|  | SI GNALI ZED | UNSI GNALI ZED |
| A | $\leq 10$ | $\leq 10$ |
| B | $>10$ and $\leq 20$ | $>10$ and $\leq 15$ |
| C | $>20$ and $\leq 35$ | $>15$ and $\leq 25$ |
| D | $>35$ and $\leq 55$ | $>25$ and $\leq 35$ |
| E | $>55$ and $\leq 80$ | $>35$ and $\leq 50$ |
| F | $>80$ | $>50$ |

Source: Highway Capacity Manual 6 ${ }^{\text {th }}$ Edition, Transportation Research Board.

Queue lengths at intersections and driveways have been estimated based upon the 95th percentile queue. HCM 6 computes the queue length for unsignalized intersections and roundabouts. For signalized intersections, Synchro 10 methodology has been utilized.

## RESULTS OF EXISTING CONDITION ANALYSIS

Existing condition intersection analysis results are summarized in Table 2. All the intersections operate at an acceptable LOS D or better.

TABLE 2. EXISTING INTERSECTION OPERATION ANALYSIS

| I NTERSECTI ON | AM PEAK HOUR |  | PM PEAK HOUR |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DELAY <br> (SECONDS) | LOS | DELAY <br> (SECONDS) | LOS |  |  |  |  |  |
| 1. W. El Camino Ave. \& I-80 Westbound Ramps | 21.2 | C | 12.9 | B |  |  |  |  |  |
| 2. W. El Camino Ave. \& I-80 Eastbound Ramps | 39.1 | D | 35.0 | D |  |  |  |  |  |
| 3. W. El Camino Ave. \& Orchard Lane | 52.4 | D | 40.9 | D |  |  |  |  |  |
| 4. W. El Camino Ave. \& W. River Dr. / N. Cove Dr. | 37.2 | D | 39.7 | D |  |  |  |  |  |
| 5. W. El Camino Ave. \& Unity Park St. (avg) | 0.1 | A | 0.1 | A |  |  |  |  |  |
| - Northbound |  |  |  |  |  | 15.5 | C | 12.3 | B |
| 6. W. El Camino Ave. \& Gateway Oaks Dr. | 37.5 | D | 32.1 | C |  |  |  |  |  |

Source: DKS Associates, 2020.

## BASELINE PROJECTS

Immediately adjacent to the project, the following land uses affect circulation and access planning:

- The Cove is a residential development east of Orchard Lane that is currently under construction and partially occupied. At buildout, it will consist of 435 single-family and 156 townhouse dwelling units. The Cove has access via intersections 4, 5, and 8.
- The Core Natomas is a 300-dwelling unit apartment complex north of Orchard Court. It is currently under construction. It will have access via intersection 8 and the cul-de-sac at the west end of Orchard Court.
- A vacant parcel is located west of the Marketplace project. It will have shared access with the Marketplace at Drive 3, and potentially via the cul-de-sac. A 120-room hotel has been assumed as future development on this parcel.


## BASELINE PROJECT TRIP GENERATION

Vehicular trip generation of the baseline projects has been estimated using ITE Trip Generation, Tenth Edition. Table 3 summarizes the baseline project components and associated ITE land use codes.

Table 4 summarizes the baseline project trip generation for daily, AM peak hour, and PM peak hour.

## BASELINE INTERSECTION GEOMETRY

Baseline intersection geometry (number of approach lanes and traffic control) is illustrated in
Figure 8.

TABLE 3. BASELINE PROJECT COMPONENTS AND ASSOCIATED ITE LAND USE CATEGORIES

| PROPERTY | COMPONENT | SIZE | ITE LAND USE <br> CODE(S) | ITE USE(S) |
| :--- | :---: | :---: | :---: | :---: |
| THE CORE <br> NATOMAS | Apartments | 300 DU | 220 | Multifamily Housing (Low-Rise) |
| THE COVE | Single-Family | 435 DU | 210 | Single Family Detached Housing |
| Townhouses <br> VACANT <br> PROPERTY | Hotela | 156 DU | 220 | Multifamily Housing (Low-Rise) |

${ }^{\text {a }}$ Assumed land use for analysis purposes.

Source: ITE Trip Generation, Tenth Edition, 2017 as updated; DKS Associates, 2020.

TABLE 4. BASELINE PROJECT TRIP GENERATION

| PROPERTY | COMPONENT | DAILY | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| THE CORE NATOMAS | Apartments | 2,227 | 31 | 104 | 135 | 99 | 58 | 157 |
| THE COVE | Single-Family | 4,021 | 79 | 235 | 314 | 263 | 154 | 417 |
|  | Townhouses | 1,139 | 17 | 56 | 73 | 55 | 33 | 88 |
|  | Total | 5,160 | 96 | 291 | 387 | 318 | 187 | 505 |
| VACANT PROPERTY | Hotel | 1,468 | 46 | 34 | 80 | 43 | 44 | 87 |

Source: ITE Trip Generation, Tenth Edition, 2017 as updated; DKS Associates, 2020.

## BASELINE TRAFFIC VOLUMES

Baseline traffic volumes were calculated by adding the trips associated with the baseline projects (The Cove, The Core Natomas, and hotel) to existing traffic volumes. To address the construction traffic and partial occupancy of the Cove in the existing traffic counts, all traffic entering and exiting the north legs of intersections 3 and 4 was removed from the study area intersections before adding the trips of the baseline projects.

Figure 9 illustrates the baseline peak hour traffic volumes used in the analysis.


FIGURE 8. BASELINE INTERSECTION LANE CONFIGURATION

| 1. I-80 WB Ramps \& W El Camino Av | 2. 1-80 EB Ramps \& W El Camino Av | 3. Orchard Ln \& W El Camino Av | 4. W River Dr / N Cove Dr \& W El Camino Av |
| :---: | :---: | :---: | :---: |
|  $\begin{aligned} & 453 \text { (268) TH } \\ & 559 \text { (174) } \mathrm{RT} \end{aligned}$ |  |  |  |
| 5. Unity Park St. \& W El Camino Av | 6. Gateway Oaks Dr \& W El Camino Av | 7. Orchard Ln \& Orchard Ct | 8. Orchard Ln \& Lone Silo Av |
|  |  |  |  |
| LEGEND  <br> $x x x(x x x)$ AM Peak (PM Peak) <br> 0 Traffic Signal <br> 0 Stop Control <br> Roundabout $\square$$\square$ | Project Site <br> (3) <br> (4) |  | Legend |

FIGURE 9. BASELINE 2020 AM AND PM PEAK HOUR VOLUMES

## RESULTS OF BASELINE CONDITION ANALYSIS

Baseline condition intersection analysis results are summarized in Table 5. All the intersections operate at an acceptable LOS D or better.

TABLE 5. BASELINE INTERSECTION OPERATION ANALYSIS

| I NTERSECTI ON | AM PEAK HOUR |  | PM PEAK HOUR |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DELAY <br> (SECONDS) | LOS | DELAY <br> (SECONDS) | LOS |  |  |  |  |  |
| 1. W. El Camino Ave. \& I-80 Westbound Ramps | 21.6 | C | 18.0 | B |  |  |  |  |  |
| 2. W. El Camino Ave. \& I-80 Eastbound Ramps | 43.9 | D | 42.2 | D |  |  |  |  |  |
| 3. W. El Camino Ave. \& Orchard Lane | 48.2 | D | 49.5 | D |  |  |  |  |  |
| 4. W. El Camino Ave. \& W. River Dr. / N. Cove Dr. | 38.9 | D | 38.2 | D |  |  |  |  |  |
| 5. W. El Camino Ave. \& Unity Park St. (avg) | 0.2 | A | 0.1 | A |  |  |  |  |  |
| - Northbound |  |  |  |  |  | 16.9 | C | 13.1 | B |
| - Southbound | 11.8 | B | 14.8 | B |  |  |  |  |  |
| 6. W. El Camino Ave. \& Gateway Oaks Dr. | 36.9 | D | 34.1 | C |  |  |  |  |  |
| 7. Orchard Ct. \& Orchard Ln. (avg) | 2.9 | A | 2.3 | A |  |  |  |  |  |
| - Northbound Left | 7.7 | A | 7.5 | A |  |  |  |  |  |
| - Eastbound | 9.4 | A | 8.7 | A |  |  |  |  |  |
| 8. Lone Silo Ave. \& Orchard Ln. | 3.3 | A | 3.8 | A |  |  |  |  |  |

Source: DKS Associates, 2020.

## PROJ ECT TRAVEL CHARACTERISTICS

## TRIP GENERATION

Vehicular trip generation of the project has been estimated using the following sources:

- ITE Trip Generation, Tenth Edition.
- ITE Trip Generation Handbook, Second Edition.
- ITE Trip Generation Handbook, Third Edition.
- Literature review of trip generation data for Dutch Brothers and Car Wash uses.

Table 6 summarizes the components of the project and adjacent properties.
Table 7 summarizes the trip generation of the project components as stand-alone uses. No credits have been taken for alternate mode uses, as travel in the area is predominantly auto oriented at this time.

TABLE 6. PROJECT COMPONENTS AND ASSOCIATED ITE LAND USE CATEGORIES

| PROPERTY | COMPONENT | SI ZE | ITE LAND USE CODE(S) | ITE USE(S) |
| :---: | :---: | :---: | :---: | :---: |
| RIVER OAKS MARKETPLACE | 7-Eleven | $4,650 \mathrm{SF}$ <br> 20 fueling positions | 960 | Super Convenience Market / Gas Station |
|  | McDonalds | 4,500 SF | 934 | Fast-Food Restaurant with Drive-Thru |
|  | Dutch Brothers | 880 SF | $938{ }^{\text {a }}$ | Coffee/Donut Shop with Drive-Thru and No Indoor Seating |
|  | Car Wash | $3,627 \mathrm{SF}$ <br> 1 Tunnel | $948{ }^{\text {b }}$ | Automated Car Wash |

${ }^{\text {a }}$ Limited data; building size out of range.
${ }^{\text {b }}$ Limited data; limited time periods.

Source: ITE Trip Generation, Tenth Edition, 2017 as updated; DKS Associates, 2020.

TABLE 7. SINGLE USE TRIP GENERATION

| PROPERTY | COMPONENT | DAILY | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| RI VER OAKS MARKETPLACE | 7-Eleven | 4,253 | 234 | 233 | 467 | 195 | 194 | 389 |
|  | McDonalds | 2,119 | 92 | 89 | 181 | 76 | 71 | 147 |
|  | Dutch Brothers | 1,793 | 108 | 107 | 215 | 81 | 81 | 162 |
|  | Car Wash | 748 | 22 | 22 | 44 | 39 | 39 | 78 |
|  | Total | 8,913 | 456 | 451 | 907 | 391 | 385 | 776 |

Source: ITE Trip Generation, Tenth Edition, 2017 as updated; DKS Associates, 2020.

## 7-ELEVEN

The 7-Eleven trip generation is calculated from the ITE land use code 960, Super Convenience Market / Gas Station. The multi-variable equations (combining building size and fueling positions) were used for the AM and PM peak hours. The daily value is based upon the average of the daily volumes calculated from building size and fuel position rates.

## MCDONALDS

All trip generation is based upon ITE rates for land use code 934, Fast-Food Restaurant with DriveThru.

## DUTCH BROTHERS

The ITE data for a Coffee/Donut Shop with Drive Thru and No Indoor Seating (Code 938) is limited and inappropriate for Dutch Brothers. The ITE data is based upon three much smaller coffee kiosks of 90 square feet each.

Fehr and Peers Associates collected PM peak hour trip generation data on February 5, 2020, at two Dutch Brothers locations (Roseville and Elk Grove) with similar characteristics. This data has been used by the City in the analysis of a Dutch Brothers project on Northgate Boulevard. The PM peak hour data is shown in Table 7 and will be used for this project.

For the AM peak hour, Crane Transportation Group compiled AM and PM peak hour data at three Dutch Brothers locations in Lodi, Oakley, and Stockton, California on October 3, 2019. Compared to the PM peak hour, the AM peak hour volumes vary from 76 percent to 171 percent. An average value of 133 percent of the PM peak hour was applied to the AM peak hour.

For daily volumes, the ratio of daily trips to peak hour trips (AM and PM combined) from the ITE data was utilized.

## CAR WASH

The ITE data for an automated car wash (Code 948) is limited to rates for the PM peak, which are used for the project.

For the AM peak hour, data collected at car washes in Montebello, Newport Beach, and Rialto in 2014 and 2015 were utilized. During the AM peak hour, the volumes varied from 45 to 72 percent of the PM peak hour volumes. An average value of 57 percent of the PM peak hour was applied to the AM peak hour.

For daily volumes, the ratio of daily trips to peak hour trips (AM and PM combined) from the Montebello car wash was utilized.

## I NTERNAL TRIPS

Because multiple uses are located on the same site, as well as off-site nearby, some patrons may visit more than one land use. This reduces the number of trips at the driveway compared to stand-alone uses, as these trips are typically made as pedestrians. The reduced trips are called internal trips.

Internal trips were calculated for the four River Oak Marketplace uses and The Core Natomas.

Although some pedestrian trips will be made to the project from The Cove, internal trips were not calculated as The Cove is not considered to be part of a mixed-use development. The design of The Cove limits direct access, as a privacy wall has been constructed along Orchard Lane and West El Camino Avenue. No internal trips were calculated for the hotel since the land use is uncertain.

## PASS-BY TRIPS

Pass-by trips are trips that access the project site that are already on the roadway network driving past the site. While these trips are counted at the driveways, they are not new trips.

## VEHICULAR TRIP GENERATION ESTIMATES

Table 8 summarizes the trip generation estimates. The project is estimated to generate 2,500 new external daily trips, 307 during the AM peak hour, and 199 during the PM peak hour. Additional trip generation information is included in the Appendix.

TABLE 8. VEHICULAR TRIP GENERATION ESTIMATES

|  | DAI LY | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| RIVER OAKS MARKETPLACE |  |  |  |  |  |  |  |
| 1. SI NGLE USE TRIPS (SEE TABLE 7) | 8,913 | 456 | 451 | 907 | 391 | 385 | 776 |
| 2. I NTERNAL TRIPS | $-3,181$ | -79 | -70 | -149 | -156 | -180 | -335 |
| 3. DRIVEWAY TRIPS (1. MI NUS 2.) | 5,731 | 377 | 381 | 758 | 235 | 205 | 441 |
| 4. PASS-BY TRIPS | -3,231 | -224 | -227 | -451 | -130 | -112 | -242 |
| 5. NEW EXTERNAL TRIPS (3. MI NUS 4.) | 2,500 | 153 | 154 | 307 | 106 | 93 | 199 |

Source: ITE Trip Generation, Tenth Edition, 2017; ITE Trip Generation Handbook, Second Edition, 2004; ITE Trip Generation Handbook, Third Edition, 2014; and DKS Associates., 2020.

## TRIP DISTRIBUTION

The distribution of trips associated with the proposed project was derived from the regional SACSIM travel model, observations of travel patterns near the site, and knowledge of the proposed access locations associated with the site. Trip distribution varies by time of day and direction of travel. Figure $\mathbf{1 0}$ illustrates the trip distribution of the new external trips on the study area network. Figure 11 illustrates the trip distribution at the project driveways.


FIGURE 10. STUDY AREA TRIP DISTRIBUTION


FIGURE 11. PROJECT DRIVEWAY TRIP DISTRIBUTION

## THRESHOLDS OF SIGNIFICANCE

Consistent with Appendix G of the CEQA Guidelines, thresholds of significance adopted by the governing jurisdictions in applicable general plans and previous environmental documents, and professional judgement, a significant impact would occur if the proposed project would:

## I NTERSECTIONS - CITY OF SACRAMENTO

- The traffic generated by the project degrades LOS from an acceptable LOS (without the project) to an unacceptable LOS (with the project),
- The LOS (without project) is unacceptable and project generated traffic increases the average vehicle delay by 5 seconds or more.
- Note: General Plan Mobility Element Policy M 1.2.2 sets forth definitions for what is considered an acceptable LOS. As previously discussed, Policy M 1.2.2 applies to the study area roadway facilities as follows:
- Intersections - LOS A-D is always to be maintained; provided, LOS E or F may be acceptable if improvements are made to the overall transportation system and/or non-vehicular transportation and transit are promoted as part of the project or a City initiated project.


## TRANSI T

- Adversely affect public transit operations,
- Fail to adequately provide access to transit.


## BICYCLE FACILITIES

- Adversely affect existing or planned bicycle facilities,
- Fail to adequately provide for access by bicycle.

PEDESTRIAN CIRCULATION

- Adversely affect existing or planned pedestrian facilities,
- Fail to adequately provide for access by pedestrians.


## CONSTRUCTION-RELATED TRAFFICIMPACTS

- Degrade an intersection or roadway to an unacceptable level,
- Cause inconveniences to motorists due to prolonged road closures, or
- Result in increased frequency of potential conflicts between vehicles, pedestrians, and bicyclists.


## BASELINE PLUS PROJECT TRAFFIC CONDITIONS

## BASELINE PLUS PROJECT INTERSECTION GEOMETRY

Baseline plus project intersection geometry is illustrated in Figure 12.

## BASELINE PLUS PROJECT TRAFFIC VOLUMES

Baseline plus project traffic volumes were calculated by adding the trips associated with the project to baseline traffic volumes. Adjustments were made to address internal trips between the project and The Core Natomas, and vehicular trips between the project and The Cove. Figure 13 illustrates the baseline plus project peak hour traffic volumes used in the analysis.


FIGURE 12. BASELINE PLUS PROJECT INTERSECTION LANE CONFIGURATION


FIGURE 13. BASELINE PLUS PROJECT 2020 AM AND PM PEAK HOUR VOLUMES

RIVER OAKS MARKETPLACE • CIRCULATION AND ACCESS ANALYSIS • AUGUST 27, 2020

## RESULTS OF BASELINE PLUS PROJECT CONDITION ANALYSIS

Baseline plus project condition intersection analysis results are summarized in Table 9. All the intersections operate at an acceptable LOS D or better.

## TABLE 9. BASELINE PLUS PROJECT INTERSECTION OPERATION ANALYSIS

| I NTERSECTI ON | AM PEAK HOUR |  | PM PEAK HOUR |  |
| :--- | :---: | :---: | :---: | :---: |
|  | DELAY <br> (SECONDS) | LOS | DELAY <br> (SECONDS) | LOS |
| 1. W. El Camino Ave. \& I-80 Westbound Ramps | 23.3 | C | 18.7 | B |
| 2. W. El Camino Ave. \& I-80 Eastbound Ramps | 54.2 | D | 42.4 | D |
| 3. W. El Camino Ave. \& Orchard Lane | 49.9 | D | 42.0 | D |
| 4. W. El Camino Ave. \& W. River Dr. / N. Cove Dr. | 38.1 | D | 38.2 | D |
| 5. W. El Camino Ave. \& Unity Park St. (avg) | 0.2 | A | 0.1 | A |
| - Northbound | 17.0 | C | 13.3 | B |
| - Southbound | 12.1 | B | 14.9 | B |
| 6. W. El Camino Ave. \& Gateway Oaks Dr. | 37.0 | D | 34.4 | C |
| 7. Orchard Ct. \& Orchard Ln. (avg) | 3.0 | A | 2.4 | A |
| - Northbound Left | 7.7 | A | 7.4 | A |
| - Eastbound | 9.4 | A | 8.9 | A |
| 8. Lone Silo Ave. \& Orchard Ln. | 3.2 | A | 3.6 | A |
| 9. W. El Camino Ave. \& Drive 1 (avg) | 1.5 | A | 0.5 | A |
| - Southbound Right | 22.9 | C | 15.4 | C |
| 10. Drive 2 \& Orchard Ln. (avg) | 4.2 | A | 3.1 | A |
| - Northbound Left | 7.9 | A | 7.6 | A |
| - Eastbound | 10.6 | B | 9.8 | A |
| 11. Orchard Ct. \& Drive 1 (avg) | 0.7 | A | 0.8 | A |
| - Northbound | 8.8 | A | 8.7 | A |
| - Westbound Left | 7.3 | A | 7.3 | A |

Source: DKS Associates, 2020.

## IMPACTS AND MITIGATION MEASURES

## Impact 1:

The proposed project would increase traffic volume and delay at study area intersections under the existing plus project scenario. Based on the analysis below, the impact is less than significant.

As summarized in Table 9, the project would increase average delay at several study area intersections. The project would increase traffic volumes at several study area intersections. The resultant operating conditions do not exceed the LOS D goals.

## Mitigation Measure 1:

None required.

## Impact 2:

The proposed project could cause potentially significant impacts to transit. Based on the analysis below, the impact is less than significant.

The proposed project would not adversely affect public transit operations. The project would not modify or impede any existing or planned transit facilities / routes.

## Mitigation Measure 2:

None required.

## I mpact 3:

The proposed project could cause potentially significant impacts to pedestrian facilities. Based on the analysis below, the impact is less than significant.

The proposed project would not adversely affect existing or planned pedestrian facilities. The project will include sidewalks along the project frontage.

## Mitigation Measure 3:

None required.

## I mpact 4:

The proposed project could cause potentially significant impacts to bicycle facilities. Based on the analysis below, the impact is less than significant.

The proposed project would not adversely affect existing or planned bicycle facilities.

## Mitigation Measure 4:

None required.

## I mpact 5:

The proposed project could cause potentially significant impacts due to construction-related activities. Based on the analysis below, the impact is less than significant.

The City Code (City Code 12.20 .030 ) requires that a construction traffic control plan be prepared and approved prior to the beginning of project construction, to the satisfaction of the City Traffic Engineer and subject to review by all affected agencies. All work performed during construction must conform to the conditions and requirements of the approved plan. The plan shall ensure that safe and efficient movement of traffic through the construction work zone(s) is maintained. At a minimum, the plan shall include the following:

- Time and day of street closures
- Proper advance warning and posted signage regarding street closures
- Provision of driveway access plan to ensure safe vehicular, pedestrian, and bicycle movements
- Safe and efficient access routes for emergency vehicles
- Provisions for pedestrian safety
- Use of manual traffic control when necessary
- Number of anticipated truck trips, and time of day of arrival and departure of trucks
- Provision of a truck circulation pattern and staging area with a limitation on the number of trucks that can be waiting and any limitations on the size and type of trucks appropriate for the surrounding transportation network
- The plan must be available at the site for inspection by the City representative during all work. With the implementation of the traffic control plan, local roadways and freeway facilities will continue to operate at acceptable operating conditions and the impact of the project would be less than significant.


## Mitigation Measure 5:

None required.

## ON-SITE OPERATIONS REVIEW AND QUEUING

The project site plan was reviewed for conformity with accepted traffic engineering principles and City Design Guidelines.

Figure 2 shows the project site plan. Access is proposed to West El Camino Avenue (right-in / right-out), Orchard Lane (full access), and Orchard Court at two locations (full access).

## INTERSECTION AND DRIVEWAY SPACING

The review of driveway spacing is based upon traffic engineering principles to maintain efficient movement for motorized vehicles, pedestrians, and bicyclists, and minimize conflicts and crashes. Research has shown that proper spacing of intersections and driveways reduces crash frequency, as motorists have ample time between decision points to react to other vehicles that may affect their movement.

West El Camino Avenue is a four-lane arterial roadway. Based upon the City Design and Procedures Manual Section 15 - Street Design Standards, minimum intersection and / or driveway spacing is 250 feet for a four-lane arterial (Table 15-7.3). The distance is measured between the nearest curb returns. The curb return is defined as the beginning of the curb radius connecting to the intersecting street. Driveway spacing for a four-lane arterial is 250 feet, measured between the inside edges of the driveways.

Orchard Lane is a two-lane minor collector. The minimum intersection spacing is 120 feet, with minimum driveway separation considered on a case by case basis.

Orchard Court is a local commercial street. The minimum intersection spacing is 120 feet, with minimum driveway separation of 10 feet.

The AASHTO "Green Book" states that "Driveways should not be situated within the functional boundary of at-grade intersections. This boundary would include the longitudinal limits of auxiliary lanes." In this context, auxiliary lanes refer to exclusive turning lanes at the intersections including taper lengths. Thus, driveways should not be located within the area of turning lanes or anticipated queuing areas.

## INTERSECTION 9 - WEST EL CAMINO AVENUE AND DRIVE 1

The baseline plus project peak hour analysis indicates that this intersection will operate at an acceptable level of service as a right-in / right-out driveway, with 32.1 seconds of average delay (LOS D) on the driveway approach during the AM peak hour, and 17.1 seconds during the PM peak hour.

A review of the site plan indicates that this driveway is located less than 250 feet from the Orchard Drive intersection, measured from the curb return and inside driveway edge. This does not conform with City Street Design Standards.

Westbound West El Camino Avenue has two westbound lanes at the project site. Along the westerly edge of the project frontage, each lane is dedicated to a specific destination; the right lane is for traffic to I-80 East, and the left lane is for traffic to I-80 West or continuing on West El Camino Avenue to El Centro Road. During the p.m. peak hour, the westbound 95th percentile queue at Intersection 2 is estimated to extend to Intersection 9. Thus, the proposed driveway is within the functional boundary of Intersection 2 . Traffic exiting the site may have difficulty accessing the left lane due to the queuing, and have the potential to block the right lane.

Recommendation 1 - Limit Drive 1 to inbound access only. Relocate the Drive 1 intersection with West El Camino Avenue to the west to achieve 250 -foot driveway spacing. Maintain 250 -foot driveway spacing to the west to the Caltrans Limited Access Line approaching the I-80 Eastbound entrance ramp. Provide a deceleration lane as long as possible.

## INTERSECTION 10 - DRIVE 2 AND ORCHARD LANE

A review of the site plan indicates that the driveway is located within the area of the Orchard Lane turning lanes. The driveway location overlaps with the southbound turning lanes. No provision has been made for a northbound left turn lane for turning movements into the driveway. Due to the proximity of the driveway to Orchard Court, it is not feasible to provide northbound left turn lanes for both Drive 2 and Orchard Court. The proposed driveway is within the functional boundaries of Intersections 3 and 7.

Recommendation 2 - Eliminate driveway access to Orchard Lane.

## INTERSECTION 11 - ORCHARD COURT AND DRIVE 1

The baseline plus project peak hour analysis indicates that this intersection will operate at an acceptable level of service as proposed. The driveway is located over 160 feet from Orchard Lane and over 300 feet from the cul-de-sac driveway (Drive 3), more than the City intersection spacing criteria. There are no proposed driveways on the north side of Orchard Court east of the cul-de-sac. This driveway location is acceptable.

## CUL-DE-SAC - ORCHARD COURT AND DRIVE 3

This driveway location is acceptable, opposite the driveway to The Core Natomas, and located over 300 feet west of Drive 1.

## DRIVEWAY THROAT LENGTHS

The "throat length" of a driveway is defined as the distance from the outer edge of the traveled way of the intersecting roadway to the first point along the driveway at which there are conflicting vehicular traffic movements. Conflicting movements include turning vehicles and vehicles entering / exiting parking stalls. Adequate throat length is critical to ensure that queued exiting vehicles do not interfere with / block entering vehicles, resulting in entering queues extending onto city sidewalks and / or streets.

## INTERSECTION 9 - WEST EL CAMINO AVENUE AND DRIVE 1

The following recommendation assumes inbound only access at Drive 1 from West El Camino Avenue.

Recommendation 3 - Provide a minimum throat length of 5 vehicles on Drive 1 entering the site.

## INTERSECTION 11 - ORCHARD COURT AND DRIVE 1

The site plan indicates a proposed throat length of about 60 feet on the Drive 1 approach to Orchard Court. This is acceptable. A minimum length of 50 feet should be maintained.

## CUL-DE-SAC - ORCHARD COURT AND DRIVE 3

The site plan indicates a proposed throat length of about 50 feet on the Drive 3 approach to the Orchard Court cul-de-sac. This is acceptable. A minimum length of 50 feet should be maintained.

## DRIVE-THRU QUEUEING ANALYSIS

The Sacramento City Code specifies the minimum stacking distance for a drive-through facility at 180 feet.

## MCDONALDS

A review of the site plan indicates that the McDonalds drive-thru lane provides approximately 180 feet of storage, meeting the City requirement.

## DUTCH BROTHERS

PM peak period observations of drive-through queuing were conducted by Fehr \& Peers on Wednesday, February 5, 2020 at the following locations:

- Dutch Brothers coffee store located at 1225 Baseline Road in Roseville, CA
- Dutch Brothers coffee store located at 8610 Elk Grove Boulevard in Elk Grove, CA

The maximum queue observed at both locations was 16 vehicles. These queued vehicles represented both motorists waiting to place their order at the kiosk, as well as motorists in queue waiting to pay and receive their order. This queue length has been utilized by the City in the previous review of the proposed Dutch Brothers location on Northgate Boulevard.

The site plan shows approximately 280 feet available. Assuming each vehicle occupies 20 feet, the maximum queue of 320 feet ( 16 vehicles) would result in an excess of 40 feet, approximately two vehicles that would need to wait within the drive aisles of the parking lot. This could temporarily hinder circulation and parking maneuvers within the site, but any queuing would be expected to be contained within the site and would not spillback to City streets or sidewalks.

## CAR WASH

A review of the site plan indicates that the Car Wash drive-thru lanes provide over 300 feet of storage, meeting the City requirement.

## VEHICULAR CIRCULATION PATTERNS

With the revision of Drive 1 to accommodate only inbound access from West El Camino Avenue, the project circulation pattern does not encourage cut-through traffic.

## BICYCLE ACCESS

On-street bicycle lanes are located along West El Camino Avenue and Orchard Lane. Access to the site is provided via the proposed driveways. Two short term bicycle spaces and two bicycle lockers are proposed at each of the four buildings, yielding a total of 16 bicycle parking spaces.

## PEDESTRIAN ACCESS

## PROJ ECT SITE

In addition to the sidewalks proposed along the street frontage on three sides of the project, the project provides several pedestrian paths / sidewalks on-site. Based upon a review of the site plan, the following recommendation has been developed:

Recommendation 4 - Provide direct pedestrian access (sidewalk / pathway) between the sidewalk on the north side of West El Camino Avenue and each of the Dutch Brothers, McDonalds, and 7-Eleven buildings.

Without implementation of this recommendation, pedestrians from the south may access the site through landscaped areas or driveways / parking lots rather than following the proposed circuitous pedestrian routes.

## ORCHARD DRIVE PEDESTRIAN CROSSINGS

Pedestrian crosswalks of Orchard Drive are provided at West El Camino Avenue (signalized) and Lone Silo Avenue (roundabout). DKS has investigated a marked crosswalk at Orchard Court.

The City of Sacramento utilizes its Pedestrian Crossing Guidelines to evaluate the installation of marked crosswalks at uncontrolled locations. Based upon Phase 1 screening, a marked crosswalk is not recommended at this location:

- The location is not 300 feet or greater from the nearest crossing. While the crossing at West El Camino Avenue is about 300 feet south, the crossing at Lone Silo Avenue is less than 300 feet north.
- The crossing does not serve a direct pedestrian route. The east side of Orchard Lane is bordered by a privacy wall, and access is not provided to the Cove at this location.
- Continuous sidewalks on the west side of Orchard Lane provide pedestrian access from both existing crosswalks.


## ON-SITE TRUCK CIRCULATION PLAN

Anticipated truck turning movements should be illustrated on the site plan, as well as staging areas for deliveries. Large vehicles, including fuel tankers, trash trucks, and delivery trucks, should not unload / load in primary access drives during peak hours of operation.

## ACCESS TO THE VACANT PARCEL TO THE WEST

The site plan illustrates a future connection to the parcel to the west at the intersection of Drive 2 and Drive 3. This connection will facilitate future travel between the parcels without the need to access the City street system. Provision of a future pedestrian connection at this location should also be accommodated.

## SUMMARY OF RECOMMENDATIONS

Figure 14 summarizes the site circulation recommendations.


FIGURE 14. SITE CIRCULATION RECOMMENDATIONS

By modifying Intersection 9 and eliminating Intersection 10, the recommendations modify the travel patterns entering and exiting the site. DKS conducted analysis of intersection operating conditions with the recommendations.

## BASELINE PLUS PROJECT WITH RECOMMENDATIONS TRIP DISTRIBUTION

Figure 15 illustrates the trip distribution at the project driveways assuming the implementation of the recommendations.

## BASELINE PLUS PROJECT WITH RECOMMENDATIONS INTERSECTION GEOMETRY

Baseline plus project with recommendations intersection geometry is illustrated in Figure 16.
bASELINE PLUS PROJECT TRAFFIC VOLUMES
Figure 17 illustrates the baseline plus project with recommendations peak hour traffic volumes used in the analysis.


FIGURE 15. PROJECT DRIVEWAY TRIP DISTRIBUTION WITH RECOMMENDATIONS


FIGURE 16. BASELINE PLUS PROJECT WITH RECOMMENDATIONS INTERSECTION LANE CONFIGURATION

| 1. I-80 WB Ramps \& W El Camino Av $\begin{aligned} & 468 \text { (294) TH } \\ & 559 \text { (174) } \mathrm{RT} \end{aligned}$ | 2. I-80 EB Ramps \& W El Camino Av |  |  |
| :---: | :---: | :---: | :---: |
|  |  |  | 8. Orchard Ln \& Lone Silo Av |
| 9. Drive 1 \& W El Camino Av $1543 \text { (1402) TH }$ | 10. Orchard Ln \& Drive 2 <br>  | 11. Drive 1 \& Orchard Ct | LEGEND |
|  |  | 5 |  |

FIGURE 17. BASELINE PLUS PROJECT WITH RECOMMENDATIONS 2020 AM AND PM PEAK HOUR VOLUMES

## RESULTS OF BASELINE PLUS PROJECT WITH RECOMMENDATIONS CONDITION ANALYSIS

Baseline plus project with recommendations condition intersection analysis results are summarized
in Table 10. All the intersections operate at an acceptable LOS D or better.

TABLE 10. BASELINE PLUS PROJECT WITH RECOMMENDATIONS I NTERSECTION OPERATION
ANALYSIS

| INTERSECTI ON | AM PEAK HOUR |  | PM PEAK HOUR |  |
| :---: | :---: | :---: | :---: | :---: |
|  | DELAY (SECONDS) | LOS | DELAY (SECONDS) | LOS |
| 1. W. El Camino Ave. \& I-80 Westbound Ramps | 23.3 | C | 18.7 | B |
| 2. W. El Camino Ave. \& I-80 Eastbound Ramps | 54.2 | D | 42.4 | D |
| 3. W. El Camino Ave. \& Orchard Lane | 51.9 | D | 41.3 | D |
| 4. W. El Camino Ave. \& W. River Dr. / N. Cove Dr. | 38.1 | D | 38.2 | D |
| 5. W. El Camino Ave. \& Unity Park St. (avg) | 0.2 | A | 0.1 | A |
| - Northbound | 17.0 | C | 13.3 | B |
| - Southbound | 12.1 | B | 14.9 | B |
| 6. W. El Camino Ave. \& Gateway Oaks Dr. | 37.0 | D | 34.4 | C |
| 7. Orchard Ct. \& Orchard Ln. (avg) | 8.4 | A | 3.8 | A |
| - Northbound Left | 8.2 | A | 7.7 | A |
| - Eastbound | 12.9 | B | 8.9 | A |
| 8. Lone Silo Ave. \& Orchard Ln. | 3.2 | A | 3.6 | A |
| 9. W. El Camino Ave. \& Drive 1 | No Control Delay |  |  |  |
| 10. Drive 2 \& Orchard Ln. | Intersection Eliminated |  |  |  |
| 11. Orchard Ct. \& Drive 1 (avg) | 8.1 | A | 6.7 | A |
| - Northbound | 10.8 | B | 9.5 | A |
| - Westbound Left | 7.7 | A | 7.5 | A |

Source: DKS Associates, 2020.

## VMT ANALYSIS

## VMT IMPACT CRITERIA - SB 743

Senate Bill 743 (Steinberg, 2018), codified in Public Resources Code section 21099, required changes to the CEQA Guidelines on the analysis of transportation impacts. In January 2019, the Natural Resources Agency updated the CEQA Guidelines in response to SB 743. The revised guidelines state, "Generally, vehicle miles traveled is the most appropriate measure of transportation impacts." In addition, "Except as provided in subdivision (b)(2) below...a project's effect on automobile delay shall not constitute a significant environmental impact." With respect to the timing of the change to the CEQA Guidelines, "A lead agency may elect to be governed by the
provisions of this section immediately. Beginning on July 1, 2020, the provisions of this section shall apply statewide." ${ }^{1}$

The most authoritative guidance on implementing the SB 743 changes comes from the Governor's Office of Planning and Research (OPR), which worked with the Natural Resources Agency to update the CEQA Guidelines. In December 2018, OPR published technical guidance recommending approaches to analyzing transportation and land use projects. Because new retail development often redistributes trips rather than creating new travel demand, the OPR guidance recommends that lead agencies analyze the net change in VMT to indicate the transportation impact of retail projects. ${ }^{2}$

The potential for VMT impacts, according to this approach, hinges on whether the project can be considered local-serving or regional. By adding retail opportunities within existing neighborhoods, local-serving retail projects can shorten trips and reduce overall VMT. In contrast, regional destination retail projects would draw customers from larger trade areas, potentially substituting for shorter trips and increasing VMT. The OPR guidance suggests that any retail projects including stores larger than 50,000 square feet might be considered regional serving retail.

## RETAIL CENTER CHARACTERISTICS

The classification of commercial centers (retail centers, shopping centers) is complicated by the many possible combinations of uses within any center. However, for purposes of managing and leasing space, the shopping center industry has developed a classification scheme with ten categories. Of the ten categories, the "Strip / Convenience" Center and the "Neighborhood Center" can usually be considered as local-serving retail. These centers, which typically range in size up to 125,000 square feet, are occupied by uses oriented to a trade area of three miles or less. The typical uses are ubiquitous throughout the area, with many nearby competitors, as well as multiple locations of specific tenants. Neighborhood centers require the support of 6,000 to 8,000 households in a one- to two-mile radius. ${ }^{3}$

## PROJECT ENVIRONS AND CHARACTERISTICS

As discussed in the description of VMT screening of retail projects, a retail project may result in a reduction of VMT if it is "local-serving retail". The following characteristics of the environs and of the project itself were evaluated.

[^0]
## NEARBY LAND USES

The project is in the South Natomas Community Plan area, which encompasses about 5,000 acres. The South Natomas Community Plan Area encompasses numerous suburban neighborhoods, employment centers, and corridors. There are over 15,000 residents in South Natomas.

Immediately adjacent to the project to the north and east are the Core Natomas and The Cove residential projects, which will consist of 891 dwelling units at buildout. South of West El Camino Avenue is the established Willowcreek neighborhood, with over 1,500 dwelling units and 4,000 residents, within 1.2 miles of the project site.

## PROJ ECT COMPONENTS

The proposed project components are retail / service uses that are common throughout the South Natomas area. They are intended to serve the local area and will compete with nearby businesses. No "unique" or destination-retail uses are proposed which would be likely to attract a substantial number of long-distance trips.

- Convenience Store - There are competing convenience stores within the site vicinity, including an AM PM market / fuel station across West El Camino Avenue.
- Restaurants / Coffee Shops - There are over twenty dining establishments within two miles of the site, including coffee shops and fast food restaurants.
- Car Wash - There are several car washes within the site vicinity, including a car wash associated with the AM PM market across West El Camino Avenue.


## PROJ ECT TRAVEL PATTERNS

The earlier transportation analysis provides quantitative estimates of project vehicular trip generation. The project is estimated to generate 8,833 vehicle trips.

- About 36 percent of the trips will be internal trips. These internal trips between uses on the site will replace automobile trips.
- About 36 percent are expected to be pass-by trips. Pass-by trips are vehicle trips that access the project site that are already on the roadway network driving past the site. These linked trips result in minimal changes in VMT.

The project also has good pedestrian access to the adjacent existing and new neighborhoods, which could reduce automobile trips to the site.

## SUMMARY

The project is considered to be local-serving retail, which is presumed to have a less than significant VMT impact based upon OPR guidance.

## APPENDIX

## 2017 TRAFFIC COUNTS

## National Data \& Surveying Services

Location: ECcertrord w E Canino o Intersection Turning Movement Count
City: Sacramento Project ID: 17-07949-001
Control: Date: 11/16/2017

| NS/EW Streets: | Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | El Centro Rd |  |  |  | El Centro Rd |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | NL | 0NT | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{SL} \end{gathered}$ | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ E L \end{gathered}$ | $\begin{gathered} 0 \\ \text { ET } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | 0EU | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WR } \end{gathered}$ | 0WU | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 0 | 0 | 5 | 0 | 180 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 48 | 7 | 255 |
| 7:15 AM | 0 | 9 | 9 | 0 | 235 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 70 | 1 | 340 |
| 7:30 AM | 0 | 5 | 7 | 0 | 261 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 74 | 3 | 373 |
| 7:45 AM | 0 | 5 | 9 | 0 | 228 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 58 | 3 | 337 |
| 8:00 AM | 0 | 4 | 9 | 0 | 253 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 50 | 3 | 344 |
| 8:15 AM | 0 | 3 | 6 | 0 | 232 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 57 | 0 | 319 |
| 8:30 AM | 0 | 4 | 10 | 0 | 229 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 58 | 1 | 330 |
| 8:45 AM | 0 | 9 | 12 | 0 | 209 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 57 | 2 | 309 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 39 | 67 | 0 | 1827 | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 117 | 0 | 472 | 20 | 2607 |
| APPROACH \%'s : | 0.00\% | 36.79\% | 63.21\% | 0.00\% | 96.56\% | 3.44\% | 0.00\% | 0.00\% |  |  |  |  | 19.21\% | 0.00\% | 77.50\% | 3.28\% |  |
| PEAK HR : |  | 7:15 AM - | 8:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL: | 0 | 23 | 34 | 0 | 977 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 70 | 0 | 252 | 10 | 1394 |
| PEAK HR FACTOR : | 0.000 | 0.639 | 0.944 | 0.000 | 0.936 | 0.636 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.761 | 0.000 | 0.851 | 0.833 |  |
|  |  | 0.7 |  |  |  | 0.9 |  |  |  |  |  |  |  | 0.8 |  |  | 0.934 |


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0NL | $\begin{gathered} 0 \\ \text { NT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{SL} \end{gathered}$ | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ET } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 0 | 8 | 11 | 0 | 85 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 146 | 2 | 270 |
| 4:15 PM | 0 | 7 | 6 | 0 | 92 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 143 | 5 | 276 |
| 4:30 PM | 0 | 16 | 13 | 0 | 78 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 188 | 3 | 320 |
| 4:45 PM | 0 | 10 | 10 | 0 | 83 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 193 | 1 | 319 |
| 5:00 PM | 0 | 5 | 14 | 0 | 82 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 204 | 7 | 347 |
| 5:15 PM | 0 | 15 | 16 | 0 | 86 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 189 | 3 | 336 |
| 5:30 PM | 0 | 7 | 6 | 0 | 111 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 208 | 2 | 368 |
| 5:45 PM | 0 | 9 | 9 | 0 | 151 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 194 | 6 | 392 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 77 | 85 | 0 | 768 | 70 | 0 | 0 | 0 | 0 | 0 | 0 | 134 | 0 | 1465 | 29 | 2628 |
| APPROACH \%'s : | 0.00\% | 47.53\% | 52.47\% | 0.00\% | 91.65\% | 8.35\% | 0.00\% | 0.00\% |  |  |  |  | 8.23\% | 0.00\% | 89.99\% | 1.78\% |  |
| PEAK HR : |  | 5:00 PM | 6:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 36 | 45 | 0 | 430 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 0 | 795 | 18 | 1443 |
| PEAK HR FACTOR : | 0.000 | 0.600 | 0.703 | 0.000 | 0.712 | 0.733 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.815 | 0.000 | 0.956 | 0.643 |  |
|  |  | 0.6 |  |  |  | 0.7 |  |  |  |  |  |  |  | 0.9 |  |  | 0.920 |

## National Data \& Surveying Services

Locaton: :sowb of famp \& w ic canlantersection Turning Movement Count
Project ID: 17-07949-00
Date: 11/16/2017

| Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NS/EW Streets: | I-80 WB Off Ramp |  |  |  | I-80 WB Off Ramp |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | $\begin{gathered} 0 \\ \mathrm{NL} \end{gathered}$ |  | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{SL} \end{gathered}$ | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{EL} \end{gathered}$ | $\begin{gathered} 0 \\ \text { ET } \end{gathered}$ | 0 | 0 | 0 | 0 | WR | 0WU | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  | ER | EU | WL | WT |  |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 82 | 0 | 19 | 0 | 0 | 83 | 113 | 0 | 0 | 45 | 74 | 0 | 416 |
| 7:15 AM | 0 | 0 | 0 | 0 | 138 | 0 | 28 | 0 | 0 | 121 | 131 | 0 | 0 | 58 | 132 | 0 | 608 |
| 7:30 AM | 0 | 0 | 0 | 0 | 176 | 0 | 22 | 0 | 0 | 134 | 143 | 0 | 0 | 75 | 118 | 0 | 668 |
| 7:45 AM | 0 | 0 | 0 | 0 | 163 | 0 | 18 | 0 | 0 | 112 | 123 | 0 | 0 | 69 | 120 | 0 | 605 |
| 8:00 AM | 0 | 0 | 0 | 0 | 153 | 0 | 13 | 0 | 0 | 133 | 139 | 0 | 0 | 60 | 89 | 0 | 587 |
| 8:15 AM | 0 | 0 | 0 | 0 | 170 | 0 | 21 | 0 | 0 | 118 | 123 | 0 | 0 | 53 | 89 | 0 | 574 |
| 8:30 AM | 0 | 0 | 0 | 0 | 162 | 0 | 29 | 0 | 0 | 111 | 136 | 0 | 0 | 47 | 88 | 0 | 573 |
| 8:45 AM | 0 | 0 | 0 | 0 | 147 | 0 | 26 | 0 | 0 | 111 | 117 | 0 | 0 | 45 | 49 | 0 | 495 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 1191 | 0 | 176 | 0 | 0 | 923 | 1025 | 0 | 0 | 452 | 759 | 0 | 4526 |
| APPROACH \%'s : |  |  |  |  | 87.13\% | 0.00\% | 12.87\% | 0.00\% | 0.00\% | 47.38\% | 52.62\% | 0.00\% | 0.00\% | 37.32\% | 62.68\% | 0.00\% |  |
| PEAK HR : |  | 7:15 AM | 8:15 A |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 630 | 0 | 81 | 0 | 0 | 500 | 536 | 0 | 0 | 262 | 459 | 0 | 2468 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.895 | 0.000 | 0.723 | 0.000 | 0.000 | 0.933 | 0.937 | 0.000 | 0.000 | 0.873 | 0.869 | 0.000 |  |
|  |  |  |  |  |  | 0.8 |  |  |  | 0.9 |  |  |  | 0.9 |  |  | 0.924 |


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0$N L$ | $\begin{gathered} 0 \\ \text { NT } \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \end{gathered}$ | $\begin{gathered} 0 \\ \text { SL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ET } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 71 | 0 | 37 | 0 | 0 | 59 | 45 | 0 | 0 | 126 | 88 | 0 | 426 |
| 4:15 PM | 0 | 0 | 0 | 0 | 74 | 0 | 29 | 0 | 0 | 55 | 51 | 0 | 0 | 131 | 90 | 0 | 430 |
| 4:30 PM | 0 | 0 | 0 | 0 | 84 | 0 | 32 | 0 | 0 | 50 | 41 | 0 | 0 | 174 | 119 | 0 | 500 |
| 4:45 PM | 0 | 0 | 0 | 0 | 121 | 0 | 28 | 0 | 0 | 55 | 37 | 0 | 0 | 186 | 121 | 0 | 548 |
| 5:00 PM | 0 | 0 | 0 | 0 | 112 | 0 | 34 | 0 | 0 | 63 | 39 | 0 | 0 | 201 | 127 | 0 | 576 |
| 5:15 PM | 0 | 0 | 0 | 0 | 121 | 0 | 24 | 0 | 0 | 57 | 45 | 0 | 0 | 186 | 89 | 0 | 522 |
| 5:30 PM | 0 | 0 | 0 | 0 | 104 | 0 | 33 | 0 | 0 | 72 | 48 | 0 | 0 | 203 | 83 | 0 | 543 |
| 5:45 PM | 0 | 0 | 0 | 0 | 88 | 0 | 26 | 0 | 0 | 96 | 78 | 0 | 0 | 191 | 83 | 0 | 562 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 775 | 0 | 243 | 0 | 0 | 507 | 384 | 0 | 0 | 1398 | 800 | 0 | 4107 |
| APPROACH \%'s : |  |  |  |  | 76.13\% | 0.00\% | 23.87\% | 0.00\% | 0.00\% | 56.90\% | 43.10\% | 0.00\% | 0.00\% | 63.60\% | 36.40\% | 0.00\% |  |
| PEAK HR : |  | 5:00 PM | 6:00 P |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 425 | 0 | 117 | 0 | 0 | 288 | 210 | 0 | 0 | 781 | 382 | 0 | 2203 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.878 | 0.000 | 0.860 | 0.000 | 0.000 | 0.750 | 0.673 | 0.000 | 0.886 |  |  |  |  |
|  |  |  |  |  | 0.928 |  |  |  | 0.716 |  |  |  |  |  |  |  | 0.956 |

## National Data \& Surveying Services

Location: :se E of fanamp w icamintersection Turning Movement Count
Project ID: 17-07949-003
Date: 11/16/2017

| Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NS/EW Streets: | I-80 EB Off Ramp |  |  |  | I-80 EB Off Ramp |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 22 | 0 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 131 | 29 | 0 | 0 | 109 | 92 | 0 | 431 |
| 7:15 AM | 20 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 229 | 29 | 0 | 0 | 157 | 116 | 0 | 579 |
| 7:30 AM | 25 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 270 | 38 | 0 | 0 | 183 | 149 | 0 | 702 |
| 7:45 AM | 20 | 0 | 80 | 0 | 0 | 0 | 0 | 0 | 0 | 250 | 25 | 0 | 0 | 161 | 190 | 0 | 726 |
| 8:00 AM | 23 | 0 | 73 | 0 | 0 | 0 | 0 | 0 | 0 | 254 | 34 | 0 | 0 | 128 | 100 | 0 | 612 |
| 8:15 AM | 34 | 0 | 81 | 0 | 0 | 0 | 0 | 0 | 0 | 259 | 27 | 0 | 0 | 121 | 63 | 0 | 585 |
| 8:30 AM | 36 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 238 | 37 | 0 | 0 | 103 | 47 | 0 | 524 |
| 8:45 AM | 18 | 0 | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 228 | 30 | 0 | 0 | 78 | 57 | 0 | 469 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 198 | 0 | 468 | 0 | 0 | 0 | 0 | 0 | 0 | 1859 | 249 | 0 | 0 | 1040 | 814 |  | 4628 |
| APPROACH \%'s : | 29.73\% | 0.00\% | 70.27\% | 0.00\% |  |  |  |  | 0.00\% | 88.19\% | 11.81\% | 0.00\% | 0.00\% | 56.09\% | 43.91\% | 0.00\% |  |
| PEAK HR : | 07:30 AM - 08:30 AM |  |  |  | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{aligned} & 1033 \\ & 0.956 \end{aligned}$ | $\begin{gathered} 124 \\ 0.816 \\ 9 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{aligned} & 593 \\ & 0.810 \end{aligned}$$0.780$ | $\begin{gathered} 502 \\ 0.661 \\ 0 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | TOTAL |
| PEAK HR VOL : | 102 | 0 | 271 | 0 |  |  |  |  |  |  |  |  |  |  |  |  | 2625 |
| PEAK HR FACTOR : | 0.750 | 0.000 | 0.836 | 0.000 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.904 |


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 0 | 0 | 0 | $\begin{gathered} 0 \\ \text { SL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{EL} \end{gathered}$ | 0 | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  | NL | NT | NR | NU |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 67 | 0 | 104 | 0 | 0 | 0 | 0 | 0 | 0 | 109 | 23 | 0 | 0 | 155 | 141 | 0 | 599 |
| 4:15 PM | 86 | 0 | 123 | 0 | 0 | 0 | 0 | 0 | 0 | 111 | 18 | 0 | 0 | 135 | 143 | 0 | 616 |
| 4:30 PM | 103 | 0 | 158 | 0 | 0 | 0 | 0 | 0 | 0 | 110 | 19 | 0 | 0 | 194 | 172 | 0 | 756 |
| 4:45 PM | 117 | 0 | 132 | 0 | 0 | 0 | 0 | 0 | 0 | 159 | 14 | 0 | 0 | 187 | 101 | 0 | 710 |
| 5:00 PM | 149 | 0 | 166 | 0 | 0 | 0 | 0 | 0 | 0 | 156 | 18 | 0 | 0 | 185 | 163 | 0 | 837 |
| 5:15 PM | 134 | 0 | 134 | 0 | 0 | 0 | 0 | 0 | 0 | 172 | 7 | 0 | 0 | 153 | 106 | 0 | 706 |
| 5:30 PM | 145 | 0 | 158 | 0 | 0 | 0 | 0 | 0 | 0 | 168 | 11 | 0 | 0 | 144 | 97 | 0 | 723 |
| 5:45 PM | 141 | 0 | 175 | 0 | 0 | 0 | 0 | 0 | 0 | 155 | 22 | 0 | 0 | 125 | 75 | 0 | 693 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 942 | 0 | 1150 | 0 | 0 | 0 | 0 | 0 | 0 | 1140 | 132 | 0 | 0 | 1278 | 998 | 0 | 5640 |
| APPROACH \%'s : | 45.03\% | 0.00\% | 54.97\% | 0.00\% |  |  |  |  | 0.00\% | 89.62\% | 10.38\% | 0.00\% | 0.00\% | 56.15\% | 43.85\% | 0.00\% |  |
| PEAK HR : |  | 4:30 PM | 5:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 503 | 0 | 590 | 0 | 0 | 0 | 0 | 0 | 0 | 597 | 58 | 0 | 0 | 719 | 542 | 0 | 3009 |
| PEAK HR FACTOR : | 0.844 | 0.000 | 0.889 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.868 | 0.763 | 0.000 | 0.000 | 0.927 | 0.788 | 0.000 |  |
|  | 0.867 |  |  |  |  |  |  |  | 0.915 |  |  |  | 0.861 |  |  |  | 0.899 |

## National Data \& Surveying Services

Location: cranar L naw we camino avelntersection Turning Movement Count
Project ID: 17-07949-004
Controi: Total


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0NL |  | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \\ \hline \end{gathered}$ | $\begin{aligned} & 0 \\ & \mathrm{SL} \end{aligned}$ |  | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | O | 0 | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | $\begin{gathered} 0 \\ E U \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 42 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 162 | 49 | 0 | 25 | 239 | 0 | 0 | 542 |
| 4:15 PM | 38 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 165 | 63 | 0 | 32 | 216 | 0 | 0 | 530 |
| 4:30 PM | 60 | 0 | 30 | 0 | 1 | 0 | 1 | 0 | 1 | 190 | 78 | 0 | 32 | 276 | 1 | 0 | 670 |
| 4:45 PM | 46 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 216 | 71 | 0 | 24 | 231 | 0 | 0 | 616 |
| 5:00 PM | 65 | 0 | 21 | 0 | 1 | 0 | 0 | 0 | 1 | 236 | 71 | 0 | 25 | 273 | 0 | 0 | 693 |
| 5:15 PM | 55 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 232 | 63 | 0 | 32 | 229 | 0 | 0 | 630 |
| 5:30 PM | 60 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 242 | 75 | 0 | 30 | 189 | 0 | 0 | 630 |
| 5:45 PM | 49 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 253 | 69 | 0 | 38 | 182 | 0 | 0 | 619 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 415 | 0 | 201 | 0 | 2 | 0 | 1 | 0 | 2 | 1696 | 539 | 0 | 238 | 1835 | 1 | 0 | 4930 |
| APPROACH \%'s : | 67.37\% | 0.00\% | 32.63\% | 0.00\% | 66.67\% | 0.00\% | 33.33\% | 0.00\% | 0.09\% | 75.82\% | 24.09\% | 0.00\% | 11.48\% | 88.48\% | 0.05\% | 0.00\% |  |
| PEAK HR : |  | 4:30 PM - | 5:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 226 | 0 | 98 | 0 | 2 | 0 | 1 | 0 | 2 | 874 | 283 | 0 | 113 | 1009 | 1 | 0 | 2609 |
| PEAK HR FACTOR : | 0.869 | 0.000 | 0.817 | 0.000 | 0.500 | 0.000 | 0.250 | 0.000 | 0.500 | 0.926 | 0.907 | 0.000 | 0.883 | 0.914 | 0.250 | 0.000 |  |
|  |  | 0.9 |  |  |  | 0.3 |  |  |  | 0.9 |  |  |  | 0.9 |  |  | 0.941 |

## National Data \& Surveying Services

Location: Wever oraw micanion avelntersection Turning Movement Count
Project ID: 17-07949-005 Control: Total


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0NL |  | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{SL} \\ \hline \end{gathered}$ |  | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | 0ET | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | $\begin{gathered} 0 \\ E U \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 162 | 13 | 0 | 20 | 276 | 0 | , | 478 |
| 4:15 PM | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 190 | 6 | 0 | 25 | 259 | 0 | 2 | 488 |
| 4:30 PM | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 213 | 5 | 0 | 21 | 335 | 0 | 1 | 582 |
| 4:45 PM | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 228 | 7 | 0 | 10 | 242 | 0 | 0 | 492 |
| 5:00 PM | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 269 | 9 | 0 | 16 | 310 | 0 | 2 | 613 |
| 5:15 PM | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 264 | 6 | 0 | 12 | 208 | 0 | 0 | 503 |
| 5:30 PM | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 252 | 8 | 0 | 24 | 236 | 0 | 0 | 526 |
| 5:45 PM | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 283 | 9 | 0 | 9 | 175 | 0 | 2 | 491 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 1861 | 63 | 0 | 137 | 2041 | 0 | 8 | 4173 |
| APPROACH \%'s : | 0.00\% | 0.00\% | 100.00\% | 0.00\% |  |  |  |  | 0.00\% | 96.73\% | 3.27\% | 0.00\% | 6.27\% | 93.37\% | 0.00\% | 0.37\% |  |
| PEAK HR : |  | 4:30 PM | 05:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 974 | 27 | 0 | 59 | 1095 | 0 | 3 | 2190 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.615 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.905 | 0.750 | 0.000 | 0.702 | 0.817 | 0.000 | 0.375 |  |
|  |  | 0.6 |  |  |  |  |  |  |  | 0.9 |  |  |  | 0.8 |  |  | 0.893 |

## National Data \& Surveying Services

Location: Unty panksta we canino alntersection Turning Movement Count
Project ID: 17-07949-006
Date: 11/16/2017

| NS/EW Streets: | Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unity Park St |  |  |  | Unity Park St |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | $\begin{gathered} 0 \\ \mathrm{NL} \end{gathered}$ | 0NT | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \end{gathered}$ | 0SL | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ET } \end{gathered}$ | 0 | 0 | 0 | 0WT | 0WR | 0WU | TOTAL |
|  |  |  |  |  |  |  |  |  |  |  | ER | EU | WL |  |  |  |  |
| 7:00 AM | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 176 | 1 | 0 | 0 | 133 | 0 | 0 | 317 |
| 7:15 AM | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 228 | 1 | 0 | 0 | 211 | 0 | 0 | 446 |
| 7:30 AM | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 286 | 0 | 0 | 0 | 275 | 0 | 0 | 566 |
| 7:45 AM | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 394 | 2 | 0 | 0 | 223 | 0 | 0 | 628 |
| 8:00 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 359 | 2 | 0 | 0 | 150 | 0 | 0 | 513 |
| 8:15 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 340 | 0 | 0 | 0 | 126 | 0 | 0 | 467 |
| 8:30 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 339 | 0 | 0 | 0 | 113 | 0 | 0 | 454 |
| 8:45 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 303 | 1 | 0 | 0 | 89 | 0 | 0 | 395 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 2425 | 7 | 0 | 0 | 1320 | 0 | 0 | 3786 |
| APPROACH \%'s : | 0.00\% | 0.00\% | 100.00\% | 0.00\% |  |  |  |  | 0.00\% | 99.71\% | 0.29\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% |  |
| PEAK HR : |  | 7:30 AM | 08:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 1379 | 4 | 0 | 0 | 774 | 0 | 0 | 2174 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.472 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.875 | 0.500 | 0.000 | 0.000 | 0.704 | 0.000 | 0.000 |  |
|  |  | 0.4 |  |  |  |  |  |  |  | 0.8 |  |  |  | 0.7 |  |  | 0.865 |


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0NL | $\begin{gathered} 0 \\ \text { NT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \\ \hline \end{gathered}$ | O | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | 0 | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 165 | 0 | 0 | 0 | 276 | 0 | 0 | 445 |
| 4:15 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 214 | 2 | 0 | 0 | 260 | 0 | 0 | 477 |
| 4:30 PM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 208 | 0 | 0 | 0 | 356 | 0 | 0 | 567 |
| 4:45 PM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 232 | 3 | 0 | 0 | 254 | 0 | 0 | 492 |
| 5:00 PM | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 273 | 3 | 0 | 0 | 343 | 0 | 0 | 623 |
| 5:15 PM | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 289 | 4 | 0 | 0 | 243 | 0 | 0 | 540 |
| 5:30 PM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 273 | 1 | 0 | 0 | 248 | 0 | 0 | 524 |
| 5:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 281 | 1 | 0 | 0 | 178 | 0 | 0 | 461 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 1935 | 14 | 0 | 0 | 2158 | 0 | 0 | 4129 |
| APPROACH \%'s : | 0.00\% | 0.00\% | 100.00\% | 0.00\% |  |  |  |  | 0.00\% | 99.28\% | 0.72\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% |  |
| PEAK HR : |  | 4:30 PM | 05:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 1002 | 10 | 0 | 0 | 1196 | 0 | 0 | 2222 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.875 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.867 | 0.625 | 0.000 | 0.000 | 0.840 | 0.000 | 0.000 |  |
|  |  |  |  |  |  |  |  |  |  | 0.8 |  |  |  | 0.8 |  |  | 0.892 |

## National Data \& Surveying Services


City: Sacramento Project ID: 17-07949-007
Date: $11 / 16 / 2017$

| Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NS/EW Streets: | Gateway Oaks Dr |  |  |  | Gateway Oaks Dr |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 42 | 6 | 22 | 1 | 30 | 3 | 9 | 0 | 24 | 92 | 51 | 2 | 26 | 84 | 53 | 12 | 457 |
| 7:15 AM | 49 | 8 | 32 | 1 | 28 | 2 | 10 | 0 | 29 | 95 | 69 | 2 | 36 | 133 | 76 | 13 | 583 |
| 7:30 AM | 67 | 26 | 32 | 2 | 31 | 7 | 8 | 0 | 45 | 136 | 92 | 5 | 47 | 191 | 95 | 21 | 805 |
| 7:45 AM | 34 | 26 | 38 | 1 | 40 | 8 | 4 | 0 | 69 | 183 | 101 | 8 | 63 | 143 | 155 | 16 | 889 |
| 8:00 AM | 43 | 27 | 31 | 0 | 35 | 9 | 9 | 0 | 72 | 141 | 109 | 4 | 71 | 80 | 168 | 14 | 813 |
| 8:15 AM | 39 | 38 | 26 | 0 | 24 | 10 | 8 | 0 | 70 | 119 | 98 | 6 | 60 | 57 | 156 | 18 | 729 |
| 8:30 AM | 17 | 17 | 22 | 0 | 42 | 8 | 10 | 0 | 64 | 128 | 120 | 2 | 45 | 76 | 121 | 14 | 686 |
| 8:45 AM | 33 | 24 | 21 | 1 | 32 | 9 | 7 | 0 | 69 | 86 | 94 | 1 | 58 | 47 | 101 | 17 | 600 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 324 | 172 | 224 | 6 | 262 | 56 | 65 | 0 | 442 | 980 | 734 | 30 | 406 | 811 | 925 | 125 | 5562 |
| APPROACH \%'s : | 44.63\% | 23.69\% | 30.85\% | 0.83\% | 68.41\% | 14.62\% | 16.97\% | 0.00\% | 20.22\% | 44.83\% | 33.58\% | 1.37\% | 17.91\% | 35.77\% | 40.80\% | 5.51\% |  |
| PEAK HR : | 07:30 AM - 08:30 AM |  |  |  | $\begin{aligned} & 130 \\ & 0.813 \end{aligned}$ | 34 | $\begin{gathered} 29 \\ 0.806 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{aligned} & 256 \\ & 0.889 \end{aligned}$ | $\begin{aligned} & 579 \\ & 0.791 \\ & \quad 0.87 \\ & \hline \end{aligned}$ | $\begin{aligned} & 400 \\ & 0.917 \\ & 1 \end{aligned}$ | $\begin{gathered} 23 \\ 0.719 \end{gathered}$ | $\begin{aligned} & 241 \\ & 0.849 \end{aligned}$ | $\begin{aligned} & 471 \\ & 0.616 \\ & \quad 0.89 \\ & \hline \end{aligned}$ | 5740.854 | $\begin{gathered} 69 \\ 0.821 \end{gathered}$ | TOTAL |
| PEAK HR VOL : | 183 | 117 | 127 | 3 |  |  |  |  |  |  |  |  |  |  |  |  | 3236 |
| PEAK HR FACTOR : | 0.683 | 0.770 | 0.836 | 0.375 |  | 0.850 |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.846 |  |  |  | 0.910 |  |  |  |  |  |  |  |  |  |  | 0.910 |


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0NL | $\begin{gathered} 0 \\ \text { NT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { NR } \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \end{gathered}$ | $\begin{gathered} 0 \\ \text { SL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | 0 | $\begin{gathered} 0 \\ \text { ER } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 73 | 7 | 72 | 1 | 124 | 33 | 65 | 0 | 15 | 116 | 31 | 6 | 32 | 99 | 24 | 17 | 715 |
| 4:15 PM | 71 | 8 | 56 | 3 | 100 | 11 | 68 | 1 | 6 | 135 | 35 | 2 | 51 | 102 | 26 | 12 | 687 |
| 4:30 PM | 104 | 13 | 103 | 0 | 108 | 37 | 92 | 0 | 10 | 161 | 33 | 5 | 41 | 103 | 17 | 24 | 851 |
| 4:45 PM | 69 | 12 | 73 | 0 | 123 | 22 | 52 | 0 | 11 | 175 | 51 | 6 | 45 | 97 | 29 | 12 | 777 |
| 5:00 PM | 114 | 16 | 109 | 2 | 131 | 33 | 75 | 0 | 12 | 201 | 54 | 4 | 32 | 111 | 30 | 12 | 936 |
| 5:15 PM | 74 | 19 | 86 | 1 | 88 | 25 | 41 | 0 | 15 | 182 | 62 | 3 | 39 | 93 | 26 | 7 | 761 |
| 5:30 PM | 75 | 13 | 50 | 1 | 86 | 11 | 51 | 0 | 9 | 181 | 65 | 4 | 33 | 106 | 26 | 25 | 736 |
| 5:45 PM | 64 | 8 | 38 | 2 | 38 | 9 | 23 | 0 | 14 | 176 | 67 | 8 | 47 | 95 | 33 | 16 | 638 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 644 | 96 | 587 | 10 | 798 | 181 | 467 | 1 | 92 | 1327 | 398 | 38 | 320 | 806 | 211 | 125 | 6101 |
| APPROACH \%'s : | 48.17\% | 7.18\% | 43.90\% | 0.75\% | 55.15\% | 12.51\% | 32.27\% | 0.07\% | 4.96\% | 71.54\% | 21.46\% | 2.05\% | 21.89\% | 55.13\% | 14.43\% | 8.55\% |  |
| PEAK HR : |  | 4:30 PM | 5:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 361 | 60 | 371 | 3 | 450 | 117 | 260 | 0 | 48 | 719 | 200 | 18 | 157 | 404 | 102 | 55 | 3325 |
| PEAK HR FACTOR : | 0.792 | 0.789 | 0.851 | 0.375 | 0.859 | 0.791 | 0.707 | 0.000 | 0.800 | 0.894 | 0.806 | 0.750 | 0.872 | 0.910 | 0.850 | 0.573 |  |
|  | 0.825 |  |  |  | 0.865 |  |  |  | $0.909{ }^{0.800}$ |  |  |  | $0.970{ }^{0.870}$ |  |  |  | 0.888 |

## 2020 TRAFFIC COUNTS

Intersection Turning Movement Count

Location: I-80 WB On/Off-Ramps \& W El Camino Ave City: Sacramento

Project ID: 20-07035-00
Control: Sianalized

| NS/ EW Streets: | Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | I-80 WB On/Off-Ramps |  |  |  | 1-80 WB On/Off-Ramps |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | ${ }_{0}^{0}$ |  | $\begin{gathered} 0 \\ N R \end{gathered}$ | $\begin{gathered} 0 \\ \text { NU } \end{gathered}$ | $\begin{gathered} 1 \\ \mathrm{SL} \end{gathered}$ | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 1WR | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ | TOTAL |
|  |  |  |  |  |  |  | SR | SU | EL | ET | ER | EU | WL | WT |  |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 161 | 0 | 28 | 0 | 0 | 85 | 157 | 0 | 0 | 63 | 111 | 0 | 605 |
| 7:15 AM | 0 | 0 | 0 | 0 | 191 | 0 | 19 | 0 | 0 | 99 | 150 | 0 | 0 | 57 | 98 | 0 | 614 |
| 7:30 AM | 0 | 0 | 0 | 0 | 177 | 0 | 24 | 0 | 0 | 144 | 118 | 0 | 0 | 73 | 99 | 0 | 635 |
| 7:45 AM | 0 | 0 | 0 | 0 | 181 | 0 | 25 | 0 | 0 | 121 | 134 | 0 | 0 | 81 | 120 | 0 | 662 |
| 8:00 AM | 0 | 0 | 0 | 0 | 156 | 0 | 25 | 0 | 0 | 142 | 127 | 0 | 0 | 47 | 85 | 0 | 582 |
| 8:15 AM | 0 | 0 | 0 | 0 | 214 | 0 | 25 | 0 | 0 | 110 | 111 | 0 | 0 | 61 | 72 | 0 | 593 |
| 8:30 AM | 0 | 0 | 0 | 0 | 182 | 0 | 28 | 0 | 0 | 74 | 139 | 0 | 0 | 47 | 73 | 0 | 543 |
| 8:45 AM | 0 | 0 | 0 | 0 | 121 | 0 | 39 | 0 | 0 | 90 | 78 | 0 | 0 | 50 | 76 | 0 | 454 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 1383 | 0 | 213 | 0 | 0 | 865 | 1014 | 0 | 0 | 479 | 734 | 0 | 4688 |
| APPROACH \% 's : |  |  |  |  | 86.65\% | 0.00\% | 13.35\% | 0.00\% | 0.00\% | 46.04\% | 53.96\% | 0.00\% | 0.00\% | 39.49\% | 60.51\% | 0.00\% |  |
| PEAK HR : |  | 7:00 AM | 8:00 A |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 710 | 0 | 96 | 0 | 0 | 449 | 559 | 0 | 0 | 274 | 428 | 0 | 2516 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.929 | 0.000 | 0.857 | 0.000 | 0.000 | 0.780 | 0.890 | 0.000 | 0.000 | 0.846 | 0.892 | 0.000 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.950 |


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0$N L$ | $\begin{gathered} 0 \\ \text { NT } \end{gathered}$ | $\begin{gathered} 0 \\ \text { NR } \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ \mathrm{NU} \\ \hline \end{gathered}$ | $\begin{gathered} 1 \\ \mathrm{SL} \\ \hline \end{gathered}$ | ST | $\begin{gathered} 1 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | 1ET |  | $\begin{gathered} 0 \\ \text { EU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 1 \\ W T \end{gathered}$ | 1 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | WR | WU |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 72 | 0 | 30 | 0 | 0 | 55 | 43 | 0 | 0 | 173 | 96 | 0 | 469 |
| 4:15 PM | 0 | 0 | 0 | 0 | 69 | 0 | 33 | 0 | 0 | 43 | 50 | 0 | 0 | 221 | 87 | 0 | 503 |
| 4:30 PM | 0 | 0 | 0 | 0 | 87 | 0 | 43 | 0 | 0 | 64 | 42 | 0 | 0 | 221 | 125 | 0 | 582 |
| 4:45 PM | 0 | 0 | 0 | 0 | 76 | 0 | 36 | 0 | 0 | 53 | 52 | 0 | 0 | 234 | 83 | 0 | 534 |
| 5:00 PM | 0 | 0 | 0 | 0 | 72 | 0 | 31 | 0 | 0 | 51 | 45 | 0 | 0 | 219 | 97 | 0 | 515 |
| 5:15 PM | 0 | 0 | 0 | 0 | 86 | 0 | 42 | 0 | 0 | 64 | 35 | 0 | 0 | 231 | 103 | 0 | 561 |
| 5:30 PM | 0 | 0 | 0 | 0 | 96 | 0 | 31 | 0 | 0 | 64 | 39 | 0 | 0 | 221 | 88 | 0 | 539 |
| 5:45 PM | 0 | 0 | 0 | 0 | 75 | 0 | 39 | 0 | 0 | 55 | 35 | 0 | 0 | 194 | 57 | 0 | 455 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 633 | 0 | 285 | 0 | 0 | 449 | 341 | 0 | 0 | 1714 | 736 |  | 4158 |
| APPROACH \% 's : |  |  |  |  | 68.95\% | 0.00\% | 31.05\% | 0.00\% | 0.00\% | 56.84\% | 43.16\% | 0.00\% | 0.00\% | 69.96\% | 30.04\% | 0.00\% |  |
| PEAK HR : |  | 4:30 PM | 5:30 P |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 321 | 0 | 152 | 0 | 0 | 232 | 174 | 0 | 0 | 905 | 408 |  | 2192 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.922 | 0.000 | 0.884 | 0.000 | 0.000 | 0.906 | 0.837 | 0.000 | 0.000 | 0.967 | 0.816 | 0.000 |  |
|  |  |  |  |  | 0.910 |  |  |  | 0.958 |  |  |  |  | 0.949 |  |  | 0.942 |

## National Data \& Surveying Services <br> Intersection Turning Movement Count



## National Data \& Surveying Services <br> Intersection Turning Movement Count

| Location: I-80 WB On/Off-Ramps \& W El Camino Ave <br> City: Sacramento <br> Control: Signalized |  |  |  |  |  |  |  |  |  |  |  |  |  | iect ID: Date: | $\begin{aligned} & 0-07035-1 \\ & / 6 / 2020 \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | HT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NS/ EW Streets: | I-80 WB On/Off-Ramps |  |  |  | I-80 WB On/Off-Ramps |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | 0$N L$ | $\begin{gathered} 0 \\ \text { NT } \\ \hline \end{gathered}$ | 0 | $\begin{gathered} 0 \\ \mathrm{NU} \end{gathered}$ | $\begin{gathered} 1 \\ \text { SL } \end{gathered}$ | $\begin{gathered} 0 \\ \text { ST } \end{gathered}$ | $\begin{gathered} 1 \\ 1 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ E L \end{gathered}$ | 1ET | 1 | 0EU | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | 1WT | WR | WU | TOTAL |
|  |  |  | NR |  |  |  |  |  |  |  | ER |  |  |  |  |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 7 | 6 | 0 | 0 | 3 | 1 | 0 | 20 |
| 7:15 AM | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 6 | 4 | 0 | 0 | 3 | 1 | 0 | 17 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 2 | 0 | 0 | 9 | 2 | 0 | 22 |
| 7:45 AM | 0 | 0 | 0 | 0 | 2 | 0 | 8 | 0 | 0 | 6 | 6 | 0 | 0 | 7 | 0 | 0 | 29 |
| 8:00 AM | 0 | 0 | 0 | 0 | 3 | 0 | 6 | 0 | 0 | 10 | 9 | 0 | 0 | 4 | 1 | 0 | 33 |
| 8:15 AM | 0 | 0 | 0 | 0 | 1 | 0 | 12 | 0 | 0 | 9 | 7 | 0 | 0 | 1 | 1 | 0 | 31 |
| 8:30 AM | 0 | 0 | 0 | 0 | 3 | 0 | 6 | 0 | 0 | 5 | 10 | 0 | 0 | 2 | 0 | 0 | 26 |
| 8:45 AM | 0 | 0 | 0 | 0 | 2 | 0 | 16 | 0 | 0 | 5 | 4 | 0 | 0 | 3 | 1 | 0 | 31 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 13 | 0 | 52 | 0 | 0 | 57 | 48 | 0 | 0 | 32 | 7 | 0 | 209 |
| APPROACH \% 's : |  |  |  |  | 20.00\% | 0.00\% | 80.00\% | 0.00\% | 0.00\% | 54.29\% | 45.71\% | 0.00\% | 0.00\% | 82.05\% | 17.95\% | 0.00\% |  |
| PEAK HR : |  | 7:00 AM | 8:00 A |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 4 | 0 | 12 | 0 | 0 | 28 | 18 | 0 | 0 | 22 | 4 | 0 | 88 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.500 | 0.000 | 0.375 | 0.000 | 0.000 | 0.778 | 0.750 | 0.000 | 0.000 | 0.611 | 0.500 | 0.000 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.759 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | NOR | OUND |  |  | SOUTH | OUND |  |  | EAST | UND |  |  | WEST | UND |  |  |
| PM | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 0 | 0 | 0 | 0 | 1 | 0 | 11 | 0 | 0 | 3 | 3 | 0 | 0 | 3 | 3 | 0 | 24 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 3 | 5 | 0 | 0 | 7 | 1 | 0 | 21 |
| 4:30 PM | 0 | 0 | 0 | 0 | 1 | 0 | 13 | 0 | 0 | 6 | 4 | 0 | 0 | 8 | 0 | 0 | 32 |
| 4:45 PM | 0 | 0 | 0 | 0 | 1 | 0 | 9 | 0 | 0 | 7 | 1 | 0 | 0 | 10 | 0 | 0 | 28 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 11 | 6 | 0 | 0 | 6 | 0 | 0 | 28 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 9 | 0 | 0 | 0 | 2 | 1 | 0 | 22 |
| 5:30 PM | 0 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 0 | 6 | 4 | 0 | 0 | 2 | 0 | 0 | 17 |
| 5:45 PM | 0 | 0 | 0 | 0 | 1 | 0 | 9 | 0 | 0 | 6 | 1 | 0 | 0 | 7 | 1 | 0 | 25 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 5 | 0 | 66 | 0 | 0 | 51 | 24 | 0 | 0 | 45 | 6 | 0 | 197 |
| APPROACH \% 's : |  |  |  |  | 7.04\% | 0.00\% | 92.96\% | 0.00\% | 0.00\% | 68.00\% | 32.00\% | 0.00\% | 0.00\% | 88.24\% | 11.76\% | 0.00\% |  |
| PEAK HR : |  | $4: 30 \mathrm{PM}$ | 5:30 P |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 2 | 0 | 37 | 0 | 0 | 33 | 11 | 0 | 0 | 26 | 1 | 0 | 110 |
| PEAK HR FACTOR : | 0.00 | 0.000 | 0.000 | 0.000 | 0.500 | 0.000 | 0.712 | 0.000 | 0.000 | 0.750 | 0.458 | 0.000 | 0.000 | 0.650 | 0.250 | 0.000 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.859 |

## National Data \& Surveying Services <br> Intersection Turning Movement Count



National Data \& Surveying Services

## Intersection Turning Movement Count <br> Location: I-80 WB On/Off-Ramps \& W El Camino Ave <br> Project ID: 20-07035-001

 City: SacramentoDate: 2/6/2020
Pedestrians (Crosswalks)

| NS/ EW Streets: | I-80 WB | ff-Ramps | I-80 WB On/Off-Ramps |  | W El Camino Ave |  | W El Camino Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  |  |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 7:00 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:15 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : APPROACH \% 's : | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
|  | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
|  | 33.33\% | 66.67\% |  |  |  |  |  |  |  |
| PEAK HR : | 07:00 AM | 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | TOTAL |
| PEAK HR VOL: PEAK HR FACTOR : | 0 | 2 |  |  |  |  |  |  | 2 |
|  |  | 0.500 |  |  |  |  |  |  | 0.500 |


| PM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | EB | WB | NB | SB | NB | SB |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 3 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 4 |
| APPROACH \% 's : | 33.33\% | 66.67\% |  |  |  |  | 0.00\% | 100.00\% |  |
| PEAK HR : | 04:30 P | 5:30 PM |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 3 |
| PEAK HR FACTOR : | 0.250 | 0.250 |  |  |  |  |  | 0.250 | 0.250 |
|  |  |  |  |  |  |  |  |  | 0.250 |

I-80 WB On/Off-Ramps \& W El Camino Ave


Start Time $7: 00 \mathrm{AM}$
Site Code:




# ALL TRAFFIC DATA 

(916) 771-8700
orders@atdtraffic.com
File Name: 20-07035-001
Date : 02/06/2020

|  | 1-80 WB On/Off-RampsSouthbound |  |  |  |  | W El Camino Ave Westbound |  |  |  |  | I-80 WB On/Off-Ramps Northbound |  |  |  |  | W El Camino AveEastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT ${ }^{\text {\| }}$ | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total | Uturns Total |
| 7:00 | 161 | 0 | 28 | 0 | 189 | 0 | 63 | 111 | 0 | 174 | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 157 | 0 | 242 | 605 | 0 |
| 7:15 | 191 | 0 | 19 | 0 | 210 | 0 | 57 | 98 | 0 | 155 | 0 | 0 | 0 | 0 | 0 | 0 | 99 | 150 | 0 | 249 | 614 | 0 |
| 7:30 | 177 | 0 | 24 | 0 | 201 | 0 | 73 | 99 | 0 | 172 | 0 | 0 | 0 | 0 | 0 | 0 | 144 | 118 | 0 | 262 | 635 | 0 |
| 7:45 | 181 | 0 | 25 | 0 | 206 | 0 | 81 | 120 | 0 | 201 | 0 | 0 | 0 | 0 | 0 | 0 | 121 | 134 | 0 | 255 | 662 | 0 |
| Total | 710 | 0 | 96 | 0 | 806 | 0 | 274 | 428 | 0 | 702 | 0 | 0 | 0 | 0 | 0 | 0 | 449 | 559 | 0 | 1008 | 2516 | 0 |
| 8:00 | 156 | 0 | 25 | 0 | 181 | 0 | 47 | 85 | 0 | 132 | 0 | 0 | 0 | 0 | 0 | 0 | 142 | 127 | 0 | 269 | 582 | 0 |
| 8:15 | 214 | 0 | 25 | 0 | 239 | 0 | 61 | 72 | 0 | 133 | 0 | 0 | 0 | 0 | 0 | 0 | 110 | 111 | 0 | 221 | 593 | 0 |
| 8:30 | 182 | 0 | 28 | 0 | 210 | 0 | 47 | 73 | 0 | 120 | 0 | 0 | 0 | 0 | 0 | 0 | 74 | 139 | 0 | 213 | 543 | 0 |
| 8:45 | 121 | 0 | 39 | 0 | 160 | 0 | 50 | 76 | 0 | 126 | 0 | 0 | 0 | 0 | 0 | 0 | 90 | 78 | 0 | 168 | 454 | 0 |
| Total | 673 | 0 | 117 | 0 | 790 | 0 | 205 | 306 | 0 | 511 | 0 | 0 | 0 | 0 | 0 | 0 | 416 | 455 | 0 | 871 | 2172 | 0 |
| 16:00 | 72 | 0 | 30 | 0 | 102 | 0 | 173 | 96 | 0 | 269 | 0 | 0 | 0 | 0 | 0 | 0 | 55 | 43 | 0 | 98 | 469 | 0 |
| 16:15 | 69 | 0 | 33 | 0 | 102 | 0 | 221 | 87 | 0 | 308 | 0 | 0 | 0 | 0 | 0 | 0 | 43 | 50 | 0 | 93 | 503 | 0 |
| 16:30 | 87 | 0 | 43 | 0 | 130 | 0 | 221 | 125 | 0 | 346 | 0 | 0 | 0 | 0 | 0 | 0 | 64 | 42 | 0 | 106 | 582 | 0 |
| 16:45 | 76 | 0 | 36 | 0 | 112 | 0 | 234 | 83 | 0 | 317 | 0 | 0 | 0 | 0 | 0 | 0 | 53 | 52 | 0 | 105 | 534 | 0 |
| Total | 304 | 0 | 142 | 0 | 446 | 0 | 849 | 391 | 0 | 1240 | 0 | 0 | 0 | 0 | 0 | 0 | 215 | 187 | 0 | 402 | 2088 | 0 |
| 17:00 | 72 | 0 | 31 | 0 | 103 | 0 | 219 | 97 | 0 | 316 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 45 | 0 | 96 | 515 | 0 |
| 17:15 | 86 | 0 | 42 | 0 | 128 | 0 | 231 | 103 | 0 | 334 | 0 | 0 | 0 | 0 | 0 | 0 | 64 | 35 | 0 | 99 | 561 | 0 |
| 17:30 | 96 | 0 | 31 | 0 | 127 | 0 | 221 | 88 | 0 | 309 | 0 | 0 | 0 | 0 | 0 | 0 | 64 | 39 | 0 | 103 | 539 | 0 |
| 17:45 | 75 | 0 | 39 | 0 | 114 | 0 | 194 | 57 | 0 | 251 | 0 | 0 | 0 | 0 | 0 | 0 | 55 | 35 | 0 | 90 | 455 | 0 |
| Total | 329 | 0 | 143 | 0 | 472 | 0 | 865 | 345 | 0 | 1210 | 0 | 0 | 0 | 0 | 0 | 0 | 234 | 154 | 0 | 388 | 2070 | 0 |
| Grand Total | 2016 | 0 | 498 | 0 | 2514 | 0 | 2193 | 1470 | 0 | 3663 | 0 | 0 | 0 | 0 | 0 | 0 | 1314 | 1355 | 0 | 2669 | 8846 | 0 |
| Apprch \% | 80.2\% | 0.0\% | 19.8\% | 0.0\% |  | 0.0\% | 59.9\% | 40.1\% | 0.0\% |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  | 0.0\% | 49.2\% | 50.8\% | 0.0\% |  |  |  |
| Total \% | 22.8\% | 0.0\% | 5.6\% | 0.0\% | 28.4\% | 0.0\% | 24.8\% | 16.6\% | 0.0\% | 41.4\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 14.9\% | 15.3\% | 0.0\% | 30.2\% | 100.0\% |  |
| $\begin{array}{\|c\|} \hline \text { AM PEAK } \\ \text { HOUR } \\ \hline \end{array}$ |  |  | $\begin{aligned} & -80 \text { WB On } \\ & \text { South } \end{aligned}$ | ff-Ramps und |  |  |  | $\begin{array}{r} \hline \text { W EI Cam } \\ \text { Westb } \end{array}$ | no Ave und |  |  |  | $\begin{array}{r} 80 \text { WB On } \\ \text { Northk } \end{array}$ | ff-Ramps und |  |  |  | $\begin{gathered} \hline \text { W EI Car } \\ \text { Easth } \\ \hline \end{gathered}$ | no Ave und |  |  |  |
| START TIME | LEFT | THRU | RIGHT ${ }^{\text {\| }}$ | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 07:00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 | 161 | 0 | 28 | 0 | 189 | 0 | 63 | 111 | 0 | 174 | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 157 | 0 | 242 | 605 |  |
| 7:15 | 191 | 0 | 19 | 0 | 210 | 0 | 57 | 98 | 0 | 155 | 0 | 0 | 0 | 0 | 0 | 0 | 99 | 150 | 0 | 249 | 614 |  |
| 7:30 | 177 | 0 | 24 | 0 | 201 | 0 | 73 | 99 | 0 | 172 | 0 | 0 | 0 | 0 | 0 | 0 | 144 | 118 | 0 | 262 | 635 |  |
| 7:45 | 181 | 0 | 25 | 0 | 206 | 0 | 81 | 120 | 0 | 201 | 0 | 0 | 0 | 0 | 0 | 0 | 121 | 134 | 0 | 255 | 662 |  |
| Total Volume | 710 | 0 | 96 | 0 | 806 | 0 | 274 | 428 | 0 | 702 | 0 | 0 | 0 | 0 | 0 | 0 | 449 | 559 | 0 | 1008 | 2516 |  |
| \% App Total | 88.1\% | 0.0\% | 11.9\% | 0.0\% |  | 0.0\% | 39.0\% | 61.0\% | 0.0\% |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  | 0.0\% | 44.5\% | 55.5\% | 0.0\% |  |  |  |
| PHF\| | . 929 | . 000 | . 857 | . 000 | . 960 | . 000 | . 846 | . 892 | . 000 | . 873 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 780 | . 890 | . 000 | . 962 | . 950 |  |
| $\begin{array}{\|c\|} \hline \text { PM PEAK } \\ \text { HOUR } \\ \hline \end{array}$ | 1-80 WB On/Off-RampsSouthbound |  |  |  |  | W El Camino AveWestbound |  |  |  |  | 1-80 WB On/Off-RampsNorthbound |  |  |  |  | $\begin{gathered} \hline \text { W El Camino Ave } \\ \text { Eastbound } \end{gathered}$ |  |  |  |  |  |  |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |  |
| Peak Hour Analysis From 16:30 to 17:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 16:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:30 | 87 | 0 | 43 | 0 | 130 | 0 | 221 | 125 | 0 | 346 | 0 | 0 | 0 | 0 | 0 | 0 | 64 | 42 | 0 | 106 | 582 |  |
| 16:45 | 76 | 0 | 36 | 0 | 112 | 0 | 234 | 83 | 0 | 317 | 0 | 0 | 0 | 0 | 0 | 0 | 53 | 52 | 0 | 105 | 534 |  |
| 17:00 | 72 | 0 | 31 | 0 | 103 | 0 | 219 | 97 | 0 | 316 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 45 | 0 | 96 | 515 |  |
| 17:15 | 86 | 0 | 42 | 0 | 128 | 0 | 231 | 103 | 0 | 334 | 0 | 0 | 0 | 0 | 0 | 0 | 64 | 35 | 0 | 99 | 561 |  |
| Total Volume | 321 | 0 | 152 | 0 | 473 | 0 | 905 | 408 | 0 | 1313 | 0 | 0 | 0 | 0 | 0 | 0 | 232 | 174 | 0 | 406 | 2192 |  |
| \% App Total | 67.9\% | 0.0\% | 32.1\% | 0.0\% |  | 0.0\% | 68.9\% | 31.1\% | 0.0\% |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  | 0.0\% | 57.1\% | 42.9\% | 0.0\% |  |  |  |
| PHF\| | . 922 | . 000 | . 884 | . 000 | . 910 | . 000 | . 967 | . 816 | . 000 | . 949 | . 000 | . 000 | . 000 | . 000 | . 000 | . 000 | . 906 | . 837 | . 000 | . 958 | . 942 |  |

## ALL TRAFFIC DATA

(916) 771-8700
orders@atdtraffic.com


## ALL TRAFFIC DATA

orders@atdtraffic.com


Intersection Turning Movement Count

Location: I-80 EB On/Off-Ramps \& W El Camino Ave City: Sacramento

Project ID: 20-07035-002
Control: Siqn

| NS/ EW Streets: | I-80 EB On/Off-Ramps |  |  |  | 1-80 EB On/Off-Ramps |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 33 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 216 | 33 | 0 | 0 | 142 | 90 | 0 | 577 |
| 7:15 AM | 24 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 252 | 35 | 0 | 0 | 130 | 125 | 0 | 632 |
| 7:30 AM | 28 | 0 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 275 | 45 | 0 | 0 | 153 | 172 | 0 | 751 |
| 7:45 AM | 32 | 0 | 114 | 0 | 0 | 0 | 0 | 0 | 0 | 262 | 41 | 0 | 0 | 153 | 210 | 0 | 812 |
| 8:00 AM | 33 | 0 | 114 | 0 | 0 | 0 | 0 | 0 | 0 | 251 | 51 | 0 | 0 | 109 | 95 | 0 | 653 |
| 8:15 AM | 29 | 0 | 83 | 0 | 0 | 0 | 0 | 0 | 0 | 284 | 33 | 0 | 0 | 102 | 65 | 0 | 596 |
| 8:30 AM | 25 | 0 | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 224 | 36 | 0 | 0 | 97 | 62 | 0 | 534 |
| 8:45 AM | 32 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 0 | 181 | 24 | 0 | 0 | 87 | 59 | 0 | 475 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES: | 236 | 0 | 700 | 0 | 0 | 0 | 0 | 0 | 0 | 1945 | 298 | 0 | 0 | 973 | 878 | 0 | 5030 |
| APPROACH \% 's : | 25.21\% | 0.00\% | 74.79\% | 0.00\% |  |  |  |  | 0.00\% | 86.71\% | 13.29\% | 0.00\% | 0.00\% | 52.57\% | 47.43\% | 0.00\% |  |
| PEAK HR : | 07:15 AM - 08:15 AM |  |  |  | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{array}{lc} 1040 & 172 \\ 0.945 & 0.843 \\ & 0.947 \\ \hline \end{array}$ |  | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{aligned} & 545 \\ & 0.891 \end{aligned}$ | ${ }_{90} \begin{aligned} & 602 \\ & 0.717\end{aligned}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | TOTAL |
| PEAK HR VOL : | 117 | 0 | 372 | 0 |  |  |  |  |  |  |  | 2848 |  |  |  |  |
| PEAK HR FACTOR : | 0.886 | 0.000 | 0.816 | 0.000 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  | 0.877 |  |  |  |  |


| PM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | $\begin{gathered} 1 \\ \text { ET } \end{gathered}$ | $\begin{gathered} 1 \\ \text { ER } \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ E U \end{gathered}$ | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | $\begin{gathered} 1 \\ \text { WT } \end{gathered}$ | $\begin{gathered} 1 \\ \text { WR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { WU } \end{gathered}$ |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 104 | 0 | 147 | 0 | 0 | 0 | 0 | O | 0 | 116 | 15 | 0 | 0 | 167 | 134 | 0 | 683 |
| 4:15 PM | 152 | 0 | 173 | 0 | 0 | 0 | 0 | 0 | 0 | 92 | 14 | 0 | 0 | 146 | 93 | 0 | 670 |
| 4:30 PM | 166 | 0 | 167 | 0 | 0 | 0 | 0 | 0 | 0 | 118 | 23 | 0 | 0 | 188 | 144 | 0 | 806 |
| 4:45 PM | 166 | 0 | 167 | 0 | 0 | 0 | 0 | 0 | 0 | 129 | 15 | 0 | 0 | 151 | 105 | 0 | 733 |
| 5:00 PM | 154 | 0 | 195 | 0 | 0 | 0 | 0 | 0 | 0 | 107 | 20 | 0 | 0 | 162 | 137 | 0 | 775 |
| 5:15 PM | 160 | 0 | 159 | 0 | 0 | 0 | 0 | 0 | 0 | 126 | 22 | 0 | 0 | 174 | 105 | 0 | 746 |
| 5:30 PM | 183 | 0 | 184 | 0 | 0 | 0 | 0 | 0 | 0 | 131 | 16 | 0 | 0 | 125 | 97 | 0 | 736 |
| 5:45 PM | 143 | 0 | 167 | 0 | 0 | 0 | 0 | 0 | 0 | 121 | 15 | 0 | 0 | 108 | 60 | 0 | 614 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 1228 | 0 | 1359 | 0 | 0 | 0 | 0 | 0 | 0 | 940 | 140 | 0 | 0 | 1221 | 875 |  | 5763 |
| APPROACH \% 's : | 47.47\% | 0.00\% | 52.53\% | 0.00\% |  |  |  |  | 0.00\% | 87.04\% | 12.96\% | 0.00\% | 0.00\% | 58.25\% | 41.75\% | 0.00\% |  |
| PEAK HR : | 04:30 PM - 05:30 PM |  |  |  | 0 | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{aligned} & 480 \\ & 0.930 \\ & 0 . \end{aligned}$ | $\begin{gathered} 80 \\ 0.870 \\ 6 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | 6750.898 | $\begin{gathered} 491 \\ 8^{0.852} \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ 0.000 \end{gathered}$ | TOTAL |
| PEAK HR VOL : | 646 | 0 | 688 | 0 |  |  |  |  |  |  |  |  |  |  |  |  | 3060 |
| PEAK HR FACTOR : | 0.973 | 0.000 | 0.882 | 0.000 | 0.000 |  |  |  |  |  |  |  |  |  |  |  | 0.949 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.878 |  |  | 0.949 |

## National Data \& Surveying Services <br> Intersection Turning Movement Count



## National Data \& Surveying Services <br> Intersection Turning Movement Count



## National Data \& Surveying Services <br> Intersection Turning Movement Count

| Location: I-80 EB On/Off-Ramps \& W El Camino Ave <br> City: Sacramento <br> Control: Signalized |  |  |  |  |  |  |  |  |  |  |  |  |  | ject ID: Date: | $\begin{aligned} & 0-07035-1 \\ & 16 / 2020 \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Bikes |  |  |  |  |  |  |  |  |  |  |  |  |
| NS/ EW Streets: | 1-80 EB On/Off-Ramps |  |  |  | 1-80 EB On/Off-Ramps |  |  |  | W El Camino Ave |  |  |  | W El Camino Ave |  |  |  |  |
| AM | NORTHBOUND |  |  |  | SOUTHBOUND |  |  |  | EASTBOUND |  |  |  | WESTBOUND |  |  |  |  |
|  | 1$N L$ |  | 1 | $\begin{gathered} 0 \\ \mathrm{NU} \end{gathered}$ | $\begin{gathered} 0 \\ \text { SL } \end{gathered}$ |  | $\begin{gathered} 0 \\ \text { SR } \end{gathered}$ | $\begin{gathered} 0 \\ \text { SU } \end{gathered}$ | $\begin{gathered} 0 \\ \text { EL } \end{gathered}$ | 1ET | 1 | 0 | $\begin{gathered} 0 \\ \text { WL } \end{gathered}$ | 1WT | $\stackrel{1}{W R}$ | WU | TOTAL |
|  |  |  | NR |  |  |  |  |  |  |  | ER | EU |  |  |  |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| APPROACH \% 's : |  |  |  |  |  |  |  |  | 0.00\% | 100.00\% | 0.00\% | 0.00\% |  |  |  |  |  |
| PEAK HR : |  | :15 AM | 08:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | NORT | OUND |  |  | SOUT | OUND |  |  | EAST | UND |  |  | WEST | UND |  |  |
| PM | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 |  |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | wu | TOTAL |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| 5:00 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| APPROACH \% 's : | 0.00\% | 0.00\% | 100.00\% | 0.00\% |  |  |  |  | 0.00\% | 100.00\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 0.00\% |  |
| PEAK HR : |  | :30 PM | 05:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL : | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| PEAK HR FACTOR : | 0.00 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.375 |

National Data \& Surveying Services

## Intersection Turning Movement Count <br> Location: I-80 EB On/Off-Ramps \& W El Camino Ave <br> Project ID: 20-07035-002

 City: SacramentoPedestrians (Crosswalks)

| NS/ EW Streets: | 1-80 EB | Ramps | 1-80 EB On/Off-Ramps |  | W El Camino Ave |  | W El Camino Ave |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  |  |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES: APPROACH \% 's: | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
|  | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
|  |  |  | 100.00\% | 0.00\% |  |  |  |  |  |
| PEAK HR : | 07:15 | 15 AM |  |  |  |  |  |  | TOTAL |
| PEAK HR VOL: PEAK HR FACTOR : | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
|  |  |  | 0.250 |  |  |  |  |  | 0.250 |


| PM | NORTH LEG |  | SOUTH LEG |  | EAST LEG |  | WEST LEG |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | WB | EB | WB | NB | SB | NB | SB |  |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : APPROACH \% 's : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | 04:30 | 30 PM |  |  |  |  |  |  |  |
| PEAK HR VOL : PEAK HR FACTOR : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## I-80 EB On/Off-Ramps \& W El Camino Ave



Start Time: $7: 00 \mathrm{AM}$
Site code
comment:






# ALL TRAFFIC DATA 

(916) 771-8700
orders@atdtraffic.com
File Name : 20-07035-002
Date : 02/06/2020


## ALL TRAFFIC DATA

(916) 771-8700
orders@atdtraffic.com


## ALL TRAFFIC DATA

orders@atdtraffic.com File Name : 20-07035-002
Date : 02/06/2020


## 2020 STREETLIGHT TRAFFIC VOLUME ESTIMATES

| StreetLight Peak Hour Volume Estimates - February 2020 Tuesday, Wednesday, Thursday |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Turning Movement |  |  |  |  |  |  |  |  |  |  |  |
|  |  | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR |
| AM Peak | 1 West El Camino Avenue \& I-80 Westbound Ramps |  |  |  | 846 |  | 282 |  | 545 | 685 |  | 273 | 222 |
| Hour | 2 West El Camino Avenue \& I-80 Eastbound Ramps | 101 |  | 186 |  |  |  |  | 1,261 | 130 |  | 394 | 488 |
|  | 3 West El Camino Avenue \& Orchard Lane | 341 | 7 | 200 | 14 | 2 | 5 | 30 | 903 | 263 | 163 | 385 | 9 |
|  | 4 West El Camino Avenue \& West River Drive | 4 | 0 | 160 | 0 | 0 | 7 | 0 | 1,035 | 0 | 281 | 531 | 38 |
|  | 5 West El Camino Avenue \& Unity Park Street | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 1,288 | 22 | 0 | 863 | 0 |
|  | 6 West El Camino Avenue \& Gateway Oaks Drive | 268 | 76 | 95 | 93 | 13 | 17 | 241 | 350 | 401 | 113 | 522 | 362 |
|  |  | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR |
| PM Peak | 1 West El Camino Avenue \& I-80 Westbound Ramps |  |  |  | 313 |  | 210 |  | 148 | 264 |  | 889 | 263 |
| Hour | 2 West El Camino Avenue \& I-80 Eastbound Ramps |  |  |  |  |  |  |  | 409 | 52 |  | 476 | 387 |
|  | 3 West El Camino Avenue \& Orchard Lane | $121$ | 1 | 134 | 12 | 1 | 4 | 2 | 638 | 98 | 188 | 699 | 0 |
|  | 4 West El Camino Avenue \& West River Drive | 0 | 0 | 89 | 5 | 0 | 5 | 6 | 779 | 28 | 64 | 864 | 5 |
|  | 5 West El Camino Avenue \& Unity Park Street | $0$ | $0$ | $13$ | 0 | $0$ | 0 | 0 | $860$ | 49 | 0 | 928 | $0$ |
|  | 6 West El Camino Avenue \& Gateway Oaks Drive | 277 | 44 | 149 | 357 | 88 | 223 | 29 | 590 | 114 | 108 | 298 | 71 |

## TRIP GENERATION MEMORANDUM

## TRIP GENERATION

DATE: July 27, 2020
TO: $\quad$ Aelita Milatzo, Pelle Clarke | City of Sacramento
FROM: Vic Maslanka, Josh Pilachowski| DKS Associates
SUBJECT: River Oaks Marketplace
Project \#19179-006

This memorandum summarizes the trip generation analysis of the River Oaks Marketplace project located at the northwest corner of West El Camino Avenue and Orchard Lane in the City of Sacramento.

## BACKGROUND

The River Oaks Marketplace project consists of 13,657 square feet of commercial space. Figure 1 illustrates the project location and adjacent properties. The project plan shows uses that include a 7-Eleven (comprised of a Community Market, Restaurant, and Fuel Station), a McDonald's Restaurant with Drive-Through, a Dutch Brothers Coffee Shop with Drive-Through, and a Car Wash. Adjacent properties include The Cove residential development across Orchard Lane to the east (currently under construction and partially occupied), The Core Natomas apartments under construction to the north, and a vacant parcel to the west.

## PROJECT DESCRIPTION AND ESTIMATED TRIP GENERATION

Vehicular trip generation of the project has been estimated using the following sources:

- ITE Trip Generation, Tenth Edition.
- ITE Trip Generation Handbook, Second Edition.
- ITE Trip Generation Handbook, Third Edition.
- Literature review of trip generation data for Dutch Brothers and Car Wash uses.


FIGURE 1: PROJECT LOCATION

## PROJ ECT COMPONENTS

Table 1 summarizes the components of the project and adjacent properties.

## SINGLE USE TRIP GENERATION

Table 2 summarizes the trip generation of the project components and adjacent properties as stand-alone uses. No credits have been taken for alternate mode uses, as travel in the area is predominantly auto oriented at this time.

## 7-ELEVEN

The 7-Eleven trip generation is calculated from the ITE land use code 960, Super Convenience Market / Gas Station. The multi-variable equations (combining building size and fueling positions) were used for the AM and PM peak hours. The daily value is based upon the average of the daily volumes calculated from building size and fuel position rates.

## MCDONALDS

All trip generation is based upon ITE rates for land use code 934, Fast-Food Restaurant with DriveThru.

TABLE 1: PROJECT COMPONENTS AND ASSOCIATED ITE LAND USE CATEGORIES

| PROPERTY | COMPONENT | SI ZE | ITE LAND USE CODE(S) | ITE USE(S) |
| :---: | :---: | :---: | :---: | :---: |
| RIVER OAKS MARKETPLACE | 7-Eleven | $4,650 \mathrm{SF}$ <br> 20 fueling positions | 960 | Super Convenience Market / Gas Station |
|  | McDonalds | 4,500 SF | 934 | Fast-Food Restaurant with Drive-Thru |
|  | Dutch Brothers | 880 SF | $938{ }^{\text {a }}$ | Coffee/Donut Shop with Drive-Thru and No Indoor Seating |
|  | Car Wash | $\begin{aligned} & 3,627 \mathrm{SF} \\ & 1 \text { Tunnel } \end{aligned}$ | $948{ }^{\text {b }}$ | Automated Car Wash |
| THE CORE NATOMAS | Apartments | 300 DU | 220 | Multifamily Housing (Low-Rise) |
| THE COVE | Single-Family | 435 DU | 210 | Single Family Detached Housing |
|  | Townhouses | 156 DU | 220 | Multifamily Housing (Low-Rise) |
| VACANT PROPERTY | Hotel ${ }^{\text {c }}$ | 120 Rooms ${ }^{\text {c }}$ | 310 | Hotel |

[^1]
## DUTCH BROTHERS

The ITE data for a Coffee/Donut Shop with Drive Thru and No Indoor Seating (Code 938) is limited and inappropriate for Dutch Brothers. The ITE data is based upon three much smaller coffee kiosks of 90 square feet each.

Fehr and Peers Associates collected PM peak hour trip generation data on February 5, 2020, at two Dutch Brothers locations (Roseville and Elk Grove) with similar characteristics. This data has been used by the City in the analysis of a Dutch Brothers project on Northgate Boulevard. The PM peak hour data is shown in Table 2 and will be used for this project.

For the AM peak hour, Crane Transportation Group compiled AM and PM peak hour data at three Dutch Brothers locations in Lodi, Oakley, and Stockton California on October 3, 2019. Compared to the PM peak hour, the AM peak hour volumes vary from 76 percent to 171 percent. An average value of 133 percent of the PM peak hour was applied to the AM peak hour.

TABLE 2: SINGLE USE TRIP GENERATION

| PROPERTY | COMPONENT | DAI LY | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| RIVER OAKS MARKETPLACE | 7-Eleven | 4,253 | 234 | 233 | 467 | 195 | 194 | 389 |
|  | McDonalds | 2,119 | 92 | 89 | 181 | 76 | 71 | 147 |
|  | Dutch Brothers | 1,793 | 108 | 107 | 215 | 81 | 81 | 162 |
|  | Car Wash | 748 | 22 | 22 | 44 | 39 | 39 | 78 |
|  | Total | 8,913 | 456 | 451 | 907 | 391 | 385 | 776 |
| THE CORE NATOMAS | Apartments | 2,227 | 31 | 104 | 135 | 99 | 58 | 157 |
| THE COVE | Single-Family | 4,021 | 79 | 235 | 314 | 263 | 154 | 417 |
|  | Townhouses | 1,139 | 17 | 56 | 73 | 55 | 33 | 88 |
|  | Total | 5,160 | 96 | 291 | 387 | 318 | 187 | 505 |
| VACANT PROPERTY | Hotel | 1,468 | 46 | 34 | 80 | 43 | 44 | 87 |

Source: ITE Trip Generation, Tenth Edition, 2017 as updated; DKS Associates, 2020.

For daily volumes, the ratio of daily trips to peak hour trips (AM and PM combined) from the ITE data was utilized.

## CAR WASH

The ITE data for an automated car wash (Code 948) is limited to rates for the PM peak, which are used for the project.

For the AM peak hour, data collected at car washes in Montebello, Newport Beach, and Rialto in 2014 and 2015 were utilized. During the AM peak hour, the volumes varied from 45 to 72 percent of the PM peak hour volumes. An average value of 57 percent of the PM peak hour was applied to the AM peak hour.

For daily volumes, the ratio of daily trips to peak hour trips (AM and PM combined) from the Montebello car wash was utilized.

## THE CORE NATOMAS

All trip generation is based upon ITE equations for land use code 220, Multifamily Housing.

## THE COVE

All trip generation is based upon ITE equations for land use codes 210 and 220, Single Family Detached Housing and Multifamily Housing, respectively.

## HOTEL

ITE equations are used for the AM and PM peak hours, and ITE rate for daily volumes. These are based upon land use code 310, Hotel.

## I NTERNAL TRIPS

Because multiple uses are located on the same site, as well as off-site nearby, some patrons may visit more than one land use. This reduces the number of trips at the driveway compared to stand-alone uses, as these trips are typically made as pedestrians. The reduced trips are called internal trips.

Internal trips were calculated for the four River Oak Marketplace uses and The Core Natomas.
Although some pedestrian trips will be made to the project from The Cove, internal trips were not calculated as The Cove is not considered to be part of a mixed-use development. The design of The Cove limits direct access, as a privacy wall has been constructed along Orchard Lane and West El Camino Avenue.

No internal trips were calculated for the hotel since the land use is uncertain.

Internal trips were calculated in a two-step process:

1. For the retail uses (7-Eleven and Car Wash), the number of internal trips between the uses was estimated.
2. Following the first step, the number of internal trips were estimated between the retail uses, restaurant uses, and apartments.
3. No internal trips were assumed between the restaurants.

Table 3 summarizes the unconstrained internal trip percentages that were applied to the uses. Because of incomplete ITE data, percentages for some time periods were estimated from available data. Each unconstrained internal trip percentage is applied at the origin and destination of the trip. The resultant constrained number of internal trips is the lesser of the origin and destination estimates.

TABLE 3: UNCONSTRAINED INTERNAL TRIP PERCENTAGES

|  |  | DAI LY | AM PEAK HOUR | PM PEAK HOUR |
| :---: | :---: | :---: | :---: | :---: |
| APPLIED TO TRIP ORIGINS |  |  |  |  |
| FROM RETAIL | TO RETAIL | 30\% | 20\% | 20\% |
|  | TO RESTAURANT | 21\% | 13\% | 29\% |
|  | TO RESI DENTIAL | 20\% | 14\% | 26\% |
| FROM RESTAURANT | TO RETAIL | 28\% | 14\% | 41\% |
|  | TO RESI DENTI AL | 11\% | 4\% | 18\% |
| FROM RESIDENTIAL | TO RETAIL | 22\% | 1\% | 42\% |
|  | TO RESTAURANT | 21\% | 20\% | 21\% |
| APPLIED TO TRIP ORIGINS |  |  |  |  |
| TO RETAIL | FROM RETAIL | 28\% | 20\% | 20\% |
|  | FROM RESTAURANT | 22\% | 14\% | 30\% |
|  | FROM RESI DENTI AL | 14\% | 17\% | 10\% |
| TO RESTAURANT | FROM RETAI L | 40\% | 50\% | 29\% |
|  | FROM RESI DENTI AL | 17\% | 20\% | 14\% |
| TO RESIDENTI AL | FROM RETAI L | 24\% | 2\% | 46\% |
|  | FROM RESTAURANT | 11\% | 5\% | 16\% |

Source: ITE Trip Generation Handbook, Second Edition, 2004; ITE Trip Generation Handbook, Third Edition, 2014; DKS Associates, 2020.

PASS-BY TRIPS
Pass-by trips are trips that access the project site that are already on the roadway network driving past the site. While these trips are counted at the driveways, they are not new trips. Table 4 summarizes the pass-by trip percentages utilized for the land use categories.

## DKS

TABLE 4: PASS-BY TRIP PERCENTAGES

| LAND USE | ITE CODE | DAILY | AM PEAK HOUR | PM PEAK HOUR |
| :--- | :---: | :---: | :---: | :---: |
| $945-$ Gasoline / <br> Service Station <br> with Convenience <br> Market | $59 \%$ | $62 \%$ | $56 \%$ |  |
| 934 - Fast-Food <br> Restaurant with <br> Drive-Through <br> Window | $50 \%$ | $49 \%$ | $50 \%$ |  |
| DUTCH BROTHERS | Estimate | $70 \%$ | $70 \%$ | $70 \%$ |
| CAR WASH | $25 \%$ | $25 \%$ | $25 \%$ |  |

Source: ITE Trip Generation Handbook, Third Edition, 2014; DKS Associates, 2020.

## 7-ELEVEN

There is no pass-by trip information for land use code 960 (Super Convenience Market / Gas Station), so land use code 945 (Gasoline / Service Station with Convenience Market) was substituted as a similar use.

## MCDONALDS

The appropriate pass-by information for land use code 934 (Fast-Food Restaurant with DriveThrough Window) was utilized.

## DUTCH BROTHERS

There is no appropriate ITE pass-by percentage for this use. The pass-by percentage was estimated at 70 percent, consistent with the recent City Dutch Brothers study on Northgate Boulevard.

## CAR WASH

There is no appropriate ITE pass-by percentage for this use. The pass-by percentage was conservatively estimated at 25 percent.

## VEHICULAR TRIP GENERATION ESTIMATES

Table 5 summarizes the trip generation estimates. The project is estimated to generate 2,500 new external daily trips, 307 during the a.m. peak hour, and 199 during the p.m. peak hour.

TABLE 5: VEHICULAR TRIP GENERATION ESTIMATES

|  | DAILY | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ENTER | EXIT | TOTAL | ENTER | EXIT | TOTAL |
| RIVER OAKS MARKETPLACE |  |  |  |  |  |  |  |
| 1. SI NGLE USE TRIPS (SEE TABLE 2) | 8,913 | 456 | 451 | 907 | 391 | 385 | 776 |
| 2. I NTERNAL TRIPS | $-3,181$ | -79 | -70 | -149 | -156 | -180 | -335 |
| 3. DRI VEWAY TRIPS (1. MI NUS 2.) | 5,731 | 377 | 381 | 758 | 235 | 205 | 441 |
| 4. PASS-BY TRI PS | $-3,231$ | -224 | -227 | -451 | -130 | $-112$ | -242 |
| 5. NEW EXTERNAL TRIPS (3. MI NUS 4.) | 2,500 | 153 | 154 | 307 | 106 | 93 | 199 |

Source: ITE Trip Generation, Tenth Edition, 2017; ITE Trip Generation Handbook, Second Edition, 2004; ITE Trip Generation Handbook, Third Edition, 2014; and DKS Associates., 2020.

## DKS

## APPENDIX

## ITE LAND USE CODES

# Land Use: 210 Single-Family Detached Housing 

## Description

Single-family detached housing includes all single-family detached homes on individual lots. A typical site surveyed is a suburban subdivision.

## Additional Data

The number of vehicles and residents had a high correlation with average weekday vehicle trip ends. The use of these variables was limited, however, because the number of vehicles and residents was often difficult to obtain or predict. The number of dwelling units was generally used as the independent variable of choice because it was usually readily available, easy to project, and had a high correlation with average weekday vehicle trip ends.

This land use included data from a wide variety of units with different sizes, price ranges, locations, and ages. Consequently, there was a wide variation in trips generated within this category. Other factors, such as geographic location and type of adjacent and nearby development, may also have had an effect on the site trip generation.

Single-family detached units had the highest trip generation rate per dwelling unit of all residential uses because they were the largest units in size and had more residents and more vehicles per unit than other residential land uses; they were generally located farther away from shopping centers, employment areas, and other trip attractors than other residential land uses; and they generally had fewer alternative modes of transportation available because they were typically not as concentrated as other residential land uses.

Time-of-day distribution data for this land use are presented in Appendix A. For the six general urban/suburban sites with data, the overall highest vehicle volumes during the AM and PM on a weekday were counted between 7:15 and 8:15 a.m. and 4:00 and 5:00 p.m., respectively. For the two sites with Saturday data, the overall highest vehicle volume was counted between 3:00 and 4:00 p.m. For the one site with Sunday data, the overall highest vehicle volume was counted between 10:15 and 11:15 a.m.

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in California, Connecticut, Delaware, Illinois, Indiana, Maryland, Minnesota, Montana, New Jersey, North Carolina, Ohio, Oregon, Pennsylvania, South Carolina, South Dakota, Tennessee, Vermont, and Virginia.

## Source Numbers

100, 105, 114, 126, 157, 167, 177, 197, 207, 211, 217, 267, 275, 293, 300, 319, 320, 356, 357, 367, $384,387,407,435,522,550,552,579,598,601,603,614,637,711,716,720,728,735,868,903$, 925, 936

# Land Use: 220 Multifamily Housing (Low-Rise) 

## Description

Low-rise multifamily housing includes apartments, townhouses, and condominiums located within the same building with at least three other dwelling units and that have one or two levels (floors). Multifamily housing (mid-rise) (Land Use 221), multifamily housing (high-rise) (Land Use 222), and off-campus student apartment (Land Use 225) are related land uses.

## Additional Data

In prior editions of Trip Generation Manual, the low-rise multifamily housing sites were further divided into rental and condominium categories. An investigation of vehicle trip data found no clear differences in trip making patterns between the rental and condominium sites within the ITE database. As more data are compiled for future editions, this land use classification can be reinvestigated.

For the three sites for which both the number of residents and the number of occupied dwelling units were available, there were an average of 2.72 residents per occupied dwelling unit.

For the two sites for which the numbers of both total dwelling units and occupied dwelling units were available, an average of 96.2 percent of the total dwelling units were occupied.

This land use included data from a wide variety of units with different sizes, price ranges, locations, and ages. Consequently, there was a wide variation in trips generated within this category. Other factors, such as geographic location and type of adjacent and nearby development, may also have had an effect on the site trip generation.

Time-of-day distribution data for this land use are presented in Appendix A. For the 10 general urban/suburban sites with data, the overall highest vehicle volumes during the AM and PM on a weekday were counted between $7: 15$ and $8: 15 \mathrm{a} . \mathrm{m}$. and 4:45 and 5:45 p.m., respectively. For the one site with Saturday data, the overall highest vehicle volume was counted between 9:45 and 10:45 a.m. For the one site with Sunday data, the overall highest vehicle volume was counted between 11:45 a.m. and 12:45 p.m.

For the one dense multi-use urban site with 24 -hour count data, the overall highest vehicle volumes during the AM and PM on a weekday were counted between 7:00 and 8:00 a.m. and 6:15 and 7:15 p.m., respectively.

For the three sites for which data were provided for both occupied dwelling units and residents, there was an average of 2.72 residents per occupied dwelling unit.

The average numbers of person trips per vehicle trip at the five general urban/suburban sites at which both person trip and vehicle trip data were collected were as follows:

- 1.13 during Weekday, Peak Hour of Adjacent Street Traffic, one hour between 7 and 9 a.m.
- 1.21 during Weekday, Peak Hour of Adjacent Street Traffic, one hour between 4 and 6 p.m.

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in British Columbia (CAN), California, District of Columbia, Florida, Georgia, Illinois, Indiana, Maine, Maryland, Minnesota, New Jersey, New York, Ontario, Oregon, Pennsylvania, South Dakota, Tennessee, Texas, Utah, Virginia, and Washington.

It is expected that the number of bedrooms and number of residents are likely correlated to the number of trips generated by a residential site. Many of the studies included in this land use did not indicate the total number of bedrooms. To assist in the future analysis of this land use, it is important that this information be collected and included in trip generation data submissions.

## Source Numbers

$168,187,188,204,211,300,305,306,319,320,321,357,390,412,418,525,530,571,579,583$, 864, 868, 869, 870, 896, 903, 918, 946, 947, 948, 951

# Land Use: 310 Hotel 

## Description

A hotel is a place of lodging that provides sleeping accommodations and supporting facilities such as restaurants, cocktail lounges, meeting and banquet rooms or convention facilities, limited recreational facilities (pool, fitness room), and/or other retail and service shops. All suites hotel (Land Use 311), business hotel (Land Use 312), motel (Land Use 320), and resort hotel (Land Use 330) are related uses.

## Additional Data

Studies of hotel employment density indicate that, on the average, a hotel will employ 0.9 employees per room. ${ }^{1}$

Twenty-five studies provided information on occupancy rates at the time the studies were conducted. The average occupancy rate for these studies was approximately 82 percent.

Some properties contained in this land use provide guest transportation services such as airport shuttles, limousine service, or golf course shuttle service, which may have an impact on the overall trip generation rates.

Time-of-day distribution data for this land use are presented in Appendix A. For the one center city core site with data, the overall highest vehicle volumes during the AM and PM on a weekday were counted between 8:30 and 9:30 a.m. and 3:15 and 4:15 p.m., respectively. On Saturday and Sunday, the peak hours were between 5:00 and 6:00 p.m. and 10:15 and 11:15 a.m., respectively.

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in California, District of Columbia, Florida, Georgia, Indiana, Minnesota, New York, Pennsylvania, South Dakota, Texas, Vermont, Virginia, and Washington.

For all lodging uses, it is important to collect data on occupied rooms as well as total rooms in order to accurately predict trip generation characteristics for the site.

Trip generation at a hotel may be related to the presence of supporting facilities such as convention facilities, restaurants, meeting/banquet space, and retail facilities. Future data submissions should specify the presence of these amenities. Reporting the level of activity at the supporting facilities such as full, empty, partially active, number of people attending a meeting/banquet during observation may also be useful in further analysis of this land use.

## Source Numbers

170, 260, 262, 277, 280, 301, 306, 357, 422, 507, 577, 728, 867, 872, 925, 951

[^2]
# Land Use: 853 <br> Convenience Market with Gasoline Pumps 

## Description

This land use includes convenience markets with gasoline pumps where the primary business is the selling of convenience items, not the fueling of motor vehicles. The sites included in this land use category have the following two specific characteristics:

- The gross floor area of the convenience market is at least 2,000 gross square feet
- The number of vehicle fueling positions is less than 10

Convenience market (Land Use 851), gasoline/service station (Land Use 944), gasoline/service station with convenience market (Land Use 945), and super convenience market/gas station (Land Use 960) are related uses.

## Additional Data

The independent variable, vehicle fueling positions, is defined as the maximum number of vehicles that can be fueled simultaneously.

Time-of-day distribution data for this land use are presented in Appendix A. For the 31 general urban/ suburban sites with data, the overall highest vehicle volumes during the AM and PM on a weekday were counted between 7:30 and 8:30 a.m. and 4:45 and 5:45 p.m., respectively.

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in Alberta (CAN), Arkansas, Delaware, Florida, Indiana, Iowa, Kentucky, Maryland, Massachusetts, Minnesota, New Hampshire, Rhode Island, South Dakota, Texas, Vermont, and Washington.

## Source Numbers

$221,274,288,300,340,350,351,352,355,359,718,810,813,853,882,883,888,926,927,936,977$

# Land Use: 934 <br> Fast-Food Restaurant with Drive-Through Window 

## Description

This category includes fast-food restaurants with drive-through windows. This type of restaurant is characterized by a large drive-through clientele, long hours of service (some are open for breakfast, all are open for lunch and dinner, some are open late at night or 24 hours a day) and high turnover rates for eat-in customers. These limited-service eating establishments do not provide table service. Non-drive-through patrons generally order at a cash register and pay before they eat. Fast casual restaurant (Land Use 930), high-turnover (sit-down) restaurant (Land Use 932), fast-food restaurant without drive-through window (Land Use 933), and fast-food restaurant with drive-through window and no indoor seating (Land Use 935) are related uses.

## Additional Data

Users should exercise caution when applying statistics during the AM peak periods, as the sites contained in the database for this land use may or may not be open for breakfast. In cases where it was confirmed that the sites were not open for breakfast, data for the AM peak hour of the adjacent street traffic were removed from the database.

The outdoor seating area is not included in the overall gross floor area. Therefore, the number of seats may be a more reliable independent variable on which to establish trip generation rates for facilities having significant outdoor seating.

Time-of-day distribution data for this land use for a weekday, Saturday, and Sunday are presented in Appendix A. For the 46 general urban/suburban sites with data, the overall highest vehicle volumes during the AM and PM on a weekday were counted between 11:45 a.m. and 12:45 p.m. and 12:00 and 1:00 p.m., respectively. For the one dense multi-use urban site with data, the same AM and PM peak hours were observed.

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in Alaska, Alberta (CAN), California, Colorado, Florida, Indiana, Kentucky, Maryland, Massachusetts, Minnesota, Montana, New Hampshire, New Jersey, New York, North Carolina, Ohio, Pennsylvania, South Dakota, Texas, Vermont, Virginia, Washington, and Wisconsin.

## Source Numbers

163, 164, 168, 180, 181, 241, 245, 278, 294, 300, 301, 319, 338, 340, 342, 358, 389, 438, 502, 552,
$577,583,584,617,640,641,704,715,728,810,866,867,869,885,886,927,935,962,977$

# Land Use: 937 <br> Coffee/Donut Shop with Drive-Through Window 

## Description

This land use includes single-tenant coffee and donut restaurants with drive-through windows. Freshly brewed coffee and a variety of coffee-related accessories are the primary retail products sold at these sites. They may also sell other refreshment items, such as donuts, bagels, muffins, cakes, sandwiches, wraps, salads, and other hot and cold beverages. Some sites may also sell newspapers, music, CDs, and books. The coffee and donut shops contained in this land use typically hold long store hours (more than 15 hours) with an early morning opening. Also, limited indoor seating is generally provided for patrons; however, table service is not provided. Coffee/donut shop without drive-through window (Land Use 936), coffee/donut shop with drive-through window and no indoor seating (Land Use 938), bread/donut/bagel shop without drive-through window (Land Use 939), and bread/donut/bagel shop with drive-through window (Land Use 940) are related uses.

## Additional Data

The sites were surveyed in the 1990s, the 2000s, and the 2010s in California, Colorado, Connecticut, Illinois, Massachusetts, Minnesota, Nevada, New Hampshire, New Jersey, New York, Ontario (CAN), Pennsylvania, Quebec (CAN), Tennessee, Vermont, Washington, and Wisconsin.

## Specialized Land Use Data

One study provided data for a coffee/donut shop with a drive-through window that also sells donuts and ice cream (source 617). The trip generating characteristics of this site differed from the sites included in this land use; therefore, trip generation information for this site is presented here and was excluded from the data plots. The site had a gross floor area of 3,300 square feet. It generated 425 vehicle trips during the weekday AM peak hour of adjacent street traffic, and 236 vehicle trips during the weekday PM peak hour of adjacent street traffic.

## Source Numbers

594, 599, 615, 617, 618, 621, 622, 635, 639, 712, 714, 725, 726, 728, 853, 854, 892, 903, 928, 959, 979, 982

# Land Use: 938 Coffee/Donut Shop with Drive-Through Window and No Indoor Seating 

## Description

This land use includes single-tenant coffee and donut restaurants with drive-through windows. Freshly brewed coffee and a variety of coffee-related accessories are the primary retail products sold at these sites. They may also sell other refreshment items, such as donuts, bagels, muffins, cakes, sandwiches, wraps, salads, and other hot and cold beverages. Some sites may also sell newspapers, music, CDs, and books. The coffee and donut shops contained in this land use typically hold long store hours (over 15 hours) with an early morning opening. Coffee/donut shop without drive-through window (Land Use 936), coffee/donut shop with drive-through window (Land Use 937), bread/donut/bagel shop without drive-through window (Land Use 939), and bread/donut/bagel shop with drive-through window (Land Use 940) are related uses.

## Additional Data

The sites were surveyed in the 1990s and the 2000s in New Hampshire, Oregon, and Washington.

## Specialized Land Use Data

A 2003 study by the Oregon Department of Transportation provided trip generation information on portable coffee stands with drive-through service (source 755). The coffee stands were portable trailers with dimensions of approximately 8 feet by 12 feet and were operated by one or two employees. All sites (stands) were located near major roadways in urban areas. The sites were surveyed between 7:00 and 9:00 a.m. The trip generation characteristics of these sites differ from the facilities typically contained in this land use; therefore, trip generation information for these sites is presented here and was excluded from the data plots. The average number of vehicle trips during the weekday AM peak hour of adjacent street traffic for the nine sites was 33 . The numbers of trips ranged between 16 and 56 .

## Source Numbers

514, 644, 755, 981

# Land Use: 945 <br> Gasoline/Service Station with Convenience Market 

## Description

This land use includes gasoline/service stations with convenience markets where the primary business is the fueling of motor vehicles. These service stations may also have ancillary facilities for servicing and repairing motor vehicles and may have a car wash. Some commonly sold convenience items are newspapers, coffee or other beverages, and snack items that are usually consumed in the car. The sites included in this land use category have the following two specific characteristics:

- The gross floor area of the convenience market is between 2,000 and 3,000 gross square feet
- The number of vehicle fueling positions is at least 10

Convenience market (Land Use 851), convenience market with gasoline pumps (Land Use 853), gasoline/service station (Land Use 944), truck stop (Land Use 950), and super convenience market/ gas station (Land Use 960) are related uses.

## Additional Data

The independent variable, vehicle fueling positions, is defined as the maximum number of vehicles that can be fueled simultaneously.

Gasoline/service stations in this land use include "pay-at-the-pump" and traditional fueling stations.
Time-of-day distribution data for this land use are presented in Appendix A. For the five general urban/suburban sites with data, the overall highest vehicle volumes during the AM and PM on a weekday were counted between 7:30 and 8:30 a.m. and 3:45 and 4:45 p.m., respectively.

A multi-variable regression analysis based on both the convenience market gross floor area (GFA) and the number of vehicle fueling positions (VFP) produced a series of fitted curve equations. The equations are in the form of:

Vehicle Trips $=[($ VFP Factor $) \times($ Number of VFP) $)]+[($ GFA Factor $) \times($ GFA $)]+($ Constant $)$
The values for the VFP factor, GFA factor, and constant are presented in the following table for each time period for which a fitted curve equation could produce an $R^{2}$ value of at least 0.50 .

| Time Period | VFP Factor | GFA Factor | Constant | R $^{2}$ |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Weekday, AM Peak Hour of Generator | 15.6 | 108 | -295 | 0.62 |  |
| Weekday, PM Peak Hour of Generator | Not Available |  |  |  |  |
| Weekday, AM Peak Hour of Adjacent Street | 15.7 | 97.3 | -284 | 0.59 |  |
| Weekday, PM Peak Hour of Adjacent Street | Not Available |  |  |  |  |

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in Alberta (CA), California, Connecticut, Florida, Indiana, Iowa, Kentucky, Minnesota, New Hampshire, New Jersey, Texas, and Wisconsin.

## Source Numbers

$245,340,350,385,440,617,813,864,865,883,888,954,960,977$

# Land Use: 948 Automated Car Wash 

## Description

An automated car wash is a facility that allows for the mechanical cleaning of the exterior of vehicles. Manual cleaning services may also be available at these facilities. Self-service car wash (Land Use 947) and car wash and detail center (Land Use 949) are related uses.

## Additional Data

The sites were surveyed in the 1990s and the 2000s in New Jersey, New York, and Washington.

## Source Numbers

552, 555, 585, 599, 954

# Land Use: 949 <br> Car Wash and Detail Center 

## Description

A car wash and detail center is a facility that provides for the manual cleaning of the exterior of vehicles as well as interior car-detailing services. Self-service car wash (Land Use 947) and automated car wash (Land Use 948) are related uses.

## Additional Data

Time-of-day distribution data for this land use are presented in Appendix A. For the one general urban/suburban site with data, the overall highest vehicle volumes during the AM and PM on a weekday were counted between 11:00 a.m. and 12:00 p.m. and 2:15 and 3:15 p.m., respectively.

The site was surveyed in the 2010s in Minnesota.

## Source Number

866

# Land Use: 960 Super Convenience Market/Gas Station 

## Description

This land use includes gasoline/service stations with convenience markets where there is significant business related to the sale of convenience items and the fueling of motor vehicles. Some commonly sold convenience items include newspapers, freshly brewed coffee, daily-made donuts, bakery items, hot and cold beverages, breakfast items, dairy items, fresh fruits, soups, light meals, ready-to-go and freshly made sandwiches and wraps, and ready-to-go salads. Stores typically also had automated teller machines (ATMs), and public restrooms. The sites included in this land use category have the following two specific characteristics:

- The gross floor area of the convenience market is at least 3,000 gross square feet
- The number of vehicle fueling positions is at least 10

Convenience market with gasoline pumps (Land Use 853) and gasoline/service station with convenience market (Land Use 945) are related uses.

## Additional Data

To reflect changing characteristics of the convenience market component of this land use, only data from the past two decades have been included in this land use.

The independent variable, vehicle fueling positions, is defined as the maximum number of vehicles that can be fueled simultaneously. Gasoline/service stations in this land use include "pay-at-the-pump" and traditional fueling stations.

A multi-variable regression analysis based on both the convenience market gross floor area (GFA) and the number of vehicle fueling positions (VFP) produced a series of fitted curve equations. The equations are in the form of:

Vehicle Trips $=[($ VFP Factor $) \times($ Number of VFP) $)]+[($ GFA Factor $) \times($ GFA $)]+($ Constant $)$
The values for the VFP factor, GFA factor, and constant are presented in the following table for each time period for which a fitted curve equation could produce an $R^{2}$ value of at least 0.50 .

| Time Period | VFP Factor | GFA Factor | Constant | $R^{2}$ |
| :--- | :---: | :---: | :---: | :---: |
| Weekday, AM Peak Hour of Generator | 10.3 | 105 | -290 | 0.62 |
| Weekday, PM Peak Hour of Generator | 6.91 | 76.0 | -133 | 0.68 |
| Weekday, AM Peak Hour of Adjacent Street | 16.1 | 135 | -483 | 0.66 |
| Weekday, PM Peak Hour of Adjacent Street | 11.5 | 82.9 | -226 | 0.51 |

The sites were surveyed in the late 1990's, 2000s and the 2010s in Florida, Iowa, Maryland, Minnesota, New Hampshire, New Jersey, Pennsylvania, Texas, Utah, and Wisconsin.

## Source Numbers

617, 813, 844, 850, 864, 865, 867, 869, 882, 888, 904, 938, 954, 960, 962

## DUTCH BROTHERS TRIP GENERATI ON STUDIES

## TRAFFIC IMPACT REPORT

# CFT - PHASE 2 <br> (Panda Express-Sonic-Dutch Brothers) PROJECT IN THE CITY OF LATHROP, CA 

December 9, 2019

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## I. INTRODUCTION

This report has been prepared at the request of the City of Lathrop to determine the potential circulation impacts due to development of a Panda Express restaurant (with drive through window), a Sonic fast food restaurant (with drive through window) and a Dutch Brothers coffee facility (with drive through window) on adjacent parcels just south of W. Lathrop Road and between Old Harlan Road and the 1-5 freeway (see Figures 1 and 2). Impacts have been determined for existing and year 2022 horizons (the cumulative year in the City's TMP circulation system improvement program) at West Lathrop Road intersections between the I-5 interchange and New Harlan Road as well as at Harlan Road/Old Harlan Road just south of the project area. Analysis has included level of service and delay at each intersection, vehicle queuing on critical approaches to select intersections and the possibility that some project traffic may use the Burger King-O'Reilly's Auto Parts parking lot (just east of Old Harlan Road and the project) for access to Harlan Road. In addition, each on-site circulation plan has been evaluated in the context of city code criteria and adequacy of expected drive through operation. Finally, recommendations have been made to improve all existing deficiencies or as well as all potential impacts due to the project.

## II. SUMMARY OF FINDINGS

## A. WITHOUT PROJECT CONDITIONS

## 1. EXISTING

- All analysis intersections are operating at acceptable levels of service and delay during the AM and PM peak traffic hours.
- There is unacceptable vehicle storage at the W. Lathrop Road/Harlan Road intersection for left turn queues on the eastbound W. Lathrop Road and northbound Harlan Road approaches, primarily during the PM peak traffic period. In addition, traffic on the eastbound Harlan Road approach to W. Lathrop Road frequently backs up to and through the Old Harlan Road intersection, primarily during the PM peak period.
- The unsignalized Harlan Road/Old Harlan Road intersection just south of the project site does not have AM or PM peak hour volumes meeting Caltrans peak hour signal Warrant \#3 volume criteria.


## 2. CUMULATIVE (YEAR 2022)

- All analysis intersections would be operating at acceptable levels of service and delay during the AM and PM peak hours.
- Unacceptable vehicle queues would lengthen at the W. Lathrop Road/Harlan Road intersection for left turns on the eastbound W. Lathrop Road approach and on the northbound Harlan Road approach, primarily during the PM peak period. Eastbound W. Lathrop Road backups from Harlan Road would also increase in length intermittently to the I-5 NB Ramps intersection.
- There would only be minor queues ( 3 cars or less) on the northbound Old Harlan Road approach to W. Lathrop Road.
- The unsignalized Harlan Road/Old Harlan Road intersection just south of the project would not have AM or PM peak hour volumes meeting Caltrans peak hour signal Warrant \#3 volume criteria.


## B. PROJECT IMPACTS

## 1. TRIP GENERATION

All three of the proposed facilities would be expected to capture a significant amount of traffic from the adjacent I-5 Freeway as well as W. Lathrop Road, Harlan Road and Old Harlan Road. While the total two-way traffic on the three project driveways combined is projected to be about 200 vehicles during the AM commute period peak traffic hour and about 210 vehicles during the PM commute period peak traffic hour, about 140 to 150 of these trips would be captured from existing traffic flow. While customers captured from I-5 would add new traffic flow to the local street system, those captured from the adjacent or nearby surface streets would just reroute their trips to/from Old Harlan Road south of W. Lathrop Road.

## 2. EXISTING + PROJECT OFE-SITE TRAFFIC IMPACTS

- All analysis intersections would maintain acceptable levels of service and delay with the addition of project traffic during the AM and PM peak hours.
- Existing unacceptable queuing on the approaches to the W. Lathrop Road/Harlan Road intersection would not be increased significantly due to project traffic. However, the project would result in extremely long $95^{\text {th }}$ percentile queues on the NB Old Harlan Road approach to W. Lathrop Road (up to 200 feet - or 8 vehicles) during the PM peak traffic hour. This backup would result in some drivers cutting through both the Chevron Gas station and

Burger King-O'Reilly's Auto Parts properties in order to find alternate routes to bypass the congestion.

- Internal circulation for both the Panda Express and Sonic restaurants meets City code criteria and should operate acceptably.
- The Dutch Brothers drive through lane(s) should have acceptable storage to accommodate anticipated queues based upon survey results at 3 other Dutch Brothers facilities in the region (Stockton, Lodi and Oakley). The only potential issue of conflict will be due to the Dutch Brothers drive through lane entrance being much closer to the Sonic driveway connection to Old Harlan Road than to the Dutch Brothers driveway connection. It is likely that the Sonic driveway will accommodate a third or more of the inbound Dutch Brothers traffic.


## 3. CUMULATIVE (YEAR 2022) + PROJECT OFF-SITE TRAFFIC IMPACTS

- There will be no new impacts due to project traffic in 2022 compared to existing conditions.
- All intersections will continue to operate acceptably with the addition of project traffic during the AM and PM peak hours.
- There will be no significant extensions of queuing on intersection approaches already experiencing unacceptable queuing. The lengthy $95^{\text {th }}$ percentile queue on the NB Old Harlan Road approach to W. Lathrop Road will extend back to 425 feet, further encouraging some drivers in the queue to use the Chevron and Burger King-O'Reilly's Auto properties as alternative travel routes.


## 4. PEDESTRIAN AND TRANSIT IMPACTS

- The three project facilities will likely attract some customers from the local neighborhood, some pedestrians (many high school students) now walking on the sidewalk on the north side of W. Lathrop Road, and some employees using the two regional transit routes that have stops at the W. Lathrop Road/Harlan Road intersection. However, while a sidewalk will be provided along the project's Old Harlan Road frontage, none will be provided on the south side of W. Lathrop Road east or west of Old Harlan Road. This will force pedestrians to walk in the street or through the Chevron and Burger King properties to access the three facilities. Also, it is likely that pedestrians on the north side of W. Lathrop Road will cross the street at a variety of locations (none with crosswalks) to access the facilities.


## C. RECOMMENDATIONS

## 1. EXISTING WITHOUT PROJECT (CITY RESPONSIBILITY)

- Reconfigure the northbound Harlan Road approach to W. Lathrop Road to provide two exclusive left turn lanes and a combined through/right turn lane.
- Remove the raised island median on Harlan road south of W. Lathrop Road at the entrance to the existing northbound left turn lane. Continue this existing turn lane south to the Burger King-O'Reilly's driveway.
- Extend the length of the left turn lane on the eastbound W. Lathrop Road approach to Harlan Road by at least 75 feet.
- Retime the W. Lathrop Road/Harlan Road signal and coordinate timing with the W. Lathrop Road/Cambridge Drive signal.


## 2. PROJECT (EXISTING AND CUMULATIVE)

- Realign the Old Harlan Road connection to Harlan Road (just south of the project) about 100 feet to the north and provide two lanes on the Old Harlan Road approach: one for left turns and one for right turns. In conjunction with this measure, restripe the median of Harlan Road just şouth of the new intersection to provide defined back-to-back left turn lanes - one for northbound left turns into Old Harlan Road, and one for southbound left turns into the driveway providing access into the Lathrop Crossing shopping center on the east side of Harlan Road.
- Provide signs adjacent to the exit lanes at each of the three project driveways showing an arrow pointing to the right and a message stating I-5 access turn right. In conjunction with this measure, also provide a sign on the southbound Old Harlan Road approach to Harlan Road with an arrow pointing left and a message stating I-5 access turn left.
- Provide sidewalks on the south side of W. Lathrop Road extending east and west of Old Harlan Road (from the I-5 Ramps intersection to the Chevron driveway).
- Provide a crosswalk at the W. Lathrop Road/I-5 NB Ramps intersection crossing W. Lathrop Road just east of the intersection. Provide pedestrian walk/don't walk signals in conjunction with the crosswalk.
- In order to ensure that Dutch Brothers customers do not congest the Sonic driveway during peak activity times, it may be necessary for Dutch Brothers to provide moveable orange cones across the internal Dutch Brothers-Sonic parking lots connection.
- Based upon input from Chevron, Burger King or O'Reilly's Auto, if there is a perceived use of either property by cut-through traffic from the project:
a. The City shall conduct an independent survey to see the extent of the issue.
b. If there is a problem, the City shall work with one or both property owners to develop measures to further reduce or eliminate cut-through traffic.
c. This survey shall be funded by the project applicant


## III. PROJECT DESCRIPTION AND LOCATION

The proposed project is comprised of two restaurants with drive through lanes and a coffee service facility with a drive through lane and limited inside seating and service. Facilities are (listed north to south):

- Panda Express (2200 square feet) with a drive through lane
- Sonic drive in ( 1608 square feet) with a drive through lane
- Dutch Brothers coffee service ( 862 square feet) with a drive through lane

Locations are schematically shown on Figure 2, while the site plan is presented in Figure 3. Each facility will have single driveway connection to the west side of Old Harlan Road and there will also be single internal driveway connections between Panda Express and Sonic and between Sonic and Dutch Brothers. There are no changes proposed to the local circulation system by this project.

## IV. SCOPE OF SERVICES (Approved by City staff)

## A. BASE ASSUMPTION

All three developments (Panda Express, Sonic \& Dutch Brothers) are considered as one project for off site evaluation purposes.

## B. ANALYSIS LOCATIONS

## Intersection Level of Service \& Queuing

- W. Lathrop Road/I-5 Southbound Ramps
- W. Lathrop Road/I-5 Northbound Ramps
- W. Lathrop Road/Old Harlan Road
- W. Lathrop Road/New Harlan Road
- Old Harlan Road/New Harlan Road


## C. TIME PERIODS TO BE STUDIED

- Weekday AM and PM commute peak traffic hours


## D. TRAFFIC COUNT LOCATIONS - WEEKDAY 7:00-9:00 AM \& 3:00-6:00 PM (ALL VEHICLES, TRUCKS, PEDS, BIKES).

Counts will be conducted when all schools are open.

- W. Lathrop Road/I-5 Southbound Ramps
- W. Lathrop Road/I-5 Northbound Ramps
- W. Lathrop Road/Old Harlan Road
- W. Lathrop Road/New Harlan Road
- Old Harlan Road/New Harlan Road
- Old Harlan Road/Driveways serving Burger King \& Chevron gas station
- W. Lathrop Road/Chevron gas station driveway
- New Harlan Road/Burger King driveway
- Drive-thru lanes at three Dutch Brothers operations (Lodi, Stockton, Oakley) - trip generation and queuing, two days each

Counts will include observations of vehicle queuing on the northbound Old and New Harlan Road approaches to W. Lathrop Road, the eastbound W. Lathrop Road approach to New Harlan Ramp.

## E. HORIZON YEARS \& ANALYSIS SCENARIOS

- Existing
- Existing + Project
- Year 2022
- Year 2022 + Project


## F. CUMULATIVE (YEAR 2022) VOLUMES

Year 2022 AM \& PM peak hour volumes will be obtained from the 2019 TMP study for the following locations.

- W. Lathrop Road/I-5 Southbound Ramps
- W. Lathrop Road/I-5 Northbound Ramps
- W. Lathrop Road/New Harlan Road

Year 2022 projections at all other analysis locations will be developed based upon existing volume interrelationships. In addition, a determination will be made how much development on the project site was included in the 2022 TMP projections. Adjustments will be made to provide true 2022 Without Project and $2022+$ Project projections.

## G. PROJECT TRIP GENERATION \& DISTRIBUTION

Project trip generation for the Panda Express \& Sonic drive-in will be based upon trip rates from the Institute of Transportation Engineers, Trip Generation Manual, 10th Edition, by the Institute of Transportation Engineers, 2017, while trip generation for the Dutch Brothers operation will be based upon three surveys of AM \& PM peak period trip generation and order line queuing conducted by Crane Transportation Group. Dutch Brothers surveys will be conducted for two days each at facilities in Stockton, Lodi and Oakley. The percentage of passby and diverted link capture of existing traffic associated with the three Lathrop restaurants will be discussed with and approved by City staff.

Project traffic will be distributed based upon local traffic flow patterns, in particular to/from the Burger King restaurant's driveways along New \& Old Harlan Road.

## H. INTERSECTION EVALUATION

## Signalized

- Level of service and $95^{\text {ni }}$ percentile queuing using Synchro-SIM traffic analysis software program. Queuing projections for 2022 and "with project" conditions will be based upon the calibrated relationship of surveyed $95^{\text {th }}$ percentile queuing at analysis intersections compared to Synchro theoretical projections.


## Unsignalized

- Level of Service - stop sign controlled approach
- Peak hour signal warrant (Caltrans volume Warrant \#3)


## I. INTERNAL CIRCULATION

Internal circulation plans for each of the three developments will be reviewed in the context of City Code criteria and good traffic engineering practice. Of particular concern will be vehicle queuing on the approach to the drive-thru lane at Dutch Brothers Coffee. Surveys at the Stockton, Lodi and Oakley Dutch Brothers operations will tabulate order line queuing for the 7:00-9:00 AM and 3:00-6:00 PM hours for the two survey days at each location.

## J. PROJECT VEHICLE DIVERSION THROUGH BURGER KING SITE

Concern has been raised by the Burger King restaurant on the east side of Old Harlan Road about project traffic passing through their site to access New Harlan Road, particularly if there is extensive queuing on the northbound Old Harlan Road approach to W. Lathrop Road. This potential impact will be evaluated.

## V. ENVIRONMENTAL SETTING

## A. EXISTING CONDITIONS

## 1. ROADWAYS \& FREEWAYS

Interstate 5 (I-5) is a six-lane freeway located just west of the project site. It extends northerly to Stockton, Sacramento and to the Oregon border; and southerly to a connection with I-205 (the most direct freeway connection to the San Francisco Bay Area) as well as Los Angeles and other southern California cities. I-5 has a tight diamond interchange with Louise Avenue, with both ramp intersections being signal controlled.

West Lathrop Road is a four-lane arterial street in the project area. The posted speed limit is 35 miles per hour. It extends easterly into the City of Manteca and an interchange with the SR 99 freeway and westerly to an interchange with the I-5 freeway (just west of the project site).
W. Lathrop Road changes name to Spartan Way just west of I-5. In the project area there are signalized intersections with the I-5 North and South bound ramps, Harlan Road and Cambridge Drive. Old Harlan Road intersects the north and south sides of W. Lathrop Road about halfway between the I-5 Northbound ramps and Harlan Road signalized intersections. A raised median along W. Lathrop Road in this area limits movements to right turns in/out only between W. Lathrop Road and Old Harlan Road.
Harlan Road is a 2- to 4-lane arterial running along the east side of the I-5 freeway. The posted speed limit is 40 miles per hour. Just south of W. Lathrop Road there are two northbound lanes and two southbound lanes that merge to a single lane north of Old Harlan Road. There is also a median continuous two-way left turn lane.

Old Harlan Road is a two-lane street extending one block between W. Lathrop Road and Harlan Road (both north and south of W. Lathrop Road). There is no posted speed limit. The section south of W. Lathrop Road adjacent to the project site is stop sign controlled on its northbound approach to W. Lathrop Road (where right turns only to/from W. Lathrop Road are allowed) and on its southbound approach to Harlan Road (where all turn movements are allowed except left turns from Old Harlan Road to northbound Harlan Road).

Figure 4 presents existing intersection geometrics and control at all analysis locales.

## 2. EXISTING (WITHOUT PROJECT) PEAK HOUR VOLUMES

Weekday AM and PM commute period (7:00-9:00 AM and 3:00-6:00 PM) traffic counts were conducted at all analysis intersections on Thursday, October 3, 2019. It was determined that the specific peak hours at the vast majority of intersections were between 7:00 and 8:00 AM and between 5:00 and 6:00 PM. Resultant AM and PM peak hour volumes are presented in Figures 5 and 6.

## 3. INTERSECTION LEVEL OF SERVICE \& DELAY

## a. Analysis Methodology

Transportation engineers and planners commonly use a grading system called level of service (LOS) to measure and describe the operational status of the local roadway network. LOS is a description of the quality of a roadway facility's operation, ranging from LOS A (indicating free flow traffic conditions with little or no delay) to LOS F (representing oversaturated conditions where traffic flows exceed design capacity, resulting in long queues and delays). Intersections, rather than roadway segments between intersections, are almost always the capacity controlling locations for any circulation system.

Signalized Intersections. For signalized intersections, the Year $20176^{\text {th }}$ Edition Highway Capacity Manual (Transportation Research Board, National Research Council) methodology was utilized. With this methodology, operations are defined by the level of service and average control delay per vehicle (measured in seconds) for the entire intersection. For a signalized intersection, control delay is the portion of the total delay attributed to traffic signal operation. This includes delay associated with deceleration, acceleration, stopping, and moving up in the queue. Table 1 summarizes the relationship between delay and LOS for signalized intersections.

Unsignalized Intersections. For unsignalized (all-way stop-controlled and side-street stopcontrolled) intersections, the Year $20176^{\text {th }}$ Edition Highway Capacity Manual (Transportation Research Board, National Research Council) methodology for unsignalized intersections was utilized. For side-street stop-controlled intersections, operations are defined by the level of service and average control delay per vehicle (measured in seconds), with delay reported for the stop sign controlled approaches or turn movements. For all-way stop-controlled intersections, operations are defined by the average control delay for the entire intersection (measured in seconds per vehicle). The delay at an unsignalized intersection incorporates delay associated with deceleration, acceleration, stopping, and moving up in the queue. Table 2 summarizes the relationship between delay and LOS for unsignalized intersections.

## b. Minimum Acceptable Operation - City of Lathrop

Signalized \& All Way Stop Intersections: Level of Service D is the poorest acceptable overall intersection operation.

Unsignalized Intersections (side street stop sign controlled): Level of Service E is the poorest acceptable side street stop sign controlled approach operation.

## c. Existing Without Project Intersection Level of Service Operation

Table 3 shows that all analysis intersections are currently operating at acceptable levels of service during the weekday AM and PM commute peak hours. The W. Lathrop Road/Harlan Road signalized intersection has a LOS C operation during both the AM and PM peak hours. At the I-5 interchange the W. Lathrop Road/Southbound Ramps intersection is also operating acceptably at LOS C during both peak hours, while the W. Lathrop Road/I-5 Northbound Ramps intersection is operating at an acceptable LOS C during the AM peak hour and LOS B during the PM peak hour. At the unsignalized Harlan Road/Old Harlan Road intersection south of the site, the stop sign controlled Old Harlan Road approach is operating at an acceptable LOS B during both peak hours. Intersection level of service worksheets are presented in Appendix A.

## 4. EXISTING (WITHOUT PROJECT) 95TH PERCENTILE VEHICLE QUEUING

## a. Analysis Methodology

Field surveys were conducted during AM and PM peak periods (under direction of Crane Transportation Group) of maximum queues every signal cycle at the following locations:

- W. Lathrop Road/Harlan Road
- W. Lathrop Road
- Eastbound left turn
- Eastbound through and right turn movements
- Harlan Road
- Northbound left turn
- Northbound through and right turn movements
- W. Lathrop Road/Old Harlan Road
- Old Harlan Road stop sign controlled northbound right turn
- W. Lathrop Road/I-5 Southbound Ramps
- W. Lathrop Road westbound left turn (to Southbound On Ramp)

Maximum queues for each 15-minute time period are presented in Appendix B.

## b. Queuing Results

## Acceptable Queuing

As shown, maximum queues were always well within available storage in the left turn lane on the westbound W. Lathrop Road approach to the I-5 Southbound On Ramp. Also, queues on the northbound Old Harlan Road approach to W. Lathrop Road were limited, ranging from 1 to 2 vehicles during any 15 -minute period.

## Unacceptable Queuing

Table 4 shows that at the W. Lathrop Road/Harlan Road intersection the left turn lane on the northbound Harlan Road approach to W. Lathrop Road had a maximum queue demand exceeding the available 235 foot left turn lane storage length during all 15 -minute periods from 3:00 to 6:00 PM, and all but one 15-minute period from 7:00 to 9:00 AM. On the eastbound W. Lathrop Road approach to Harlan Road the maximum queue demand for the 320 foot left turn lane exceeded or met available storage for all but two 15 -minute time periods between 3:00 and 6:00 PM, while there was only one 15-minute period from 7:00 to 9:00 PM where demand met or exceeded storage. The W. Lathrop Road through and through/right turn lane queues on the eastbound approach to Harlan Road backed up to and through the Old Harlan Road intersection about half the time during the 3:00 to 6:00 PM period, but not at all from 7:00 to 9:00 AM. (See Figure 7) It should be noted that the "Maximum" queues described above were usually longer than the " $95^{\text {th }}$ percentile" queues used for evaluation purposes.

## 5. INTERSECTION SIGNAL WARRANT EVALUATION

## a. Analysis Methodology

Traffic signals are used to provide an orderly flow of traffic through an intersection. Many times they are needed to offer side street traffic an opportunity to access a major road where high volumes and/or high vehicle speeds block crossing or turn movements. They do not, however, increase the capacity of an intersection (i.e., increase the overall intersection's ability to accommodate additional vehicles) and, in fact, often slightly reduce the number of total vehicles that can pass through an intersection in a given period of time. Signals can also cause an increase in traffic accidents if installed at inappropriate locations.

There are 10 possible tests for determining whether a traffic signal should be considered for installation. These tests, called "warrants", consider criteria such as actual traffic volume, pedestrian volume, presence of school children, and accident history. The intersection volume data together with the available collision histories were compared to warrants contained in the Manual on Uniform Traffic Control Devices (MUTCD), Federal Highway Administration,

2012, and the Manual on Unified Traffic Control Devices Federal Highway Administration, 2003 California Supplement (2014) Revision 3, which has been adopted by the State of California as a replacement for Caltrans Traffic Manual. Section 4C of the MUTCD provides guidelines, or warrants, which may indicate need for a traffic signal at an unsignalized intersection. As indicated in the MUTCD, satisfaction of one or more warrants does not necessarily require immediate installation of a traffic signal. It is merely an indication that the local jurisdiction should begin monitoring conditions at that location and that a signal may ultimately be required.

Warrant 3, the peak hour volume warrant, is often used as an initial check of signalization needs since peak hour volume data is typically available and this warrant is usually the first one to be met. Warrant 3 is based on a logarithmic curve and takes only the hour with the highest volume of the day into account. Please see Appendix $\mathbf{C}$ for the warrant chart.

## b. Existing Warrant Evaluation

- Table 5 shows that existing AM and PM peak hour volumes at the unsignalized Harlan Road/Old Harlan Road intersection do not meet Caltrans Signal Warrant \#3 volume criteria levels.


## 6. TRANSIT SERVICE

There are two San Joaquin Regional Transit Routes serving the project area:
Route 90 running along W. Lathrop Road and Route 97 running along Harlan Road.
(See Figure 8.) Each route is briefly detailed below.
Route 90 - Runs between Stockton and Tracy
Monday to Friday
Bus stops - Eastbound: east of Harlan Road at Cambridge Drive

- Westbound: just west of Harlan Road

Route 97 - Runs between Stockton and Tracy
Monday to Friday
Bus stops - Northbound: just north of W. Lathrop Road

- Southbound: just south of W. Lathrop Road

There are sidewalks at each transit stop, but no shelters. Also, there is no existing sidewalk system in place along the south side of W. Lathrop Road connecting the bus stops to Old Harlan Road.

## 7. PEDESTRIAN \& BICYCLE FACILITIES

## a. Pedestrian

Sidewalks are in place in the project area along the following streets (see Figure 9):

- Old Harlan Road west side - adjacent to the project site
- Old Harlan Road east side - adjacent to the Burger King - O'Reilly Auto Property
- Harlan Road (south of W. Lathrop Road) west side - adjacent to the Burger King O'Reilly Auto Property north to W. Lathrop Road
- Harlan Road (south of W. Lathrop Road) east side - continuous
- W. Lathrop Road north side - continuous from Harlan Road west through the I-5 interchange to Lathrop High School
- W. Lathrop Road south side - from Harlan Road west to the Chevron gas station driveway
Figure 10 shows that the largest number of pedestrians in the project area during both the AM and PM peak hours was along the north side of W. Lathrop Road: up to 20 pedestrians walking westbound during the AM commute peak hour and 16 pedestrians (some westbound and some eastbound) during the PM commute peak hour. There were only 3 pedestrians along the south side of the street - during the PM peak hour. Along Old Harlan Road there were no pedestrians during the AM peak hour and only 2 during the PM peak hour.


## b. Bicycles

There are Class II striped and signed bicycle lanes along both sides of Harlan Road just north and south of W. Lathrop Road. The southbound bicycle lane along the west side of the street ends several hundred feet south of W. Lathrop Road. There are no bicycle lanes along either W. Lathrop Road or Old Harlan Road (see Figure 9).

Figure 11 shows that along W. Lathrop Road at Old Harlan Road the number of bike riders was 8 during the AM peak hour and 2 during the PM peak hour, while along Harlan Road at Old Harlan Road the number of bike riders was 0 during the AM peak hour and 5 during the PM peak hour. There were no bike riders along Old Harlan Road during the AM peak hour and 5 during the PM peak hour.

## B. CUMULATIVE (WITHOUT PROJECT) CONDITIONS

## 1. HORIZON YEAR

The cumulative horizon year for project analysis in this study as directed by City staff was 2022.

## 2. CUMULATIVE (WITHOUT PROJECT) PEAK HOUR VOLUMES

The source of cumulative weekday AM and PM peak hour (without project) volumes was the 2018 TMP study for the City of Lathrop by Crane Transportation Group, which developed volume projections for the years 2020 and 2022. At City direction year 2022 projections were used as the cumulative horizon for this study. Figures 12 and 13 present resultant cumulative (without project) weekday AM and PM peak hour volumes.

## 3. CUMULATIVE (WITHOUT PROJECT) YEAR 2022 ROADWAY NETWORK

No circulation system improvements are programmed in the project area by 2022*

## 4. CUMULATIVE (WITHOUT PROJECT) YEAR 2022 INTERSECTION LEVEL OF SERVICE \& DELAY

Table 3 shows that by 2022 all analysis intersections will be operating at acceptable levels of service during both the AM and PM peak traffic hours. The W. Lathrop Road/Harlan Road and W. Lathrop Road/I-5 Northbound Ramps signalized intersections will be operating at an acceptable LOS C during both peak hours, while the I-5 Southbound Ramps signalized intersection will be operating at an acceptable LOS D during the AM peak hour and LOS C during the PM peak hour. At the unsignalized Harlan Road/Old Harlan Road intersection the Old Harlan Road stop sign controlled approach will be operating at an acceptable LOS B during both peak hours.

## 5. CUMULATIVE (WITHOUT PROJECT) 95TH PERCENTILE VEHICLE QUEUING AT THE W. LATHROP ROAD/I-5 INTERCHANGE

Table 6 shows that by 2022, 95th percentile unacceptable queuing at the W. Lathrop Road/Harlan Road intersection in the eastbound approach and northbound approach left turn

[^3]lanes will be further lengthened. In addition, the frequency of the eastbound W. Lathrop Road through and through/right turn lanes backing up to and past Old Harlan Road will be increased during the PM peak hour. Along W. Lathrop Road at the I-5 interchange the 95th percentile queuing in the left turn lane on the westbound approach to the southbound on ramp should be within available storage during both commute peak hours. Also, $95^{\text {th }}$ percentile queues on the northbound Old Harlan Road approach to W. Lathrop Road will increase by 1 vehicle during both peak hours (up to 2 vehicles during the AM peak hour and 3 vehicles during the PM peak hour). See Figure 14.

## 6. CUMULATIVE (WITHOUT PROJECT) SIGNAL WARRANT EVALUATION

Table 5 shows that the unsignalized Harlan Road/Old Harlan Road intersection will not have AM or PM peak hour volumes meeting Caltrans Peak Hour Warrant \#3 volume criteria levels by 2022.

## VI. PROJECT IMPACTS

## A. EVALUATION CRITERIA (as approved by the City Engineer)

The addition of project traffic would result in unacceptable operation if:

## 1. SIGNALIZED OR ALL-WAY-STOP INTERSECTIONS

- Without Project acceptable LOS A, B, C or D operation is degraded to LOS E or F.
or
- Without Project unacceptable LOS E or F operation has vehicle control delay increased by 5 seconds or greater.


## 2. UNSIGNALIZED SIDE STREET STOP SIGN CONTROLLED INTERSECTIONS

- Without Project acceptable LOS A, B, C, D or E operation of the stop sign controlled intersection approach is degraded to LOS F operation and the intersection meets peak hour signal Warrant \#3 volume criteria levels (with the project).
or
- Without Project unacceptable LOS F operation of the stop sign controlled approach has vehicle control delay increased by 5 seconds or greater and the intersection meets peak hour signal Warrant \#3 volume criteria levels (with the project).


## 3. SIGNAL WARRANTS

- Without Project volumes at an unsignalized intersection do not meet Caltrans peak hour Warrant \#3 volume criteria and the addition of project traffic increases volumes to meet Warrant \#3 volume criteria levels.
or
- Without Project volumes at an unsignalized intersection already meet Caltrans peak hour Warrant \#3 volume criteria and the addition of project traffic increases total volumes passing through the intersection by 2 percent or greater.
or
- Without Project peak hour $95^{\text {th }}$ percentile queuing in the lane approaching a stop sign controlled intersection will be increased by 100 feet or more and will likely result in traffic diversion to alternate routes.


## 4. 95TH PERCENTILE VEHICLE QUEUING (BASED UPON SYNCHRO SIMTRAFFIC SOFTWARE)

- Without Project peak hour 95th percentile queuing in the lanes approaching a signalized intersection is less than available storage and the addition of project traffic increases the 95th percentile queue to exceed available storage in one or more of the approach lanes.
or
- Without Project peak hour 95th percentile queuing in one or more of the lanes approaching a signalized intersection is already greater than available storage and the addition of project traffic to the entire intersection increases the 95th percentile queuing in any of the lanes operating unacceptably by greater than 20 feet.


## 5. PEDESTRIAN \& BICYCLE RIDERS

-. The addition of project traffic will result in significant safety impacts to local pedestrian and/or bicycle circulation, or will not provide acceptable on- or off-site pedestrian or bicycle facilities for employees or customers.

## 6. SAFETY

- If, in the opinion of the registered traffic engineer conducting the study, the addition of project traffic or a design feature of the project will result in a significant circulation system safety impact.


## B. PROJECT TRIP GENERATION

## 1. METHODÓLOGY

Trip generation projections were developed individually for the three restaurant facilities. Trip rates for the Panda Express and Sonic restaurants with drive through windows were obtained from the traffic engineering professions standard source of trip rate data, Trip Generation Manual $10^{\text {th }}$ Edition by the Institute of Transportation Engineers (ITE), 2017. Trip rates for Dutch Brothers were obtained based upon trip generation surveys at three existing Dutch Brothers operations in the region: Stockton, Lodi and Oakley. Dutch Brothers trip rate survey results were tabulated and then compared to ITE trip rates for coffee/donut shops with drive through windows (with and without indoor seating). Please see Appendix D for a comparison of trip rates. After review of the findings it was determined in consultation with City staff that the trip rates from the Stockton facility would provide a conservative projection of the trips expected from the
proposed Lathrop facility. It should be noted that the Panda Express restaurant will not be open during the 7-8 AM commute peak traffic hour.

## 2. GROSS TRIP GENERATION VERSUS NET NEW AREA TRAFFIC

Table 7 presents the gross AM and PM peak hour trip generation that would be expected from the Panda Express, Sonic and Dutch Brothers operations. These projections reflect the traffic expected on each facility's driveway. However, they do not reflect existing traffic that each restaurant will attract from the I-5 freeway or from the ambient traffic already traveling along W. Lathrop Road, Harlan Road and Old Harlan Road (passby or diverted link trip capture).

Table 8 presents the percentage of traffic each operation would be expected to capture from the I- 5 freeway versus the local streets. Results were worked out in consultation with City staff. As shown, freeway capture was projected to range from $45 \%$ for Dutch Brothers down to $25 \%$ for Panda Express, while local street system capture was projected to be 30 to $35 \%$ for all three operations. Resultant net new local area traffic then ranged from $20 \%$ for Dutch Brothers up to 45\% for Panda Express.

## 3. VOLUMES

Table 9 presents the sum of gross, captured and net new area traffic from the three restaurants. Results are summarized as follows.

| Project Trip Generation Scenario | TWO WAY TRIPS |  |
| :--- | :---: | :---: |
|  | AM PEAK HOUR | PM PEAK HOUR |
| Gross Trip Generation <br> Trips Captured from I-5 freeway or nearby <br> streets | 201 | 210 |
| Net new trips attracted from remainder of <br> Lathrop or north Manteca | 152 | 142 |

## C. PROJECT TRIP DISTRIBUTION

AM and PM peak hour traffic from each of the three facilities was distributed to the local roadway network as shown in Appendix D, while the total project peak hour traffic increments are presented in Figures 15 and 16 for AM and PM peak hour conditions, respectively. Net new traffic was distributed primarily to/from nearby residential areas, while diverted link trip capture from Harlan Road and W. Lathrop Road favored vehicle flow with ease of access to Old Harlan Road adjacent to the site. Passby capture was just from Old Harlan Road. Distribution of all outbound traffic back to the I-5 freeway or to west of I-5 was assumed via northbound Old Harlan Road to W. Lathrop Road - right tuirn to the eastbound W. Lathrop Road left turn lane at Harlan Road and then a U turn to westbound W. Lathrop Road. This would be the most direct route back to the I-5 interchange and for evaluation purposes would result in the most potentially significant operational impacts.

Figures 17 and 18 present resultant Existing + Project AM and PM peak hour volumes, while Figures 19 and 20 present resultant year 2022 AM and PM peak hour volumes.

## D. EXISTING + PROJECT OFF-SITE TRAFFIC IMPACTS

## IMPACT 1: Intersection Level of Service

Table 3 shows that all analysis intersections would maintain acceptable AM and PM peak hour levels of service with the addition of project traffic. No improvements required.

## IMPACT 2: 95th Percentile Vehicle Queuing

Table 4 shows that the addition of project traffic would result in one queuing impact (see Figure 21):

- The PM peak hour $95^{\text {th }}$ percentile queue on the northbound Old. Harlan Road approach to W. Lathrop Road would be increased by more than 100 feet (up to 120 feet - or 5 vehicles). Minor diversion of some backed up drivers through the Chevron or Burger King-O'Reilly Auto parcels could be possible. Improvements recommended.


## IMPACT 3: Intersection Signal Warrant

Table 5 shows that the addition of project traffic to the Harlan Road/Old Harlan Road intersection would not increase AM or PM peak hour volumes to meet or exceed Caltrans Peak Hour Warrant \#3 volume criteria levels. No improvements required.

## E. CUMULATIVE + PROJECT OFF-SITE TRAFFIC IMPACTS

## IMPACT 4: Intersection Level of Service

Table 3 shows that all analysis intersections would maintain acceptable AM and PM peak hour levels of service with the addition of project traffic. No improvements required.

## IMPACT 5: 95th Percentile Vehicle Queuing

Table 6 shows that the addition of project traffic would result in one queuing impact (see Figure 22):

- The PM peak hour $95^{\text {th }}$ percentile queue on the northbound Old Harlan Road approach to W. Lathrop Road would be increased by more than 100 feet ( 360 feet or 18 vehicles). Major diversion of backed up drivers through the Chevron and Burger King-O'Reilly's Auto parcels would be expected. In addition, some project drivers would travel south on Old Harlan Road and make an illegal left turn to proceed north on Harlan Road to the W. Lathrop Road intersection. Improvements recommended.


## IMPACT 6: Intersection Signal Warrants

Table 5 shows that the addition of project traffic to the Harlan Road/Old Harlan Road intersection would not increase AM or PM peak hour volumes to meet or exceed Caltrans Peak Hour Warrant \#3 volume criteria levels. No improvements required.

## F. NON-TRAFFIC IMPACTS

## IMPACT 7: Transit Impacts

Transit stops for San Joaquin Regional Transit Routes 90 and 97 are located in close proximity to the W. Lathrop Road/Harlan Road intersection. However, while there will be a sidewalk along the project's Old Harlan Road frontage there is no sidewalk extending to the east along the south side of W. Lathrop Road along the Chevron gas station frontage to Old Harlan Road, or a crosswalk across the south leg of Old Harlan Road at its connection to W. Lathrop Road. Therefore, all project transit users would be required to cross Old Harlan Road at a variety of locations and walk through either the Chevron service area or the Burger King parking lot as part of their trip between the project facilities and any of the bus stops. Improvements recommended.

## IMPACT 8: Pedestrian Impacts

A sidewalk will be provided along the project's Old Harlan Road frontage. However, no sidewalk is being provided along the project's W. Lathrop Road frontage. Based upon discussion with City staff it is likely that Lathrop High School students walking along the north side of W. Lathrop Road (where a sidewalk is provided) will patronize one or more of the project facilities, particularly Dutch Brothers and Sonic. Since a crosswalk of W. Lathrop Road nearest the project is at the Harlan Road signal, it is likely that some students will cross W. Lathrop Road at the I-5 Northbound Ramps signalized intersection to the west (where there is no crosswalk) or at Old Harlan Road, where there is also no crosswalk, but a raised median. Crossings at both locations without crosswalks presents safety issues. Also, if a crosswalk is provided at the I-5 Northbound Ramps intersection there will be no sidewalk along the south side of W. Lathrop Road between the Northbound Ramps intersection and Old Harlan Road. In addition, the lack of a sidewalk on the south side of W. Lathrop Road just east of Old Harlan Road (see Transit Impacts above) will force all residents of the neighborhood east of Harlan Road who want to walk to any of the project facilities to use the Chevron service area or Burger King parking lot as travel routes. Improvements recommended.

## IMPACT 9: Bicycle Impacts

Bicycle racks will be provided at each of the three facilities (based upon City code criteria requirements). Bike riders will have access to the partial set of Class II bicycle lanes along Harlan Road via Old Harlan Road (or via the Burger King parking lot). No improvements required.

## IMPACT 10: Dutch Brothers Drive Through Window Queues

Surveys were conducted from 7:00-9:00 AM and 3:00-6:00 PM at three Dutch Brothers operations of drive through window queue lengths. Surveys were conducted for two days each at locations in Stockton, Lodi and Oakley. Appendix E presents detailed survey results. Maximum queues at all three locations never exceeded 13 vehicles from 7:00-9:00 AM, nor 10 vehicles from 3:00-6:00 PM. Based upon the Dutch Brothers site plan for Lathrop (see Figure 23), they will have room for 16 vehicles to queue in their drive through lanes. Therefore, proposed storage should be acceptable. The only minor issue with the Dutch Brothers drive through lanes entrance is that it is much closer to the Sonic driveway along Old Harlan Road than to the Dutch Brothers driveway. It is likely that at least a third of Dutch Brothers customers will use the Sonic driveway for inbound access. There could be intermittent periods from 7:00-9:00 AM when minor congestion could result at the Sonic-Dutch Brothers internal parking lot connection.
Improvements recommended.

## IMPACT 11: Project Internal Circulation

Circulation flow through all three properties meets City code criteria and appears acceptable, with the one exception listed in IMPACT 10 regarding use if the Sonic driveway by many inbound customers to Dutch Brothers. No additional improvements required.

## VII. RECOMMENDED IMPROVEMENTS

## 1. EXISTING WITHOUT PROJECT (City Responsibility)- See Figure 24

- Reconfigure the northbound Harlan Road approach to W. Lathrop Road to provide two exclusive left turn lanes and a combined through/right turn lane.
- Remove the raised island median on Harlan road south of W. Lathrop Road at the entrance to the existing northbound left turn lane. Continue this existing turn lane south to the Burger King-O'Reilly's driveway.
- Extend the length of the left turn lane on the eastbound W. Lathrop Road approach to Harlan Road by at least 75 feet.
- Retime the W. Lathrop Road/Harlan Road signal and coordinate timing with the W. Lathrop Road/Cambridge signal.


## 2. PROJECT (EXISTING AND CUMULATIVE) - See Figure 25

- Realign the Old Harlan Road connection to Harlan Road (just south of the project) about 100 feet to the north and provide two lanes on the Old Harlan Road approach: one for left turns and one for right turns. In conjunction with this measure, restripe the median of Harlan Road just south of the new intersection to provide defined back-to-back left turn lanes - one for northbound left turns into Old Harlan Road, and one for southbound left turns into the driveway providing access into the Lathrop Crossing shopping center on the east side of Harlan Road.
- Provide signs adjacent to the exit lanes at each of the three project driveways showing an arrow pointing to the right and a message stating I-5 access turn right. In conjunction with this measure, also provide a sign on the southbound Old Harlan Road approach to Harlan Road with an arrow pointing left and a message stating I-5 access turn left.
- Provide sidewalks on the south side of W. Lathrop Road extending east and west of Old Harlan Road (from the I-5 Ramps intersection to the Chevron driveway).
- Provide a crosswalk at the W. Lathrop Road/I-5 NB Ramps intersection crossing W. Lathrop Road just east of the intersection. Provide pedestrian walk/don't walk signals in conjunction with the crosswalk.
- In order to ensure that Dutch Brothers customers do not congest the Sonic driveway during peak activity times, it may be necessary for Dutch Brothers to provide moveable orange cones across the internal Dutch Brothers-Sonic parking lots connection.
- Based upon input from Chevron, Burger King or O'Reilly's Auto if there is a perceived use of either property by cut-through traffic from the project:
a. The City shall conduct an independent survey to see the extent of the issue.
b. If there is a problem, the City shall work with one or both property owners to develop measures to further reduce or eliminate cut-through traffic.
c. This survey shall be funded by the project applicant.


## Tables

TABLE 1
SIGNALIZED INTERSECTION LOS CRITERIA

| $\begin{array}{c}\text { Level of } \\ \text { Service }\end{array}$ | Description | $\begin{array}{c}\text { Average Control Delay } \\ \text { (Seconds Per Vehicle) }\end{array}$ |
| :---: | :---: | :---: |
| A | $\begin{array}{c}\text { Operations with very low delay occurring with favorable progression } \\ \text { and/or short cycle lengths. }\end{array}$ | $\leq 10.0$ |
| B | Operations with low delay occurring with good progression and/or |  |
| short cycle lengths. |  |  |$] 10.0$ to 20.0

Source: Year 2017 6th Edition Highway Capacity Mamal (Transportation Research Board).

## TABLE 2

UNSIGNALIZED INTERSECTION LOS CRITERIA

| Level of <br> Service | DESCRIPTION | Average Control Delay <br> (Seconds Per Vehicle) |
| :---: | :---: | :---: |
| A | Little or no delays | $\leq 10.0$ |
| B | Short traffic delays | 10.0 to 15.0 |
| C | Average traffic delays | 15.0 to 25.0 |
| D | Long traffic delays | 25.0 to 35.0 |
| E | Very long traffic delays | 35.0 to 50.0 |
| F | Extreme traffic delays with intersection capacity exceeded <br> (for an all-way stop), or with approach/turn movement <br> capacity exceeded (for a side street stop controlled <br> intersection) | $>50.0$ |

Source: Year 2017 6th Edition Highway Capacity Manual (Transportation Research Board).

TABLE 3

## INTERSECTION LEVEL OF SERVICE WITH AND WITHOUT PROJECT

## EXISTING (YEAR 2019)

| INTERSECTION | AM PEAK HOUR |  | PM PEAK HOUR |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { W/O } \\ \text { PROJECT } \end{gathered}$ | $\begin{gathered} \text { WITH } \\ \text { PROJECT } \end{gathered}$ | $\begin{gathered} \text { W/O } \\ \text { PROJECT } \end{gathered}$ | $\begin{gathered} \text { WITH } \\ \text { PROJECT } \\ \hline \end{gathered}$ |
| W. LATHROP RD/SB I-5 RAMPS | C-34.3 ${ }^{(1)}$ | D-37.3 | C-32.3 | C-32.8 |
| W. LATHROP RD/NB I-5 RAMPS | C-25.7 ${ }^{(1)}$ | C-28.0 | B-16.2 | B-18.8 |
| W. LATHROP RD/HARLAN RD | $\mathrm{C}-23.3{ }^{(1)}$ | C-23.6 | C-25.5 | C-26.1 |
| HARLAN RD/OLD HARLAN RD | B-10.0 ${ }^{(2)}$ | B-10.3 | B-11.3 | B-11.6 |

CUMULATIVE (YEAR 2022)

| INTERSECTION | AM PEAK HOUR |  | PM PEAK HOUR |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { W/O } \\ \text { PROJECT } \end{gathered}$ | $\begin{gathered} \text { WITH } \\ \text { PROJECT } \end{gathered}$ | $\begin{gathered} \text { W/O } \\ \text { PROJECT } \end{gathered}$ | $\begin{gathered} \text { WITH } \\ \text { PROJECT } \end{gathered}$ |
| W. LATHROP RD/SB I-5 RAMPS | D-38.9 ${ }^{(1)}$ | D-41.3 | C-34.4 | D-37.3 |
| W. LATHROP RD/NB I-5 RAMPS | C-30.7 ${ }^{(1)}$ | C-33.4 | C-31.8 | C-34.7 |
| W. LATHROP RD/HARLAN RD | C-25.2 ${ }^{(1)}$ | C-25.5 | C-29.3 | C-30.3 |
| HARLAN RD/OLD HARLAN RD | B-10.3 ${ }^{(2)}$ | B-10.5 | B-11.9 | B-12.3 |

Signalized level of service - control delay in seconds.
Side street stop sign control - NB right turn level of service/delay in seconds.

- Year 2017 6th Edition Highway Capacity Manual (Transportation Research Board) Methodology
- Synchro Level of Service software

[^4]TABLE 4

## EXISTING 95 ${ }^{\text {TH }}$ PERCENTILE TURN LANE QUEUING* WITH \& WITHOUT PROJECT

| LOCATION | QUEUE (in Feet) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
|  | W/O PROJECT (Field Surveyed) |  | $\begin{gathered} \text { WITH } \\ \text { PROJECT } \\ \hline \end{gathered}$ | W/O PROJECT (Field Surveyed) |  | $\begin{gathered} \text { WITH } \\ \text { PROJECT } \end{gathered}$ |
| W. LATHROP RD/HARLAN RD |  |  |  |  |  |  |
| EBL | 260 | $(320)^{(1)}$ | 280 | 340 | $(320)^{(1)}$ | 360 |
| EBT | 160 | (330-530) ${ }^{(2)}$ | 180 | 480 | $(330-530)^{(2)}$ | 500 |
| NBL | 320 | $(235)^{(1)}$. | 320 | 340 | (235) ${ }^{(1)}$ | 340 |
| NBT | 160 |  | 160 | 200 |  | 200 |
| W.LATHROP/OLD HARLAN RD | 20 |  | 60 | 40 |  | 160** |
| NBR |  |  |  |  |  |  |
| W.LATHROP RD/I-5 SB RAMPS | 180 | $(420)^{(1)}$ | 200 | 240 | $(420)^{(1)}$ | 260 |
| WBL |  |  |  |  |  |  |

* Queuing results broken down into 20 -foot segments.
** Theoretical result only. Assumes all NB vehicles on Old Harlan Rd wait to turn right at W. Lathrop Rd. It is likely some vehicles in this queue will use the Chevron and Burger King parking service aisles to access Harlan Rd and W. Lathrop Rd.
(1) $=(320)=$ Storage distance (feet).
${ }^{(2)}=(330-530)=$ Storage length to Old Harlan Rd/I-5 NB Ramps.
Synchro software queuing results for + project conditions.
Source: Field Surveys under direction of Crane Transportation Group Wednesday October 3, 2019.
Compiled by Crane Transportation Group

TABLE 5
INTERSECTION SIGNAL WARRANT EVALUATION
(Do Volumes Meet Caltrans Warrant \#3 Volume Criteria Levels?)

Harlan Road/Old Harlan Road
(South of W. Lathrop Road)

EXISTING (2019)

| AM PEAK HOUR |  | PM PEAK HOUR |  |
| :---: | :---: | :---: | :---: |
| WITHOUT <br> PROJECT | WITH PROJECT | WITHOUT <br> PROJECT | WITH PROJECT |
| NO | NO | NO | NO |

CUMULATIVE (2022)


TABLE 6

## CUMULATIVE YEAR 2022 95 ${ }^{\text {TH }}$ PERCENTILE TURN LANE QUEUING WITH \& WITHOUT PROJECT

| LOCATION | QUEUE (in Feet) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
|  | W/O PROJECT <br> (Field Surveyed) |  | $\begin{gathered} \text { WITH } \\ \text { PROJECT } \end{gathered}$ | W/O PROJECT <br> (Field Surveyed) |  | $\begin{gathered} \text { WITH } \\ \text { PROJECT } \end{gathered}$ |
| W. LATHROP RD/HARLAN RD |  |  |  |  |  |  |
| EBL | 280 | $(320)^{(1)}$ | 300 | 400 | $(320)^{(1)}$ | 400 |
| EBT | 220 | (330-530) ${ }^{(2)}$ | 240 | 580 | $(330-530)^{(2)}$ | 580 |
| NBL |  | $(235)^{(1)}$ | 340 | 340 | $(235)^{(1)}$ | 340 |
| NBT | 180 |  | 180 | 240 |  | 240 |
| W.LATHROP/OLD HARLAN RD | 40 |  | 80 | 60 |  | 60 |
| NBR | 40 |  |  |  |  |  |
| W.LATHROP RD/I-5 SB RAMPS | 180 | $(420)^{(1)}$ | 200 | 240 | $(420)^{(1)}$ | 240 |
| WBL |  |  |  |  |  |  |

* Queuing results broken down into 20 -foot segments.
** Theoretical result only. Assumes all NB vehicles on Old Harlan Rd wait to turn right at W. Lathrop Rd. It is likely some vehicles in this queue will use the Chevron and Burger King parking service aisles to access Harlan Rd and W. Lathrop Rd.
(1) $=(320)=$ Storage distance (feet).
(2) $=(330-530)=$ Storage length to Old Harlan Rd/I-5 NB Ramps.

Synchro software queuing results for + project conditions.
Source: Field Surveys under direction of Crane Transportation Group Wednesday October 3, 2019.
Compiled by Crane Transportation Group

## TABLE 7

## Project Gross Trip Generation

## DUTCH BROTHERS <br> (With Drive Through)

| $\begin{gathered} \text { SIZE } \\ \text { (Square Ft) } \end{gathered}$ | AM PEAK HOUR TRIPS |  |  |  | PM PEAK HOUR TRIPS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IN |  | OUT |  | IN |  | OUT |  |
|  | Rate/ <br> Sq Ft | Vol | Rate/ <br> Sq Ft | Vol | Rate/ Sq Ft | Vol | Rate/ <br> $\mathbf{S q} \mathbf{F t}$ | Vol |
| 862 | 77.8 | 67 | 77.8 | 67 | 48.2 | 42 | 48.2 | 42 |

PANDA EXPRESS
(With Drive Through)

| $*$ <br> SIZE <br> (Square Ft) | AM PEAK HOUR TRIPS |  |  | PM PEAK HOUR TRIPS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IN |  | OUT |  | IN |  | OUT |  |
|  | Rate/ <br> Sq Ft | Vol | Rate/ <br> Sq Ft | Vol | Rate/ <br> Sq Ft | Vol | Rate/ <br> Sq Ft | Vol |
| 2200 | N/A* | 2 | N/A* | 0 | 17.0 | 38 | 15.67 | 35 |

*Not open for breakfast

## SONIC

(With Drive Through)

| $\begin{gathered} \text { SIZE } \\ \text { (Square Ft) } \end{gathered}$ | AM PEAK HOUR TRIPS |  |  |  | PM PEAK HOUR TRIPS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IN |  | OUT |  | IN |  | OUT |  |
|  | Rate/ Sq Ft | Vol | $\begin{gathered} \text { Rate/ } \\ \text { Sq Ft } \\ \hline \end{gathered}$ | Vol | Rate/ Sq Ft | VoI | Rate/ Sq Ft | VoI |
| 1608 | 20.5 | 33 | 19.7 | 32 | 17.0 | 28 | 15.67 | 25 |

Trip Rate Source for Dutch Brothers: Surveys of Existing Dutch Brothers operations in Stockton and Lodi, California. - See Appendix E.

Trip Rate Source for Panda Express and Sonic: Trip Generation Manual 10th Edition by the Institute of Transportation Engineers, 2017.

Compiled by: Crane Transportation Group

## TABLE 8

## Project Passby and Diverted Link Trip Capture

|  | I-5 Freeway <br> Diverted Trips | Local Street System <br>  <br> Diverted Link Trips | Primary Trips |
| :---: | :---: | :---: | :---: |
| Dutch Brothers | $45 \%$ | $35 \%$ | $20 \%$ |
| Panda Express | $25 \%$ | $30 \%$ | $45 \%$ |
| Sonic | $35 \%$ | $30 \%$ | $35 \%$ |

Sources: Trip Generation Handbook by the Institute of Transportation Engineers 2017
Lathrop City Staff
Crane Transportation Group

TABLE 9
(3 Facilities)

# Total Project Gross Trip Generation 

Total of Inbound and Outbound Trips on 3 Project Driveways


Total Project Trips Attracted from Freeway or Ambient Traffic on nearby streets

| AM PEAK HOUR TRIPS |  |  | PM PEAK HOUR TRIPS |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| IN | OUT | Total <br> 2 way | IN | OUT | TotaI <br> 2 way |
| 77 | 75 | 150 | 73 | 69 | 142 |

Net new Project Trips being Attracted to Development Area from other section of Lathrop or Manteca

| AM PEAK HOUR TRIPS |  |  | PM PEAK HOUR TRIPS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IN | OUT | Total <br> 2 way | IN | OUT | Total <br> 2 way |  |
| 25 | 24 | 49 | 35 | 33 | 68 |  |

## Figures




Figure 2

CFT LATHROP - PHASE II


Figure 3


Figure 4
Existing Intersection Approach Lane


Figure 5
Existing AM Peak Hour Volumes (without Project) Thursday October 3, 2019-7:00-8:00 AM


Figure 6


Figure 7
Existing (without Project) 95th\% Queues Exceeding Storage


Figure 8
Transit Routes in Vicinity of Project Site


Figure 9
Existing Sidewalks and Bicycle Lanes and Those Proposed by Project


Figure 10


Figure 11


Figure 12


Figure 13
Cumulative (Year 2022)
Weekday PM Peak Hour Volumes (without Project)


Figure 14


Figure 15
Project Traffic Increment (AM Peak Hour)


Figure 16
Project Traffic Increment (PM Peak Hour)


Figure 17


Figure 18


Figure 19


Figure 20
Cumulative (Year 2022)
Weekday PM Peak Hour Volumes (with Project)


Figure 21
Existing + Project 95th\% Queues Exceeding Storage


Figure 22


Figure 23
Dutch Brothers Drive Thru Queueing


Figure 24
Existing and Cumulative (Year 2022) Recommended Improvements (without Project)


Figure 25
$:$

## Appendices

## Appendix D

## Dutch Brothers Trip Rates

## Appendix D

Trip Rates

## Dutch Brothers Survey Locations near Lathrop

versus
Institute of Transportation Engineers Trip Generation Manual

| Survey Locations | Size of Facility (Square Ft) | AM PEAK HOUR TRIPS |  |  |  | PM PEAK HOUR TRIPS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | IN |  | OUT |  | IN |  | OUT |  |
|  |  | Trips | $\begin{array}{\|l} \hline \text { Rate/ } \\ 1000 \\ \text { Sq Ft } \\ \hline \end{array}$ | Trips | Rate/ 1000 $\mathrm{Sq} \mathbf{F t}$ | Trips | Rate/ 1000 <br> Sq Ft | Trips | $\begin{gathered} \hline \text { Rate } / \\ 1000 \\ \text { Sq Ft } \\ \hline \end{gathered}$ |
| Stockton | 810 | 63 | 77.8 | 57 | 70.4 | 31 | 38.3 | 39 | 48.2 |
| Lodi | 1500 | 48 | 32 | 51 | 34 | 29 | 19.3 | 36 | 24.0 |
| Oakley | 295 | 38 | 128.8 | 32 | 108.5 | 49 | 166.1 | 43 | 145.8 |
| Average of 3 Survey Locations |  |  | 79.5 |  | 71.0 |  | 74.6 |  | 72.7 |
| ITE RATE (1) Coffee/Donut Shop + Drive through window with indoor seating | N/A | N/A | 45.4 | N/A | 43.6 | N/A | 21.7 | N/A | 21.7 |
| ITE RATE (1) Coffee/Donut Shop + Drive through window without indoor seating | N/A | N/A | 168.5 | N/A | 168.5 | N/A | 41.7 | N/A | 41.7 |

Trip Rates: Dutch Brothers Surveys - Crane Transportation Group
I.T.E. - Trip Generation Manual $10^{\text {th }}$ Edition by the Institute of Transportation Engineers, 2017

## Appendix E

# Dutch Brothers Drive Through Lane Queue <br> Count Summaries <br> (Stockton, Lodi \& Oakley) 

Table E1
Dutch Brothers Queue Comparison
Lodi, Oakley and Stockton AM and PM Peak Periods
Thursday Oct 3, 2019


[^5]| Lodi, CA |  | Oakley, CA | Stockton, CA |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1- N/O Side | 2-5/0 Side |
| Time: | Max Queue | Max Queue | Max Queue | Max Queue |
| 3:05 PM | 2 | 6 | 2 | 2 |
| 3:10 PM | 2 | 9 | 0 | 3 |
| 3:15 PM | 1 | 7 | 0 | 3 |
| 3:20 PM | 2 | 8 | 3 | 2 |
| 3:25 PM | 3 | 7 | 1 | 2 |
| 3:30 PM | 2 | 8 | 7 | 3 |
| 3:35 PM | 3 | 8 | 3 | 3 |
| 3:40 PM | 5 | 6 | 1 | 2 |
| 3:45 PM. | 4 | 7 | 0 | 2 |
| 3:50 PM | 4 | 7 | 0 | 6 |
| 3:55 PM | 2 | 10 | 2 | 4 |
| 4:00 PM | 2 | 9 | 3 | 1 |
| 4:05 PM | 3 | 8 | 2 | 6 |
| 4:10 PM | 1 | 6 | 0 | 3 |
| 4:15 PM | 2 | 4 | 0 | 0 |
| 4:20 PM | 1 | 4 | 2 | 0 |
| 4:25 PM | 3 | 4 | 0 | 0 |
| 4:30 PM | 2 | 4 | 0 | 3 |
| 4:35 PM | 2 | 3 | 0 | 2 |
| 4:40 PM | 3 | 5 | 0 | 3 |
| 4:45 PiN | 2 | 5 | 0 | 2 |
| 4:50 PM | 2 | 5 | 0 | 2 |
| 4:55 PM | 2 | 3 | 0 | 2 |
| 5:00 PM | 6 | 4 | 0 | 0 |
| 5:05 PM | 3 | 2 | 0 | 1 |
| 5:10 PM | 2 | 4 | 0 | 1 |
| 5:15 PM | 3 | 5 | 0 | 2 |
| 5:20 PM | 2 | 7 | 0 | 1 |
| S:25 PM | 3 | 8 | 3 | 0 |
| 5:30 PM | 2 | 9 | 0 | 1 |
| 5:35 PM | 2 | 7 | 0 | 0 |
| 5:40 PM | 1 | 6 | 0 | 3 |
| 5:45 PM | 2 | 5 | 0 | 1 |
| 5:50 PM | 2 | 7 | 0 | 1 |
| 5:55 PM | 0 | 7 | 0 | 2 |
| 6:00 PM. | 0 | 4 | 0 | 1 |

## CAR WASH TRIP GENERATION STUDIES

# (1) Stantec 

# Oakland Road Hotel and Car Wash Transportation Analysis Report 

City of San Jose

May 22, 2019

Prepared for:
Blue Wave Express Car Wash

Prepared by:
Stantec Consulting Services Inc.

## Sign-off Sheet

This document entitled Oakland Road Hotel and Car Wash Transportation Analysis Report was prepared by Stantec Consulting Services Inc. ("Stantec") for the account of Blue Wave Express Car Wash (the "Client").

(signature)
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## Executive Summary

This transportation analysis has been prepared for the proposed Oakland Road hotel and Blue Wave car wash located on Oakland Road in the City of San Jose. A transportation analysis is required for this project in compliance with the City of San Jose's Transportation Impact Policy (Council Policy 5-1) and the Santa Clara County's Congestion Management Program (CMP). The analysis has been prepared in conformance with the requirements contained in the City's Transportation Analysis Handbook (2018).

The project site is located at the southwest corner of Oakland Road and Horning Street. The existing site is located on four separate parcels, which are to be combined and divided into two new parcels for the development of a 116-room business hotel on the north parcel (approximately 1.8 acres) and a drive-through car wash on the south parcel (approximately 0.8 acres). The car wash site also includes self-serve vacuum stalls and associated site improvements. A shared access drive aisle is to be constructed from Oakland Road for access to both proposed sites. A driveway is also proposed on Horning Street.

Project trips were calculated based on ITE trip rates and an existing car wash case study driveway count. Location based reduction for Suburban with Multifamily Housing area was applied to the hotel component of the project. Furthermore, trips generated by the existing development on the site were subtracted from the project trip generation to obtain net new project vehicle trips. A reduction for car wash pass-by trips was not taken, which results in a conservatively high trip generation estimate. The proposed project will generate 45 new vehicle trips during the AM peak hour, 62 new vehicle trips during the PM peak hour, and 723 new vehicle trips daily.

The proposed land uses cannot be evaluated with the City's VMT Evaluation Tool or with the Travel Demand Model because hotel does not fall into one of the designated land use categories. Therefore, the proposed hotel and car wash project trip generation estimates were converted to an equivalent amount of retail square footage based on the daily trips. The resulting retail square footage was compared with the CEQA VMT Analysis Screening Criteria in the Transportation Handbook 2018 to determine conformance to Council Policy 5-1. Based on the daily baseline vehicle trip generation for the proposed project, the project is equivalent to 38,000 square feet of retail uses, which exempts the project from a detailed CEQA VMT analysis per the small infill screening criteria of 100,000 square feet or less of retail space. The project site is located within two miles of the Mineta San Jose Airport, Civic Center, and Downtown San Jose. These local facilities will attract a large portion of the proposed business hotel trips. Furthermore, the proposed hotel will increase employment density (jobs/commercial acres in half-mile buffer), resulting in a lower VMT for the project than the existing VMT for the area. Additionally, motorists will choose a car wash that is convenient rather than drive miles out of their way to a car wash. If the proposed car wash is more convenient than an existing car wash, then motorists will divert existing car wash trips to the proposed car wash. Furthermore, the majority of car wash trips would be pass-by or diverted trips where the motorist stops at the car wash on their way to another destination.

The net new project trips were distributed to the surrounding street network based on levels and locations of development in relation to the project site. Separate distribution patterns for the business hotel and car wash were developed. The business hotel trips were primarily distributed to the Mineta San Jose Airport, Civic Center, and Downtown San Jose, while the car wash trips were distributed to surrounding residential and commercial areas.

The study area was defined and approved by City staff, and five signalized intersections and two stop-controlled intersections in proximity of the project site were identified as the study intersections. Peak hour turning movement counts were collected in July and September 2018 at the study intersections.

Background conditions were developed by adding trips from approved but not yet constructed projects in the City's ATI database to the existing intersection volumes. These background volumes provide the conditions against which the project impacts are evaluated.

The net new project vehicle-trips were added to the background volumes. The delay and LOS for background plus project conditions were compared with the background delay and LOS. Three study intersections operate at deficient LOS under background conditions; however, the project has no adverse effect on these or any of the study intersections.

The City adopted the US-101/Oakland Road/Mabury Road Transportation Development Policy (TDP) in 2007 which defines the interchange capacity available, identifies the required improvements for future development in the area, establishes a traffic fee program for new development in the area to fund the improvements, and allows the LOS of signalized intersections covered by the TDP to temporarily exceed the City's LOS standards until the required improvements are constructed. Major regional transportation projects that are recognized as necessary to provide adequate access to the US 101 freeway and the planned BART station include modification of the US 101/Oakland Road interchange and construction of the US 101/Mabury Road interchange. The City Council established a Traffic Impact Fee program to cover the unfunded cost of the Planned Improvements. Based on the trip distribution and assignment, the project adds 14 PM peak hour trips to the Oakland Road/US 101 interchange. This volume of project trips could be reduced if the business hotel were to provide a shuttle service for guests to and from destinations such as the airport.

The project entrance on Oakland Road opposite Boardwalk Way is proposed to be signalized. The raised median would be modified, and the existing residential development on the east side of Oakland Road (Modern Ice Townhomes) would be given full access to Oakland Road. This location would operate at LOS F without a signal. With a signal, the intersection operates at LOS B during the AM and PM peak hours. A signal and median break at this location would provide pedestrian connectivity between the residential uses on the east side and the commercial uses on the west side of Oakland Road and a controlled crossing of Oakland Road for bicyclists.

The project has no adverse effect on the surrounding streets and no off-site mitigation is necessary.

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### 1.0 INIRODUCTION

This transportation analysis has been prepared for the proposed Oakland Road hotel and Blue Wave car wash located on Oakland Road in the City of San Jose. A transportation analysis is required for this project in compliance with the City of San Jose's Transportation Analysis Policy (Council Policy 5-1) and the Santa Clara County's Congestion Management Program (CMP). The analysis has been prepared in conformance with the requirements contained in the City's Transportation Analysis Handbook (2018). This report summarizes the project's potential transportation impacts, if any, and presents appropriate mitigation measures, if necessary.

### 1.1 PROJ ECTDESCRIPIION

The project site is located on the west side of Oakland Road between Horning Street and Madera Avenue.
Figure 1-1 illustrates the location of the project site. The existing site is located on four separate parcels, which are to be combined and divided into two new parcels for the development of a 116-room business hotel on the north parcel (approximately 1.8 acres) and an automated drive-through car wash on the south parcel (approximately 0.8 acres). The car wash site also includes self-serve vacuum stalls and associated site improvements. A shared access drive aisle is to be constructed from Oakland Road for access to both proposed sites. This driveway is opposite Boardwalk Way, and the existing median break is proposed to be modified to provide full access to the project driveway, as well as Boardwalk Way, from Oakland Road. A traffic signal at this location has been evaluated. A driveway is also proposed on Horning Street. Figure 1-2 illustrates the proposed site plan.

The project site is currently developed with permitted auto-related businesses such as a tire and wheel shop, truck and car wash, and graphic design/car wrap business.

### 1.2 CEQA TRANSPORIATION ANALYSIS SCOPE

Council Policy 5-1 aligns with California Senate Bill 743 (SB 743) that establishes the thresholds for transportation impacts under the California Environmental Quality Act (CEQA), removing transportation "Level of Service" (LOS) based on delay and congestion and replacing it with "Vehicle-Miles Traveled" (VMT). VMT refers to the amount of and distance of automobile travel in a day attributed to a development project. VMT is measured by multiplying the total vehicle trips generated by a development project by the average distance of those trips. In the City of San Jose, VMT is calculated using the Origin-Destination VMT method, which measures the full distance of vehicle travel with one end within the project.

Increased vehicle travel associated with development projects results in several undesirable consequences. Increased vehicle travel leads to increased greenhouse gases and poor air quality, leads to health issues such as chronic diseases (associated with poor air quality and reduced physical activity) and worse mental health, has negative effects on other road users such as pedestrians, cyclists, and transit users, results in more vehicle collisions, requires more infrastructure which increases impermeable surfaces (raising flood risks and polluting waterways) and loss of natural habitat, and increases interactions with nature leading to more collisions with wildlife. SB 743 attempts to diminish these undesirable outcomes by encouraging development that reduces vehicle travel.

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Figure 1-1
ProjectSite Location


Figure 1-2

## OAKLAND ROAD HOTEL AND CAR WASH TRANSPORTATION ANALYSIS REPORT

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The intention of SB 743 is to "promote the reduction of greenhouse gas emissions, the development of multimodal transportation networks, and a diversity of land uses." VMT exceeding an applicable threshold of significance may indicate a significant impact. If a project is found to have a significant impact on VMT, the impact must be reduced by modifying the project VMT to an acceptable level and/or mitigating the impact through multimodal transportation improvements or establishing a Trip Cap.

A project could have a significant transportation impact on the environment if it:
a) Conflicts with a plan, ordinance, or policy addressing the circulation system, including transit, roadways, bicycle lanes, and pedestrian paths
b) Conflicts or is inconsistent with CEQA Guidelines Section 15064.2, Subdivision (b)(1)
c) Substantially increases hazards due to a geometric design feature or incompatible use
d) Results in inadequate emergency access.

The City has chosen a net increase in the total existing VMT for the region (i.e. the Bay Area's Metropolitan Planning Organization's boundaries) as the determination of significant transportation impact. For development projects that do not meet the City's screening criteria, the VMT analysis consists of a comparison of the project's potential impacts related to VMT and other significance criteria. For retail, hotel, or school projects, the total VMT for the region without and with the project is calculated. The threshold for significance for retail projects is a net increase in the existing regional total VMT.

A detailed CEQA transportation analysis is not required if a project meets the City's screening criteria. New retail development typically redistributes existing trips instead of creating new trips. Local-serving retail projects may shorten vehicle-trips and reduce VMT by diverting trips from existing local retail to new local retail without measurably increasing trips outside the local area. The City has defined retail projects below 100,000 square feet as local-serving shopping centers. Therefore, it is presumed that retail projects no larger than 100,000 square feet will have a less than significant VMT impact and do not require a detailed CEQA transportation analysis.

As City staff outlined in the workscope letter for this project dated May 17, 2018, the proposed land uses cannot be evaluated with the City's VMT Evaluation Tool or with the Travel Demand Model. The VMT Evaluation Tool has four categories of land uses (Residential, Office, Retail, and Industrial), and hotel does not fall into any of the designated land use categories. Therefore, both the business hotel and the car wash require a qualitative evaluation and comparison to retail land uses as defined in Council Policy 5-1. The proposed hotel and car wash project trip generation estimates are converted to an equivalent amount of retail square footage based on the daily trips. The resulting retail square footage is compared with the CEQA VMT Analysis Screening Criteria in the Transportation Handbook 2018 to determine conformance to Council Policy 5-1 for the proposed 116-room hotel and automated car wash.

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### 1.3 LOCAL TRANSPORIATION ANALYSIS SCOPE

The project is subject to the City's Local Transportation Analysis (LTA) as specified in the Council Policy 5-1 and must comply with methodology included in the City's Transportation Analysis Handbook. The project's effects on transportation, access, circulation, and related safety elements in the proximate area of the project are evaluated. The traffic study provides near term impact analysis of the proposed project as required by the City. The analysis will address project impacts compared with the background no-project scenario.

Seven study intersections have been identified by Public Works staff, and the project's effects on the operation of these study intersections were evaluated under background conditions. Five of the study intersections are controlled by traffic signals, and the remaining two study intersections are two-way stop-controlled T-intersections, although both stop-controlled intersections are restricted to right turns only because of the raised median along Oakland Road.

The following intersections are included in the analysis:

| $\frac{\text { Intersection }}{}$ | Control | Jurisdiction |
| :--- | :---: | :---: |
| 1. Oakland Road \& Mabury Road | Two-Way Stop Sign | San Jose |
| 2. Oakland Road \& US 101 NB | Signal | San Jose/Caltrans |
| 3. Oakland Road \& US 101 SB | Signal | San Jose/Caltrans |
| 4. Oakland Road \& Horning Street | Two-Way Stop Sign | San Jose |
| 5. Oakland Road \& Hedding Street | Signal | San Jose |
| 6. 11th Street \& Hedding Street | Signal | San Jose |
| 7. 10th Street \& Hedding Street | Signal | San Jose |

The US 101 interchange study intersections are identified on the CMP network. They are outside of an Infill Opportunity Zone (IOZ).

The project site is designated as Combined Industrial/Commercial (CIC) in the City's Envision San Jose 2040 General Plan (February 2018). Hotel is a permitted use in CIC, and car wash is a conditional permit use. The project is consistent with the current General Plan; therefore, a General Plan Amendment (GPA) long-range transportation analysis is not required.

The project site is located south of the US 101 interchange at Oakland Road. The interchange is the subject of the City's adopted US 101/Oakland Road/Mabury Road Transportation Development Policy (TDP) which recognizes that the interchange is severely constrained and establishes a mitigation program for impacts to the US 101/Oakland Road interchange.

Two study intersections (Oakland Road/US 101 NB ramps and Oakland Road/US 101 SB ramps) are identified as Congestion Management Program (CMP) monitoring locations. An analysis based on the VTA CMP guidelines was not prepared since the proposed project generates less than 100 net new peak hour vehicle trips; however, the City's guidelines are intended to be consistent with the VTA Transportation Impact Analysis Guidelines, to promote consistency across jurisdictions within Santa Clara County.

The following scenarios are evaluated:

- Existing Scenario: Existing LOS
- Background Scenario: Existing + Approved Projects LOS
- Background Plus Project Scenario: Existing + Approved Projects + Proposed Project LOS


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Project level of service and potential negative project effects are based on Highway Capacity Manual (HCM) delay methodology. Table 1-1 summarizes the correspondence between LOS and average vehicle delay. Traffix software is utilized to calculate the vehicle delay at the study intersections. An adverse effect on intersection operations occurs when the analysis demonstrates that the project causes the operations standard at a study intersection to fall below LOS D with the addition of project vehicle-trips to baseline conditions. For intersections already operating at LOS E or F under background conditions, the criteria for determining adverse intersection operations from the project impact is:

- An increase in average critical delay by 4.0 seconds or more AND an increase in the critical V/C ratio of 0.010 or more; OR
- A decrease in the average critical delay AND an increase in critical V/C ratio of 0.010 or more.

It should be noted that a potential adverse effect is not a CEQA measure.

### 1.4 REPORTORGANIZATION

Chapter 2.0 of this report provides the transportation setting for the impact analysis, including existing roadway conditions, peak hour and daily traffic volumes, pedestrian, bicycle, and transit facilities, and traffic conditions field observations. Chapter 3.0 describes the CEQA conditions. Chapter 4.0 focuses on the LTA and potential traffic impacts of the proposed project under near term conditions, with project trip generation, distribution, and assignment presented in this chapter. Sections presenting additional site analyses and operational effects are included in Chapter 4.0. Chapter 5.0 summarizes the conclusions of the transportation analysis.

Introduction
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Table 1-1 Intersection Level of Service Ranges


### 2.0 EXISTING TRANSPORTATION CONDIIIONS

This chapter describes the transportation setting for the proposed project. The existing roadway network, intersection conditions, and existing traffic volumes are presented.

### 2.1 VEHICLE-MILES TRAVELED

From the Transportation Analysis Handbook, VMT is the total miles of travel by personal motorized vehicles a project is expected to generate in a day. VMT is calculated using the Origin-Destination VMT method, which measures the full distance of personal motorized vehicle-trips with one end within the project. VMT that promotes the reduction of greenhouse gas emissions, the development of multimodal transportation networks, and a diversity of land uses shall be used as a basis for determining significant transportation impacts in California to appropriately balance the needs of congestion management with statewide goals related to infill development, the promotion of public health through active transportation, and the reduction of greenhouse gas emissions.

The City uses an Excel-based VMT Evaluation Tool to evaluate whether proposed development projects would generate VMT impacts. The VMT for the half-mile radius surrounding the project site is based on the City's travel demand model and adjusted to the parcel level.

The City's VMT Evaluation Tool was used to determine the existing VMT for the study area. The VMT for the area is 15.43 per non-industrial worker. This is above the City's threshold of 12.22 per worker. The half-mile radius area around the project site includes residential developments and mostly industrial space. The VMT for the area is higher than the City's threshold since the workers in the area may not live in the surrounding residential developments and have to drive farther to home than the City's threshold.

Figure 2-1 illustrates the VMT per capita heat map for a one-half mile radius around the project site. This shows that the majority of the area surrounding the project site is classified as Regional Average VMT Areas.

### 2.2 ROADWAY NEIWORK

The project is located on the west side of Oakland Road between Horning Road and Madera Avenue. Project traffic will access the local transportation network via Oakland Road, Hedding Street, and Horning Street. Regional access to the study area will be provided primarily by US 101. None of the streets in the study area are identified as a Vision Zero Priority Safety Corridor. The study area is identified as a Suburban with Multifamily Housing place type.

Figure 2-2 illustrates the surrounding street network and shows the existing lane configurations at the study intersections.

Oakland Road is a six-lane road north of the study area which narrows to five lanes for a short distance north of Commercial Street. South of Commercial Street, Oakland Road is a four-lane road with a raised median and left- and right-turn pockets at the US 101 interchange and at Hedding Street. The raised median restricts traffic at Mabury


Figure 2-1
City of San J ose VMTper J ob Heat Map


Figure 2-2

## OAKLAND ROAD HOTEL AND CAR WASH TRANSPORTATION ANALYSIS REPORT

## Existing Transportation Conditions

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Road, Horning Street, Madera Avenue, and Berryessa Road to right turns only. A median break at Boardwalk Way allows the southbound left-turn movement onto Boardwalk Way, but westbound traffic from Boardwalk Way onto Oakland Road is restricted to right turns only. South of the study area, Oakland Road becomes N. 13th Street south of Hedding Street. Oakland Road is classified on the City's General Plan Transportation Network as a City Connector Street north of US 101, a Main Street from US 101 to Jackson Street south of the study area, and a Local Connector Street south of Jackson Street. The speed limit on Oakland Road in the project vicinity is 40 mph north of US 101, 35 mph between US 101 and Hedding Street, and 25 mph south of Hedding Street. Signals are provided at US 101 northbound ramps, US 101 southbound ramps, and Hedding Street within the study area and at Commercial Street just north of the study area.

Hedding Street is a two-lane road in the project vicinity with a two-way left-turn painted median and turn pockets at the intersections. Hedding Street is classified as an On-Street Primary Bicycle Facility through the study area, Class II bike lanes are provided. On-street parking is prohibited. The speed limit on Hedding Street in the project vicinity is 30 mph west of Oakland Road and 35 mph east of Oakland Road. The intersections at 10th Street, 11th Street, and Oakland Road in the study area are signalized. Hedding Street crosses train tracks west of 10th Street. The at-grade crossing has flashing warning lights and automatic gates.

10th Street is classified as a City Connector Street north of Madera Avenue and a Local Connector Street south of Madera Avenue. 10th Street is a four-lane undivided street north of Hedding Street. South of Hedding Street, 10th Street is a wide one-way street southbound. The speed limit is 35 mph on 10th Street north of Hedding Street and 30 mph south of Hedding Street. Class II bike lanes are provided on 10th Street north of Hedding Street, but the striping is very faded in places. On-street parking is not allowed.

11th Street is a one-way street northbound that ends at Hedding Street. It is striped with two lanes that widens to three lanes at the intersection with Hedding Street. 11th Street is classified as a Local Connector Street. The speed limit on 11th Street is 30 mph . On-street parking is permitted, and a Class II bike lane is provided northbound

Horning Street is not classified on the City's Transportation Network Diagram. Horning Street begins at 10th Street west of the project site and ends at Oakland Road. It is a wide two-lane street with no centerline stripe. The speed limit is 35 mph and on-street parking is allowed. Horning Street is controlled by a stop sign at the 10th Street and the Oakland Road intersections.

Madera Avenue is not classified on the City's Transportation Network Diagram. Madera Avenue also begins at 10th Street and ends at Oakland Road. Madera Avenue is a two-lane street with a $25-\mathrm{mph}$ speed limit. On-street parking is allowed. Madera Avenue is controlled by a stop sign at the 10th Street and the Oakland Road intersections.

US 101 (Bayshore Freeway) provides regional access to the project vicinity. US 101 is an eight-lane freeway with six general purpose lanes and two high occupancy vehicle (HOV) lanes in the study area. A diamond interchange is provided at Oakland Road north of the project site. US 101 provides an interchange with I-880 approximately one-half mile west of the project study area and an interchange with I-280/I-680 approximately three miles southeast of the study area.

### 2.3 TRAFTC VOLUMES

Peak hour intersection turning movement volumes at four of the seven study intersections were counted in September 2018 by All Traffic Data Services, and peak hour turning movement volumes at three study intersections and average daily traffic (ADT) volumes at seven mid-block locations were counted in July 2018 by NDS. The peak hour counts included pedestrians and bicycles. The mid-block counts included truck classification counts at three of the locations. Peak hour and ADT count data is included in Appendix B. The intersection counts that were collected in July 2018 were adjusted to match the September 2018 counts at the adjacent intersections.

The existing AM peak hour intersection turning movement volumes and mid-block ADT volumes are illustrated in Figure 2-3. Existing PM peak hour intersection turning movement volumes are illustrated in Figure 2-4.

Table 2-1 summarizes the delay and LOS for the study intersections under existing conditions (Traffix delay calculation worksheets are presented in Appendix D). This is provided for information only, since the project impacts are evaluated under background conditions presented later in the report (Chapter 4.0). The delay for the signalized intersections is based on the average delay for all movements, while the delay for the stop-controlled intersections is the delay on the approach controlled by the stop sign. As this table shows, the signalized intersections at the US 101 ramps are operating at LOS C or better during the AM and PM peak hours, and the signalized intersections along Hedding Street are operating at acceptable LOS D or better during the AM and PM peak hours. The stop-controlled intersection of Oakland Road and Mabury Road is operating at acceptable LOS C or better during the AM and PM peak hours, but the stop-controlled intersection of Oakland Road and Horning Street is operating at LOS E during the PM peak hour.

## Table 2-1 Existing Delay and Level of Service Summary

|  |  | AM Peak Hour |  | PM Peak Hour |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Intersection | Control | Delay | LOS | Delay | LOS |
| 1. Oakland \& Mabury | Stop Sign | 18.2 sec | C | 12.7 sec | B |
| 2. Oakland \& US 101 NB ${ }^{1}$ | Signal | 33.4 sec | C | 24.2 sec | C |
| 3. Oakland \& US 101 SB ${ }^{1}$ | Signal | 27.0 sec | C | 29.4 sec | C |
| 4. Oakland \& Horning | Stop Sign | 10.5 sec | B | 45.1 sec | E |
| 5. Oakland \& Hedding | Signal | 44.5 sec | D | 43.4 sec | D |
| 6. 11th St \& Hedding | Signal | 29.0 sec | C | 15.9 sec | B |
| 7. 10th St \& Hedding | Signal | 21.0 sec | C | 37.5 sec | D |
| Notes: <br> 1 US 101/Oakland/Mabury TDP intersection and CMP intersection <br> sec = Seconds of delay per vehicle <br> LOS = Level of service <br> Highlight indicates LOS E or F$\quad$ |  |  |  |  |  |

### 2.4 PEDESTRIAN AND BICYCLE FACILTIES

From the peak hour counts and field observations, pedestrian and bicycle traffic is light during the AM peak hour and moderate during the PM peak hour in the study area. Sidewalks are available and in acceptable condition along Oakland Road and Hedding Street in the study area, with the exception of the north side of Hedding Street between 11th Street and 10th Street where the sidewalk becomes a dirt path. Not all curb ramps along Oakland Road or


Figure 2-3
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Figure 2-4

Existing Transportation Conditions
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Hedding Street are ADA-compliant. A sidewalk is provided on the east side of 10th Street north of Hedding Street but does not exist on the west side. Sidewalks are provided on both sides of 10th Street south of Hedding Street, on 11th Street south of Hedding Street, and on Madera Avenue. Sidewalks are missing on portions of Horning Street.

Class II bike lanes are provided on Oakland Road north of Commercial Street and south of Boardwalk Way, but they are not carried through the US 101 interchange area. Santa Clara Valley Transportation Authority (VTA) rates Oakland Road between Hedding Street and US 101 as a "High Caution" area on the Santa Clara Valley Bikeways Map which indicates high traffic volumes, high traffic speeds, high number of vehicles turning right, and narrow travel area for bicycles. Class II bike lanes are provided on Hedding Street which is designated as an On-Street Primary Bicycle Facility. Class II bike lanes are provided in both directions on 10th Street north of Hedding Street but are not striped on the one-way portion of 10th Street south of Hedding Street, although "Bike Lane" signs are posted. Northbound Class II bike lanes are striped on 11th Street south of Hedding Street. All of the bike facilities are in good repair, with the exception of 10th Street north of Hedding Street where the bike lane striping is badly faded in some places.

There are no designated bike facilities on Horning Street or Madera Avenue.
Figure 2-5 illustrates the bike facilities in the project vicinity.

Planned improvements at the US-101/Oakland Road interchange include widening of the bridge deck to accommodate an additional lane over the freeway. The deck widening will also include additional width for bike lanes and sidewalks along Oakland Road.

### 2.5 TRANSITFACILIIES AND SERVICES

Several local and express bus routes are located in the study area.

VTA provides local and community bus routes along Oakland Road and Hedding Street and two express routes along US 101 in the study area. Route 66 travels along Oakland Road from north of Commercial Street to Hedding Street with bus stops on Oakland Road adjacent to the project site. Route 66 continues west along Hedding Street past 10th Street. Route 65 travels from the Oakland Road/Hedding Street intersection south along 13th Street south of the study area. Route 12 travels from the Civic Center area west of the study area to east of the study area along Hedding Street. Similarly, Route 62 travels from west of the study area to east of the study area via Hedding Street. Bus stops are located along Hedding Street in the study area.

VTA provides express Route 121 and Route 122 through the study area via US 101; however, bus stops for these routes are not provided in the study area.

Monterey-Salinas Transit (MST) provides an Amtrak thruway bus route that travels between Mineta San Jose International Airport and King City to the south. MST Route 86 travels through the study area via US 101 and does not provide any bus stops in the study area.

Figure 2-6 illustrates the transit routes in the study area.


Figure 2-5


Figure 2-6

Existing Transportation Conditions
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### 2.6 OBSERVED TRANSPORTATION CONDIIONS

Traffic conditions in the field were observed during the AM peak period (beginning 8 AM) on Tuesday July 24, 2018 and during the PM peak period (beginning 4 PM) on Monday July 23, 2018 by Stantec staff.

During the AM peak period, there was mild traffic observed at Mabury Road and at US 101 northbound on-ramp. Mild pedestrian traffic on Oakland Road. No congestion was observed at the intersection of Oakland Road and Hedding Street. Similarly, along Hedding Street very little congestion was observed between Oakland Road and 10th Street. Few pedestrians or bicyclists were observed during the AM peak period along Hedding Street.

During the PM peak period, congestion observed at 10th Street and 11th Street caused eastbound traffic on Hedding Street to back up past 7th Street. A moderate amount of pedestrian traffic was observed along Hedding Street. Considerable traffic turning left onto Oakland Road from eastbound Hedding Street caused congestion at the intersection of Oakland Road and Hedding Street. The ramp meter at the US 101 southbound on-ramp from Oakland Road backs traffic approximately 250 feet from the meter to Oakland Road, but vehicles do not spill out onto Oakland Road. Moderate traffic was observed at Mabury Road due to vehicles backing up from the Commercial Street intersection. Southbound on Oakland Road, traffic backs up from the US 101 northbound on-ramp ramp meter to Oakland Road and causes moderate impact on the intersection at Commercial Street.

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### 3.0 CEQA TRANSPORIATION ANALYSIS

City staff has confirmed that the project is exempt from a detailed CEQA VMT analysis since it is equivalent to less than 100,000 square foot retail development based on the trip generation. Similar to local-serving retail trips, the proposed hotel and car wash trips would typically redistribute existing trips instead of creating new trips. The project trips may shorten vehicle-trips and reduce VMT by diverting existing trips from established locations to the new hotel and car wash without measurably increasing trips outside the local area.

### 3.1 VEHICLE-MILES TRAVELED ANALYSIS

The City has developed screening criteria to determine when a detailed CEQA transportation analysis would not be required. A detailed CEQA transportation analysis is not required if a project meets the City's screening criteria. Projects that are expected to result in less-than-significant VMT impacts based on project description, characteristics, or location would not require a detailed CEQA transportation analysis.

The City has defined "Local-Serving Retail" as a type of project that will not result in significant transportation impacts on the transportation system and will conform to the City's General Plan and other City goals and policies. As defined in Council Policy 5-1, local-serving retail typically diverts existing trips from established local retail to new local retail without measurably increasing trips outside of the area. In recognition of this effect, retail commercial projects up to a combined total of 100,000 gross square feet meet the City's screening criteria and do not require a detailed VMT analysis.

A 100,000 square foot retail project would generate 3,775 daily trips based on Institute of Transportation Engineers (ITE) trip rate. The proposed project generates 1,429 daily baseline vehicle-trips (discussed in Chapter 4.0, Section 4.4.1). The project is equivalent to 38,000 square feet of local-serving retail based on the project's daily baseline vehicle trip total; therefore, the project is less than the criteria of 100,000 square feet of retail and is exempt from a detailed VMT analysis.

To demonstrate the local serving nature of the proposed project, Figure 3-1 illustrates the locations of hotels proximate to the project site. This figure shows the project's proximity to the Mineta San Jose Airport. Also in the general vicinity are the Civic Center and Downtown San Jose. The hotel component of the project will be oriented toward business travelers. Many of the proposed hotel's visitors will choose this hotel for its location within two miles of the airport as well as its proximity to the Civic Center or Downtown San Jose (i.e., less than two miles). It is presumed that the majority of hotel customers would divert trips to the proposed hotel from other existing local hotels and, therefore, would not generate new hotel trips in the region.

Figure 3-2 illustrates the locations of car wash facilities proximate to the project. The project site is surrounded by several existing car wash facilities, either at gas stations or stand-alone. Motorists will choose a car wash that is convenient rather than drive miles out of their way to a car wash. If the proposed car wash is more convenient than an existing car wash, then motorists divert existing car wash trips to the proposed car wash. Furthermore, the majority of car wash trips would be pass-by or diverted trips where the motorist stops at the car wash on their way to another destination.

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Figure 3-1
Hotel Locations in the Vic inity of the Project Site


Figure 3-2
Car Wash Locations in the Vicinity of the Project Site

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Per San Diego Association of Governments (SANDAG) (Not So) Brief Guide of Vehicular Traffic Generation Rates for the San Diego Region, the weighted average hotel trip length of all trips, including guests and staff, is 7.6 miles. A gas station has a weighted average trip length, including customers and staff, of 2.8 miles, and the proposed car wash would have a similar average trip length. Both of these land uses have much shorter average trip lengths than the VMT for the area of 15.43 per non-industrial worker; therefore, the project would reduce the overall VMT for the area.

The proposed project is in conformance with Council Policy 5-1.

### 3.2 OTHER J URISDIC TIONS

The project is adjacent to US 101 freeway. The Oakland Road/US 101 interchange ramps are under Caltrans jurisdiction and are included in the list of study intersections. The study area is completely within the City of San Jose, and no other City's intersections or roadways are analyzed.

### 3.2.1 Methodology

Study intersections at the US 101/Oakland Road interchange are under Caltrans jurisdiction. Caltrans uses HCM delay methodology to determine peak hour impacts at ramp intersections. Caltrans analysis methodology is consistent with the HCM analysis that the City uses in the LTA.

The project adds less than 100 trips to the freeway; therefore, a mainline freeway analysis is not performed.

### 3.2.2 Signific ance Criteria

The significance criteria that the City uses was applied to the Oakland Road/US 101 ramp intersections to determine impacts to Caltrans intersections.

### 3.2.3 Project Impacts and Mitigation Measures

Project impacts to the Oakland Road/US 101 ramp intersections are discussed in the following chapter.

### 4.0 LOCAL TRANSPORIATION ANALYSIS

This chapter addresses the potential project impacts based on the City's local transportation analysis (LTA), and identifies significant project impacts, if any, based on the methodology in the City's Transportation Analysis Handbook.

### 4.1 BICYCLE AND PEDESIRIAN

The project is not expected to generate a significant amount of pedestrian or bicycle traffic. Business hotel guests are expected to use rental cars, ride-sharing services (i.e., Uber/Lyft), or hotel shuttle services (if provided); however, a portion of hotel employees might walk or bike to the site. Car wash customers will drive their vehicle to the car wash site. The automated car wash will have a minimal number of employees who might walk or bike to the site. The project is not expected to have a noticeable effect on the pedestrian or bicycle network.

### 4.2 TRANSIT

As discussed below, the project is located within a Suburban with Multifamily Housing area. There is a bus route that travels along the project frontage and several that travel along Hedding Street south of the site; however, there is a low percentage of transit use expected. Business hotel guests are more likely to use the hotel's airport shuttle (if provided) or ride-sharing services such as Uber or Lyft than to take public transit to and from the hotel. Customers of the car wash will drive their personal car to the site. The most common users of transit to the site will be employees of the hotel or car wash. However, the project is not expected to have a noticeable effect on transit use in the study area.

### 4.3 TRANSPORIATION DEMAND MANAGEMENT

A transportation demand management plan will be prepared for the project site.

### 4.4 INIERSECTION OPERATION ANALYSIS

The LTA is based on the peak hour analysis of seven study intersections. The analysis examines the project's impacts based on the HCM delay methodology. Conditions with the proposed project are compared with background conditions to determine significant project impacts.

### 4.4.1 Trip Generation

The project site is currently developed with several businesses, mostly automobile related such as a tire shop, auto and truck hand wash, print shop for car wraps, propane sales, etc., and one single-family residence. These businesses are currently generating traffic that is included in the existing intersection turning movement counts. The site currently has approximately 10 employees, which can vary depending on the weather (auto/truck hand wash).

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The proposed project is comprised of two components, a 116-room business hotel and an automated car wash.
Table 4-1 summarizes the daily total trip generation for the proposed project and during the weekday AM and PM peak hours.

Table 4-1 Project Trip Generation Summary


Trips generated by the project were estimated based on land use-based trip rates. Estimates of project trips are generally calculated based on average trip rates per a known variable, such as square feet for office or retail uses or dwelling units for residential developments. The Institute of Transportation Engineers (ITE) publishes a comprehensive manual with trip rates for hundreds of specific land use categories based on decades of data collected in the field. ITE's Trip Generation Manual is the industry standard for determining trip generation for developments.

## Hotel

Daily and peak hour trip generation rates for the proposed hotel were obtained from ITE's Trip Generation Manual, 10th Edition trip rates for Business Hotel (Category 312). These trip rates are based on the number of guest rooms of the proposed business hotel. The hotel component of the proposed project will generate approximately 466 daily vehicle trips, 45 AM peak hour vehicle trips, and 37 PM peak hour vehicle trips.

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## Car Wash

As thorough as ITE's Trip Generation Manual is, there are categories of land uses with little or no trip rate data. The proposed automated car wash is one such category (Category 948). The Trip Generation Manual contains trip rates for weekday PM peak hour, but no data is available for daily or AM peak hour trips. In the absence of viable published trip rates, case study data is used. A case study of an existing car wash with identical layout and operating characteristics in Los Angeles County was used to determine the AM and daily trips for the proposed car wash. The car wash used in the case study is located in Montebello on the corner of Montebello Boulevard and Washington Boulevard. This case study car wash has been in operation since 2013, and the counts were collected in 2014. The hours of operation are 7 AM to 7 PM except during the summer when they are open until 8 PM. Information on the number of staff at the time of the counts is not available. The car wash component of the project is estimated to generate 49 AM peak hour trips, 78 PM peak hour trips, and 963 daily trips. The peak hour and daily trip count data for the car wash site case study is provided in Appendix $\mathbf{F}$.

The peak hour and daily trips being used for the analysis were compared with the trips that the car wash would generate if SANDAG trip rates for Car Wash - Automatic from the (Not So) Brief Guide of Vehicular Traffic Generation Rates for the San Diego Region (April 2002) were applied to the project. Compared with SANDAG trip rates, the project trip generation used in this analysis is 13 trips higher during the AM peak hour, 4 trips lower during the PM peak hour, and 63 trips higher daily. The trips used in this analysis are conservatively high during the AM peak hour and daily, and approximately equivalent during the PM peak hour. A comparison summary of the car wash trips is included in Appendix F.

The project's baseline vehicle trip total is 1,429 daily trips, of which 94 occur during the AM peak hour and 115 occur during the PM peak hour.

## Trip Generation Reduction Factors

Trip generation reduction factors applied to the baseline project trip generation total are discussed below.

## Internal Capture

The proposed project's land use combination of business hotel and automated car wash is forecasted to have nominal to no internal capture trips; therefore, no internal adjustment was made to the project trip generation estimate.

## Location Based Adjustment

The project site location meets the description of a Suburban with Multifamily Housing area defined by the VMT Tool. The Transportation Analysis Handbook specifies 88 percent vehicle mode share for "Suburban with Multifamily Housing" area. Therefore, 12 percent of estimated business hotel project trip generation have been decreased per location-based adjustment. No adjustment credit for project site location transit was applied to the proposed car wash portion of the project trip generation because the nature of the self-serve car wash business would only draw patronage via consumers driving their own vehicles. The total Suburban with Multifamily Housing area reduction is 5 vehicle trips during the AM peak hour, 4 vehicle trips during the PM peak hour, and 61 daily vehicle trips.

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The proposed business hotel will most likely operate a shuttle service between the hotel and Mineta San Jose International Airport. However, without a known hotel operator with a commitment to provide free shuttle service, no reduction in the project trip generation for shuttle trips was assumed for the proposed hotel.

## Existing Site Traffic

The project site is currently developed with several automobile-related businesses. These businesses are currently generating traffic that is included in the existing intersection turning movement counts. Stantec conducted peak hour driveway counts at all ten of the existing project site driveways during AM and PM peak hours to determine existing trip generation from the site. Counts conducted at the driveways have been deducted from the proposed AM and PM peak hour trip estimates to calculate the net new trips from the proposed project. The total for the existing uses might be slightly low since the driveway counts do not include any site traffic that may have parked on the street adjacent to the site.

The average daily traffic estimate of the existing site was calculated by interpolating the collected AM and PM peak hour volume data. SANDAG rates specify that a car wash land use generates approximately 4 percent of its daily trips during the AM peak hour and 9 percent during the PM peak hour. Similarly, the SANDAG rates estimate that a hotel land use generates 6 percent of total daily trips during the AM peak hour and 8 percent during the PM peak hour. Using the hotel land use's more conservative peak hour traffic to daily traffic ratio of 14:100 compared to the car wash's ratio of 13:100, the sum of existing site's AM and PM peak hour trips have been divided by 14 percent to interpolate the estimated total daily traffic. The collected existing driveway count data is provided in Appendix B. The existing land uses on the project site currently generate 42 AM peak hour trips, 49 PM peak hour trips, and approximately 650 daily trips.

It is generally preferable to collect actual count data for existing uses rather than calculate the trips based on trip rates, especially when some of the existing businesses on the site do not easily fall into the ITE categories. However, an estimate of existing trips based on ITE trip rates was prepared assuming Car Wash and Detail Center (ITE 949) and Auto Care Center (ITE 942) land uses for comparison. The actual counted driveway total was compared with the ITE trip rate estimate and is summarized in Appendix F. The actual counted driveway total is lower than the ITE trip estimate during the peak hours, with the actual counted driveway total 10 trips lower than the ITE trip estimate during the AM peak hour and 35 trips lower during the PM peak hour. This results in a conservatively high net external project vehicle trip estimate.

## Net External Vehicle Trips

With the reductions for Urban Low-Transit area and existing development on-site, the proposed project will generate 45 new vehicle trips during the AM peak hour, 62 new vehicle trips during the PM peak hour, and 723 new vehicle trips daily. This trip generation estimate is conservatively high since a pass-by reduction for the car wash, which would be significant, was not taken.

### 4.4.2 Project Trip Distribution

Project trips were distributed and assigned to the surrounding streets manually. Separate distribution estimates were developed for the business hotel and the car wash. These distribution estimates were developed using engineering judgement based on levels and locations of development and locations of other existing hotels and car washes in

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relation to the location of the project site. Trips to and from the business hotel are more likely to be distributed to the airport, Civic Center, and Downtown San Jose areas than the car wash, which is more likely to draw traffic from the surrounding residential and business areas.

Figure 4-1 illustrates the business hotel general distribution. As this figure shows, the Mineta San Jose International Airport, approximately 2.5 miles from the project site, is estimated to attract approximately 50 percent of the business hotel traffic. The most direct route to the project site from the airport might be via US 101; however, congestion on US 101 during the peak hours would discourage many hotel guests from taking that route. With smartphone apps providing driving directions based on real-time traffic conditions, there are alternative routes using the local streets to and from the airport which would provide a competitive drive time between the hotel and airport. These alternate routes were assumed to be along 10th Street, 4th Street, and 1st Street via Horning Street or Hedding Street, with a small amount of business hotel traffic using I-880 to access the south end of the airport via Airport Boulevard. Approximately 22.5 percent of non-airport traffic is distributed to the I-880 and US 101 freeways, 2.5 percent to Oakland Road north of US 101, 10 percent to Hedding Street east of US 101, 5 percent south of Hedding Street, and 10 percent to Hedding Street west of 1st Street.

Figure 4-2 illustrates the car wash distribution. The car wash will attract customers more locally from the surrounding residential and commercial areas. Approximately 10 percent is distributed to Oakland Road north of US 101, 10 percent is distributed to Hedding Street east of US 101, 40 percent is distributed south of Hedding Street, 10 percent is distributed to Hedding Street west of 4th Street, and 30 percent is distributed northwest of the project site along 10th Street via Horning Street. The same distribution was assumed for existing site traffic since existing uses are auto-related retail businesses.

### 4.4.3 Project Trip Assignment

The peak hour project trips identified in Section 4.4.1 were assigned to the surrounding roadway network according to the general hotel and car wash distribution presented in the previous Section. Turn restrictions and one-way streets were taken into consideration when assigning the peak hour project trips to the study intersection turning movements. The peak hour business hotel intersection turning movement trips and the car wash intersection turning movement trips were added together, and the existing site peak hour intersection turning movement trips were subtracted from the business hotel and car wash total to produce the net intersection turning movement trips generated by the proposed project.

Figure 4-3 illustrates the net AM peak hour vehicle trips at the study intersections, and Figure 4-4 illustrates the net PM peak hour vehicle trips for the project site (individual business hotel, automated car wash, and existing site peak hour intersection turning movement trips are provided in Appendix G). The project driveway volumes in these exhitbits represent the total adjusted vehicle trips generated by the proposed project, while the off-site study intersection volumes show the net external vehicle trips (i.e., new project trips less the existing site trips).

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Figure 4-1
General Project Distribution - Business Hotel


Figure 4-2


Figure 4-3


Figure 4-4

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## US-101 Oakland/Mabury TDP

The City adopted the US-101/Oakland/Mabury Transportation Development Policy (TDP) in 2007 which "is intended to achieve all of the following: (1) management of traffic congestion generated by near-term new development in the vicinity of the US-101/Oakland interchange; (2) promotion of General Plan goals for economic development and housing; and (3) improvement of the US-101/Oakland Road interchange and construction of the new US-101/Mabury Road interchange to accommodate new development." The TDP defines the interchange capacity available, identifies the required improvements for future development in the area, explains the funding to complete the required improvements, establishes a traffic fee program for new development in the area to fund the improvements, promotes industrial land use in the area, and allows the LOS of signalized intersections covered by the TDP to temporarily exceed the City's LOS standards until the required improvements are constructed.

Future intersection impacts caused by future developments are expected to occur at US 101 northbound/Oakland Road ramps, US 101 southbound/Oakland Road ramps, and Oakland Road/Commercial Road intersection. Major regional transportation projects that are recognized as necessary to provide adequate access to the US 101 freeway and the planned BART station include modification of the US 101/Oakland Road interchange and construction of the US 101/Mabury Road interchange. The proposed project adds traffic to the "Policy Interchange Intersections" of US 101 northbound/Oakland Road ramps and US 101 southbound/Oakland Road ramps.

The TDP established PM peak hour vehicle trips as the measurement for interchange capacity impacts. Any trip traversing through one or more Policy Interchange Intersection during the PM peak hour is regarded as one interchange trip, whether they access the US 101 freeway or not. Construction of the Planned Improvements will increase the interchange capacity, making approximately 1,153 PM peak hour trips available to accommodate new development. Figure 4-5 illustrates the Planned Improvements.

Various funding sources for the Planned Improvements are identified in the TDP. The City Council established a Traffic Impact Fee program to cover the unfunded cost of the Planned Improvements. The Traffic Impact Fee program requires new development that adds traffic to the Policy Interchange Intersections to make a fair share financial contribution to the cost of the Planned Improvements. The Traffic Impact Fee for each interchange PM peak hour trip for fiscal year 2019 is $\$ 38,623$.

The TDP and its Traffic Impact Fee program applies to all new residential and commercial development that generates vehicular trips at any of the Policy Interchange Intersections. Based on the trip distribution and assignment, the project adds 14 PM peak hour trips to the Oakland Road/US 101 interchange. This volume of project trips could be reduced if the business hotel were to provide a shuttle service for guests to and from destinations such as the airport.


Figure 4-5

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### 4.4.4 Background Conditions

The City maintains a database of vehicle-trips of approved but not yet constructed projects, known as the Approved Trip Inventory (ATI), for use in the LTA. City staff provided ATI volumes at the study intersections for this analysis. The ATI volumes were added to the existing count data to represent background conditions. Appendix C summarizes the ATI projects and trips at the study intersections. The ATI peak hour volumes were added to the existing intersection turning movement volumes to produce the AM and PM peak hour background volumes against which the project impacts are evaluated.

Figure 4-6 illustrates AM peak hour background intersection volumes, and Figure 4-7 illustrates PM peak hour background intersection volumes. Table 4-2 summarizes the delay and corresponding LOS under background conditions.

Table 4-2 Background Delay and Level of Service Summary

| Intersection | Control | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay | LOS | Delay | LOS |
| 1. Oakland \& Mabury | Stop Sign | 32.0 sec | D | 15.5 sec | C |
| 2. Oakland \& US 101 NB ${ }^{1}$ | Signal | 56.2 sec | E | 56.7 sec | E |
| 3. Oakland \& US 101 SB ${ }^{1}$ | Signal | 29.2 sec | C | 69.5 sec | E |
| 4. Oakland \& Horning | Stop Sign | 11.9 sec | B | 222.6 sec | F |
| 5. Oakland \& Hedding | Signal | 51.8 sec | D | 52.7 sec | D |
| 6. 11th St \& Hedding | Signal | 36.3 sec | D | 17.8 sec | B |
| 7. 10th St \& Hedding | Signal | 23.4 sec | C | 46.6 sec | D |
| Notes: <br> ${ }^{1}$ US 101/Oakland/Mabury TDP intersection and CMP intersection |  |  |  |  |  |

As this table shows, during the AM peak hour, the study intersection at Oakland Road and US 101 northbound ramps will operate at LOS E under background conditions. During the PM peak hour, the study intersections of Oakland Road and US 101 northbound ramps and Oakland Road and US 101 southbound ramps will operate at LOS E with the addition of ATI volumes. The stop-controlled intersection of Oakland Road and Horning Street will operate at LOS F during the PM peak hour under background conditions. The remaining study intersections will operate at acceptable LOS D or better during the AM or PM peak hour.


Figure 4-6


Figure 4-7

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### 4.4.5 Background plus Project Conditions

The net peak hour project trips presented in Section 4.4 .3 were added to the background intersection volumes presented in the previous Section to produce background plus project conditions.

Figure 4-8 illustrates AM peak hour background plus project intersection volumes, and Figure 4-9 illustrates PM peak hour background plus project intersection volumes.

Table 4-3 summarizes the delay and LOS under background plus project conditions and compares it with background conditions. As this table shows, the intersection of Oakland Road and US 101 northbound ramps will operate at LOS E during the AM and PM peak hour with the addition of project vehicle-trips; however, the increase in delay is less than 1.0 second and the increase in V/C is less than 0.010 . The intersection of Oakland Road and US 101 southbound ramps will operate at LOS E during the PM peak hour with the addition of project vehicle-trips, but the increase in delay is less than 1.0 second and the increase in V/C is less than 0.010 .

The stop-controlled intersection of Oakland Road and Horning Street will operate at LOS F during the PM peak hour under background conditions. The project increases the delay for the eastbound right-turn traffic by 4.7 seconds, a 2 percent increase. However, the Traffix software may be overestimating the delay for the eastbound right-turn movement since the signal at the adjacent intersection at US 101 southbound would create gaps in the southbound through traffic allowing the eastbound right-turn movement to turn. Furthermore, signalization of the intersection is not recommended since stopping the southbound through movement could create queues that might back up to the US 101 southbound ramps.

The remaining study intersections will operate at LOS D or better during the AM and PM peak hour.

As discussed in Chapter 1.0, an adverse effect on intersection operations occurs when the analysis demonstrates that the project causes the operations standard at a study intersection to fall below LOS D with the addition of project vehicle-trips to baseline conditions. For signalized intersections already operating at LOS E or F under background conditions, the criteria for determining adverse intersection operations from the project impact is:

- An increase in average critical delay by 4.0 seconds or more AND an increase in the critical V/C ratio of 0.010 or more; OR
- A decrease in the average critical delay AND an increase in critical V/C ratio of 0.010 or more.

Based on these criteria, none of the study intersections are adversely affected by the proposed project.

### 4.4.6 Project Entrance Analysis

The project entrance on Oakland Road was analyzed. The raised median on Oakland Road currently restricts outbound vehicles from Boardwalk Way opposite the location of the proposed driveway to right turns only. An existing median break allows inbound left turns from southbound Oakland Road to Boardwalk Way. This southbound left-turn pocket also allows vehicles turning right from Horning Street to make a U-turn to travel northbound on Oakland Road. This southbound left-turn pocket is approximately 175 feet long. The proposed project would modify the raised median to allow full access at the project entrance, which would also allow westbound left turns from Boardwalk Way to southbound Oakland Road. A signal is proposed at the project entrance and protected northbound and southbound


Figure 4-8


Figure 4-9

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Table 4-3 Background Plus Project Delay and Level of Service Summary

| Intersection | Control | Background |  |  |  | Background + Project |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  | Adverse Effect? |
|  |  | Delay | LOS | Delay | LOS | Delay | LOS | Incr. in Delay | Incr. in V/C | Delay | LOS | Incr. in Delay | Incr. in V/C |  |
| 1. Oakland \& Mabury | Stop Sign | 32.0 sec | D | 15.5 sec | C | 32.1 sec | D | 0.1 sec | N/A | 15.5 sec | C | 0.0 sec | N/A | No |
| 2. Oakland \& US 101 NB ${ }^{1}$ | Signal | 56.2 sec | E | 56.7 sec | E | 56.7 sec | E | 0.5 sec | 0.004 | $\mathbf{5 7 . 5} \mathrm{sec}$ | E | 0.8 sec | 0.003 | No |
| 3. Oakland \& US 101 SB ${ }^{1}$ | Signal | 29.2 sec | C | 69.5 sec | E | 29.3 sec | C | 0.1 sec | 0.004 | 70.1 sec | E | 0.6 sec | 0.003 | No |
| 4. Oakland \& Horning | Stop Sign | 11.9 sec | B | 222.6 sec | F | 12.0 sec | B | 0.1 sec | N/A | 227.3 sec | F | 4.7 sec | N/A | No |
| 5. Oakland \& Hedding | Signal | 51.8 sec | D | 52.7 sec | D | 52.1 sec | D | 0.3 sec | 0.005 | 53.1 sec | D | 0.4 sec | 0.003 | No |
| 6. 11th St \& Hedding | Signal | 36.3 sec | D | 17.8 sec | B | 36.6 sec | D | 0.3 sec | 0.004 | 17.8 sec | B | 0.0 sec | 0.006 | No |
| 7. 10th St \& Hedding | Signal | 23.4 sec | C | 46.6 sec | D | 23.5 sec | C | 0.1 sec | 0.004 | 47.1 sec | D | 0.5 sec | 0.005 | No |
| Notes: <br> ${ }^{1}$ US 101/Oakland/Mabury | TDP inter |  |  |  |  |  |  |  |  |  |  |  |  |  |

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left-turn phasing was assumed. Split phasing was assumed for the eastbound and westbound movements since the westbound leg is not wide enough for a separate left-turn lane, and the through volumes are expected to be nominal. To analyze the proposed project entrance, an estimate was made of the number of peak hour westbound left-turn vehicles which might exit Boardwalk Way if full access is allowed based on trip generation and distribution information contained in the approved Transportation Impact Analysis prepared in 2005 for the Modern Ice Townhomes development.

The project entrance on Oakland Road would operate at LOS B during the AM and PM peak hours with a signal. The project entrance on Horning Street will not be signalized. This driveway will operate at LOS B during the AM peak hour and LOS C during the PM peak hour (delay and LOS calculations for the project driveways are included in Appendix D).

### 4.5 QUEUING ANALYSIS

The Traffix calculations provide vehicle queue information to determine the amount of left-turn storage required to accommodate the traffic demand. The proposed project driveway on Oakland Road is approximately 525 feet north of Hedding Street. The median on Oakland Road will be modified to provide a northbound left-turn pocket into the proposed project driveway. The northbound left-turn pocket into the proposed project driveway cannot be so long that it interferes with the existing southbound left-turn pocket at Hedding Street, which is approximately 120 feet long.

The Traffix calculations provide queue information to determine left-turn storage needs for the left-turn pockets along Oakland Road. Queues are expressed in number of vehicles.

Table 4-4 summarizes the southbound queue at Hedding Street and the queues at the proposed project driveway.

The maximum average eastbound queue exiting the project site during the peak hours is one vehicle which requires approximately 25 feet of storage. The maximum northbound left-turn queue into the site is two vehicles (approximately 50 feet); therefore, the City's minimum left-turn storage length of 90 feet with a 90 -foot taper for a $35-\mathrm{mph}$ street will be sufficient to accommodate the northbound left-turn queue. The maximum average southbound left-turn/U-turn queue on Oakland Road is eight vehicles (approximately 200 feet). This turn pocket is currently approximately 175 feet long and may need to be lengthened to accommodate the anticipated queue. The maximum average queue westbound on Boardwalk Way is three vehicles which would require approximately 75 feet. These queue lengths are based on estimates of the Modern Ice Townhomes development peak hour volumes expected to use a signalized full-access intersection in the future.

The average southbound left-turn queue at Hedding Street increases from 12 vehicles ( 300 feet) under existing conditions to 22 vehicles ( 550 feet) with the addition of ATI volumes under background conditions. The addition of project traffic has no impact on the southbound left-turn queue length. However, the southbound left-turn queue will back up to approximately the project driveway.

Table 4-5 summarizes the approximate turn pocket lengths at the project entrance on Oakland Road based on the anticipated peak hour queues. These pocket lengths should be confirmed during the signal design permit process.

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## Table 4-4 Queue Analysis Summary

| Left-Turn Pocket | Existing |  |  |  | Background |  |  |  | Background + Project (with signal) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  |
|  | Vehs | Length (ft) | Vehs | Length (ft) | Vehs | Length (ft) | Vehs | Length (ft) | Vehs | Length (ft) | Vehs | Length (ft) |
| Hedding Street |  |  |  |  |  |  |  |  |  |  |  |  |
| Southbound | 5 | 125 | 12 | 300 | 11 | 275 | 22 | 550 | 11 | 275 | 22 | 550 |
| Project Driveway |  |  |  |  |  |  |  |  |  |  |  |  |
| Northbound | N/A | -- | N/A | -- | N/A | -- | N/A | -- | 1 | 25 | 2 | 50 |
| Southbound | < 1 | 25 | 2 | 50 | < 1 | 25 | 3 | 75 | 3 | 75 | 8 | 200 |
| Eastbound | N/A | -- | N/A | -- | N/A | -- | N/A | -- | 1 | 25 | <1 | 25 |
| Westbound | < 1 | 25 | < 1 | 25 | < 1 | 25 | < 1 | 25 | 3 | 75 | 1 | 25 |
| N/A - Not applicable |  |  |  |  |  |  |  |  |  |  |  |  |

Table 4-5 Oakland Road Left-Turn Pocket Length Summary

| Left-Turn Pocket | Existing | Background | Background + Project <br> (with signal) |
| :--- | :---: | :---: | :---: |
| Project Driveway | -- | -- | 90 ft |
| Northbound | 175 ft | 175 ft | 200 ft |
| Southbound | -- | -- | 25 ft |
| Eastbound | 150 ft | 150 ft | 150 ft |
| Westbound * |  |  |  |
| * Shared left-turn and right-turn lane |  |  |  |

### 4.6 SIGNALWARRANT

The project proposes to modify the raised median to allow full access at the proposed project entrance opposite Boardwalk Way. This entrance is proposed to be signalized. The minimum peak hour side street volume required to satisfy the peak hour signal warrant is 100 vehicles. Since westbound left turns are currently prevented by the raised median on Oakland Road, future westbound left turns were estimated from the trip generation and distribution estimates in the Modern Ice Transportation Impact Analysis. The estimated westbound AM peak hour volume is 91 vehicles. A signal is not warranted at this location, although the basis for satisfaction of the warrant is the estimated peak hour traffic from Boardwalk Way, and the estimate is very close to satisfying the peak hour warrant. Installation of a signal and opening of the median to allow westbound left turns could result in a higher volume on Boardwalk Way than estimated here which would satisfy the signal warrant. With a signal, the intersection will operate at LOS B during the AM and PM peak hours. Without the signal, the intersection would operate at LOS F.

Besides providing the proposed development with left-turn access to Oakland Road, the signal will provide protected westbound left-turn access to Oakland Road for motorists in the Modern Ice Townhomes development, a movement that is not currently allowed. The existing median on Oakland Road currently prevents westbound left turns from Boardwalk Way to southbound Oakland Road, and motorists from the townhomes development wishing to travel on Hedding Street or to other destinations toward the south must cut through on the residential streets of 14th Street, 15th Street, 16th Street, 17th Street, or Bayshore Road to Hedding Street. Furthermore, the intersections of these residential streets with Hedding Street are not signalized, which makes turning left onto Hedding Street difficult during peak periods. The proposed signal at Boardwalk Way will provide outbound Modern Ice Townhomes motorists with access to the signal at Oakland Road and Hedding Street. In addition, the signal will provide protected left-turn phasing for southbound traffic at Boardwalk Way which is currently an unprotected movement.

The signal will provide controlled bicycle and pedestrian crossing of Oakland Road at Boardwalk Way. The existing median prevents bicycle crossings of Oakland Road between US 101 and Hedding Street, with the exception of southbound bicycles turning left at Boardwalk Way. However, inexperienced or timid bicyclists avoid turning left at Boardwalk Way since they have to cross two lanes of southbound traffic to enter the left-turn pocket and make the left turn during gaps in two lanes of oncoming northbound traffic. The lack of median breaks to allow bicyclists to cross Oakland Road leads to dangerous wrong-way riding on Oakland Road. The proposed signal and median break provide a controlled crossing of Oakland Road approximately halfway between US 101 and Hedding Street.

The existing median on Oakland Road also discourages pedestrian crossings. At this time the only protected crosswalks across Oakland Road in the study area are located at the signals at Hedding Street and at Commercial Street north of US 101. Pedestrian crossing of Oakland Road at the signals at the US 101 interchange is prohibited. Pedestrians aren't prohibited from crossing Oakland Road at any of the intersections between US 101 and Hedding Street; however, they must dash across the street during gaps in traffic and scramble across the raised median. Pedestrians with mobility challenges are prevented from crossing at these intersections. The proposed signal and median break at Boardwalk Way will provide an accessible and controlled crossing of Oakland Road to promote pedestrian connectivity between the residential uses on the east side of Oakland Road and the commercial uses on the west side.

### 4.7 STIE CIRCULATION AND ACCESS

Two driveways will provide access to the project site. The main driveway is located on Oakland Road opposite Boardwalk Way providing access to the two parcels. This driveway will provide full access to Oakland Road. A second driveway is located on Horning Avenue at the western edge of the site.

Pedestrian access is shown on the site plan in Figure 1-2. Crosswalks at the new signalized intersection with Oakland Road opposite Boardwalk Way will be provided across the west, east, and south legs of the intersection. The proposed signal will provide a new controlled crossing of Oakland Road for pedestrians. The sidewalk along the project frontage on Horning Street will be improved. Connections between the hotel and the sidewalk on Horning Street and Oakland Road will be provided. Pedestrian access from Oakland Road to the proposed car wash will be provided by a sidewalk on the south side of the main access aisle.

## Council Policy 6-10

The City Council approved Council Policy 6-10-Criteria for the Review of Drive-Through Uses in 1979 and updated the policy in 1990. The purpose of the policy is to provide guidelines for the development of drive-through facilities within the City. According to Council Policy 6-10, development shall be restricted to Commercial Zoning Districts, designated as $\mathrm{C}-1, \mathrm{C}-2$, and $\mathrm{C}-3$, and to Planned Development (PD) zoning; however, the current CIC zoning is a Commercial Zoning District which did not exist at the time the policy was written and is consistent with the policy.

Stacking at the car wash will be provided for five vehicles between the pay station and the first parking space as shown in Figure 4-10. Stacking for a total of 13 vehicles is provided between the pay station and the main access aisle. The car wash requires stacking for 5 vehicles based on the City Municipal Code and Council Policy 6-10.

The proposed car wash meets the following Traffic Criteria:
A. Primary ingress and egress of the proposed car wash is from the Oakland Road, a four-lane major street
B. The drive-through stacking is situated so that overflow from the stacking lane queues on-site along the western edge of the car wash parcel. The total stacking capacity is 13 vehicles; therefore, the overflow capacity ( 8 vehicles) is more than 50 percent of the required stacking ( 5 vehicles)
C. The ingress and egress point does not conflict with turning movements of street intersections
D. The ingress and egress point is more than 300 feet from the nearest signalized intersection
E. The drive-through stacking lane is separated physically from the parking lot and provides stacking for 5 vehicles between the pay station and the first parking space
F. There is no pedestrian crossing of the drive-through lane
G. The proposed car wash drive-through stacking lane is located at the western edge of the car wash parcel, approximately 175 feet from the new signalized intersection.


Figure 4-10

### 4.8 DELVERY, WASTE, AND MOVING TRUCKS

The site plan has been designed to accommodate trucks.
An on-site loading zone for deliveries is provided for the business hotel in the northeast area of the hotel parking lot. The space is approximately 30 feet long. Delivery trucks can access the site from either Horning Street or Oakland Road and circulate through the hotel parking lot to and from the loading zone. The car wash does not require a designated loading zone.

Separate trash enclosures are provided for the business hotel and the car wash. The trash enclosure for the business hotel is located on the eastern edge of the property adjacent to the building and across from the loading zone. A garbage truck can enter and exit the site and access the hotel trash enclosure from either Horning Street or Oakland Road and circulate through the hotel parking lot. The car wash trash enclosure is located along the main drive aisle in the northwest area of the car wash parcel. A garbage truck can access the car wash trash enclosure from the main drive aisle and will not need to enter the car wash area.

Once the business hotel is furnished and open to guests, large moving trucks are not expected at the hotel. Business hotel guests will not arrive with large moving trucks. Similarly, car wash customers will not arrive with large moving trucks.

### 4.9 PARKING

Parking on the hotel parcel will be provided for 100 vehicles consisting of 56 regular parking spaces, 4 ADA spaces, and 40 compact spaces. The hotel requires one space per room plus one space per employee based on the City Municipal Code. The 116 -room business hotel is anticipated to employ 8 people; therefore, the business hotel requires 124 spaces based on the City Code. The business hotel does not meet the minimum City Code parking requirement.

A Transportation Demand Management (TDM) plan will be required for the project. The TDM will result in a 20 percent reduction in the business hotel parking demand. With the 20 percent TDM reduction, the business hotel will require 100 parking spaces, and the business hotel satisfies the parking requirement.

Parking on the car wash parcel will be provided for 12 vehicles consisting of 3 employee spaces, 8 regular vacuum spaces, and 1 ADA accessible vacuum space. Stacking for 13 vehicles between the pay station and the main drive aisle will be provided. The car wash requires one space per employee plus stacking for 5 vehicles ( 20 feet per car) based on City Code. The proposed car wash is anticipated to employ 3 people; therefore, the car wash requires 3 parking spaces and stacking for 5 vehicles per City Code. The car wash meets the City Code parking requirement.

Bicycle parking will be provided for 13 bikes on the hotel parcel. City Code requires 1 bicycle space plus 1 space per 10 rooms. Based on the City Code, the business hotel requires 13 bicycle parking spaces. Bicycle parking will be provided for 1 bike on the car wash parcel. City Code requires 1 bicycle space per 10 employees for car wash facilities. The proposed car wash requires 1 bicycle space based on the City Code.

Local Transportation Analysis
May 2019

### 4.10 NEIGHBORHOOD TRAFAC INTRUSION

The project will generate little peak hour traffic above what is already generated from the site. The hotel traffic is expected to be attracted to the airport, Civic Center, and Downtown San Jose areas and will keep to the main streets and freeway. The car wash traffic will be attracted from the surrounding residential and commercial areas, but cut-through traffic through the neighborhoods is not expected to be an issue.

Conclusions
May 2019

### 5.0 CONCLUSIONS

The proposed project consists of a 116-room business hotel and automated car wash. The project is located on Oakland Road between Horning Street and Madera Avenue. The project site will have two driveways, one on Oakland Road and one on Horning Street.

Project trips were calculated based on ITE trip rates and an existing car wash case study driveway count. Location based reduction for Suburban with Multifamily Housing area was applied to the hotel component of the project. Furthermore, trips generated by the existing development on the site were subtracted from the project trip generation to obtain net new project vehicle trips. The proposed project will generate 45 new vehicle trips during the AM peak hour, 62 new vehicle trips during the PM peak hour, and 723 new vehicle trips daily.

The City's VMT Evaluation Tool has four categories of land uses (Residential, Office, Retail, and Industrial), and hotel does not fall into any of the designated land use categories. The proposed land uses cannot be evaluated with the VMT Evaluation Tool or with the Travel Demand Model. Therefore, both the business hotel and the car wash require a qualitative evaluation and comparison to retail land uses as defined in Council Policy 5-1. The proposed hotel and car wash project trip generation estimates were converted to an equivalent amount of retail square footage based on the daily trips. The resulting retail square footage was compared with the CEQA VMT Analysis Screening Criteria in the Transportation Handbook 2018 to determine conformance to Council Policy 5-1 for the proposed 116-room hotel and automated car wash. Based on the daily trip generation for the proposed project, the project is equivalent to 38,000 square feet of retail uses, which exempts the project from a CEQA VMT analysis. The project site is located within two miles of the Mineta San Jose Airport, Civic Center, and Downtown San Jose. These local facilities will attract a large portion of the proposed hotel trips, resulting in a lower VMT for the project than existing VMT for the area of 15.43 per non-industrial worker. Additionally, motorists will choose a car wash that is convenient rather than drive miles out of their way to a car wash. If the proposed car wash is more convenient than an existing car wash, then motorists will divert existing car wash trips to the proposed car wash. Furthermore, the majority of car wash trips would be pass-by or diverted trips where the motorist stops at the car wash on their way to another destination.

The net new project trips were distributed to the surrounding street network based on levels and locations of development in relation to the project site. Separate distribution patterns for the business hotel and car wash were developed. The business hotel trips were primarily distributed to the Mineta San Jose Airport, Civic Center, and Downtown San Jose, while the car wash trips were distributed to surrounding residential and commercial areas.

The study area was defined with concurrence of the City, and five signalized intersections and two stop-controlled intersections in proximity of the project site were identified as the study intersections. Peak hour turning movement counts were collected in July and September 2018 at the study intersections.

Background conditions were developed by adding trips from approved but not yet constructed projects in the City's ATI database to the existing intersection volumes. These background volumes provide the conditions against which the project impacts are evaluated.

Conclusions
May 2019

The net new project vehicle-trips were added to the background volumes. The delay and LOS for background plus project conditions were compared with the background delay and LOS. Three study intersections operate at deficient LOS under background conditions; however, the project has no adverse effect on these or any of the study intersections.

The City adopted the US-101/Oakland/Mabury Transportation Development Policy (TDP) in 2007 which defines the interchange capacity available, identifies the required improvements for future development in the area, explains the funding to complete the required improvements, establishes a traffic fee program for new development in the area to fund the improvements, promotes industrial land use in the area, and allows the LOS of signalized intersections covered by the TDP to temporarily exceed the City's LOS standards until the required improvements are constructed. Major regional transportation projects that are recognized as necessary to provide adequate access to the US 101 freeway and the planned BART station include modification of the US 101/Oakland Road interchange and construction of the US 101/Mabury Road interchange. The City Council established a Traffic Impact Fee program to cover the unfunded cost of the Planned Improvements. Based on the trip distribution and assignment, the project adds 14 PM peak hour trips to the Oakland Road/US 101 interchange. This volume of project trips could be reduced if the business hotel were to provide a shuttle service for guests to and from destinations such as the airport.

The project entrance on Oakland Road opposite Boardwalk Way is proposed to be signalized. The raised median would be modified, and the existing residential development on the east side of Oakland Road (Modern Ice Townhomes) would be given full access to Oakland Road. This location would operate at LOS F without a signal. With a signal, the intersection operates at LOS B during the AM and PM peak hours. A signal and median break at this location would provide an accessible crossing of Oakland Road to promote pedestrian connectivity and a controlled crossing for bicyclists.

The project has no adverse effect on the surrounding streets and no off-site mitigation is necessary.

References
May 2019

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Kunzman Associates, lnc.

April 15, 2015

Mr. Tod Ridgeway
RIDGEWAY DEVELOPMENT COMPANY
2804 Lafayette Avenue
Newport Beach, CA 92663

Dear Mr. Ridgeway:

## INTRODUCTION

The firm of Kunzman Associates, Inc. is pleased to provide this trip generation analysis for the Newport Beach Car Wash site located at 150 Newport Center Drive Car in the City of Newport Beach.

Although this is a technical report, every effort has been made to write the report clearly and concisely. To assist the reader with those terms unique to transportation engineering, a glossary of terms is provided within Appendix A.

## EXISTING TRAFFIC COUNTS

Traffic counts were obtained at the 150 Newport Center Drive Car Wash driveway over three (3) average weekdays: Tuesday (March 24, 2015), Wednesday (March 25, 2015), and Thursday (March 26, 2015). The 150 Newport Center Drive Car Wash driveway is shown on Figure 1. The 24-hour two-way tube counts are included in Appendix B.

## TRIP GENERATION

The 150 Newport Center Drive Car Wash traffic counts were averaged for the three weekdays. The 150 Newport Center Drive Car Wash (based upon the traffic counts) currently generates approximately 819 daily vehicle trips, 54 of which occur during the morning ${ }^{1}$ peak hour and 75 of which occur during the evening peak hour (see Table 1). It should be noted that the car wash does not open prior to 10 AM.

[^6]Mr. Tod Ridgeway
RIDGEWAY DEVELOPMENT COMPANY
April 15, 2015

It been a pleasure to serve your needs on the Newport Beach Car Wash project. Should you have any questions or if we can be of further assistance, please do not hesitate to call at (714) 973-8383.

Sincerely,

KUNZMAN ASSOCIATES, INC.
Chur
Carl Ballard, liED GA
Principal

KUNZMAN ASSOCIATES, INC.


Principal
\#6069

## Table 1

## 150 Newport Center Drive Car Wash Count Summary

| Day of Week | Date | Peak Hour |  |  |  |  |  | Daily |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Morning ${ }^{1}$ |  |  | Evening |  |  |  |  |  |
|  |  | In | Out | Total | In | Out | Total | In | Out | Total |
| Tuesday | March 24, 2015 | 29 | 30 | 59 | 28 | 37 | 65 | 380 | 379 | 759 |
| Wednesday | March 25, 2015 | 28 | 16 | 44 | 35 | 52 | 87 | 403 | 403 | 806 |
| Thursday | March 26, 2015 | 34 | 25 | 59 | 37 | 38 | 75 | 444 | 448 | 892 |
| Average |  | 30 | 24 | 54 | 33 | 42 | 75 | 409 | 410 | 819 |

[^7]

Nunzman Associates, inc.

Kunzman Associates, Inc.

## MATT'S EXPRESS CAR WASH

## TRAFFIC IMPACT ANALYSIS (REVISED)

## April 22, 2014

Prepared by:

Robert Kunzman
Carl Ballard, LEED GA
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## I. Introduction

The purpose of this revised report is to provide an assessment of the traffic impacts resulting from the proposed development of the Matt's Express Car Wash project, and to identify the traffic mitigation measures necessary to maintain the established Level of Service standard for the elements of the impacted roadway system. The traffic issues related to the proposed land uses and development have been evaluated in the context of the California Environmental Quality Act.

The City of Redlands is the lead agency responsible for preparation of the traffic impact analysis, in accordance with the California Environmental Quality Act authorizing legislation. This report analyzes traffic impacts for the anticipated opening date with full occupancy of the development in Year 2015, at which time it will be generating traffic at its full potential, and for the Year 2035.

Although this is a technical report, every effort has been made to write the report clearly and concisely. To assist the reader with those terms unique to transportation engineering, a glossary of terms is provided in Appendix A.

## A. Project Description

The proposed development is located at the southwest corner of the Tennessee Street and Lugonia Avenue intersection in the City of Redlands. A vicinity map showing the project location is provided on Figure 1.

The approximately 1.06 acre project site is proposed to be developed with an automated car wash facility including 8,974 square feet of building area. Figure 2 illustrates the project site plan.

## B. Study Area

Regional access to the project site is provided by the I-10 and SR-210 Freeways. Local access is provided by various roadways in the vicinity of the site. The north-south roadway which will be most affected by the project is Tennessee Street. The east-west roadway which will be most affected by the project is Lugonia Avenue.

A series of scoping discussions were conducted with the City of Redlands to define the desired analysis locations for each future analysis year. In addition, staff from the City of Redlands has also been contacted to discuss the project and its associated travel patterns.

No analysis is required further than 5 miles from the project site. The roadway elements that must be analyzed are dependent on both the analysis year (project Opening Year or Year 2035) and project generated traffic volumes. The identification of the study area, and the intersections and highway segments requiring analysis, was based on an estimate of the two-way traffic volumes on the roadway segments near the project site. All arterial segments have been included in the analysis when the anticipated project volume equals or exceeds 50 two-way trips in the peak hours. The requirement is 100 two-way peak hour trips for freeways.

The project does not contribute traffic greater than the freeway threshold volume of 100 two-way peak hour trips. The project does not contribute traffic greater than the arterial link threshold volume of 50 two-way trips in the morning and evening peak hours in the adjacent County of San Bernardino.

## C. Analysis Methodology

The analysis of the traffic impacts from the proposed development and the assessment of the required mitigation measures were based on an evaluation of the existing and forecast traffic conditions in the vicinity of the site with and without the project. The following analysis years are considered in this report:

- Existing Conditions (2014)
- Existing Plus Project Conditions
- Project Opening Year Conditions (2015)
- Horizon Year Conditions (2035)

Existing intersection traffic conditions were established through morning and evening peak hour traffic counts obtained by Kunzman Associates, Inc. in January 2014 (see Appendix B).

In addition, truck classification counts were conducted at the study area intersections. The existing percent of trucks were used in the conversion of trucks to Passenger Car Equivalent's (see Appendix C).

Trip generation has been estimated based on a manual vehicular count of the existing Matt's Express Car Wash facility located in the City of Rialto on January 16, 2014.

To determine the trip distributions for the proposed project, peak hour traffic counts of the existing directional distribution of traffic for existing areas in the vicinity of the site, and other additional information on future development and traffic impacts in the area were reviewed.

The average daily traffic volume forecasts have been determined using the growth increment approach on the East Valley Traffic Model Year 2000 and Year 2035 average daily traffic volume forecasts (see Appendix C). This difference defines the growth in traffic over the 35 year period. The incremental growth in average daily traffic volume has been factored to reflect the forecast growth between Year 2014 and Year 2035. For this purpose, linear growth between the Year 2000 base condition and the forecast Year 2035 condition was assumed. Since the increment between Year 2014 and Year 2035 is 21 years of the 35 year time frame, a factor of 0.6 (i.e., 21/35) was used.

The Year 2035 without project daily and peak hour directional roadway segment volume forecasts have been determined using the growth increment approach on the East Valley Traffic Model Year 2000 and Year 2035 peak hour volumes. The growth increment calculation worksheets are shown in Appendix C. Current peak hour intersection approach/departure data is a necessary input to this approach. The existing traffic count data serves as both the starting point for the refinement process, and also provides important insight into current travel patterns and the relationship between peak hour and
daily traffic conditions. The initial turning movement proportions are estimated based upon the relationship of each approach leg's forecast traffic volume to the other legs forecast volumes at the intersection. The initial estimate of turning movement proportions is then entered into a spreadsheet program consistent with the National Cooperative Highway Research Program Report 255. A linear programming algorithm is used to calculate individual turning movements that match the known directional roadway segment volumes computed in the previous step. This program computes a likely set of intersection turning movements from intersection approach counts and the initial turning proportions from each approach leg.

The Opening Year (2015) traffic volumes have been interpolated from the Year 2035 traffic volumes based upon a portion of the future growth increment.

Project traffic volumes were then added to the model traffic volumes. Quality control checks and forecast adjustments were performed as necessary to ensure that all future traffic volume forecasts reflect a minimum of $10 \%$ growth over existing traffic volumes. The result of this traffic forecasting procedure is a series of traffic volumes suitable for traffic operations analysis.

The technique used to assess the capacity needs of an intersection is known as the Intersection Delay Method (see Appendix D) based on the Highway Capacity Manual Transportation Research Board Special Report 209. To calculate delay, the volume of traffic using the intersection is compared with the capacity of the intersection. The signalized intersections are considered deficient (Level of Service F) if the overall intersection critical volume to capacity ratio equals or exceeds 1.0 , even if the level of service defined by the delay value is below the defined Level of Service standard. The volume to capacity ratio is defined as the critical volumes divided by the intersection capacity. A volume to capacity ratio greater than 1.0 implies an infinite queue.

The Level of Service analysis for signalized intersections has been performed using optimized signal timing. This analysis has included an assumed lost time of two seconds per phase. Signal timing optimization has considered pedestrian safety and signal coordination requirements. Appropriate time for pedestrian crossings has also been considered in the signalized intersection analysis. The following formula has been used to calculate the pedestrian minimum times for all Highway Capacity Manual runs:
[(Curb to curb distance) / (4 feet/second)] +7 seconds.
For existing and Opening Year traffic conditions, saturation flow rates of 1,800 vehicles per hour of green for through and right turn lanes and 1,700 vehicles per lane for single left turn lanes, 1,600 vehicles per lane for dual left turn lanes and 1,500 vehicles per lane for triple left turn lanes have been assumed for the capacity analysis.

For Year 2035 traffic conditions, saturation flow rates of 1,900 vehicles per hour of green for through and right turn lanes and 1,800 vehicles per lane for single left turn lanes, 1,700 vehicles per lane for dual left turn lanes and 1,800 vehicles per lane for double right turn lanes have been assumed for the capacity analysis.

The peak hour traffic volumes have been adjusted to peak 15 minute volumes for analysis purposes using the existing observed peak 15 minute to peak hour factors for all scenarios analyzed. Where feasible improvements in accordance with the local jurisdiction's General Plan and which result in acceptable operations cannot be identified, the Year 2035 peak hour factor has been adjusted upwards to 0.95 . This is to account for the effects of congestion on peak spreading. Peak spreading refers to the tendency of traffic to spread more evenly across time as congestion increases.

The traffic mitigation needs anticipated at the time of the project opening with full occupancy and for the Year 2035 were combined into a summary of mitigation requirements and costs. The mitigation cost responsibility for the proposed development was estimated based on the percent of the increase in traffic from the existing condition to the Year 2035 that was attributed to the project-generated traffic.

## D. Definition of Deficiency and Significant Impact

The following definitions of deficiencies and significant impacts have been developed in accordance with the City of Redlands requirements.

## 1. Definition of Deficiency

The definition of an intersection deficiency has been obtained from the City of Redlands General Plan. The General Plan states that peak hour intersection operations of Level of Service C or better are generally acceptable. Therefore, any intersection operating at Level of Service D to F will be considered deficient. This project is located in the Redlands East Valley area where the peak hour intersection operations of Level of Service D or better are generally acceptable. Therefore, any intersection operating at Level of Service E or F will be considered deficient.

For freeway facilities, the Congestion Management Program controls the definition of deficiency for purposes of this study. The Congestion Management Program definition of deficiency is based on maintaining a Level of Service standard of Level of Service E or better, except where an existing Level of Service F condition is identified in the Congestion Management Program document (San Bernardino County Congestion Management Program Table 2-1). A Congestion Management Program deficiency is, therefore, defined as any freeway segment operating or projected to operate at Level of Service F, unless the segment is identified explicitly in the Congestion Management Program document.

The identification of a Congestion Management Program deficiency requires further analysis in satisfaction of Congestion Management Program requirements, including:

- Evaluation of the mitigation measures required to restore traffic operations to an acceptable level with respect to Congestion Management Program Level of Service standards.

■ Calculation of the project share of new traffic on the impacted Congestion Management Program facility during peak hours of traffic.

■ Estimation of the cost required to implement the improvements required to restore traffic operations to an acceptable Level of Service as described above.

This study incorporates each of these aspects for all locations where a Congestion Management Program deficiency is identified.

## 2. Definition of Significant Impact

The identification of significant impacts is a requirement of the California Environmental Quality Act. The City of Redlands General Plan and Circulation Element have been adopted in accordance with California Environmental Quality Act requirements, and any roadway improvements within the City of Redlands that are consistent with these documents are not considered a significant impact, so long as the project contributes its "fair share" funding for improvements.

A traffic impact is considered significant if the project both: i) contributes measurable traffic to and ii) substantially and adversely changes the Level of Service at any off-site location projected to experience deficient operations under foreseeable cumulative conditions, where feasible improvements consistent with the City of Redlands General Plan cannot be constructed.


Figure 2
Site Plan


## II. Existing Conditions

## A. Existing Roadway System

Figure 3 identifies the existing conditions for study area roadways. The number of through lanes for existing roadways and the existing intersection controls are identified.

Regional access to the project site is provided by the I-10 and SR-210 Freeways. Local access is provided by various roadways in the vicinity of the site. The north-south roadway which will be most affected by the project is Tennessee Street. The east-west roadway which will be most affected by the project is Lugonia Avenue.

## B. Existing Volumes

Figure 4 depicts the existing average daily traffic volumes. The existing average daily traffic volumes were obtained by Kunzman Associates, Inc. using the following formula for each intersection leg:

$$
\text { PM Peak Hour (Approach + Exit Volume) x } 11.5 \text { = Daily Leg Volume. }
$$

This is a conservative estimate and may over estimate the average daily traffic volumes.

Existing intersection traffic conditions were established through morning and evening peak hour traffic counts obtained by Kunzman Associates, Inc. from January 2014 (see Appendix B) and shown on Figures 5 and 6, respectively. Explicit peak hour factors have been calculated using the data collected for this effort as well. The morning and evening peak hour traffic volumes were identified by counting the two-hour periods from 7:00 AM - 9:00 AM and 4:00 PM - 6:00 PM.

In addition, truck classification counts were conducted at the study area intersections. The existing percent of trucks were used in the conversion of trucks to Passenger Car Equivalent's (see Appendix C).

## C. Existing Level of Service

The Existing delay and Level of Service for intersections in the vicinity of the project are shown in Table 1. For Existing traffic conditions, the study area intersections are currently operating within acceptable Levels of Service, except for the following study area intersection that currently operates at an unacceptable Level of Service during the evening peak hour:

Tennessee Street (NS) at:
Project South Access - \#3

Existing delay worksheets are provided in Appendix D.

## D. Existing Traffic Signal Warrant Analysis

A traffic signal appears to currently be warranted at the following study area intersection for existing traffic conditions (see Appendix E):

Tennessee Street (NS) at:
Project South Access (EW) - \#3

The unsignalized intersection has been evaluated for a traffic signal using the California Department of Transportation Warrant 3 Peak Hour traffic signal warrant analysis, as specified in the California Manual of Uniform Traffic Control Devices.

Per discussions with the City of Redlands staff and engineering judgment, a traffic signal is not recommended at this location because of its close proximity to the existing traffic signal located at Tennessee Street and Lugonia Avenue.

## E. Planned Transportation Improvements and Relationship to General Plan

The City of Redlands General Plan Circulation Element is shown on Figure 7. Existing and future roadways are included in the Circulation Element of the General Plan and are graphically depicted on Figure 7. This figure shows the nature and extent of arterial highways that are needed to adequately serve the ultimate development depicted by the Land Use Element of the General Plan. The City of Redlands General Plan roadway crosssections are shown on Figure 8.

Table 1

Existing Intersection Delay and Level of Service

| Intersection | Traffic <br> Control ${ }^{3}$ | Intersection Approach Lanes ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  | Peak Hour Delay-LOS ${ }^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |  |  |
|  |  | L | T | R | L | T | R | L | T | R | L | T | R | Morning | Evening |
| Tennessee Street (NS) at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lugonia Avenue (EW) - \#1 | TS | 1 | 1 | 1 | 1 | 1 | d | 1 | 2 | 1 | 1 | 0.5 | 0.5 | 27.1-C | 36.4-D |
| Project South Access (EW) - \#3 | CSS | 0 | 1.5 | 0.5 | 0.5 | 1.5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 16.3-C | 37.5-E |

[^8]${ }^{2}$ Delay and level of service calculated using the following analysis software: Traffix, Version 7.9.0215. Per the Highway Capacity Manual, overall average intersection delay and level of service are shown for intersections with traffic signal or all way stop control. For intersections with cross street stop control, the delay and level of service for the worst individual movement (or movements sharing a single lane) are shown.

[^9]Figure 3
Existing Through Travel Lanes and Intersection Controls


Figure 4
Existing Average Daily Traffic Volumes


Figure 5 Existing Morning Peak Hour Intersection Turning Movement Volumes


Figure 6
Existing Evening Peak Hour Intersection Turning Movement Volumes

Figure 7
City of Redlands General Plan Circulation Element

Legend

|  | Freeway |
| :---: | :---: |
|  | Major Arterial |
| $\underline{\square}$ | Minor Arterial |
| - | Collector |
| \|1/II| | Linear Park |
| $\longrightarrow$ | Rail Corridor |
| 톺․ | Major Arterial (Proposed) |
| 5ne | Minor Arterial (Proposed) |
| - | Collector (Proposed) |

Figure 8
City of Redlands General Plan Roadway Cross-Sections

## LOCPAL



## colt EcTor - Rasidanila



GOLLECTOR = IndustriaI


MANER ARTERIAL - 2 LANAK + L II TUTH


MINOR AFTEREAL - 4 Lanes Undivided


MAMDR ARTERTAL - 6 Larms Divided


## III. Project Traffic

## A. Project Description

The approximately 1.06 acre project site is proposed to be developed with an automated car wash facility including 8,974 square feet of building area. The project will have access to Tennessee Street.

## B. Trip Generation

The trips generated by the project are determined by multiplying an appropriate trip generation rate by the quantity of land use. Trip generation rates are predicated on the assumption that energy costs, the availability of roadway capacity, the availability of vehicles to drive, and life styles remain similar to what are known today. A major change in these variables may affect trip generation rates.

The trip generation rates for a carwash have been documented by the Institute of Transportation Engineers, Trip Generation, 9th Edition, 2012 in Land Use Codes 947 and 948. Land Use Code 947 is based on the number of car washing stalls and Land Use Code 948 is based on the square footage of the car wash or the number of wash stalls.

Land Use Code 947 is projected to generate approximately (not reported) daily vehicle trips, (not reported) of which will occur during the morning peak hour and 6 of which will occur during the evening peak hour.

Land Use Code 948 is projected to generate approximately (not reported) daily vehicle trips, (not reported) of which will occur during the morning peak hour and 119 or 78 of which will occur during the evening peak hour.

It should be noted that the Institute of Transportation Engineers does not provide a Land Use Code that exactly represents the proposed project and if they did they do not provide the required data to conduct this traffic impact analysis.

The trip generation rates for a carwash have been documented by the San Diego Association of Governments, NOT SO BRIEF GUIDE OF VEHICULAR TRAFFIC GENERATION RATES FOR THE SAN DIEGO REGION, April 2002. The Automatic Carwash Land Use is based on a carwash facility as a whole.

An Automatic Carwash site is projected to generate approximately 900 daily vehicle trips, 36 of which will occur during the morning peak hour and 82 of which will occur during the evening peak hour.

This trip generation for the site was originally proposed for this analysis but the City of Redlands suggested that the applicants existing facility in the City of Rialto be surveyed to determine the exact trip generation of a nearly identical site.

Trip generation rates were determined for daily traffic, morning peak hour inbound and outbound traffic, and evening peak hour inbound and outbound traffic for the proposed land use. By multiplying the trip generation rates by the land use quantity, the traffic volumes are determined. Table 2 shows the project trip generation, which is based upon a manual vehicular count of the existing Matt's Express Car Wash facility located in the City of Rialto on January 16, 2014.

As shown in Table 2, the proposed development is projected to generate approximately 944 daily vehicle trips, 58 of which will occur during the morning peak hour and 134 of which will occur during the evening peak hour.

As a double check of this data, one week of data from January 2014, February 2014, March 2014, and April 2014 were provided to us by the applicant. This data has been processed to determine the daily, morning peak hour, and evening peak hour traffic volumes.

The minimum average day during a week site generation was 742 daily vehicle trips, 32 of which occurred during the morning peak hour and 50 of which occurred during the evening peak hour.

The average average day during a week site generation was 832 daily vehicle trips, 44 of which occurred during the morning peak hour and 86 of which occurred during the evening peak hour.

The maximum average day during a week site generation was 958 daily vehicle trips, 50 of which occurred during the morning peak hour and 104 of which occurred during the evening peak hour.

It should be noted that the proposed Redlands facility is going to be at a different price point than the Rialto facility. The price of a carwash at the proposed Redlands facility is a 225 percent increase of the price of a carwash at the Rialto facility. The Redlands facility is projected to have less vehicle trips.

The trip generation used in this analysis is a conservative representation of the trips that are likely to be seen at the proposed project site.

## C. Trip Distribution

Figures 9 and 10 contain the directional distributions of the project traffic for the proposed land use.

To determine the trip distributions for the proposed project, peak hour traffic counts of the existing directional distribution of traffic for existing areas in the vicinity of the site, and other additional information on future development and traffic impacts in the area were reviewed.

## D. Trip Assignment

Based on the identified trip generation and distributions, project average daily traffic volumes have been calculated and shown on Figure 11. Morning and evening peak hour intersection turning movement volumes expected from the project are shown on Figures 12 and 13 , respectively.

## E. Traffic Contribution Test

No analysis is required further than 5 miles from the project site. The roadway elements that must be analyzed are dependent on both the analysis year (project Opening Year or Year 2035) and project generated traffic volumes. The identification of the study area, and the intersections and highway segments requiring analysis, was based on an estimate of the two-way traffic volumes on the roadway segments near the project site. All arterial segments have been included in the analysis when the anticipated project volume equals or exceeds 50 two-way trips in the peak hours. The requirement is 100 two-way peak hour trips for freeways. Figure 14 graphically depicts the project traffic contribution test volumes on all of the roadway segments adjacent to the potential intersection analysis locations until the project volume contribution has clearly dropped below the 50 trip threshold.

The project does not contribute traffic greater than the freeway threshold volume of 100 two-way peak hour trips. The project does not contribute traffic greater than the arterial link threshold volume of 50 two-way trips in the morning and evening peak hours in the adjacent County of San Bernardino.

Table 2

## Project Trip Generation ${ }^{1}$

| Land Use | Quantity | Units ${ }^{2}$ | Peak Hour |  |  |  |  |  | Daily |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Morning |  |  | Evening |  |  |  |
|  |  |  | Inbound | Outbound | Total | Inbound | Outbound | Total |  |
| Trip Generation Rates |  |  |  |  |  |  |  |  |  |
| Automatic Carwash |  | Site | 29.00 | 29.00 | 58.00 | 67.00 | 67.00 | 134.00 | 944.00 |
| Trips Generated |  |  |  |  |  |  |  |  |  |
| Automatic Carwash | 1 | Site | 29 | 29 | 58 | 67 | 67 | 134 | 944 |

[^10]Figure 9
Project Outbound Trip Distribution




Figure 12
Project Morning Peak Hour Intersection Turning Movement Volumes


Figure 13

## Project Evening Peak Hour Intersection Turning Movement Volumes



Figure 14
Project Contribution Test Volumes

$27=$ Project Evening Peak Hour Volumes


## IV. Future Conditions

## A. Future Volumes

As described within Section I.C., the Year 2035 average daily traffic volume forecasts with the project are developed using a growth increment process based on volumes predicted by the East Valley Traffic Model Year 2000 and Year 2035 traffic models. The growth increment for Year 2035 on each roadway segment is the increase in East Valley Traffic Model volumes from existing Year 2014 to Year 2035. The final Year 2035 roadway segment volume used for analysis purposes is then determined by adding the Year 2035 growth increment volume to the existing counted volume.

The Opening Year (2015) traffic projections have been interpolated between Year 2035 traffic volumes and existing traffic volumes utilizing a portion of the growth increment (see Section I.C.). Project traffic volumes for all future projections were estimated using the manual approach.

## 1. Existing Plus Project

The average daily traffic volumes for Existing Plus Project traffic conditions have been determined. Existing Plus Project average daily traffic volumes are shown on Figure 15.
2. Opening Year (2015) Without Project

The average daily traffic volumes for Opening Year (2015) Without Project traffic conditions have been determined as described above using the growth interpolation process (see Section I.C.). Opening Year (2015) Without Project average daily traffic volumes are shown on Figure 16.
3. Opening Year (2015) With Project

The average daily traffic volumes for Opening Year (2015) With Project traffic conditions have been determined as described above using the volume addition process (see Section I.C.). Opening Year (2015) With Project average daily traffic volumes are shown on Figure 17.
4. Year 2035 Without Project

The average daily traffic volumes for Year 2035 Without Project traffic conditions have been determined as described above using the growth increment process (see Section I.C.). Year 2035 Without Project average daily traffic volumes are shown on Figure 18.
5. Year 2035 With Project

The average daily traffic volumes for Year 2035 With Project traffic conditions have been determined as described above using the volume addition process (see Section I.C.). Year 2035 With Project average daily traffic volumes are shown on Figure 19.

## B. Future Level of Service

1. Existing Plus Project

The Existing Plus Project delay and Level of Service for the study area roadway network are shown in Table 3. Table 3 shows delay values based on the existing geometrics at the study area intersections. Existing Plus Project delay calculation worksheets are provided in Appendix D. Existing Plus Project morning and evening peak hour intersection turning movement volumes are shown on Figures 20 and 21, respectively.

For Existing Plus Project traffic conditions, the following study area intersection is projected to operate at an unacceptable Level of Service during the evening peak hour:

Tennessee Street (NS) at:
Project South Access - \#3

For Existing Plus Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.

## 2. Opening Year (2015) Without Project

The Opening Year (2015) Without Project delay and Level of Service for the study area roadway network without the proposed project are shown in Table 4. Table 4 shows delay values based on the existing geometrics at the study area intersections. Opening Year (2015) Without Project delay calculation worksheets are provided in Appendix D. Opening Year (2015) Without Project morning and evening peak hour intersection turning movement volumes are shown on Figures 22 and 23, respectively.

For Opening Year (2015) Without Project traffic conditions, the following study area intersection is projected to operate at an unacceptable Level of Service during the evening peak hour:

Tennessee Street (NS) at:
South Project Access - \#3

For Opening Year (2015) Without Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.
3. Opening Year (2015) With Project

The Opening Year (2015) With Project delay and Level of Service for the study area roadway network with the proposed project are shown in Table 5 . Table 5 shows delay values based on the existing geometrics at the study area intersections. Opening Year (2015) With Project delay calculation worksheets are provided in Appendix D. Opening Year (2015) With Project morning and evening peak hour intersection turning movement volumes are shown on Figures 24 and 25, respectively.

For Opening Year (2015) With Project traffic conditions, the following study area intersection is projected to operate at an unacceptable Level of Service during the evening peak hours:

```
Tennessee Street (NS) at:
    South Project Access - #3
```

For Opening Year (2015) With Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.
4. Year 2035 Without Project

The Year 2035 delay and Level of Service for the study area roadway network without the proposed project are shown in Table 6. Table 6 shows delay values based on the existing geometrics at the study area intersections. Year 2035 Without Project delay calculation worksheets are provided in Appendix D. Year 2035 Without Project morning and evening peak hour intersection turning movement volumes are shown on Figures 26 and 27, respectively.

For Year 2035 Without Project traffic conditions, the following study area intersections are projected to operate at unacceptable Levels of Service during the peak hours:

```
Tennessee Street (NS) at:
    Lugonia Avenue - #1
    Project South Access - #3
```

For Year 2035 Without Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.
5. Year 2035 With Project

The Year 2035 With Project delay and Level of Service for the study area roadway network with the proposed project are shown in Table 7. Table 7 shows delay values based on the existing geometrics at the study area intersections. Year 2035 With Project delay calculation worksheets are provided in Appendix D. Year 2035 With Project morning and evening peak hour intersection turning movement volumes are shown on Figures 28 and 29, respectively.

For Year 2035 With Project traffic conditions, the following study area intersections are projected to operate at unacceptable Levels of Service during the peak hours:

Tennessee Street (NS) at:
Lugonia Avenue - \#1
Project South Access - \#3

For Year 2035 With Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.

Table 3

Existing Plus Project Intersection Delay and Level of Service

| Intersection | Traffic Control ${ }^{3}$ | Intersection Approach Lanes ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  | Peak Hour$\text { Delay-LOS }{ }^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |  |  |
|  |  | L | T | R | L | T | R | L | T | R | L | T | R | Morning | Evening |
| Tennessee Street (NS) at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lugonia Avenue (EW) - \#1 | TS | 1 | 1 | 1 | 1 | 1 | d | 1 | 2 | 1 | 1 | 0.5 | 0.5 | 27.1-C | 36.7-D |
| Project Project Access (EW) - \#2 | CSS | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | $\underline{1}$ | 0 | 0 | 0 | 10.4-B | 12.9-B |
| Project South Access (EW) - \#3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - Without Improvements | CSS | 0 | 1.5 | 0.5 | 0.5 | 1.5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 19.2-C | 68.3-F |
| - With Improvements - No Traffic Signal | CSS | $\underline{1}$ | 1.5 | 0.5 | $\underline{1}$ | 1.5 | 0.5 | 0 | $\underline{1}$ | 0 | 0 | 1 | 0 | 19.2-C | 68.2-F |
| - With Improvements - Traffic Signal | TS | $\underline{1}$ | 1.5 | 0.5 | $\underline{1}$ | 1.5 | 0.5 | 0 | $\underline{1}$ | 0 | 0 | 1 | 0 | 8.0-A | 7.9-A |

[^11]${ }^{2}$ Delay and level of service calculated using the following analysis software: Traffix, Version 7.9.0215. Per the Highway Capacity Manual, overall average intersection
delay and level of service are shown for intersections with traffic signal or all way stop control. For intersections with cross street stop control, the delay and level of service for the worst individual movement (or movements sharing a single lane) are shown.
${ }^{3}$ TS = Traffic Signal; CSS = Cross Street Stop

Table 4

## Opening Year (2015) Without Project Intersection Delay and Level of Service

| Intersection | Traffic Control ${ }^{3}$ | Intersection Approach Lanes ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  | Peak Hour Delay-LOS ${ }^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |  |  |
|  |  | L | T | R | L | T | R | L | T | R | L | T | R | Morning | Evening |
| Tennessee Street (NS) at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lugonia Avenue (EW) - \#1 | TS | 1 | 1 | 1 | 1 | 1 | d | 1 | 2 | 1 | 1 | 0.5 | 0.5 | 27.5-C | 36.0-D |
| Project South Access (EW) - \#3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - Without Improvements | CSS | 0 | 1.5 | 0.5 | 0.5 | 1.5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 17.3-C | 42.2-E |
| - With Improvements | TS | 0 | 1.5 | 0.5 | $\underline{1}$ | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 7.7-A | 6.8-A |

[^12][^13]
## Table 5

## Opening Year (2015) With Project Intersection Delay and Level of Service

| Intersection | Traffic Control ${ }^{3}$ | Intersection Approach Lanes ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  | Peak Hour Delay-LOS ${ }^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |  |  |
|  |  | L | T | R | L | T | R | L | T | R | L | T | R | Morning | Evening |
| Tennessee Street (NS) at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lugonia Avenue (EW) - \#1 | TS | 1 | 1 | 1 | 1 | 1 | d | 1 | 2 | 1 | 1 | 0.5 | 0.5 | 27.8-C | 37.7-D |
| Project North Access (EW) - \#2 | CSS | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | $\underline{1}$ | 0 | 0 | 0 | 10.4-B | 13.2-B |
| Project South Access (EW) - \#3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - Without Improvements | CSS | 0 | 1.5 | 0.5 | 0.5 | 1.5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 20.7-C | 82.3-F |
| - With Improvements - No Traffic Signal | CSS | $\underline{1}$ | 1.5 | 0.5 | $\underline{1}$ | 1.5 | 0.5 | 0 | $\underline{1}$ | 0 | 0 | 1 | 0 | 20.7-C | 82.1-F |
| - With Improvements - Traffic Signal | TS | $\underline{1}$ | 1.5 | 0.5 | 1 | 1.5 | 0.5 | 0 | 1 | 0 | 0 | 1 | 0 | 8.1-A | 7.9-A |

[^14]${ }^{2}$ Delay and level of service calculated using the following analysis software: Traffix, Version 7.9.0215. Per the Highway Capacity Manual, overall average intersection
delay and level of service are shown for intersections with traffic signal or all way stop control. For intersections with cross street stop control, the delay and level of service for the worst individual movement (or movements sharing a single lane) are shown.
${ }^{3}$ TS $=$ Traffic Signal; CSS $=$ Cross Street Stop

Table 6

Year 2035 Without Project Intersection Delay and Level of Service

| Intersection | Traffic Control ${ }^{3}$ | Intersection Approach Lanes ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  | Peak Hour Delay-LOS ${ }^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |  |  |
|  |  | L | T | R | L | T | R | L | T | R | L | T | R | Morning | Evening |
| Tennessee Street (NS) at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lugonia Avenue (EW) - \#1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - Without Improvements | TS | 1 | 1 | 1 | 1 | 1 | d | 1 | 2 | 1 | 1 | 0.5 | 0.5 | 46.3-D | 64.3-E |
| - With Improvements | TS ${ }^{4}$ | 1 | 1 | 1 | 1 | 1 | d | 1 | 2 | 1 | 1 | 0.5 | 0.5 | 43.5-D | 49.9-D |
| Project South Access (EW) - \#3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - Without Improvements | CSS | 0 | 1.5 | 0.5 | 0.5 | 1.5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 53.2-F | 99.9-F ${ }^{5}$ |
| - With Improvements | TS | 0 | 1.5 | 0.5 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2.8-A | 2.2-A |

[^15][^16]${ }^{3}$ TS = Traffic Signal; CSS = Cross Street Stop
${ }^{4}$ Traffic signal improvements proposed.
${ }^{5}$ 99.9-F = Delay High, Intersection Unstable, Level of Service F.

## Table 7

## Year 2035 With Project Intersection Delay and Level of Service

| Intersection | Traffic Control ${ }^{3}$ | Intersection Approach Lanes ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  | Peak Hour Delay-LOS ${ }^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |  |  |
|  |  | L | T | R | L | T | R | L | T | R | L | T | R | Morning | Evening |
| Tennessee Street (NS) at: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lugonia Avenue (EW) - \#1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - Without Improvements | TS | 1 | 1 | 1 | 1 | 1 | d | 1 | 2 | 1 | 1 | 0.5 | 0.5 | 46.8-D | 70.6-E |
| - With Improvements | $\underline{T S}{ }^{4}$ | 1 | 1 | 1 | 1 | 1 | d | 1 | 2 | 1 | 1 | 0.5 | 0.5 | 44.0-D | 43.3-D |
| Project North Access (EW) - \#2 | CSS | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | $\underline{1}$ | 0 | 0 | 0 | 11.4-B | 19.4-C |
| Project South Access (EW) - \#3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - Without Improvements | CSS | 0 | 1.5 | 0.5 | 0.5 | 1.5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 98.1-F | 99.9-F ${ }^{5}$ |
| - With Improvements - No Traffic Signal | CSS | 1 | 1.5 | 0.5 | 1 | 1.5 | 0.5 | 0 | $\underline{1}$ | 0 | 0 | 1 | 0 | 98.0-F | 99.9-F |
| - With Improvements - Traffic Signal | TS | 1 | 1.5 | 0.5 | 1 | 1.5 | 0.5 | 0 | $\underline{1}$ | 0 | 0 | 1 | 0 | 3.3-A | 3.0-A |

[^17]${ }^{2}$ Delay and level of service calculated using the following analysis software: Traffix, Version 7.9.0215. Per the Highway Capacity Manual, overall average intersection delay and level of service are shown for intersections with traffic signal or all way stop control. For intersections with cross street stop control, the delay and level of service for the worst individual movement (or movements sharing a single lane) are shown

[^18]${ }^{5}$ 99.9-F = Delay High, Intersection Unstable, Level of Service F.

Figure 15
Existing Plus Project Average Daily Traffic Volumes


Figure 16
Opening Year (2015) Without Project Average Daily Traffic Volumes


Figure 17
Opening Year (2015) With Project Average Daily Traffic Volumes


Figure 18
Year 2035 Without Project Average Daily Traffic Volumes


Figure 19

## Year 2035 With Project Average Daily Traffic Volumes




Figure 21
Existing Plus Project Evening Peak Hour Intersection Turning Movement Volumes


Figure 22
Opening Year (2015) Without Project Morning Peak Hour Intersection Turning Movement Volumes


Figure 23
Opening Year (2015) Without Project
Evening Peak Hour Intersection Turning Movement Volumes


Figure 24
Opening Year (2015) With Project Morning Peak Hour Intersection Turning Movement Volumes


Figure 25
Opening Year (2015) With Project Evening Peak Hour Intersection Turning Movement Volumes


Figure 26
Year 2035 Without Project Morning Peak Hour Intersection Turning Movement Volumes


Figure 27
Year 2035 Without Project Evening Peak Hour Intersection Turning Movement Volumes


Figure 28
Year 2035 With Project Morning Peak Hour Intersection Turning Movement Volumes


Figure 29
Year 2035 With Project Evening Peak Hour Intersection Turning Movement Volumes


## V. Project Mitigation

## A. Required Improvements and Costs

Improvements that will eliminate all anticipated roadway operational deficiencies throughout the study area have been identified for Existing Plus Project, Opening Year (2015), and Year 2035 traffic conditions. The improvements were determined through the operations analysis of Section IV.

The approximate costs for the Year 2035 improvements have generally been estimated using cost guidelines in the Congestion Management Program Handbook (see Appendix F). A unit cost of $\$ 400,000$ for installation of a traffic signal has been substituted for the somewhat lower value cited in the Congestion Management Program materials. For adding a through lane, a unit cost of $\$ 289,720$ has been assumed. The needed improvements and resulting costs are summarized in Table 8 for the study area intersections.

The total cost of needed and unfunded intersection improvements is $\$ 320,000$.

## B. Project Contribution and Fair Share Costs

The project fair share contributions have also been calculated for Year 2035 improvement locations. The project share of cost has been based on the proportion of project peak hour traffic contributed to the improvement location relative to the total new peak hour Year 2035 traffic volume.

Table 8 presents a summary of improvement cost and project cost shares at the Year 2035 intersection improvement locations. The intersection fair share cost calculations are based on the evening peak hour traffic volumes. As shown in Table 8, the project's fair share of identified intersection costs is $\$ 13,529$.

The dollar figures are rough order of magnitude estimates only. They are intended only for the discussion purposes of this traffic impact analysis, and do not imply any legal responsibility or formula for contributions or mitigation.

As mitigation for the potential traffic impacts, the proposed project shall contribute through an adopted traffic impact fee program in addition to any fair share contributions shown within the traffic study which is not covered within this fee program.

Table 8
Project Fair Share Intersection Traffic Contribution

| Intersection | Improvement | Cost ${ }^{1}$ | $\begin{gathered} \text { Type } \\ \text { of } \\ \text { Improvement } \\ \hline \end{gathered}$ | Peak Hour | Existing Traffic | Year 2035 <br> With <br> Project <br> Traffic | $\begin{aligned} & \text { Project } \\ & \text { Traffic } \end{aligned}$ | Total <br> New <br> Traffic | Project <br> \% of <br> New <br> Traffic | $\begin{gathered} \text { Project } \\ \text { Cost } \\ \text { Share } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tennessee Street (NS) at: |  |  |  |  |  |  |  |  |  |  |
| Lugonia Avenue (EW) - \#1 |  |  |  | Morning | 1,222 | 2,332 | 42 | 1,110 | 3.8\% | \$1,892 |
|  | Install a Northbound Right Turn Overlap | \$50,000 | Fair Share | Evening | 2,539 | 4,481 | 100 | 1,942 | 5.1\% | \$2,575 |
|  |  |  |  | Morning | 848 | 1,648 | 58 | 800 | 7.3\% | \$10,000 |
|  | Install a Northbound Left Turn Lane | \$10,000 | Project | Evening | 1,519 | 2,913 | 133 | 1,394 | 9.5\% | \$10,000 |
| Project South Access (EW) - \#3 |  |  |  | Morning | 848 | 1,648 | 58 | 800 | 7.3\% | \$725 |
|  | Install a Southbound Left Turn Lane | \$10,000 | Fair Share | Evening | 1,519 | 2,913 | 133 | 1,394 | 9.5\% | \$954 |
|  |  |  |  | Morning | 848 | 1,648 | 58 | 800 | 0.0\% | \$0 |
|  | Install a Traffic Signal ${ }^{2}$ | \$250,000 | Not Recommended | Evening | 1,519 | 2,913 | 133 | 1,394 | 0.0\% | \$0 |
| Total |  | \$320,000 |  |  |  |  |  |  |  | \$13,529 |

${ }^{1}$ See Appendix F.
${ }^{2}$ Per discussions with City of Redlands staff and engineering judgment, a traffic signal is not recommended at this location because of it's close proximity to the existing traffic signal located at Tennessee Street and Lugonia Avenue.

## VI. Conclusions and Recommendations

## A. Summary

The traffic issues related to the proposed land use and development have been evaluated in the context of the California Environmental Quality Act.

The City of Redlands is the lead agency responsible for preparation of the traffic impact analysis, in accordance with the California Environmental Quality Act authorizing legislation. This report analyzes traffic impacts for the anticipated opening date with full occupancy of the development in Year 2015, at which time it will be generating traffic at its full potential, and for the Year 2035.

A series of scoping discussions were conducted with the City of Redlands to define the desired analysis locations for each future analysis year. In addition, staff from the City of Redlands has also been contacted to discuss the project and its associated travel patterns.

No analysis is required further than 5 miles from the project site. The roadway elements that must be analyzed are dependent on both the analysis year (project Opening Year or Year 2035) and project generated traffic volumes. The identification of the study area, and the intersections and highway segments requiring analysis, was based on an estimate of the two-way traffic volumes on the roadway segments near the project site. All arterial segments have been included in the analysis when the anticipated project volume equals or exceeds 50 two-way trips in the peak hours. The requirement is 100 two-way peak hour trips for freeways.

The project does not contribute traffic greater than the freeway threshold volume of 100 two-way peak hour trips. The project does not contribute traffic greater than the arterial link threshold volume of 50 two-way trips in the morning and evening peak hours in the adjacent County of San Bernardino.

The average daily traffic volume forecasts have been determined using the growth increment approach on the East Valley Traffic Model Year 2000 and Year 2035 average daily traffic volume forecasts (see Appendix C). This difference defines the growth in traffic over the 35 year period. The incremental growth in average daily traffic volume has been factored to reflect the forecast growth between Year 2014 and Year 2035. For this purpose, linear growth between the Year 2000 base condition and the forecast Year 2035 condition was assumed. Since the increment between Year 2014 and Year 2035 is 21 years of the 35 year time frame, a factor of 0.6 (i.e., $21 / 35$ ) was used.

The Year 2035 without project daily and peak hour directional roadway segment volume forecasts have been determined using the growth increment approach on the East Valley Traffic Model Year 2000 and Year 2035 peak hour volumes. The growth increment calculation worksheets are shown in Appendix C. Current peak hour intersection approach/departure data is a necessary input to this approach. The existing traffic count data serves as both the starting point for the refinement process, and also provides
important insight into current travel patterns and the relationship between peak hour and daily traffic conditions. The initial turning movement proportions are estimated based upon the relationship of each approach leg's forecast traffic volume to the other legs forecast volumes at the intersection. The initial estimate of turning movement proportions is then entered into a spreadsheet program consistent with the National Cooperative Highway Research Program Report 255. A linear programming algorithm is used to calculate individual turning movements that match the known directional roadway segment volumes computed in the previous step. This program computes a likely set of intersection turning movements from intersection approach counts and the initial turning proportions from each approach leg.

The Opening Year (2015) traffic volumes have been interpolated from the Year 2035 traffic volumes based upon a portion of the future growth increment.

Project traffic volumes were then added to the East Valley Traffic Model traffic volumes. Quality control checks and forecast adjustments were performed as necessary to ensure that all future traffic volume forecasts reflect a minimum of $10 \%$ growth over existing traffic volumes. The result of this traffic forecasting procedure is a series of traffic volumes suitable for traffic operations analysis.

## B. Existing Conditions

Regional access to the project site is provided by the I-10 Freeway and SR-210 Freeway. Local access is provided by various roadways in the vicinity of the site. The east-west roadway which will be most affected by the project is Lugonia Avenue. The north-south roadway which will be most affected by the project is Tennessee Street.

For Existing traffic conditions, the study area intersections are currently operating within acceptable Levels of Service, except for the following study area intersection that currently operates at an unacceptable Level of Service during the evening peak hour:

Tennessee Street (NS) at:
Project South Access - \#3
A traffic signal appears to currently be warranted at the following study area intersection for existing traffic conditions (see Appendix E):

Tennessee Street (NS) at:
Project South Access (EW) - \#3
The unsignalized intersection has been evaluated for a traffic signal using the California Department of Transportation Warrant 3 Peak Hour traffic signal warrant analysis, as specified in the California Manual of Uniform Traffic Control Devices.

Per discussions with the City of Redlands staff and engineering judgment, a traffic signal is not recommended at this location because of its close proximity to the existing traffic signal located at Tennessee Street and Lugonia Avenue.

## C. Project Traffic

Trip generation rates were determined for daily traffic and morning peak hour inbound and outbound traffic, and evening peak hour inbound and outbound traffic for the proposed land use. By multiplying the trip generation rates by the land use quantity, the traffic volumes are determined. Project trip generation is based upon a manual vehicular count of the existing Matt's Express Car Wash facility located in the City of Rialto on January 16, 2014.

The proposed development is projected to generate approximately 944 daily vehicle trips, 58 of which will occur during the morning peak hour and 134 of which will occur during the evening peak hour.

To determine the trip distributions for the proposed project, peak hour traffic counts of the existing directional distribution of traffic for existing areas in the vicinity of the site, and other additional information on future development and traffic impacts in the area were reviewed.

## D. Future Conditions

An Existing Plus Project, Opening Year (2015) analysis, and Year 2035 analysis are included in this report. The Existing Plus Project traffic operations analysis is summarized in Table 3. Opening Year (2015) traffic operations analysis has been completed for the morning and evening peak hours and are shown in Tables 4 and 5. Morning and evening peak hour traffic operations analysis are summarized in Tables 6 and 7 for the Year 2035.

## 1. Existing Plus Project

For Existing Plus Project traffic conditions, the following study area intersection is projected to operate at an unacceptable Level of Service during the evening peak hour:

Tennessee Street (NS) at:
Project South Access - \#3
For Existing Plus Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.

## 2. Opening Year (2015) Without Project

For Opening Year (2015) Without Project traffic conditions, the following study area intersection is projected to operate at an unacceptable Level of Service during the evening peak hour:

Tennessee Street (NS) at:
South Project Access - \#3

For Opening Year (2015) Without Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.
3. Opening Year (2015) With Project

For Opening Year (2015) With Project traffic conditions, the following study area intersection is projected to operate at an unacceptable Level of Service during the evening peak hours:

Tennessee Street (NS) at:
South Project Access - \#3

For Opening Year (2015) With Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.
4. Year 2035 Without Project

For Year 2035 Without Project traffic conditions, the following study area intersections are projected to operate at unacceptable Levels of Service during the peak hours:

```
Tennessee Street (NS) at:
    Lugonia Avenue - #1
    Project South Access - #3
```

For Year 2035 Without Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.
5. Year 2035 With Project

For Year 2035 With Project traffic conditions, the following study area intersections are projected to operate at unacceptable Levels of Service during the peak hours:

Tennessee Street (NS) at:
Lugonia Avenue - \#1
Project South Access - \#3

For Year 2035 With Project traffic conditions, the study area intersections are projected to operate within acceptable Levels of Service during the peak hours, with improvements.

## E. Cost Summary

Improvements that will eliminate all anticipated roadway operational deficiencies throughout the study area have been identified for Existing Plus Project, Opening Year
(2013), and Year 2035 traffic conditions. The improvements were determined through the operations analysis of Section IV.

The total cost of needed and unfunded intersection improvements is $\$ 320,000$.

Table 8 presents a summary of improvement cost and project cost shares at the Year 2035 intersection improvement locations. The intersection fair share cost calculations are based on the evening peak hour traffic volumes. As shown in Table 8, the project's fair share of identified intersection costs is $\$ 13,529$.

The dollar figures are rough order of magnitude estimates only. They are intended only for the discussion purposes of this traffic impact analysis, and do not imply any legal responsibility or formula for contributions or mitigation.

As mitigation for the potential traffic impacts, the proposed project shall contribute through an adopted traffic impact fee program in addition to any fair share contributions shown within the traffic study which is not covered within this fee program.

## F. Recommendations

The recommendations in this section address on-site improvements, off-site improvements and the phasing of all necessary study area transportation improvements.

## 1. On-Site Improvements

On-site improvements and improvements adjacent to the site will be required in conjunction with the proposed development to ensure adequate circulation within the project itself (see Figure 30 ).

Construct Lugonia Avenue from the west project boundary to Tennessee Street at its ultimate half-section width as a Major Arterial (110 foot right-of-way) including landscaping and parkway improvements in conjunction with development, as necessary.

Construct Tennessee Street from the south project boundary to Lugonia Avenue at its ultimate half-section width as a Collector (64 foot right-of-way) including landscaping and parkway improvements in conjunction with development, as necessary.
"KEEP CLEAR" should be painted at the intersection of Tennessee Street and Project South Access to prevent vehicles from blocking the roadway preventing vehicles desiring to enter and exit the project site.

Sight distance at project accesses shall comply with standard California Department of Transportation and City of Redlands sight distance standards. The final grading, landscaping, and street improvement plans shall demonstrate that sight distance standards are met. Such plans must be reviewed by the City and approved as consistent with this measure prior to issue of grading permits.

On-site traffic signing and striping should be implemented in conjunction with detailed construction plans for the project.

The site should provide sufficient parking spaces to meet City of Redlands parking code requirements in order to service on-site parking demand.

## 2. Off-Site Improvements

The necessary off-site improvement recommendations were described in previous sections of this report. The project should contribute towards the cost of necessary study area improvements on a fair share or "pro-rata" basis.

As is the case for any roadway design, the City of Redlands should periodically review traffic operations in the vicinity of the project once the project is constructed to assure that the traffic operations are satisfactory.

Participate in the phased construction of off-site traffic signals through payment of traffic signal mitigation fees. The traffic signals within the study area at buildout should specifically include an interconnect of the traffic signals to function in a coordinated system.

Figure 30 Circulation Recommendations


Sight distance at project accesses shall comply with standard California Department of Transportation and City of Redlands sight distance standards. The final grading, landscaping, and street improvement plans shall demonstrate that sight distance standards are met. Such plans must be reviewed by the City and approved as consistent with this measure prior to issue of grading permits.

On-site traffic signing and striping should be implemented in conjunction with detailed construction plans for the project.

The site should provide sufficient parking spaces to meet City of Redlands parking code requirements in order to service on-site parking demand.

The project should contribute towards the cost of necessary study area improvements on a fair share or "pro-rata" basis.

As is the case for any roadway design, the City of Redlands should periodically review traffic operations in the vicinity of the project once the project is constructed to assure that the traffic operations are satisfactory.

Participate in the phased construction of off-site traffic signals through payment of traffic signal mitigation fees. The traffic signals within the study area at buildout should specifically include an interconnect of the traffic signals to function in a coordinated system.

## I NTERNAL TRIP CALCULATI ONS

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# INTERSECTION ANALYSIS 

EXISTING CONDITIONS
AM PEAK HOUR


## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.


## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

|  | $\rangle$ | $\rightarrow$ | 7 | 7 |  | 4 | 4 | $\dagger$ | $p$ | $\downarrow$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 个4 | 「 | \％ | 个4 | 「 | \％${ }^{1 / 8}$ | $\stackrel{1}{1}$ |  | ${ }^{*}$ | 4 | F |
| Traffic Volume（veh／h） | 32 | 1308 | 71 | 55 | 693 | 0 | 448 | 7 | 120 | 14 | 2 | 6 |
| Future Volume（veh／h） | 32 | 1308 | 71 | 55 | 693 | 9 | 448 | 7 | 120 | 14 | 2 | 6 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 32 | 1308 | 71 | 55 | 693 | 9 | 448 | 7 | 120 | 14 | 2 | 6 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 350 | 1429 | 637 | 99 | 903 | 403 | 446 | 9 | 154 | 477 | 464 | 393 |
| Arrive On Green | 0.20 | 0.40 | 0.40 | 0.06 | 0.25 | 0.25 | 0.13 | 0.10 | 0.10 | 0.27 | 0.25 | 0.25 |
| Sat Flow，veh／h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 3456 | 88 | 1510 | 1781 | 1870 | 1585 |
| Grp Volume（v），veh／h | 32 | 1308 | 71 | 55 | 693 | 9 | 448 | 0 | 127 | 14 | 2 | 6 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1728 | 0 | 1598 | 1781 | 1870 | 1585 |
| Q Serve（g＿s），s | 1.8 | 41.8 | 3.4 | 3.6 | 21.7 | 0.5 | 15.5 | 0.0 | 9.3 | 0.7 | 0.1 | 0.2 |
| Cycle Q Clear（g＿c），s | 1.8 | 41.8 | 3.4 | 3.6 | 21.7 | 0.5 | 15.5 | 0.0 | 9.3 | 0.7 | 0.1 | 0.2 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.94 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 350 | 1429 | 637 | 99 | 903 | 403 | 446 | 0 | 163 | 477 | 464 | 393 |
| V／C Ratio（X） | 0.09 | 0.92 | 0.11 | 0.55 | 0.77 | 0.02 | 1.00 | 0.00 | 0.78 | 0.03 | 0.00 | 0.02 |
| Avail Cap（c＿a），veh／h | 350 | 1593 | 711 | 111 | 1567 | 699 | 446 | 0 | 394 | 477 | 464 | 393 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.93 | 0.93 | 0.93 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 39.5 | 34.0 | 22.5 | 55.2 | 41.5 | 33.6 | 52.3 | 0.0 | 52.6 | 32.4 | 34.0 | 13.1 |
| Incr Delay（d2），s／veh | 0.0 | 7.6 | 0.0 | 6.2 | 1.9 | 0.0 | 43.5 | 0.0 | 30.3 | 0.0 | 0.0 | 0.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（ $50 \%$ ），veh／ln | 0.8 | 18.5 | 1.2 | 1.8 | 9.4 | 0.2 | 9.4 | 0.0 | 5.1 | 0.3 | 0.0 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 39.5 | 41.6 | 22.5 | 61.4 | 43.3 | 33.6 | 95.8 | 0.0 | 82.9 | 32.4 | 34.0 | 13.1 |
| LnGrp LOS | D | D | C | E | D | C | F | A | F | C | C | B |
| Approach Vol，veh／h |  | 1411 |  |  | 757 |  |  | 575 |  |  | 22 |  |
| Approach Delay，s／veh |  | 40.6 |  |  | 44.5 |  |  | 92.9 |  |  | 27.3 |  |
| Approach LOS |  | D |  |  | D |  |  | F |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s | 37.6 | 17.6 | 11.2 | 53.6 | 20.0 | 35.2 | 29.0 | 35.9 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 5.4 | ＊ 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 5.4 | ＊ 5.4 |  |  |  |  |
| Max Green Setting（Gmax），s | 9.3 | ＊30 | 7.5 | 53.8 | 15.5 | 23.4 | 8.4 | ＊53 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 2.7 | 11.3 | 5.6 | 43.8 | 17.5 | 2.2 | 3.8 | 23.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 0.9 | 0.0 | 4.4 | 0.0 | 0.0 | 0.0 | 6.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 52.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 1\% |  | ${ }^{7}$ | 44 | 「 | ${ }^{17}$ | $\uparrow$ |  | ${ }^{*}$ | $\hat{F}$ |  |
| Traffic Volume (veh/h) | 0 | 1274 | 34 | 196 | 749 | 38 | 0 | 0 | 47 | 0 | 0 | 8 |
| Future Volume (veh/h) | 0 | 1274 | 34 | 196 | 749 | 38 | 0 | 0 | 47 | 0 | 0 | 8 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 0 | 1274 | 34 | 196 | 749 | 38 | 0 | 0 | 47 | 0 | 0 | 8 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 1 | 1348 | 36 | 223 | 1933 | 862 | 1 | 0 | 580 | 1 | 0 | 580 |
| Arrive On Green | 0.00 | 0.38 | 0.38 | 0.13 | 0.54 | 0.54 | 0.00 | 0.00 | 0.37 | 0.00 | 0.00 | 0.37 |
| Sat Flow, veh/h | 1781 | 3536 | 94 | 1781 | 3554 | 1585 | 1781 | 0 | 1585 | 1781 | 0 | 1585 |
| Grp Volume(v), veh/h | 0 | 640 | 668 | 196 | 749 | 38 | 0 | 0 | 47 | 0 | 0 | 8 |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1777 | 1853 | 1781 | 1777 | 1585 | 1781 | 0 | 1585 | 1781 | 0 | 1585 |
| Q Serve(g_s), s | 0.0 | 41.8 | 41.9 | 13.0 | 14.6 | 1.3 | 0.0 | 0.0 | 2.3 | 0.0 | 0.0 | 0.4 |
| Cycle Q Clear(g_c), s | 0.0 | 41.8 | 41.9 | 13.0 | 14.6 | 1.3 | 0.0 | 0.0 | 2.3 | 0.0 | 0.0 | 0.4 |
| Prop In Lane | 1.00 |  | 0.05 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 1 | 677 | 707 | 223 | 1933 | 862 | 1 | 0 | 580 | 1 | 0 | 580 |
| V/C Ratio(X) | 0.00 | 0.94 | 0.95 | 0.88 | 0.39 | 0.04 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.01 |
| Avail Cap(c_a), veh/h | 191 | 690 | 720 | 245 | 1933 | 862 | 181 | 0 | 580 | 200 | 0 | 580 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 0.29 | 0.29 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 35.9 | 35.9 | 51.6 | 15.8 | 12.8 | 0.0 | 0.0 | 24.9 | 0.0 | 0.0 | 24.2 |
| Incr Delay (d2), s/veh | 0.0 | 8.6 | 8.5 | 26.8 | 0.1 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/In | 0.0 | 18.7 | 19.5 | 7.3 | 5.6 | 0.5 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 | 0.2 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 0.0 | 44.5 | 44.4 | 78.4 | 15.9 | 12.8 | 0.0 | 0.0 | 25.1 | 0.0 | 0.0 | 24.3 |
| LnGrp LOS | A | D | D | E | B | B | A | A | C | A | A | C |
| Approach Vol, veh/h |  | 1308 |  |  | 983 |  |  | 47 |  |  | 8 |  |
| Approach Delay, s/veh |  | 44.5 |  |  | 28.3 |  |  | 25.1 |  |  | 24.3 |  |
| Approach LOS |  | D |  |  | C |  |  | C |  |  | C |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 0.0 | 49.3 | 19.5 | 51.1 | 0.0 | 49.3 | 0.0 | 70.7 |
| Change Period (Y+Rc), s | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 |
| Max Green Setting (Gmax), s | 13.5 | 23.6 | 16.5 | 46.6 | 12.2 | 24.9 | 12.9 | 50.2 |
| Max Q Clear Time (g_c+11), s | 0.0 | 4.3 | 15.0 | 43.9 | 0.0 | 2.4 | 0.0 | 16.6 |
| Green Ext Time (p_c), s | 0.0 | 0.2 | 0.1 | 1.9 | 0.0 | 0.0 | 0.0 | 5.4 |

## Intersection Summary

HCM 6th Ctrl Delay 37.2

HCM 6th LOS D

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | 性 |  |  | 个t |  |  |  | F |  |  | 7 |  |
| Traffic Vol, veh/h | 0 | 1476 | 4 | 0 | 852 | 0 | 0 | 0 | 17 | 0 | 0 | 0 |  |
| Future Vol, veh/h | 0 | 1476 | 4 | 0 | 852 | 0 | 0 | 0 | 17 | 0 | 0 | 0 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - |  | None |  |
| Storage Length | - | - | - | - | - | - | - | - | 0 | - | - | 0 |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 0 | 1476 | 4 | 0 | 852 | 0 | 0 | 0 | 17 | 0 | 0 | 0 |  |



HCM 6th Signalized Intersection Summary
6：Gateway Oaks Drive \＆West El Camino Avenue
08／03／2020

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％${ }^{1 / 4}$ | 个巾4 | 「 | \％${ }^{1 / 1}$ | 个4 | 「 | \％${ }^{1+1}$ | 个4 | 「 | \％${ }^{1 / 1}$ | 个4 | F |
| Traffic Volume（veh／h） | 313 | 624 | 431 | 351 | 525 | 574 | 209 | 117 | 127 | 130 | 34 | 32 |
| Future Volume（veh／h） | 313 | 624 | 431 | 351 | 525 | 574 | 209 | 117 | 127 | 130 | 34 | 32 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 313 | 624 | 431 | 351 | 525 | 574 | 209 | 117 | 127 | 130 | 34 | 32 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 477 | 1898 | 589 | 440 | 1280 | 571 | 475 | 583 | 260 | 426 | 528 | 236 |
| Arrive On Green | 0.14 | 0.37 | 0.37 | 0.13 | 0.36 | 0.36 | 0.14 | 0.16 | 0.16 | 0.12 | 0.15 | 0.15 |
| Sat Flow，veh／h | 3456 | 5106 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 |
| Grp Volume（v），veh／h | 313 | 624 | 431 | 351 | 525 | 574 | 209 | 117 | 127 | 130 | 34 | 32 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 |
| Q Serve（g＿s），s | 8.1 | 8.2 | 22.1 | 9.3 | 10.4 | 33.9 | 5.2 | 2.7 | 6.9 | 3.2 | 0.8 | 1.7 |
| Cycle Q Clear（g＿c），s | 8.1 | 8.2 | 22.1 | 9.3 | 10.4 | 33.9 | 5.2 | 2.7 | 6.9 | 3.2 | 0.8 | 1.7 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 477 | 1898 | 589 | 440 | 1280 | 571 | 475 | 583 | 260 | 426 | 528 | 236 |
| V／C Ratio（X） | 0.66 | 0.33 | 0.73 | 0.80 | 0.41 | 1.01 | 0.44 | 0.20 | 0.49 | 0.31 | 0.06 | 0.14 |
| Avail Cap（c＿a），veh／h | 477 | 1898 | 589 | 551 | 1280 | 571 | 477 | 1178 | 525 | 440 | 1136 | 507 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 38.5 | 21.2 | 25.5 | 39.9 | 22.6 | 30.1 | 37.3 | 34.0 | 35.8 | 37.6 | 34.4 | 34.8 |
| Incr Delay（d2），s／veh | 2.6 | 0.0 | 4.1 | 5.1 | 0.1 | 39.1 | 0.2 | 0.1 | 0.5 | 0.1 | 0.0 | 0.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 3.4 | 3.1 | 8.7 | 4.1 | 4.1 | 18.5 | 2.2 | 1.2 | 2.7 | 1.4 | 0.3 | 0.6 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 41.1 | 21.2 | 29.6 | 44.9 | 22.7 | 69.2 | 37.5 | 34.1 | 36.3 | 37.7 | 34.5 | 34.9 |
| LnGrp LOS | D | C | C | D | C | F | D | C | D | D | C | C |
| Approach Vol，veh／h |  | 1368 |  |  | 1450 |  |  | 453 |  |  | 196 |  |
| Approach Delay，s／veh |  | 28.4 |  |  | 46.5 |  |  | 36.3 |  |  | 36.7 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 18.1 | 38.7 | 18.0 | 19.3 | 17.0 | 39.8 | 16.6 | 20.7 |  |
| Change Period（ $Y+R \mathrm{R}$ ），s | ＊5．1 | ＊ 4.8 | ＊ 5.1 | ＊ 5.3 | 5.0 | ＊4．8 | 5.0 | ＊ 5.3 |  |
| Max Green Setting（Gmax），s | ＊13 | ＊ 34 | ＊ 13 | ＊ 30 | 15.0 | ＊ 32 | 12.0 | ＊31 |  |
| Max Q Clear Time（g＿c＋1），s | 10.1 | 35.9 | 7.2 | 3.7 | 11.3 | 24.1 | 5.2 | 8.9 |  |
| Green Ext Time（p＿c），s | 0.2 | 0.0 | 0.2 | 0.1 | 0.3 | 2.3 | 0.1 | 0.6 |  |

Intersection Summary
HCM 6th Ctrl Delay 37.5
HCM 6th LOS D

## Notes

User approved pedestrian interval to be less than phase max green．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

# INTERSECTION ANALYSIS EXISTING CONDITIONS <br> PM PEAK HOUR 

|  | * |  |  | 4 | ( | $\pm$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |
| Lane Configurations |  | 4 | 4 |  | ${ }^{1}$ | F |  |
| Traffic Volume (veh/h) | 0 | 232 | 905 | 0 | 321 | 152 |  |
| Future Volume (veh/h) | 0 | 232 | 905 | 0 | 321 | 152 |  |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  |  | 1.00 | 1.00 | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Work Zone On Approach |  | No | No |  | No |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1870 | 1870 | 0 | 1870 | 1870 |  |
| Adj Flow Rate, veh/h | 0 | 232 | 905 | 0 | 321 | 0 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Percent Heavy Veh, \% | 0 | 2 | 2 | 0 | 2 | 2 |  |
| Cap, veh/h | 0 | 1206 | 1206 | 0 | 393 |  |  |
| Arrive On Green | 0.00 | 0.64 | 0.64 | 0.00 | 0.22 | 0.00 |  |
| Sat Flow, veh/h | 0 | 1870 | 1870 | 0 | 1781 | 1585 |  |
| Grp Volume(v), veh/h | 0 | 232 | 905 | 0 | 321 | 0 |  |
| Grp Sat Flow(s),veh/h/ln | 0 | 1870 | 1870 | 0 | 1781 | 1585 |  |
| Q Serve(g_s), s | 0.0 | 2.8 | 18.3 | 0.0 | 9.4 | 0.0 |  |
| Cycle Q Clear(g_c), s | 0.0 | 2.8 | 18.3 | 0.0 | 9.4 | 0.0 |  |
| Prop In Lane | 0.00 |  |  | 0.00 | 1.00 | 1.00 |  |
| Lane Grp Cap(c), veh/h | 0 | 1206 | 1206 | 0 | 393 |  |  |
| V/C Ratio(X) | 0.00 | 0.19 | 0.75 | 0.00 | 0.82 |  |  |
| Avail Cap(c_a), veh/h | 0 | 1206 | 1206 | 0 | 858 |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 |  |
| Uniform Delay (d), s/veh | 0.0 | 4.0 | 6.7 | 0.0 | 20.4 | 0.0 |  |
| Incr Delay (d2), s/veh | 0.0 | 0.4 | 4.3 | 0.0 | 4.2 | 0.0 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 0.0 | 0.6 | 4.8 | 0.0 | 3.7 | 0.0 |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 0.0 | 4.3 | 11.0 | 0.0 | 24.6 | 0.0 |  |
| LnGrp LOS | A | A | B | A | C |  |  |
| Approach Vol, veh/h |  | 232 | 905 |  | 321 | A |  |
| Approach Delay, s/veh |  | 4.3 | 11.0 |  | 24.6 |  |  |
| Approach LOS |  | A | B |  | C |  |  |
| Timer - Assigned Phs |  | 2 |  |  |  | 6 | 8 |
| Phs Duration ( $G+Y+R c$ ), $s$ |  | 39.4 |  |  |  | 39.4 | 15.6 |
| Change Period (Y+Rc), s |  | 3.9 |  |  |  | 3.9 | 3.5 |
| Max Green Setting (Gmax), s |  | 21.1 |  |  |  | 21.1 | 26.5 |
| Max Q Clear Time (g_c+11), s |  | 4.8 |  |  |  | 20.3 | 11.4 |
| Green Ext Time (p_c), s |  | 0.6 |  |  |  | 0.4 | 0.8 |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 12.9 |  |  |  |  |
|  |  |  | B |  |  |  |  |

## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

|  | $\rightarrow$ |  | 7 | $4$ | 4 | $p$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |
| Lane Configurations | 4 |  |  | 4 | ${ }^{1}$ | 「 |  |
| Traffic Volume (veh/h) | 480 | 0 | 0 | 675 | 646 | 688 |  |
| Future Volume (veh/h) | 480 | 0 | 0 | 675 | 646 | 688 |  |
| Initial Q $(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Work Zone On Approach | No |  |  | No | No |  |  |
| Adj Sat Flow, veh/h/ln | 1870 | 0 | 0 | 1870 | 1870 | 1870 |  |
| Adj Flow Rate, veh/h | 480 | 0 | 0 | 675 | 646 | 688 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Percent Heavy Veh, \% | 2 | 0 | 0 | 2 | 2 | 2 |  |
| Cap, veh/h | 898 | 0 | 0 | 898 | 801 | 713 |  |
| Arrive On Green | 0.48 | 0.00 | 0.00 | 0.48 | 0.45 | 0.45 |  |
| Sat Flow, veh/h | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Grp Volume(v), veh/h | 480 | 0 | 0 | 675 | 646 | 688 |  |
| Grp Sat Flow(s),veh/h/ln | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Q Serve(g_s), s | 19.7 | 0.0 | 0.0 | 32.3 | 34.4 | 46.4 |  |
| Cycle Q Clear(g_c), s | 19.7 | 0.0 | 0.0 | 32.3 | 34.4 | 46.4 |  |
| Prop In Lane |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  |
| Lane Grp Cap(c), veh/h | 898 | 0 | 0 | 898 | 801 | 713 |  |
| V/C Ratio(X) | 0.53 | 0.00 | 0.00 | 0.75 | 0.81 | 0.96 |  |
| Avail Cap(c_a), veh/h | 898 | 0 | 0 | 898 | 834 | 742 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 20.0 | 0.0 | 0.0 | 23.3 | 26.1 | 29.4 |  |
| Incr Delay (d2), s/veh | 2.3 | 0.0 | 0.0 | 5.8 | 5.2 | 23.9 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 8.5 | 0.0 | 0.0 | 14.5 | 14.6 | 20.8 |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 22.3 | 0.0 | 0.0 | 29.0 | 31.3 | 53.3 |  |
| LnGrp LOS | C | A | A | C | C | D |  |
| Approach Vol, veh/h | 480 |  |  | 675 | 1334 |  |  |
| Approach Delay, s/veh | 22.3 |  |  | 29.0 | 42.7 |  |  |
| Approach LOS | C |  |  | C | D |  |  |
| Timer - Assigned Phs |  | 2 |  |  |  | 6 | 8 |
| Phs Duration (G+Y+Rc), s |  | 57.0 |  |  |  | 57.0 | 53.0 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s |  | * 4.2 |  |  |  | * 4.2 | 3.5 |
| Max Green Setting (Gmax), s |  | * 51 |  |  |  | * 51 | 51.5 |
| Max Q Clear Time (g_c+l1), s |  | 21.7 |  |  |  | 34.3 | 48.4 |
| Green Ext Time (p_c), s |  | 1.7 |  |  |  | 2.4 | 1.1 |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 35.0 |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

|  | $\rangle$ | $\rightarrow$ | 7 | 7 | $\checkmark$ | 4 | 4 | $\dagger$ | $p$ | ＊ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 个4 | F＇ | ${ }^{*}$ | 个4 | 「 | \％${ }^{17}$ | $\hat{\beta}$ |  | ${ }^{7}$ | 4 | F |
| Traffic Volume（veh／h） | 2 | 881 | 285 | 113 | 1009 | 0 | 226 | 1 | 98 | 12 | 1 | 4 |
| Future Volume（veh／h） | 2 | 881 | 285 | 113 | 1009 | 0 | 226 | 1 | 98 | 12 | 1 | 4 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／n | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 2 | 881 | 285 | 113 | 1009 | 0 | 226 | 1 | 98 | 12 | 1 | 4 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 125 | 1263 | 563 | 141 | 1269 | 566 | 268 | 2 | 160 | 519 | 604 | 512 |
| Arrive On Green | 0.07 | 0.36 | 0.36 | 0.08 | 0.36 | 0.00 | 0.08 | 0.10 | 0.10 | 0.29 | 0.32 | 0.32 |
| Sat Flow，veh／h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 3456 | 16 | 1571 | 1781 | 1870 | 1585 |
| Grp Volume（v），veh／h | 2 | 881 | 285 | 113 | 1009 | 0 | 226 | 0 | 99 | 12 |  | 4 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1728 | 0 | 1587 | 1781 | 1870 | 1585 |
| Q Serve（g＿s），s | 0.1 | 25.5 | 17.0 | 7.5 | 30.6 | 0.0 | 7.7 | 0.0 | 7.2 | 0.6 | 0.0 | 0.2 |
| Cycle Q Clear（g＿c），s | 0.1 | 25.5 | 17.0 | 7.5 | 30.6 | 0.0 | 7.7 | 0.0 | 7.2 | 0.6 | 0.0 | 0.2 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 125 | 1263 | 563 | 141 | 1269 | 566 | 268 | 0 | 161 | 519 | 604 | 512 |
| V／C Ratio（X） | 0.02 | 0.70 | 0.51 | 0.80 | 0.80 | 0.00 | 0.84 | 0.00 | 0.61 | 0.02 | 0.00 | 0.01 |
| Avail Cap（c＿a），veh／h | 125 | 1706 | 761 | 143 | 1741 | 777 | 268 | 0 | 321 | 519 | 604 | 512 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.64 | 0.64 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 52.0 | 33.1 | 30.4 | 54.3 | 34.6 | 0.0 | 54.6 | 0.0 | 51.6 | 30.3 | 27.5 | 16.1 |
| Incr Delay（d2），s／veh | 0.0 | 0.4 | 0.3 | 19.4 | 1.5 | 0.0 | 21.7 | 0.0 | 16.2 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（ $50 \%$ ），veh／ln | 0.1 | 10.5 | 6.3 | 4.0 | 12.9 | 0.0 | 4.2 | 0.0 | 3.6 | 0.3 | 0.0 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 52.0 | 33.5 | 30.7 | 73.8 | 36.1 | 0.0 | 76.4 | 0.0 | 67.8 | 30.3 | 27.5 | 16.1 |
| LnGrp LOS | D | C | C | E | D | A | E | A | E | C | C | B |
| Approach Vol，veh／h |  | 1168 |  |  | 1122 |  |  | 325 |  |  | 17 |  |
| Approach Delay，s／veh |  | 32.8 |  |  | 39.9 |  |  | 73.8 |  |  | 26.8 |  |
| Approach LOS |  | C |  |  | D |  |  | E |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s | 40.4 | 17.6 | 14.0 | 48.1 | 13.8 | 44.2 | 13.8 | 48.2 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 5.4 | ＊ 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 5.4 | ＊ 5.4 |  |  |  |  |
| Max Green Setting（Gmax），s | 8.7 | ＊24 | 9.6 | 57.6 | 9.3 | 23.7 | 8.4 | ＊59 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 2.6 | 9.2 | 9.5 | 27.5 | 9.7 | 2.2 | 2.1 | 32.6 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 0.5 | 0.0 | 4.4 | 0.0 | 0.0 | 0.0 | 10.3 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 40.9 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个t |  | \% | 个4 | F | ${ }^{7}$ | $\hat{\beta}$ |  | \% | $\hat{\beta}$ |  |
| Traffic Volume (veh/h) | 6 | 981 | 27 | 64 | 1095 | 5 | 0 | 0 | 32 | 5 | 0 | 5 |
| Future Volume (veh/h) | 6 | 981 | 27 | 64 | 1095 | 5 | 0 | 0 | 32 | 5 | 0 | 5 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 6 | 981 | 27 | 64 | 1095 | 5 | 0 | 0 | 32 | 5 | 0 | 5 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 35 | 1143 | 31 | 147 | 1373 | 613 | 1 | 0 | 653 | 31 | 0 | 739 |
| Arrive On Green | 0.02 | 0.32 | 0.32 | 0.08 | 0.39 | 0.39 | 0.00 | 0.00 | 0.41 | 0.02 | 0.00 | 0.47 |
| Sat Flow, veh/h | 1781 | 3532 | 97 | 1781 | 3554 | 1585 | 1781 | 0 | 1585 | 1781 | 0 | 1585 |
| Grp Volume(v), veh/h | 6 | 493 | 515 | 64 | 1095 | 5 | 0 | 0 | 32 | 5 | 0 | 5 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1853 | 1781 | 1777 | 1585 | 1781 | 0 | 1585 | 1781 | 0 | 1585 |
| Q Serve(g_s), s | 0.4 | 31.2 | 31.2 | 4.1 | 32.8 | 0.2 | 0.0 | 0.0 | 1.5 | 0.3 | 0.0 | 0.2 |
| Cycle Q Clear(g_c), s | 0.4 | 31.2 | 31.2 | 4.1 | 32.8 | 0.2 | 0.0 | 0.0 | 1.5 | 0.3 | 0.0 | 0.2 |
| Prop In Lane | 1.00 |  | 0.05 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 35 | 575 | 600 | 147 | 1373 | 613 | 1 | 0 | 653 | 31 | 0 | 739 |
| V/C Ratio(X) | 0.17 | 0.86 | 0.86 | 0.44 | 0.80 | 0.01 | 0.00 | 0.00 | 0.05 | 0.16 | 0.00 | 0.01 |
| Avail Cap(c_a), veh/h | 191 | 755 | 787 | 171 | 1469 | 655 | 181 | 0 | 653 | 200 | 0 | 739 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.73 | 0.73 | 0.73 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 57.9 | 38.0 | 38.0 | 52.4 | 32.6 | 22.7 | 0.0 | 0.0 | 21.2 | 58.1 | 0.0 | 17.1 |
| Incr Delay (d2), s/veh | 1.7 | 5.8 | 5.6 | 2.0 | 3.0 | 0.0 | 0.0 | 0.0 | 0.1 | 2.4 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.2 | 13.9 | 14.4 | 1.9 | 14.0 | 0.1 | 0.0 | 0.0 | 0.6 | 0.2 | 0.0 | 0.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 59.6 | 43.8 | 43.6 | 54.5 | 35.6 | 22.7 | 0.0 | 0.0 | 21.3 | 60.5 | 0.0 | 17.1 |
| LnGrp LOS | E | D | D | D | D | C | A | A | C | E | A | B |
| Approach Vol, veh/h |  | 1014 |  |  | 1164 |  |  | 32 |  |  | 10 |  |
| Approach Delay, s/veh |  | 43.8 |  |  | 36.6 |  |  | 21.3 |  |  | 38.8 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | D |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c), s$ | 6.6 | 54.8 | 14.4 | 44.2 | 0.0 | 61.4 | 6.8 | 51.8 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$, s | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 |
| Max Green Setting (Gmax), s | 13.5 | 24.2 | 11.5 | 51.0 | 12.2 | 25.5 | 12.9 | 49.6 |
| Max Q Clear Time (g_c+11), s | 2.3 | 3.5 | 6.1 | 33.2 | 0.0 | 2.2 | 2.4 | 34.8 |
| Green Ext Time (p_c), s | 0.0 | 0.1 | 0.0 | 5.6 | 0.0 | 0.0 | 0.0 | 6.3 |

Intersection Summary
HCM 6th Ctrl Delay 39.7

HCM 6th LOS D

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 1t |  |  | 1t |  |  |  | F |  |  | 「 |
| Traffic Vol, veh/h | 0 | 1009 | 10 | 0 | 1196 | 0 | 0 | 0 | 14 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 1009 | 10 | 0 | 1196 | 0 | 0 | 0 | 14 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Fr | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 0 | - | - | 0 |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1009 | 10 | 0 | 1196 | 0 | 0 | 0 | 14 | 0 | 0 | 0 |



HCM 6th Signalized Intersection Summary
6：Gateway Oaks Drive \＆West El Camino Avenue
08／03／2020

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ 71 | 个个中 | 「 | \％${ }^{1+1}$ | 个4 | 「 | \％${ }^{1+1}$ | 个4 | 「 | \％${ }^{1 / 4}$ | 个个 | ¢ |
| Traffic Volume（veh／h） | 77 | 724 | 201 | 245 | 404 | 102 | 366 | 60 | 371 | 450 | 117 | 260 |
| Future Volume（veh／h） | 77 | 724 | 201 | 245 | 404 | 102 | 366 | 60 | 371 | 450 | 117 | 260 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 77 | 724 | 201 | 245 | 404 | 102 | 366 | 60 | 371 | 450 | 117 | 260 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 452 | 984 | 306 | 502 | 732 | 327 | 546 | 922 | 411 | 547 | 919 | 410 |
| Arrive On Green | 0.13 | 0.19 | 0.19 | 0.15 | 0.21 | 0.21 | 0.16 | 0.26 | 0.26 | 0.16 | 0.26 | 0.26 |
| Sat Flow，veh／h | 3456 | 5106 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 |
| Grp Volume（v），veh／h | 77 | 724 | 201 | 245 | 404 | 102 | 366 | 60 | 371 | 450 | 117 | 260 |
| Grp Sat Flow（s），veh／h／n | 1728 | 1702 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 |
| Q Serve（g＿s），s | 1.6 | 11.0 | 9.6 | 5.4 | 8.4 | 4.5 | 8.2 | 1.0 | 18.6 | 10.4 | 2.1 | 12.0 |
| Cycle Q Clear（g＿c），s | 1.6 | 11.0 | 9.6 | 5.4 | 8.4 | 4.5 | 8.2 | 1.0 | 18.6 | 10.4 | 2.1 | 12.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 452 | 984 | 306 | 502 | 732 | 327 | 546 | 922 | 411 | 547 | 919 | 410 |
| V／C Ratio（X） | 0.17 | 0.74 | 0.66 | 0.49 | 0.55 | 0.31 | 0.67 | 0.07 | 0.90 | 0.82 | 0.13 | 0.63 |
| Avail Cap（c＿a），veh／h | 546 | 1626 | 505 | 504 | 1097 | 489 | 760 | 1326 | 591 | 882 | 1447 | 645 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 31.8 | 31.2 | 30.7 | 32.4 | 29.3 | 27.7 | 32.6 | 23.0 | 29.5 | 33.5 | 23.4 | 27.1 |
| Incr Delay（d2），s／veh | 0.1 | 0.4 | 0.9 | 0.3 | 0.2 | 0.2 | 0.5 | 0.0 | 10.3 | 1.5 | 0.0 | 0.6 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.6 | 4.2 | 3.7 | 2.1 | 3.4 | 1.7 | 3.4 | 0.4 | 8.0 | 4.3 | 0.9 | 4.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 31.9 | 31.7 | 31.6 | 32.6 | 29.5 | 27.9 | 33.2 | 23.0 | 39.8 | 35.0 | 23.4 | 27.7 |
| LnGrp LOS | C | C | C | C | C | C | C | C | D | D | C |  |
| Approach Vol，veh／h |  | 1002 |  |  | 751 |  |  | 797 |  |  | 827 |  |
| Approach Delay，s／veh |  | 31.7 |  |  | 30.3 |  |  | 35.5 |  |  | 31.1 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | C |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 15.9 | 21.8 | 18.1 | 26.6 | 17.0 | 20.7 | 18.0 | 26.7 |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | ＊5．1 | ＊ 4.8 | ＊ 5.1 | ＊ 5.3 | 5.0 | ＊ 4.8 | 5.0 | ＊ 5.3 |  |
| Max Green Setting（Gmax），s | ＊13 | ＊ 25 | ＊18 | ＊34 | 12.0 | ＊ 26 | 21.0 | ＊31 |  |
| Max Q Clear Time（g＿c +11 ），s | 3.6 | 10.4 | 10.2 | 14.0 | 7.4 | 13.0 | 12.4 | 20.6 |  |
| Green Ext Time（p＿c），s | 0.1 | 1.5 | 0.5 | 0.9 | 0.2 | 2.9 | 0.7 | 0.7 |  |

Intersection Summary

| HCM 6th Ctrl Delay | 32.1 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

# INTERSECTION ANALYSIS BASELINE CONDITIONS AM PEAK HOUR 



## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

|  | $\rightarrow$ |  | 7 | $\Perp$ | 4 | \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |
| Lane Configurations | 4 |  |  | 4 | \% | 7 |  |
| Traffic Volume (veh/h) | 1059 | 0 | 0 | 635 | 117 | 393 |  |
| Future Volume (veh/h) | 1059 | 0 | 0 | 635 | 117 | 393 |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Work Zone On Approach | No |  |  | No | No |  |  |
| Adj Sat Flow, veh/h/ln | 1870 | 0 | 0 | 1870 | 1870 | 1870 |  |
| Adj Flow Rate, veh/h | 1059 | 0 | 0 | 635 | 117 | 393 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Percent Heavy Veh, \% | 2 | 0 | 0 | 2 | 2 | 2 |  |
| Cap, veh/h | 1374 | 0 | 0 | 1374 | 348 | 310 |  |
| Arrive On Green | 0.73 | 0.00 | 0.00 | 0.73 | 0.20 | 0.20 |  |
| Sat Flow, veh/h | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Grp Volume(v), veh/h | 1059 | 0 | 0 | 635 | 117 | 393 |  |
| Grp Sat Flow(s),veh/h/ln | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Q Serve(g_s), s | 38.1 | 0.0 | 0.0 | 15.0 | 6.2 | 21.5 |  |
| Cycle Q Clear(g_c), s | 38.1 | 0.0 | 0.0 | 15.0 | 6.2 | 21.5 |  |
| Prop In Lane |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  |
| Lane Grp Cap(c), veh/h | 1374 | 0 | 0 | 1374 | 348 | 310 |  |
| V/C Ratio(X) | 0.77 | 0.00 | 0.00 | 0.46 | 0.34 | 1.27 |  |
| Avail Cap(c_a), veh/h | 1374 | 0 | 0 | 1379 | 348 | 310 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 8.9 | 0.0 | 0.0 | 5.9 | 38.1 | 44.3 |  |
| Incr Delay (d2), s/veh | 4.2 | 0.0 | 0.0 | 1.1 | 0.2 | 143.9 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 12.9 | 0.0 | 0.0 | 4.9 | 2.6 | 20.5 |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 13.2 | 0.0 | 0.0 | 7.0 | 38.3 | 188.1 |  |
| LnGrp LOS | B | A | A | A | D | F |  |
| Approach Vol, veh/h | 1059 |  |  | 635 | 510 |  |  |
| Approach Delay, s/veh | 13.2 |  |  | 7.0 | 153.8 |  |  |
| Approach LOS | B |  |  | A | F |  |  |
| Timer - Assigned Phs |  | 2 |  |  |  | 6 | 8 |
| Phs Duration (G+Y+Rc), s |  | 85.0 |  |  |  | 85.0 | 25.0 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | * 4.2 |  |  |  | * 4.2 | 3.5 |
| Max Green Setting (Gmax), s |  | * 81 |  |  |  | * 81 | 21.5 |
| Max Q Clear Time (g_c+l1), s |  | 40.1 |  |  |  | 17.0 | 23.5 |
| Green Ext Time (p_c), s |  | 5.9 |  |  |  | 2.5 | 0.0 |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 43.9 |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

|  | 4 | $\rightarrow$ | 7 | 7 | - | 4 | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个4 | F | \% | 个4 | F | \% ${ }^{1 / 7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume (veh/h) | 57 | 1321 | 71 | 57 | 769 | 35 | 435 | , | 122 | 49 | 7 | 175 |
| Future Volume (veh/h) | 57 | 1321 | 71 | 57 | 769 | 35 | 435 | 4 | 122 | 49 | 7 | 175 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 57 | 1321 | 71 | 57 | 769 | 35 | 435 | 4 | 122 | 49 | 7 | 175 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 310 | 1440 | 642 | 99 | 994 | 443 | 446 | 5 | 157 | 472 | 458 | 388 |
| Arrive On Green | 0.17 | 0.41 | 0.41 | 0.06 | 0.28 | 0.28 | 0.13 | 0.10 | 0.10 | 0.26 | 0.24 | 0.24 |
| Sat Flow, veh/h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 3456 | 51 | 1542 | 1781 | 1870 | 1585 |
| Grp Volume(v), veh/h | 57 | 1321 | 71 | 57 | 769 | 35 | 435 | 0 | 126 | 49 | 7 | 175 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1728 | 0 | 1593 | 1781 | 1870 | 1585 |
| Q Serve(g_s), s | 3.3 | 42.2 | 3.3 | 3.7 | 23.9 | 2.0 | 15.0 | 0.0 | 9.3 | 2.5 | 0.3 | 7.3 |
| Cycle Q Clear (g_c), s | 3.3 | 42.2 | 3.3 | 3.7 | 23.9 | 2.0 | 15.0 | 0.0 | 9.3 | 2.5 | 0.3 | 7.3 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.97 | 1.00 |  | 1.00 |
| Lane Grp Cap (c), veh/h | 310 | 1440 | 642 | 99 | 994 | 443 | 446 | 0 | 162 | 472 | 458 | 388 |
| V/C Ratio(X) | 0.18 | 0.92 | 0.11 | 0.57 | 0.77 | 0.08 | 0.97 | 0.00 | 0.78 | 0.10 | 0.02 | 0.45 |
| Avail Cap(c_a), veh/h | 310 | 1593 | 711 | 111 | 1567 | 699 | 446 | 0 | 393 | 472 | 458 | 388 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 0.90 | 0.90 | 0.90 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 42.3 | 33.8 | 22.2 | 55.3 | 39.7 | 31.8 | 52.1 | 0.0 | 52.6 | 33.3 | 34.3 | 16.3 |
| Incr Delay (d2), s/veh | 0.1 | 7.9 | 0.0 | 6.9 | 1.7 | 0.1 | 36.0 | 0.0 | 30.0 | 0.0 | 0.1 | 3.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.4 | 18.7 | 1.2 | 1.8 | 10.3 | 0.7 | 8.7 | 0.0 | 5.0 | 1.1 | 0.2 | 4.5 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 42.4 | 41.7 | 22.3 | 62.1 | 41.4 | 31.9 | 88.0 | 0.0 | 82.6 | 33.4 | 34.4 | 20.0 |
| LnGrp LOS | D | D | C | E | D | C | F | A | F | C | C | C |
| Approach Vol, veh/h |  | 1449 |  |  | 861 |  |  | 561 |  |  | 231 |  |
| Approach Delay, s/veh |  | 40.8 |  |  | 42.4 |  |  | 86.8 |  |  | 23.3 |  |
| Approach LOS |  | D |  |  | D |  |  | F |  |  | C |  |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 37.2 | 17.6 | 11.2 | 54.0 | 20.0 | 34.8 | 26.3 | 38.9 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 5.4 | * 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 5.4 | * 5.4 |  |  |  |  |
| Max Green Setting (Gmax), s | 9.3 | *30 | 7.5 | 53.8 | 15.5 | 23.4 | 8.4 | *53 |  |  |  |  |
| Max Q Clear Time (g_c+1), s | 4.5 | 11.3 | 5.7 | 44.2 | 17.0 | 9.3 | 5.3 | 25.9 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 0.9 | 0.0 | 4.4 | 0.0 | 0.3 | 0.0 | 7.7 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 48.2 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个10 |  | \% | 个4 | F' | \% | $\hat{\square}$ |  | ${ }^{4}$ | 1 |  |
| Traffic Volume (veh/h) | 15 | 1308 | 35 | 196 | 801 | 25 | 13 | 0 | 47 | 122 |  | 47 |
| Future Volume (veh/h) | 15 | 1308 | 35 | 196 | 801 | 25 | 13 | 0 | 47 | 122 | 3 | 47 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 15 | 1308 | 35 | 196 | 801 | 25 | 13 | 0 | 47 | 122 | 3 | 47 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 75 | 1363 | 36 | 223 | 1665 | 743 | 64 | 0 | 339 | 197 | 28 | 434 |
| Arrive On Green | 0.04 | 0.39 | 0.39 | 0.13 | 0.47 | 0.47 | 0.04 | 0.00 | 0.21 | 0.11 | 0.29 | 0.29 |
| Sat Flow, veh/h | 1781 | 3536 | 95 | 1781 | 3554 | 1585 | 1781 | 0 | 1585 | 1781 | 96 | 1504 |
| Grp Volume(v), veh/h | 15 | 657 | 686 | 196 | 801 | 25 | 13 | 0 | 47 | 122 | 0 | 50 |
| Grp Sat Flow(s),veh/h/n | 1781 | 1777 | 1853 | 1781 | 1777 | 1585 | 1781 | 0 | 1585 | 1781 | 0 | 1600 |
| Q Serve(g_s), s | 1.0 | 43.2 | 43.3 | 13.0 | 18.6 | 1.0 | 0.9 | 0.0 | 2.9 | 7.8 | 0.0 | 2.8 |
| Cycle Q Clear(g_c), s | 1.0 | 43.2 | 43.3 | 13.0 | 18.6 | 1.0 | 0.9 | 0.0 | 2.9 | 7.8 | 0.0 | 2.8 |
| Prop In Lane | 1.00 |  | 0.05 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.94 |
| Lane Grp Cap(c), veh/h | 75 | 685 | 715 | 223 | 1665 | 743 | 64 | 0 | 339 | 197 | 0 | 461 |
| V/C Ratio(X) | 0.20 | 0.96 | 0.96 | 0.88 | 0.48 | 0.03 | 0.20 | 0.00 | 0.14 | 0.62 | 0.00 | 0.11 |
| Avail Cap(c_a), veh/h | 191 | 690 | 720 | 245 | 1665 | 743 | 181 | 0 | 339 | 200 | 0 | 461 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 0.14 | 0.14 | 0.14 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 55.5 | 35.9 | 36.0 | 51.6 | 21.9 | 17.2 | 56.2 | 0.0 | 38.2 | 51.0 | 0.0 | 31.4 |
| Incr Delay (d2), s/veh | 0.2 | 6.0 | 5.9 | 26.8 | 0.2 | 0.0 | 1.6 | 0.0 | 0.9 | 5.6 | 0.0 | 0.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.4 | 18.8 | 19.6 | 7.3 | 7.4 | 0.4 | 0.4 | 0.0 | 1.2 | 3.8 | 0.0 | 1.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 55.7 | 41.9 | 41.9 | 78.4 | 22.1 | 17.2 | 57.8 | 0.0 | 39.1 | 56.5 | 0.0 | 31.8 |
| LnGrp LOS | E | D | D | E | C | B | E | A | D | E | A | C |
| Approach Vol, veh/h |  | 1358 |  |  | 1022 |  |  | 60 |  |  | 172 |  |
| Approach Delay, s/veh |  | 42.1 |  |  | 32.8 |  |  | 43.1 |  |  | 49.3 |  |
| Approach LOS |  | D |  |  | C |  |  | D |  |  | D |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 17.8 | 31.0 | 19.5 | 51.7 | 8.8 | 40.0 | 9.6 | 61.6 |
| Change Period (Y+Rc), s | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 |
| Max Green Setting (Gmax), s | 13.5 | 23.6 | 16.5 | 46.6 | 12.2 | 24.9 | 12.9 | 50.2 |
| Max Q Clear Time (g_c+11), s | 9.8 | 4.9 | 15.0 | 45.3 | 2.9 | 4.8 | 3.0 | 20.6 |
| Green Ext Time (p_c), s | 0.1 | 0.2 | 0.1 | 0.9 | 0.0 | 0.2 | 0.0 | 5.7 |

## Intersection Summary

HCM 6th Ctrl Delay 38.9

HCM 6th LOS D



HCM 6th Signalized Intersection Summary
6：Gateway Oaks Drive \＆West El Camino Avenue
08／03／2020

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％${ }^{1 / 1}$ | 个巾4 | 「 | \％${ }^{1 / 1}$ | 个4 | 「 | \％${ }^{1+1}$ | 个4 | 「 | \％${ }^{1 / 1}$ | 个4 | F |
| Traffic Volume（veh／h） | 321 | 765 | 437 | 351 | 568 | 574 | 206 | 117 | 127 | 130 | 34 | 42 |
| Future Volume（veh／h） | 321 | 765 | 437 | 351 | 568 | 574 | 206 | 117 | 127 | 130 | 34 | 42 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 321 | 765 | 437 | 351 | 568 | 574 | 206 | 117 | 127 | 130 | 34 | 42 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 477 | 1898 | 589 | 440 | 1280 | 571 | 475 | 583 | 260 | 426 | 528 | 236 |
| Arrive On Green | 0.14 | 0.37 | 0.37 | 0.13 | 0.36 | 0.36 | 0.14 | 0.16 | 0.16 | 0.12 | 0.15 | 0.15 |
| Sat Flow，veh／h | 3456 | 5106 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 |
| Grp Volume（v），veh／h | 321 | 765 | 437 | 351 | 568 | 574 | 206 | 117 | 127 | 130 | 34 | 42 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 |
| Q Serve（g＿s），s | 8.3 | 10.4 | 22.5 | 9.3 | 11.5 | 33.9 | 5.1 | 2.7 | 6.9 | 3.2 | 0.8 | 2.2 |
| Cycle Q Clear（g＿c），s | 8.3 | 10.4 | 22.5 | 9.3 | 11.5 | 33.9 | 5.1 | 2.7 | 6.9 | 3.2 | 0.8 | 2.2 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 477 | 1898 | 589 | 440 | 1280 | 571 | 475 | 583 | 260 | 426 | 528 | 236 |
| V／C Ratio（X） | 0.67 | 0.40 | 0.74 | 0.80 | 0.44 | 1.01 | 0.43 | 0.20 | 0.49 | 0.31 | 0.06 | 0.18 |
| Avail Cap（c＿a），veh／h | 477 | 1898 | 589 | 551 | 1280 | 571 | 477 | 1178 | 525 | 441 | 1136 | 507 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 38.5 | 21.8 | 25.6 | 39.9 | 22.9 | 30.1 | 37.2 | 34.0 | 35.8 | 37.6 | 34.4 | 35.0 |
| Incr Delay（d2），s／veh | 3.0 | 0.1 | 4.4 | 5.1 | 0.1 | 39.1 | 0.2 | 0.1 | 0.5 | 0.1 | 0.0 | 0.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 3.6 | 3.9 | 8.9 | 4.1 | 4.5 | 18.5 | 2.2 | 1.2 | 2.7 | 1.4 | 0.3 | 0.8 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 41.6 | 21.9 | 30.1 | 44.9 | 23.0 | 69.2 | 37.5 | 34.1 | 36.3 | 37.7 | 34.5 | 35.2 |
| LnGrp LOS | D | C | C | D | C | F | D | C | D | D | C | D |
| Approach Vol，veh／h |  | 1523 |  |  | 1493 |  |  | 450 |  |  | 206 |  |
| Approach Delay，s／veh |  | 28.4 |  |  | 45.9 |  |  | 36.3 |  |  | 36.7 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phs Duration（ $G+Y+R \mathrm{C})$ ，$s$ | 18.1 | 38.7 | 18.0 | 19.3 | 17.0 | 39.8 | 16.6 | 20.7 |  |
| Change Period（ $Y+\mathrm{Rc}$ ），s | ＊ 5.1 | ＊4．8 | ＊ 5.1 | ＊5．3 | 5.0 | ＊4．8 | 5.0 | ＊ 5.3 |  |
| Max Green Setting（Gmax），s | ＊13 | ＊ 34 | ＊ 13 | ＊ 30 | 15.0 | ＊ 32 | 12.0 | ＊31 |  |
| Max Q Clear Time（g＿c +11 ），s | 10.3 | 35.9 | 7.1 | 4.2 | 11.3 | 24.5 | 5.2 | 8.9 |  |
| Green Ext Time（p＿c），s | 0.2 | 0.0 | 0.2 | 0.2 | 0.3 | 2.6 | 0.1 | 0.6 |  |

Intersection Summary

| HCM 6th Ctrl Delay | 36.9 |
| :--- | ---: |
| HCM 6th LOS | $D$ |

## Notes

User approved pedestrian interval to be less than phase max green．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．




# INTERSECTION ANALYSIS <br> BASELINE CONDITIONS 

PM PEAK HOUR


## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

|  | $\rightarrow$ |  | 7 | $\Perp$ | 4 | \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |
| Lane Configurations | 4 |  |  | 4 | ${ }^{1 /}$ | 7 |  |
| Traffic Volume (veh/h) | 637 | 0 | 0 | 734 | 646 | 763 |  |
| Future Volume (veh/h) | 637 | 0 | 0 | 734 | 646 | 763 |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Work Zone On Approach | No |  |  | No | No |  |  |
| Adj Sat Flow, veh/h/ln | 1870 | 0 | 0 | 1870 | 1870 | 1870 |  |
| Adj Flow Rate, veh/h | 637 | 0 | 0 | 734 | 646 | 763 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Percent Heavy Veh, \% | 2 | 0 | 0 | 2 | 2 | 2 |  |
| Cap, veh/h | 864 | 0 | 0 | 864 | 834 | 742 |  |
| Arrive On Green | 0.46 | 0.00 | 0.00 | 0.46 | 0.47 | 0.47 |  |
| Sat Flow, veh/h | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Grp Volume(v), veh/h | 637 | 0 | 0 | 734 | 646 | 763 |  |
| Grp Sat Flow(s),veh/h/ln | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Q Serve(g_s), s | 30.6 | 0.0 | 0.0 | 38.2 | 33.3 | 51.5 |  |
| Cycle Q Clear(g_c), s | 30.6 | 0.0 | 0.0 | 38.2 | 33.3 | 51.5 |  |
| Prop In Lane |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  |
| Lane Grp Cap(c), veh/h | 864 | 0 | 0 | 864 | 834 | 742 |  |
| V/C Ratio(X) | 0.74 | 0.00 | 0.00 | 0.85 | 0.77 | 1.03 |  |
| Avail Cap(c_a), veh/h | 864 | 0 | 0 | 869 | 834 | 742 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 24.2 | 0.0 | 0.0 | 26.2 | 24.4 | 29.2 |  |
| Incr Delay (d2), s/veh | 5.6 | 0.0 | 0.0 | 10.2 | 4.2 | 40.4 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 13.8 | 0.0 | 0.0 | 18.1 | 13.8 | 26.0 |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 29.7 | 0.0 | 0.0 | 36.5 | 28.6 | 69.7 |  |
| LnGrp LOS | C | A | A | D | C | F |  |
| Approach Vol, veh/h | 637 |  |  | 734 | 1409 |  |  |
| Approach Delay, s/veh | 29.7 |  |  | 36.5 | 50.8 |  |  |
| Approach LOS | C |  |  | D | D |  |  |
| Timer - Assigned Phs |  | 2 |  |  |  | 6 | 8 |
| Phs Duration (G+Y+Rc), s |  | 55.0 |  |  |  | 55.0 | 55.0 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | * 4.2 |  |  |  | * 4.2 | 3.5 |
| Max Green Setting (Gmax), s |  | * 51 |  |  |  | * 51 | 51.5 |
| Max Q Clear Time (g_c+l1), s |  | 32.6 |  |  |  | 40.2 | 53.5 |
| Green Ext Time (p_c), s |  | 2.3 |  |  |  | 2.3 | 0.0 |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 42.2 |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

|  | $\rangle$ | $\rightarrow$ | 7 | 7 | 4 | 4 | 4 | $\dagger$ | $p$ | － | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 个4 | 「 | \％ | 个4 | F | \％${ }^{17}$ | $\hat{F}$ |  | ${ }^{7}$ | 4 | F |
| Traffic Volume（veh／h） | 165 | 949 | 285 | 114 | 1045 | 64 | 220 | 5 | 97 | 53 | 4 | 90 |
| Future Volume（veh／h） | 165 | 949 | 285 | 114 | 1045 | 64 | 220 | 5 | 97 | 53 | 4 | 90 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 165 | 949 | 285 | 114 | 1045 | 64 | 220 | 5 | 97 | 53 | 4 | 90 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 125 | 1308 | 583 | 142 | 1315 | 587 | 268 | 8 | 154 | 496 | 580 | 491 |
| Arrive On Green | 0.07 | 0.37 | 0.37 | 0.08 | 0.37 | 0.37 | 0.08 | 0.10 | 0.10 | 0.28 | 0.31 | 0.31 |
| Sat Flow，veh／h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 3456 | 78 | 1519 | 1781 | 1870 | 1585 |
| Grp Volume（v），veh／h | 165 | 949 | 285 | 114 | 1045 | 64 | 220 | 0 | 102 | 53 | 4 | 90 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1728 | 0 | 1597 | 1781 | 1870 | 1585 |
| Q Serve（g＿s），s | 8.4 | 27.6 | 16.6 | 7.6 | 31.5 | 3.2 | 7.5 | 0.0 | 7.4 | 2.7 | 0.2 | 3.8 |
| Cycle Q Clear（g＿c），s | 8.4 | 27.6 | 16.6 | 7.6 | 31.5 | 3.2 | 7.5 | 0.0 | 7.4 | 2.7 | 0.2 | 3.8 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.95 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 125 | 1308 | 583 | 142 | 1315 | 587 | 268 | 0 | 162 | 496 | 580 | 491 |
| V／C Ratio（X） | 1.32 | 0.73 | 0.49 | 0.80 | 0.79 | 0.11 | 0.82 | 0.00 | 0.63 | 0.11 | 0.01 | 0.18 |
| Avail Cap（c＿a），veh／h | 125 | 1706 | 761 | 143 | 1741 | 777 | 268 | 0 | 323 | 496 | 580 | 491 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.41 | 0.41 | 0.41 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 55.8 | 32.7 | 29.2 | 54.3 | 33.7 | 24.8 | 54.5 | 0.0 | 51.7 | 32.2 | 28.6 | 17.9 |
| Incr Delay（d2），s／veh | 190.6 | 0.7 | 0.2 | 13.4 | 1.0 | 0.0 | 18.9 | 0.0 | 17.0 | 0.0 | 0.0 | 0.8 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 10.3 | 11.5 | 6.1 | 3.8 | 13.1 | 1.2 | 4.0 | 0.0 | 3.7 | 1.2 | 0.1 | 1.9 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 246.4 | 33.4 | 29.5 | 67.7 | 34.7 | 24.9 | 73.4 | 0.0 | 68.7 | 32.2 | 28.7 | 18.7 |
| LnGrp LOS | F | C | C | E | C | C | E | A | E | C | C | B |
| Approach Vol，veh／h |  | 1399 |  |  | 1223 |  |  | 322 |  |  | 147 |  |
| Approach Delay，s／veh |  | 57.7 |  |  | 37.3 |  |  | 71.9 |  |  | 23.9 |  |
| Approach LOS |  | E |  |  | D |  |  | E |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 38.8 | 17.6 | 14.1 | 49.6 | 13.8 | 42.6 | 13.8 | 49.8 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 5.4 | ＊ 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 5.4 | ＊5．4 |  |  |  |  |
| Max Green Setting（Gmax），s | 8.7 | ＊24 | 9.6 | 57.6 | 9.3 | 23.7 | 8.4 | ＊59 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 4.7 | 9.4 | 9.6 | 29.6 | 9.5 | 5.8 | 10.4 | 33.5 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 0.6 | 0.0 | 4.8 | 0.0 | 0.1 | 0.0 | 10.9 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 49.5 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 性 |  | \% | 个4 | F | ${ }^{7}$ | F |  | \% | 1 |  |
| Traffic Volume (veh/h) | 73 | 1022 | 27 | 64 | 1171 | 60 | 7 | 3 | 32 | 105 | 2 | 22 |
| Future Volume (veh/h) | 73 | 1022 | 27 | 64 | 1171 | 60 | 7 | 3 | 32 | 105 | 2 | 22 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 73 | 1022 | 27 | 64 | 1171 | 60 | 7 | 3 | 32 | 105 | 2 | 22 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 175 | 1372 | 36 | 147 | 1322 | 590 | 38 | 35 | 376 | 194 | 46 | 506 |
| Arrive On Green | 0.10 | 0.39 | 0.39 | 0.08 | 0.37 | 0.37 | 0.02 | 0.26 | 0.26 | 0.11 | 0.34 | 0.34 |
| Sat Flow, veh/h | 1781 | 3537 | 93 | 1781 | 3554 | 1585 | 1781 | 138 | 1468 | 1781 | 134 | 1472 |
| Grp Volume(v), veh/h | 73 | 513 | 536 | 64 | 1171 | 60 | 7 | 0 | 35 | 105 | 0 | 24 |
| Grp Sat Flow(s),veh/h/n | 1781 | 1777 | 1854 | 1781 | 1777 | 1585 | 1781 | 0 | 1606 | 1781 | 0 | 1605 |
| Q Serve(g_s), s | 4.6 | 29.8 | 29.9 | 4.1 | 37.0 | 3.0 | 0.5 | 0.0 | 2.0 | 6.7 | 0.0 | 1.2 |
| Cycle Q Clear(g_c), s | 4.6 | 29.8 | 29.9 | 4.1 | 37.0 | 3.0 | 0.5 | 0.0 | 2.0 | 6.7 | 0.0 | 1.2 |
| Prop In Lane | 1.00 |  | 0.05 | 1.00 |  | 1.00 | 1.00 |  | 0.91 | 1.00 |  | 0.92 |
| Lane Grp Cap(c), veh/h | 175 | 689 | 719 | 147 | 1322 | 590 | 38 | 0 | 411 | 194 | 0 | 552 |
| V/C Ratio(X) | 0.42 | 0.74 | 0.75 | 0.44 | 0.89 | 0.10 | 0.19 | 0.00 | 0.09 | 0.54 | 0.00 | 0.04 |
| Avail Cap(c_a), veh/h | 191 | 755 | 788 | 171 | 1469 | 655 | 181 | 0 | 411 | 200 | 0 | 552 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.9 | 31.6 | 31.6 | 52.4 | 35.3 | 24.6 | 57.7 | 0.0 | 34.0 | 50.6 | 0.0 | 26.2 |
| Incr Delay (d2), s/veh | 0.1 | 0.3 | 0.3 | 2.0 | 6.4 | 0.1 | 2.3 | 0.0 | 0.4 | 2.7 | 0.0 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.0 | 12.2 | 12.7 | 1.9 | 16.4 | 1.1 | 0.2 | 0.0 | 0.8 | 3.1 | 0.0 | 0.5 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 51.0 | 32.0 | 31.9 | 54.5 | 41.7 | 24.7 | 60.1 | 0.0 | 34.4 | 53.3 | 0.0 | 26.4 |
| LnGrp LOS | D | C | C | D | D | C | E | A | C | D | A | C |
| Approach Vol, veh/h |  | 1122 |  |  | 1295 |  |  | 42 |  |  | 129 |  |
| Approach Delay, s/veh |  | 33.2 |  |  | 41.5 |  |  | 38.7 |  |  | 48.3 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 17.6 | 36.1 | 14.4 | 51.9 | 7.0 | 46.6 | 16.3 | 50.0 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$, s | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 |
| Max Green Setting (Gmax), s | 13.5 | 24.2 | 11.5 | 51.0 | 12.2 | 25.5 | 12.9 | 49.6 |
| Max Q Clear Time (g_c+11), s | 8.7 | 4.0 | 6.1 | 31.9 | 2.5 | 3.2 | 6.6 | 39.0 |
| Green Ext Time (p_c), s | 0.1 | 0.1 | 0.0 | 6.1 | 0.0 | 0.1 | 0.1 | 5.6 |

## Intersection Summary

HCM 6th Ctrl Delay 38.2

HCM 6th LOS D

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 19 |  |  | $1 \psi^{*}$ |  |  |  | 「 |  |  | F' |
| Traffic Vol, veh/h | 0 | 1150 | 10 | 0 | 1314 | 89 | 0 | 0 | 14 | 0 | 0 | 13 |
| Future Vol, veh/h | 0 | 1150 | 10 | 0 | 1314 | 89 | 0 | 0 | 14 | 0 | 0 | 13 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 0 | - | - | 0 |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1150 | 10 | 0 | 1314 | 89 | 0 | 0 | 14 | 0 | 0 | 13 |



HCM 6th Signalized Intersection Summary
6：Gateway Oaks Drive \＆West El Camino Avenue
08／03／2020

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％${ }^{1 / 1}$ | 个巾4 | 「 | \％${ }^{1+1}$ | 个个 | 「 | \％${ }^{*}$ | 个4 | 「 | \％${ }^{1+1}$ | 个4 | F |
| Traffic Volume（veh／h） | 82 | 847 | 215 | 245 | 584 | 102 | 374 | 60 | 371 | 450 | 117 | 280 |
| Future Volume（veh／h） | 82 | 847 | 215 | 245 | 584 | 102 | 374 | 60 | 371 | 450 | 117 | 280 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 82 | 847 | 215 | 245 | 584 | 102 | 374 | 60 | 371 | 450 | 117 | 280 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 447 | 1098 | 341 | 478 | 792 | 353 | 519 | 916 | 409 | 541 | 936 | 417 |
| Arrive On Green | 0.13 | 0.22 | 0.22 | 0.14 | 0.22 | 0.22 | 0.15 | 0.26 | 0.26 | 0.16 | 0.26 | 0.26 |
| Sat Flow，veh／h | 3456 | 5106 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 |
| Grp Volume（v），veh／h | 82 | 847 | 215 | 245 | 584 | 102 | 374 | 60 | 371 | 450 | 117 | 280 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 |
| Q Serve（g＿s），s | 1.8 | 13.5 | 10.7 | 5.7 | 13.2 | 4.6 | 8.9 | 1.1 | 19.6 | 10.9 | 2.2 | 13.7 |
| Cycle Q Clear（g＿c），s | 1.8 | 13.5 | 10.7 | 5.7 | 13.2 | 4.6 | 8.9 | 1.1 | 19.6 | 10.9 | 2.2 | 13.7 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 447 | 1098 | 341 | 478 | 792 | 353 | 519 | 916 | 409 | 541 | 936 | 417 |
| V／C Ratio（X） | 0.18 | 0.77 | 0.63 | 0.51 | 0.74 | 0.29 | 0.72 | 0.07 | 0.91 | 0.83 | 0.13 | 0.67 |
| Avail Cap（c＿a），veh／h | 519 | 1545 | 480 | 479 | 1043 | 465 | 722 | 1260 | 562 | 838 | 1375 | 613 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 33.6 | 32.0 | 30.9 | 34.6 | 31.3 | 27.9 | 35.1 | 24.2 | 31.1 | 35.4 | 24.3 | 28.5 |
| Incr Delay（d2），s／veh | 0.1 | 0.9 | 0.7 | 0.4 | 1.2 | 0.2 | 1.0 | 0.0 | 12.5 | 2.3 | 0.0 | 0.7 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.7 | 5.3 | 4.0 | 2.3 | 5.4 | 1.7 | 3.7 | 0.5 | 8.7 | 4.7 | 0.9 | 5.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 33.7 | 32.9 | 31.6 | 35.0 | 32.5 | 28.1 | 36.1 | 24.3 | 43.6 | 37.7 | 24.3 | 29.2 |
| LnGrp LOS | C | C | C | D | C | C | D | C | D | D | C | C |
| Approach Vol，veh／h |  | 1144 |  |  | 931 |  |  | 805 |  |  | 847 |  |
| Approach Delay，s／veh |  | 32.7 |  |  | 32.7 |  |  | 38.7 |  |  | 33.1 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | C |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 16.3 | 24.1 | 18.1 | 28.1 | 17.0 | 23.4 | 18.6 | 27.6 |
| Change Period（Y＋Rc），s | ${ }^{*} 5.1$ | ${ }^{*} 4.8$ | ${ }^{*} 5.1$ | ${ }^{*} 5.3$ | 5.0 | ${ }^{*} 4.8$ | 5.0 | ${ }^{*} 5.3$ |
| Max Green Setting（Gmax），s | ${ }^{*} 13$ | ${ }^{*} 25$ | ${ }^{*} 18$ | ${ }^{*} 34$ | 12.0 | ${ }^{*} 26$ | 21.0 | ${ }^{*} 31$ |
| Max Q Clear Time（g＿c＋11），s | 3.8 | 15.2 | 10.9 | 15.7 | 7.7 | 15.5 | 12.9 | 21.6 |
| Green Ext Time（p＿c），s | 0.1 | 1.9 | 0.5 | 0.9 | 0.2 | 3.1 | 0.6 | 0.7 |

Intersection Summary

| HCM 6th Ctrl Delay | 34.1 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．




# INTERSECTION ANALYSIS <br> BASELINE PLUS PROJECT CONDITIONS <br> AM PEAK HOUR 



## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

|  | $\rightarrow$ |  | 7 | $\Perp$ | 4 | \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |
| Lane Configurations | 4 |  |  | 4 | ${ }^{7}$ | 7 |  |
| Traffic Volume (veh/h) | 1115 | 0 | 0 | 695 | 117 | 429 |  |
| Future Volume (veh/h) | 1115 | 0 | 0 | 695 | 117 | 429 |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Work Zone On Approach | No |  |  | No | No |  |  |
| Adj Sat Flow, veh/h/ln | 1870 | 0 | 0 | 1870 | 1870 | 1870 |  |
| Adj Flow Rate, veh/h | 1115 | 0 | 0 | 695 | 117 | 429 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Percent Heavy Veh, \% | 2 | 0 | 0 | 2 | 2 | 2 |  |
| Cap, veh/h | 1374 | 0 | 0 | 1374 | 348 | 310 |  |
| Arrive On Green | 0.73 | 0.00 | 0.00 | 0.73 | 0.20 | 0.20 |  |
| Sat Flow, veh/h | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Grp Volume(v), veh/h | 1115 | 0 | 0 | 695 | 117 | 429 |  |
| Grp Sat Flow(s),veh/h/ln | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Q Serve(g_s), s | 43.1 | 0.0 | 0.0 | 17.3 | 6.2 | 21.5 |  |
| Cycle Q Clear(g_c), s | 43.1 | 0.0 | 0.0 | 17.3 | 6.2 | 21.5 |  |
| Prop In Lane |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  |
| Lane Grp Cap(c), veh/h | 1374 | 0 | 0 | 1374 | 348 | 310 |  |
| V/C Ratio(X) | 0.81 | 0.00 | 0.00 | 0.51 | 0.34 | 1.38 |  |
| Avail Cap(c_a), veh/h | 1374 | 0 | 0 | 1379 | 348 | 310 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 9.6 | 0.0 | 0.0 | 6.2 | 38.1 | 44.3 |  |
| Incr Delay (d2), s/veh | 5.3 | 0.0 | 0.0 | 1.3 | 0.2 | 192.0 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 14.7 | 0.0 | 0.0 | 5.6 | 2.6 | 24.6 |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 14.9 | 0.0 | 0.0 | 7.5 | 38.3 | 236.2 |  |
| LnGrp LOS | B | A | A | A | D | F |  |
| Approach Vol, veh/h | 1115 |  |  | 695 | 546 |  |  |
| Approach Delay, s/veh | 14.9 |  |  | 7.5 | 193.8 |  |  |
| Approach LOS | B |  |  | A | F |  |  |
| Timer - Assigned Phs |  | 2 |  |  |  | 6 | 8 |
| Phs Duration (G+Y+Rc), s |  | 85.0 |  |  |  | 85.0 | 25.0 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | * 4.2 |  |  |  | * 4.2 | 3.5 |
| Max Green Setting (Gmax), s |  | * 81 |  |  |  | * 81 | 21.5 |
| Max Q Clear Time (g_c+l1), s |  | 45.1 |  |  |  | 19.3 | 23.5 |
| Green Ext Time (p_c), s |  | 6.5 |  |  |  | 2.9 | 0.0 |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 54.2 |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

|  | 4 | $\rightarrow$ | 7 | $\checkmark$ |  | 4 | 4 | 4 | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 个4 | 7 | \＃ | 个个 | F | ＊＊ | $\hat{\beta}$ |  | \％ | $\uparrow$ | F |
| Traffic Volume（veh／h） | 308 | 1222 | 71 | 57 | 806 | 46 | 438 | 9 | 122 | 161 | 18 | 170 |
| Future Volume（veh／h） | 308 | 1222 | 71 | 57 | 806 | 46 | 438 | 9 | 122 | 161 | 18 | 170 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 308 | 1222 | 71 | 57 | 806 | 46 | 438 | 9 | 122 | 161 | 18 | 170 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 335 | 1379 | 615 | 99 | 882 | 393 | 500 | 11 | 154 | 499 | 461 | 391 |
| Arrive On Green | 0.19 | 0.39 | 0.39 | 0.06 | 0.25 | 0.25 | 0.14 | 0.10 | 0.10 | 0.28 | 0.25 | 0.25 |
| Sat Flow，veh／h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 3456 | 110 | 1492 | 1781 | 1870 | 1585 |
| Grp Volume（v），veh／h | 308 | 1222 | 71 | 57 | 806 | 46 | 438 | 0 | 131 | 161 | 18 | 170 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1728 | 0 | 1602 | 1781 | 1870 | 1585 |
| Q Serve（g＿s），s | 20.4 | 38.5 | 3.4 | 3.7 | 26.5 | 2.7 | 14.9 | 0.0 | 9.6 | 8.6 | 0.9 | 6.9 |
| Cycle Q Clear（g＿c），s | 20.4 | 38.5 | 3.4 | 3.7 | 26.5 | 2.7 | 14.9 | 0.0 | 9.6 | 8.6 | 0.9 | 6.9 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.93 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 335 | 1379 | 615 | 99 | 882 | 393 | 500 | 0 | 166 | 499 | 461 | 391 |
| V／C Ratio（X） | 0.92 | 0.89 | 0.12 | 0.57 | 0.91 | 0.12 | 0.88 | 0.00 | 0.79 | 0.32 | 0.04 | 0.44 |
| Avail Cap（c＿a），veh／h | 408 | 1522 | 679 | 99 | 906 | 404 | 541 | 0 | 367 | 499 | 461 | 391 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.88 | 0.88 | 0.88 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 47.8 | 34.3 | 23.5 | 55.3 | 43.9 | 34.9 | 50.2 | 0.0 | 52.5 | 34.2 | 34.4 | 15.2 |
| Incr Delay（d2），s／veh | 21.1 | 5.8 | 0.0 | 8.4 | 12.3 | 0.2 | 14.7 | 0.0 | 31.0 | 0.1 | 0.2 | 3.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 10.7 | 16.8 | 1.3 | 1.9 | 12.7 | 1.0 | 7.4 | 0.0 | 5.3 | 3.8 | 0.4 | 4.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 68.9 | 40.1 | 23.6 | 63.6 | 56.2 | 35.1 | 65.0 | 0.0 | 83.5 | 34.3 | 34.6 | 18.7 |
| LnGrp LOS | E | D | C | E | E | D | E | A | F | C | C | B |
| Approach Vol，veh／h |  | 1601 |  |  | 909 |  |  | 569 |  |  | 349 |  |
| Approach Delay，s／veh |  | 44.9 |  |  | 55.6 |  |  | 69.2 |  |  | 26.7 |  |
| Approach LOS |  | D |  |  | E |  |  | E |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 39.0 | 17.8 | 11.2 | 52.0 | 21.9 | 35.0 | 28.0 | 35.2 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s | 5.4 | ＊ 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 5.4 | ＊5．4 |  |  |  |  |
| Max Green Setting（Gmax），s | 14.6 | ＊28 | 6.7 | 51.4 | 18.8 | 23.3 | 27.5 | ＊31 |  |  |  |  |
| Max Q Clear Time（g＿c＋1），s | 10.6 | 11.6 | 5.7 | 40.5 | 16.9 | 8.9 | 22.4 | 28.5 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.1 | 0.8 | 0.0 | 4.3 | 0.5 | 0.3 | 0.2 | 1.3 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 49.9 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个t |  | \% | 个 $\uparrow$ | F | ${ }^{7}$ | $\hat{F}$ |  | \% | $\hat{\beta}$ |  |
| Traffic Volume (veh/h) | 15 | 1320 | 35 | 196 | 850 | 25 | 13 | 0 | 47 | 122 | 3 | 46 |
| Future Volume (veh/h) | 15 | 1320 | 35 | 196 | 850 | 25 | 13 | 0 | 47 | 122 | 3 | 46 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 15 | 1320 | 35 | 196 | 850 | 25 | 13 | 0 | 47 | 122 | 3 | 46 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 75 | 1368 | 36 | 223 | 1670 | 745 | 64 | 0 | 337 | 197 | 28 | 431 |
| Arrive On Green | 0.04 | 0.39 | 0.39 | 0.13 | 0.47 | 0.47 | 0.04 | 0.00 | 0.21 | 0.11 | 0.29 | 0.29 |
| Sat Flow, veh/h | 1781 | 3537 | 94 | 1781 | 3554 | 1585 | 1781 | 0 | 1585 | 1781 | 98 | 1502 |
| Grp Volume(v), veh/h | 15 | 663 | 692 | 196 | 850 | 25 | 13 | 0 | 47 | 122 | 0 | 49 |
| Grp Sat Flow(s),veh/h/n | 1781 | 1777 | 1853 | 1781 | 1777 | 1585 | 1781 | 0 | 1585 | 1781 | 0 | 1600 |
| Q Serve(g_s), s | 1.0 | 43.8 | 43.9 | 13.0 | 20.0 | 1.0 | 0.9 | 0.0 | 2.9 | 7.8 | 0.0 | 2.7 |
| Cycle Q Clear(g_c), s | 1.0 | 43.8 | 43.9 | 13.0 | 20.0 | 1.0 | 0.9 | 0.0 | 2.9 | 7.8 | 0.0 | 2.7 |
| Prop In Lane | 1.00 |  | 0.05 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.94 |
| Lane Grp Cap(c), veh/h | 75 | 687 | 717 | 223 | 1670 | 745 | 64 | 0 | 337 | 197 | 0 | 459 |
| V/C Ratio(X) | 0.20 | 0.96 | 0.97 | 0.88 | 0.51 | 0.03 | 0.20 | 0.00 | 0.14 | 0.62 | 0.00 | 0.11 |
| Avail Cap(c_a), veh/h | 191 | 690 | 720 | 245 | 1670 | 745 | 181 | 0 | 337 | 200 | 0 | 459 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 55.5 | 36.0 | 36.0 | 51.6 | 22.2 | 17.1 | 56.2 | 0.0 | 38.4 | 51.0 | 0.0 | 31.5 |
| Incr Delay (d2), s/veh | 0.1 | 4.6 | 4.6 | 26.8 | 0.3 | 0.0 | 1.6 | 0.0 | 0.9 | 5.6 | 0.0 | 0.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.4 | 18.7 | 19.6 | 7.3 | 8.0 | 0.4 | 0.4 | 0.0 | 1.2 | 3.8 | 0.0 | 1.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 55.6 | 40.6 | 40.6 | 78.4 | 22.4 | 17.2 | 57.8 | 0.0 | 39.2 | 56.5 | 0.0 | 31.9 |
| LnGrp LOS | E | D | D | E | C | B | E | A | D | E | A | C |
| Approach Vol, veh/h |  | 1370 |  |  | 1071 |  |  | 60 |  |  | 171 |  |
| Approach Delay, s/veh |  | 40.8 |  |  | 32.5 |  |  | 43.2 |  |  | 49.5 |  |
| Approach LOS |  | D |  |  | C |  |  | D |  |  | D |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 17.8 | 30.9 | 19.5 | 51.8 | 8.8 | 39.9 | 9.6 | 61.8 |
| Change Period (Y+Rc), s | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 |
| Max Green Setting (Gmax), s | 13.5 | 23.6 | 16.5 | 46.6 | 12.2 | 24.9 | 12.9 | 50.2 |
| Max Q Clear Time (g_c $\mathbf{c} 11$ ), s | 9.8 | 4.9 | 15.0 | 45.9 | 2.9 | 4.7 | 3.0 | 22.0 |
| Green Ext Time (p_c), s | 0.1 | 0.2 | 0.1 | 0.6 | 0.0 | 0.2 | 0.0 | 6.1 |

## Intersection Summary

HCM 6th Ctrl Delay 38.1

HCM 6th LOS D

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 中F |  |  | 1\% |  |  |  | 7 |  |  | 7 |
| Traffic Vol, veh/h | 0 | 1643 | 4 | 0 | 914 | 36 | 0 | 0 | 17 | 0 | 0 | 26 |
| Future Vol, veh/h | 0 | 1643 | 4 | 0 | 914 | 36 | 0 | 0 | 17 | 0 | 0 | 26 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 0 | - | - | 0 |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1643 | 4 | 0 | 914 | 36 | 0 | 0 | 17 | 0 | 0 | 26 |



HCM 6th Signalized Intersection Summary
6：Gateway Oaks Drive \＆West El Camino Avenue
08／03／2020

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％${ }^{1 / 4}$ | 个巾4 | 「 | \％${ }^{1 / 1}$ | 个4 | 「 | \％${ }^{1 / 1}$ | 个4 | 「 | \％${ }^{1 / 1}$ | 个4 | F |
| Traffic Volume（veh／h） | 324 | 767 | 445 | 351 | 602 | 574 | 220 | 117 | 127 | 130 | 34 | 44 |
| Future Volume（veh／h） | 324 | 767 | 445 | 351 | 602 | 574 | 220 | 117 | 127 | 130 | 34 | 44 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 324 | 767 | 445 | 351 | 602 | 574 | 220 | 117 | 127 | 130 | 34 | 44 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 477 | 1898 | 589 | 440 | 1279 | 571 | 476 | 583 | 260 | 426 | 528 | 236 |
| Arrive On Green | 0.14 | 0.37 | 0.37 | 0.13 | 0.36 | 0.36 | 0.14 | 0.16 | 0.16 | 0.12 | 0.15 | 0.15 |
| Sat Flow，veh／h | 3456 | 5106 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 |
| Grp Volume（v），veh／h | 324 | 767 | 445 | 351 | 602 | 574 | 220 | 117 | 127 | 130 | 34 | 44 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 |
| Q Serve（g＿s），s | 8.4 | 10.5 | 23.1 | 9.3 | 12.3 | 33.9 | 5.5 | 2.7 | 6.9 | 3.2 | 0.8 | 2.3 |
| Cycle Q Clear（g＿c），s | 8.4 | 10.5 | 23.1 | 9.3 | 12.3 | 33.9 | 5.5 | 2.7 | 6.9 | 3.2 | 0.8 | 2.3 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 477 | 1898 | 589 | 440 | 1279 | 571 | 476 | 583 | 260 | 426 | 528 | 236 |
| V／C Ratio（X） | 0.68 | 0.40 | 0.76 | 0.80 | 0.47 | 1.01 | 0.46 | 0.20 | 0.49 | 0.31 | 0.06 | 0.19 |
| Avail Cap（c＿a），veh／h | 477 | 1898 | 589 | 551 | 1279 | 571 | 477 | 1178 | 525 | 440 | 1136 | 507 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 38.6 | 21.9 | 25.8 | 39.9 | 23.2 | 30.1 | 37.4 | 34.0 | 35.8 | 37.6 | 34.4 | 35.1 |
| Incr Delay（d2），s／veh | 3.2 | 0.1 | 5.0 | 5.1 | 0.1 | 39.1 | 0.3 | 0.1 | 0.5 | 0.1 | 0.0 | 0.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 3.6 | 3.9 | 9.2 | 4.1 | 4.8 | 18.5 | 2.3 | 1.2 | 2.7 | 1.4 | 0.3 | 0.9 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 41.8 | 21.9 | 30.8 | 45.0 | 23.3 | 69.2 | 37.7 | 34.1 | 36.3 | 37.8 | 34.5 | 35.2 |
| LnGrp LOS | D | C | C | D | C | F | D | C | D | D | C | D |
| Approach Vol，veh／h |  | 1536 |  |  | 1527 |  |  | 464 |  |  | 208 |  |
| Approach Delay，s／veh |  | 28.7 |  |  | 45.6 |  |  | 36.4 |  |  | 36.7 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 18.1 | 38.7 | 18.1 | 19.3 | 17.0 | 39.8 | 16.6 | 20.8 |  |
| Change Period（ $Y+R \mathrm{R}$ ），s | ＊5．1 | ＊ 4.8 | ＊ 5.1 | ＊ 5.3 | 5.0 | ＊4．8 | 5.0 | ＊ 5.3 |  |
| Max Green Setting（Gmax），s | ＊13 | ＊ 34 | ＊13 | ＊ 30 | 15.0 | ＊ 32 | 12.0 | ＊31 |  |
| Max Q Clear Time（g＿c＋1），s | 10.4 | 35.9 | 7.5 | 4.3 | 11.3 | 25.1 | 5.2 | 8.9 |  |
| Green Ext Time（p＿c），s | 0.2 | 0.0 | 0.2 | 0.2 | 0.3 | 2.5 | 0.1 | 0.6 |  |

Intersection Summary

| HCM 6th Ctrl Delay | 37.0 |
| :--- | ---: |
| HCM 6th LOS | $D$ |

## Notes

User approved pedestrian interval to be less than phase max green．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个4 | 个. | $\mathbf{F}$ |  | $\mathbf{F}$ |
| Traffic Vol, veh/h | 0 | 1543 | 1279 | 234 | 0 | 221 |
| Future Vol, veh/h | 0 | 1543 | 1279 | 234 | 0 | 221 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1543 | 1279 | 234 | 0 | 221 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | Y |  |
| Traffic Vol, veh/h | 54 | 4 | 4 | 60 | 2 | 4 |
| Future Vol, veh/h | 54 | 4 | 4 | 60 | 2 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 54 | 4 | 4 | 60 | 2 | 4 |



|  | $\rightarrow$ | 4 | * | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | SBL | SBR |
| Lane Group Flow (vph) | 468 | 311 | 765 | 96 |
| v/c Ratio | 0.65 | 0.43 | 0.90 | 0.06 |
| Control Delay | 19.7 | 15.4 | 29.5 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 19.7 | 15.4 | 29.5 | 0.1 |
| Queue Length 50th (ft) | 134 | 80 | 183 | 0 |
| Queue Length 95th (ft) | 208 | 129 | \#421 | 0 |
| Internal Link Dist (ft) | 294 | 252 | 765 |  |
| Turn Bay Length (ft) |  |  |  | 800 |
| Base Capacity (vph) | 741 | 741 | 877 | 1583 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.63 | 0.42 | 0.87 | 0.06 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longerQueue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |

Queues
2: Eastbound I-80 Ramp \& West El Camino Avenue

|  | $\rightarrow$ |  | 4 | 7 |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | NBL | NBR |
| Lane Group Flow (vph) | 1115 | 695 | 117 | 429 |
| v/c Ratio | 0.86 | 0.53 | 0.28 | 0.89 |
| Control Delay | 20.8 | 9.6 | 37.8 | 48.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 20.8 | 9.6 | 37.8 | 48.9 |
| Queue Length 50th (ft) | 622 | 246 | 64 | 188 |
| Queue Length 95th (ft) | 670 | 248 | 127 | \#425 |
| Internal Link Dist (ft) | 249 | 128 | 477 |  |
| Turn Bay Length (ft) |  |  |  | 150 |
| Base Capacity (vph) | 1368 | 1373 | 413 | 483 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.82 | 0.51 | 0.28 | 0.89 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longerQueue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |

Queues
3: Orchard Lane \& West El Camino Avenue

|  | 7 | $\rightarrow$ | 7 | $\dagger$ | 4 | 4 | 4 | $\dagger$ | $\downarrow$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Group Flow (vph) | 308 | 1222 | 71 | 57 | 806 | 46 | 438 | 131 | 161 | 18 | 170 |
| v/c Ratio | 0.86 | 0.85 | 0.10 | 0.38 | 0.78 | 0.08 | 0.79 | 0.34 | 0.57 | 0.05 | 0.40 |
| Control Delay | 68.0 | 38.1 | 0.3 | 36.6 | 38.4 | 4.2 | 59.6 | 12.9 | 55.1 | 46.7 | 10.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 68.0 | 38.1 | 0.3 | 36.6 | 38.4 | 4.2 | 59.6 | 12.9 | 55.1 | 46.7 | 10.2 |
| Queue Length 50th (ft) | 229 | 431 | 0 | 42 | 344 | 2 | 165 | 6 | 117 | 12 | 0 |
| Queue Length 95th (ft) | \#348 | 512 | 0 | 86 | 417 | 26 | \#245 | 66 | 186 | 35 | 64 |
| Internal Link Dist (ft) |  | 183 |  |  | 844 |  |  | 420 |  | 204 |  |
| Turn Bay Length (ft) | 295 |  | 240 | 295 |  | 135 | 155 |  | 70 |  | 240 |
| Base Capacity (vph) | 410 | 1547 | 778 | 152 | 1042 | 579 | 566 | 480 | 283 | 410 | 481 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | O | 0 |  | 0 | 0 | 0 |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.75 | 0.79 | 0.09 | 0.38 | 0.77 | 0.08 | 0.77 | 0.27 | 0.57 | 0.04 | 0.35 |

Intersection Summary
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Queues
4: West River Drive/River Oaks Way \& West El Camino Avenue

|  | $\rangle$ | $\rightarrow$ | $\dagger$ |  | 4 | 4 | $\dagger$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 15 | 1355 | 196 | 850 | 25 | 13 | 47 | 122 | 49 |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.08 | 0.97 | 0.84 | 0.48 | 0.03 | 0.07 | 0.09 | 0.61 | 0.10 |
| Control Delay | 34.1 | 58.0 | 80.6 | 21.9 | 0.1 | 49.9 | 0.4 | 64.8 | 12.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.1 | 58.0 | 80.6 | 21.9 | 0.1 | 49.9 | 0.4 | 64.8 | 12.6 |
| Queue Length 50th ( t ) | 9 | 579 | 149 | 189 | 0 | 9 | 0 | 91 | 2 |
| Queue Length 95th (ft) | m13 | \#714 | \#271 | 326 | 0 | 30 | 0 | \#158 | 35 |
| Internal Link Dist (ft) |  | 844 |  | 641 |  |  | 474 |  | 441 |
| Turn Bay Length (ft) |  |  | 155 |  | 165 | 100 |  | 100 |  |
| Base Capacity (vph) | 190 | 1391 | 243 | 1788 | 851 | 179 | 510 | 199 | 498 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.08 | 0.97 | 0.81 | 0.48 | 0.03 | 0.07 | 0.09 | 0.61 | 0.10 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |
| m Volume for 95th perc | queue | metered | by upstr | am sign |  |  |  |  |  |

Queues
6: Gateway Oaks Drive \& West El Camino Avenue

|  | 4 | $\rightarrow$ | 7 | 7 | - | 4 | 4 | $\dagger$ | p |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 324 | 767 | 445 | 351 | 602 | 574 | 220 | 117 | 127 | 130 | 34 | 44 |
| v/c Ratio | 0.58 | 0.62 | 0.62 | 0.62 | 0.69 | 0.70 | 0.30 | 0.18 | 0.32 | 0.25 | 0.05 | 0.12 |
| Control Delay | 36.2 | 29.4 | 6.9 | 36.5 | 31.6 | 7.4 | 31.1 | 29.2 | 8.5 | 32.5 | 29.4 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 36.2 | 29.4 | 6.9 | 36.5 | 31.6 | 7.4 | 31.1 | 29.2 | 8.5 | 32.5 | 29.4 | 0.6 |
| Queue Length 50th (tt) | 77 | 123 | 0 | 84 | 143 | 0 | 51 | 25 | 0 | 29 | 7 | 0 |
| Queue Length 95th (ft) | 129 | 168 | 69 | 135 | 196 | 77 | 90 | 52 | 46 | 59 | 21 | 0 |
| Internal Link Dist (ft) |  | 185 |  |  | 456 |  |  | 405 |  |  | 335 |  |
| Turn Bay Length (ft) | 175 |  | 150 | 190 |  | 190 | 140 |  | 140 | 230 |  | 230 |
| Base Capacity (vph) | 562 | 2032 | 899 | 649 | 1512 | 1005 | 734 | 1392 | 699 | 519 | 1343 | 674 |
| Starvation Cap Reductn | , | 0 | 0 | , | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.58 | 0.38 | 0.49 | 0.54 | 0.40 | 0.57 | 0.30 | 0.08 | 0.18 | 0.25 | 0.03 | 0.07 |

[^19]
## INTERSECTION ANALYSIS <br> BASELINE PLUS PROJECT CONDITIONS

PM PEAK HOUR


## Notes

Unsignalized Delay for [SBR] is excluded from calculations of the approach delay and intersection delay.

|  | $\rightarrow$ |  | 7 | $\Perp$ | 4 | \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |
| Lane Configurations | 4 |  |  | 4 | ${ }^{1 /}$ | 7 |  |
| Traffic Volume (veh/h) | 674 | 0 | 0 | 747 | 646 | 759 |  |
| Future Volume (veh/h) | 674 | 0 | 0 | 747 | 646 | 759 |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Work Zone On Approach | No |  |  | No | No |  |  |
| Adj Sat Flow, veh/h/ln | 1870 | 0 | 0 | 1870 | 1870 | 1870 |  |
| Adj Flow Rate, veh/h | 674 | 0 | 0 | 747 | 646 | 759 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Percent Heavy Veh, \% | 2 | 0 | 0 | 2 | 2 | 2 |  |
| Cap, veh/h | 864 | 0 | 0 | 864 | 834 | 742 |  |
| Arrive On Green | 0.46 | 0.00 | 0.00 | 0.46 | 0.47 | 0.47 |  |
| Sat Flow, veh/h | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Grp Volume(v), veh/h | 674 | 0 | 0 | 747 | 646 | 759 |  |
| Grp Sat Flow(s),veh/h/ln | 1870 | 0 | 0 | 1870 | 1781 | 1585 |  |
| Q Serve(g_s), s | 33.4 | 0.0 | 0.0 | 39.4 | 33.3 | 51.5 |  |
| Cycle Q Clear(g_c), s | 33.4 | 0.0 | 0.0 | 39.4 | 33.3 | 51.5 |  |
| Prop In Lane |  | 0.00 | 0.00 |  | 1.00 | 1.00 |  |
| Lane Grp Cap(c), veh/h | 864 | 0 | 0 | 864 | 834 | 742 |  |
| V/C Ratio(X) | 0.78 | 0.00 | 0.00 | 0.86 | 0.77 | 1.02 |  |
| Avail Cap(c_a), veh/h | 864 | 0 | 0 | 869 | 834 | 742 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 24.9 | 0.0 | 0.0 | 26.5 | 24.4 | 29.2 |  |
| Incr Delay (d2), s/veh | 6.9 | 0.0 | 0.0 | 11.3 | 4.2 | 38.9 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 15.3 | 0.0 | 0.0 | 18.8 | 13.8 | 25.7 |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 31.8 | 0.0 | 0.0 | 37.8 | 28.6 | 68.2 |  |
| LnGrp LOS | C | A | A | D | C | F |  |
| Approach Vol, veh/h | 674 |  |  | 747 | 1405 |  |  |
| Approach Delay, s/veh | 31.8 |  |  | 37.8 | 50.0 |  |  |
| Approach LOS | C |  |  | D | D |  |  |
| Timer - Assigned Phs |  | 2 |  |  |  | 6 | 8 |
| Phs Duration (G+Y+Rc), s |  | 55.0 |  |  |  | 55.0 | 55.0 |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | * 4.2 |  |  |  | * 4.2 | 3.5 |
| Max Green Setting (Gmax), s |  | * 51 |  |  |  | * 51 | 51.5 |
| Max Q Clear Time (g_c+l1), s |  | 35.4 |  |  |  | 41.4 | 53.5 |
| Green Ext Time (p_c), s |  | 2.4 |  |  |  | 2.2 | 0.0 |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 42.4 |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |

## Notes

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

|  | 4 | $\rightarrow$ | 7 | $\checkmark$ |  | 4 | 4 | 4 | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 虫 | 「 | \％ | 个个 | 「 | \％${ }^{\text {\％}}$ | $\uparrow$ |  | \％ | $\uparrow$ | F |
| Traffic Volume（veh／h） | 290 | 893 | 285 | 114 | 1074 | 47 | 221 | 5 | 97 | 126 | － | 77 |
| Future Volume（veh／h） | 290 | 893 | 285 | 114 | 1074 | 47 | 221 | 5 | 97 | 126 | 6 | 77 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 290 | 893 | 285 | 114 | 1074 | 47 | 221 | 5 | 97 | 126 | 6 | 77 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 317 | 1525 | 680 | 144 | 1153 | 514 | 281 | 8 | 154 | 384 | 456 | 386 |
| Arrive On Green | 0.18 | 0.43 | 0.43 | 0.08 | 0.32 | 0.32 | 0.08 | 0.10 | 0.10 | 0.22 | 0.24 | 0.24 |
| Sat Flow，veh／h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 3456 | 78 | 1519 | 1781 | 1870 | 1585 |
| Grp Volume（v），veh／h | 290 | 893 | 285 | 114 | 1074 | 47 | 221 | 0 | 102 | 126 | 6 | 77 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1728 | 0 | 1597 | 1781 | 1870 | 1585 |
| Q Serve（g＿s），s | 19.2 | 23.0 | 15.0 | 7.5 | 35.1 | 2.5 | 7.5 | 0.0 | 7.4 | 7.2 | 0.3 | 3.0 |
| Cycle Q Clear（g＿c），s | 19.2 | 23.0 | 15.0 | 7.5 | 35.1 | 2.5 | 7.5 | 0.0 | 7.4 | 7.2 | 0.3 | 3.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.95 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 317 | 1525 | 680 | 144 | 1153 | 514 | 281 | 0 | 162 | 384 | 456 | 386 |
| V／C Ratio（X） | 0.91 | 0.59 | 0.42 | 0.79 | 0.93 | 0.09 | 0.79 | 0.00 | 0.63 | 0.33 | 0.01 | 0.20 |
| Avail Cap（c＿a），veh／h | 379 | 1525 | 680 | 226 | 1173 | 523 | 343 | 0 | 309 | 384 | 456 | 386 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.40 | 0.40 | 0.40 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 48.4 | 26.1 | 23.8 | 54.1 | 39.2 | 28.2 | 54.1 | 0.0 | 51.7 | 39.7 | 34.4 | 15.0 |
| Incr Delay（d2），s／veh | 22.0 | 0.4 | 0.2 | 5.6 | 6.2 | 0.0 | 10.7 | 0.0 | 17.0 | 0.2 | 0.1 | 1.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 10.2 | 9.3 | 5.4 | 3.5 | 15.6 | 0.9 | 3.7 | 0.0 | 3.7 | 3.2 | 0.1 | 1.8 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 70.4 | 26.5 | 24.0 | 59.8 | 45.5 | 28.3 | 64.8 | 0.0 | 68.7 | 39.9 | 34.5 | 16.2 |
| LnGrp LOS | E | C | C | E | D | C | E | A | E | D | C | B |
| Approach Vol，veh／h |  | 1468 |  |  | 1235 |  |  | 323 |  |  | 209 |  |
| Approach Delay，s／veh |  | 34.7 |  |  | 46.1 |  |  | 66.0 |  |  | 31.0 |  |
| Approach LOS |  | C |  |  | D |  |  | E |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 31.3 | 17.6 | 14.2 | 56.9 | 14.3 | 34.6 | 26.8 | 44.3 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s | 5.4 | ＊ 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 5.4 | ＊ 5.4 |  |  |  |  |
| Max Green Setting（Gmax），s | 11.9 | ＊23 | 15.2 | 49.9 | 11.9 | 23.2 | 25.5 | ＊40 |  |  |  |  |
| Max Q Clear Time（g＿c＋1），s | 9.2 | 9.4 | 9.5 | 25.0 | 9.5 | 5.0 | 21.2 | 37.1 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 0.5 | 0.2 | 4.4 | 0.2 | 0.1 | 0.2 | 1.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 42.0 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 中t |  | \% | 个4 | F | \% | F |  | \% | 1 |  |
| Traffic Volume (veh/h) | 73 | 1048 | 26 | 64 | 1183 | 60 | 6 | 3 | 32 | 104 | 2 | 22 |
| Future Volume (veh/h) | 73 | 1048 | 26 | 64 | 1183 | 60 | 6 | 3 | 32 | 104 | 2 | 22 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 73 | 1048 | 26 | 64 | 1183 | 60 | 6 | 3 | 32 | 104 | 2 | 22 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 175 | 1384 | 34 | 147 | 1331 | 594 | 33 | 35 | 372 | 194 | 46 | 506 |
| Arrive On Green | 0.10 | 0.39 | 0.39 | 0.08 | 0.37 | 0.37 | 0.02 | 0.25 | 0.25 | 0.11 | 0.34 | 0.34 |
| Sat Flow, veh/h | 1781 | 3543 | 88 | 1781 | 3554 | 1585 | 1781 | 138 | 1468 | 1781 | 134 | 1472 |
| Grp Volume(v), veh/h | 73 | 525 | 549 | 64 | 1183 | 60 | 6 | 0 | 35 | 104 | 0 | 24 |
| Grp Sat Flow(s),veh/h/n | 1781 | 1777 | 1855 | 1781 | 1777 | 1585 | 1781 | 0 | 1606 | 1781 | 0 | 1605 |
| Q Serve(g_s), s | 4.6 | 30.7 | 30.7 | 4.1 | 37.4 | 3.0 | 0.4 | 0.0 | 2.0 | 6.6 | 0.0 | 1.2 |
| Cycle Q Clear(g_c), s | 4.6 | 30.7 | 30.7 | 4.1 | 37.4 | 3.0 | 0.4 | 0.0 | 2.0 | 6.6 | 0.0 | 1.2 |
| Prop In Lane | 1.00 |  | 0.05 | 1.00 |  | 1.00 | 1.00 |  | 0.91 | 1.00 |  | 0.92 |
| Lane Grp Cap(c), veh/h | 175 | 694 | 724 | 147 | 1331 | 594 | 33 | 0 | 407 | 194 | 0 | 552 |
| V/C Ratio(X) | 0.42 | 0.76 | 0.76 | 0.44 | 0.89 | 0.10 | 0.18 | 0.00 | 0.09 | 0.54 | 0.00 | 0.04 |
| Avail Cap(c_a), veh/h | 191 | 755 | 788 | 171 | 1469 | 655 | 181 | 0 | 407 | 200 | 0 | 552 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.09 | 0.09 | 0.09 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.9 | 31.7 | 31.7 | 52.4 | 35.2 | 24.4 | 58.0 | 0.0 | 34.2 | 50.6 | 0.0 | 26.2 |
| Incr Delay (d2), s/veh | 0.1 | 0.4 | 0.4 | 2.0 | 6.6 | 0.1 | 2.6 | 0.0 | 0.4 | 2.6 | 0.0 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.0 | 12.6 | 13.1 | 1.9 | 16.6 | 1.1 | 0.2 | 0.0 | 0.8 | 3.1 | 0.0 | 0.5 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 51.0 | 32.0 | 32.0 | 54.5 | 41.8 | 24.5 | 60.6 | 0.0 | 34.6 | 53.2 | 0.0 | 26.4 |
| LnGrp LOS | D | C | C | D | D | C | E | A | C | D | A | C |
| Approach Vol, veh/h |  | 1147 |  |  | 1307 |  |  | 41 |  |  | 128 |  |
| Approach Delay, s/veh |  | 33.2 |  |  | 41.6 |  |  | 38.4 |  |  | 48.2 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |


|  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration $(G+Y+R c)$ s | 17.6 | 35.8 | 14.4 | 52.3 | 6.7 | 46.7 | 16.3 | 50.4 |
| Change Period (Y+Rc), s | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 4.5 | 5.4 |
| Max Green Setting (Gmax), s | 13.5 | 24.2 | 11.5 | 51.0 | 12.2 | 25.5 | 12.9 | 49.6 |
| Max Q Clear Time (g_c+11), s | 8.6 | 4.0 | 6.1 | 32.7 | 2.4 | 3.2 | 6.6 | 39.4 |
| Green Ext Time (p_c), s | 0.1 | 0.1 | 0.0 | 6.2 | 0.0 | 0.1 | 0.1 | 5.5 |

Intersection Summary
HCM 6th Ctrl Delay 38.2

HCM 6th LOS D

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 19 |  |  | $1 \%$ |  |  |  | 「 |  |  | F' |
| Traffic Vol, veh/h | 0 | 1175 | 10 | 0 | 1326 | 89 | 0 | 0 | 14 | 0 | 0 | 13 |
| Future Vol, veh/h | 0 | 1175 | 10 | 0 | 1326 | 89 | 0 | 0 | 14 | 0 | 0 | 13 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 0 | - | - | 0 |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1175 | 10 | 0 | 1326 | 89 | 0 | 0 | 14 | 0 | 0 | 13 |



HCM 6th Signalized Intersection Summary
6：Gateway Oaks Drive \＆West El Camino Avenue
08／03／2020

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％${ }^{1 / 4}$ | 个巾4 | 「 | \％${ }^{1+1}$ | 个4 | 「 | \％${ }^{1+1}$ | 个4 | 「 | \％${ }^{1+1}$ | 个个 | 7 |
| Traffic Volume（veh／h） | 84 | 862 | 223 | 245 | 575 | 102 | 387 | 60 | 371 | 450 | 117 | 288 |
| Future Volume（veh／h） | 84 | 862 | 223 | 245 | 575 | 102 | 387 | 60 | 371 | 450 | 117 | 288 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 84 | 862 | 223 | 245 | 575 | 102 | 387 | 60 | 371 | 450 | 117 | 288 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 448 | 1111 | 345 | 475 | 797 | 355 | 516 | 916 | 408 | 541 | 938 | 418 |
| Arrive On Green | 0.13 | 0.22 | 0.22 | 0.14 | 0.22 | 0.22 | 0.15 | 0.26 | 0.26 | 0.16 | 0.26 | 0.26 |
| Sat Flow，veh／h | 3456 | 5106 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 | 3456 | 3554 | 1585 |
| Grp Volume（v），veh／h | 84 | 862 | 223 | 245 | 575 | 102 | 387 | 60 | 371 | 450 | 117 | 288 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 | 1728 | 1777 | 1585 |
| Q Serve（g＿s），s | 1.9 | 13.8 | 11.2 | 5.7 | 13.0 | 4.6 | 9.3 | 1.1 | 19.8 | 11.0 | 2.2 | 14.2 |
| Cycle Q Clear（g＿c），s | 1.9 | 13.8 | 11.2 | 5.7 | 13.0 | 4.6 | 9.3 | 1.1 | 19.8 | 11.0 | 2.2 | 14.2 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 448 | 1111 | 345 | 475 | 797 | 355 | 516 | 916 | 408 | 541 | 938 | 418 |
| V／C Ratio（X） | 0.19 | 0.78 | 0.65 | 0.52 | 0.72 | 0.29 | 0.75 | 0.07 | 0.91 | 0.83 | 0.12 | 0.69 |
| Avail Cap（c＿a），veh／h | 516 | 1536 | 477 | 476 | 1036 | 462 | 718 | 1252 | 559 | 833 | 1367 | 610 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 33.8 | 32.1 | 31.0 | 34.9 | 31.3 | 28.0 | 35.5 | 24.4 | 31.3 | 35.6 | 24.4 | 28.8 |
| Incr Delay（d2），s／veh | 0.1 | 1.1 | 0.8 | 0.4 | 1.1 | 0.2 | 1.6 | 0.0 | 12.7 | 2.5 | 0.0 | 0.8 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.8 | 5.4 | 4.2 | 2.3 | 5.3 | 1.7 | 4.0 | 0.5 | 8.7 | 4.7 | 0.9 | 5.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 33.9 | 33.1 | 31.8 | 35.3 | 32.3 | 28.2 | 37.1 | 24.4 | 44.1 | 38.1 | 24.4 | 29.6 |
| LnGrp LOS | C | C | C | D | C | C | D | C | D | D | C | C |
| Approach Vol，veh／h |  | 1169 |  |  | 922 |  |  | 818 |  |  | 855 |  |
| Approach Delay，s／veh |  | 32.9 |  |  | 32.7 |  |  | 39.3 |  |  | 33.4 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | C |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），$s$ | 16.4 | 24.3 | 18.1 | 28.3 | 17.0 | 23.8 | 18.6 | 27.7 |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | ＊5．1 | ＊ 4.8 | ＊ 5.1 | ＊ 5.3 | 5.0 | ＊4．8 | 5.0 | ＊ 5.3 |  |
| Max Green Setting（Gmax），s | ＊13 | ＊ 25 | ＊18 | ＊ 34 | 12.0 | ＊ 26 | 21.0 | ＊31 |  |
| Max Q Clear Time（g＿c +11 ），s | 3.9 | 15.0 | 11.3 | 16.2 | 7.7 | 15.8 | 13.0 | 21.8 |  |
| Green Ext Time（p＿c），s | 0.1 | 1.9 | 0.5 | 0.9 | 0.2 | 3.1 | 0.6 | 0.7 |  |

Intersection Summary

| HCM 6th Ctrl Delay | 34.4 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个4 | 个. | $\mathbf{F}$ |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 0 | 1434 | 1217 | 138 | 0 | 91 |
| Future Vol, veh/h | 0 | 1434 | 1217 | 138 | 0 | 91 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | 0 | - | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1434 | 1217 | 138 | 0 | 91 |


| Major/Minor M | Major1 |  |  |  | inor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | - | 609 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | - | - | - | 3.32 |
| Pot Cap-1 Maneuver | 0 | - | - | - | 0 | 438 |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | - | 438 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | VB |  | SB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 15.4 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt EBT WBT WBR SBLn1 |  |  |  |  |  |  |
| Capacity (veh/h) |  | - | - | - | 438 |  |
| HCM Lane V/C Ratio |  | - | - | - | 0.208 |  |
| HCM Control Delay (s) |  | - | - | - | 15.4 |  |
| HCM Lane LOS |  | - | - | - | C |  |
| HCM 95th \%tile Q(veh) |  | - | - | - | 0.8 |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | b |  |  | -1 | Y |  |
| Traffic Vol, veh/h | 47 | 4 | 4 | 57 | 2 | 5 |
| Future Vol, veh/h | 47 | 4 | 4 | 57 | 2 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 47 | 4 | 4 | 57 | 2 | 5 |



|  | $\rightarrow$ | $\leftarrow$ | - | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | SBL | SBR |
| Lane Group Flow (vph) | 294 | 932 | 454 | 152 |
| v/c Ratio | 0.31 | 0.98 | 0.73 | 0.10 |
| Control Delay | 10.4 | 44.0 | 21.9 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 10.4 | 44.0 | 21.9 | 0.1 |
| Queue Length 50th (ft) | 51 | 274 | 124 | 0 |
| Queue Length 95th (ft) | 118 | \#591 | 172 | 0 |
| Internal Link Dist (tt) | 294 | 252 | 765 |  |
| Turn Bay Length (t) |  |  |  | 800 |
| Base Capacity (vph) | 953 | 953 | 852 | 1583 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.31 | 0.98 | 0.53 | 0.10 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |

Queues
2: Eastbound I-80 Ramp \& West El Camino Avenue

|  | $\rightarrow$ |  | 4 | 7 |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | NBL | NBR |
| Lane Group Flow (vph) | 674 | 747 | 646 | 759 |
| v/c Ratio | 0.75 | 0.82 | 0.82 | 0.96 |
| Control Delay | 30.2 | 34.4 | 36.1 | 46.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.2 | 34.4 | 36.1 | 46.5 |
| Queue Length 50th (ft) | 397 | 466 | 365 | 400 |
| Queue Length 95th (t) | 549 | \#694 | 529 | \#678 |
| Internal Link Dist (ft) | 249 | 128 | 477 |  |
| Turn Bay Length (ft) |  |  |  | 150 |
| Base Capacity (vph) | 905 | 910 | 831 | 828 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.74 | 0.82 | 0.78 | 0.92 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longerQueue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |

Queues
3: Orchard Lane \& West El Camino Avenue

|  | $\stackrel{ }{*}$ | $\rightarrow$ |  | 7 | 4 | 4 | 4 | $\uparrow$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Group Flow (vph) | 302 | 893 | 285 | 114 | 1074 | 47 | 221 | 102 | 126 | 6 | 77 |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.88 | 0.57 | 0.33 | 0.56 | 0.83 | 0.07 | 0.64 | 0.31 | 0.61 | 0.02 | 0.19 |
| Control Delay | 73.6 | 26.5 | 3.5 | 26.2 | 35.4 | 2.0 | 60.7 | 13.7 | 62.5 | 44.7 | 1.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 73.6 | 26.5 | 3.5 | 26.2 | 35.4 | 2.0 | 60.7 | 13.7 | 62.5 | 44.7 | 1.1 |
| Queue Length 50th (t) | 224 | 243 | 0 | 75 | 468 | 0 | 84 | 4 | 95 | 4 | 0 |
| Queue Length 95th (ft) | \#363 | 341 | 51 | m89 | 534 | m0 | 128 | 57 | 154 | 17 | 0 |
| Internal Link Dist (t) |  | 183 |  |  | 844 |  |  | 420 |  | 204 |  |
| Turn Bay Length ( ft ) | 295 |  | 240 | 295 |  | 135 | 155 |  | 70 |  | 240 |
| Base Capacity (vph) | 376 | 1587 | 867 | 237 | 1302 | 684 | 356 | 410 | 208 | 394 | 455 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.80 | 0.56 | 0.33 | 0.48 | 0.82 | 0.07 | 0.62 | 0.25 | 0.61 | 0.02 | 0.17 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| m Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |

Queues
4: West River Drive/River Oaks Way \& West El Camino Avenue

|  | 4 | $\rightarrow$ | 7 | $\leftarrow$ | 4 | 4 | $\dagger$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 73 | 1074 | 64 | 1183 | 60 | 6 | 35 | 104 | 24 |
| v/c Ratio | 0.38 | 0.76 | 0.39 | 0.86 | 0.09 | 0.03 | 0.08 | 0.52 | 0.04 |
| Control Delay | 39.0 | 37.3 | 58.4 | 41.0 | 0.9 | 49.2 | 15.0 | 60.4 | 14.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 39.0 | 37.3 | 58.4 | 41.0 | 0.9 | 49.2 | 15.0 | 60.4 | 14.2 |
| Queue Length 50th ( t ) | 55 | 410 | 47 | 426 | 0 | 4 | 2 | 77 | 1 |
| Queue Length 95th (ft) | m78 | 492 | 93 | 510 | 6 | 18 | 30 | 136 | 25 |
| Internal Link Dist (tt) |  | 844 |  | 641 |  |  | 474 |  | 441 |
| Turn Bay Length (ft) |  |  | 155 |  | 165 | 100 |  | 100 |  |
| Base Capacity (vph) | 190 | 1501 | 169 | 1462 | 715 | 179 | 434 | 199 | 620 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.38 | 0.72 | 0.38 | 0.81 | 0.08 | 0.03 | 0.08 | 0.52 | 0.04 |

Intersection Summary
m Volume for 95 th percentile queue is metered by upstream signal.

Queues
6: Gateway Oaks Drive \& West El Camino Avenue
08/03/2020

|  | 4 | $\rightarrow$ | * | 7 |  | 4 | 4 | $\uparrow$ | 1 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 84 | 862 | 223 | 245 | 575 | 102 | 387 | 60 | 371 | 450 | 117 | 288 |
| v/c Ratio | 0.16 | 0.72 | 0.42 | 0.50 | 0.59 | 0.19 | 0.65 | 0.09 | 0.72 | 0.71 | 0.16 | 0.53 |
| Control Delay | 35.8 | 34.2 | 7.7 | 40.1 | 32.1 | 4.9 | 39.8 | 30.2 | 19.7 | 40.2 | 29.2 | 9.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 35.8 | 34.2 | 7.7 | 40.1 | 32.1 | 4.9 | 39.8 | 30.2 | 19.7 | 40.2 | 29.2 | 9.0 |
| Queue Length 50th (ft) | 19 | 146 | 4 | 59 | 141 | 0 | 96 | 13 | 53 | 111 | 26 | 8 |
| Queue Length 95th (ft) | 50 | 237 | 64 | 122 | 243 | 30 | 175 | 33 | 167 | 197 | 54 | 75 |
| Internal Link Dist (ft) |  | 185 |  |  | 456 |  |  | 405 |  |  | 335 |  |
| Turn Bay Length ( ft ) | 175 |  | 150 | 190 |  | 190 | 140 |  | 140 | 230 |  | 230 |
| Base Capacity (vph) | 531 | 1585 | 639 | 490 | 1130 | 589 | 739 | 1293 | 741 | 858 | 1411 | 793 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.16 | 0.54 | 0.35 | 0.50 | 0.51 | 0.17 | 0.52 | 0.05 | 0.50 | 0.52 | 0.08 | 0.36 |

[^20]
## INTERSECTION ANALYSIS

## BASELINE PLUS PROJECT WITH RECOMMENDATIONS CONDITIONS

## AM PEAK HOUR

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个个 | 「 | ${ }^{4}$ | 个4 | 「 | \％${ }^{1 / 4}$ | $\hat{F}$ |  | \％ | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 260 | 1211 | 71 | 57 | 806 | 46 | 438 | 9 | 122 | 173 | 18 | 402 |
| Future Volume（veh／h） | 260 | 1211 | 71 | 57 | 806 | 46 | 438 | 9 | 122 | 173 | 18 | 402 |
| Initial $Q(Q b)$ ，veh | 0 | ， | 0 | 0 | ， | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 260 | 1211 | 71 | 57 | 806 | 46 | 438 | 9 | 122 | 173 | 18 | 402 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 312 | 1333 | 594 | 99 | 882 | 393 | 500 | 11 | 154 | 522 | 485 | 411 |
| Arrive On Green | 0.18 | 0.38 | 0.38 | 0.06 | 0.25 | 0.25 | 0.14 | 0.10 | 0.10 | 0.29 | 0.26 | 0.26 |
| Sat Flow，veh／h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 3456 | 110 | 1492 | 1781 | 1870 | 1585 |
| Grp Volume（v），veh／h | 260 | 1211 | 71 | 57 | 806 | 46 | 438 | 0 | 131 | 173 | 18 | 402 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1728 | 0 | 1602 | 1781 | 1870 | 1585 |
| Q Serve（g＿s），s | 16.9 | 38.8 | 3.5 | 3.7 | 26.5 | 2.7 | 14.9 | 0.0 | 9.6 | 9.1 | 0.9 | 19.4 |
| Cycle Q Clear（g＿c），s | 16.9 | 38.8 | 3.5 | 3.7 | 26.5 | 2.7 | 14.9 | 0.0 | 9.6 | 9.1 | 0.9 | 19.4 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.93 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 312 | 1333 | 594 | 99 | 882 | 393 | 500 | 0 | 166 | 522 | 485 | 411 |
| V／C Ratio（X） | 0.83 | 0.91 | 0.12 | 0.57 | 0.91 | 0.12 | 0.88 | 0.00 | 0.79 | 0.33 | 0.04 | 0.98 |
| Avail Cap（c＿a），veh／h | 408 | 1522 | 679 | 99 | 906 | 404 | 541 | 0 | 367 | 522 | 485 | 411 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.88 | 0.88 | 0.88 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 47.8 | 35.6 | 24.5 | 55.3 | 43.9 | 34.9 | 50.2 | 0.0 | 52.5 | 33.2 | 33.2 | 18.2 |
| Incr Delay（d2），s／veh | 8.6 | 7.1 | 0.0 | 8.4 | 12.3 | 0.2 | 14.7 | 0.0 | 31.0 | 0.1 | 0.1 | 39.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 8.0 | 17.2 | 1.3 | 1.9 | 12.7 | 1.0 | 7.4 | 0.0 | 5.3 | 4.0 | 0.4 | 11.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 56.3 | 42.7 | 24.6 | 63.6 | 56.2 | 35.1 | 65.0 | 0.0 | 83.5 | 33.3 | 33.4 | 57.4 |
| LnGrp LOS | E | D | C | E | E | D | E | A | F | C | C | E |
| Approach Vol，veh／h |  | 1542 |  |  | 909 |  |  | 569 |  |  | 593 |  |
| Approach Delay，s／veh |  | 44.2 |  |  | 55.6 |  |  | 69.2 |  |  | 49.6 |  |
| Approach LOS |  | D |  |  | E |  |  | E |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 40.6 | 17.8 | 11.2 | 50.4 | 21.9 | 36.5 | 26.4 | 35.2 |
| Change Period（Y＋Rc），s | 5.4 | ${ }^{*} 5.4$ | 4.5 | 5.4 | 4.5 | 5.4 | 5.4 | ${ }^{*} 5.4$ |
| Max Green Setting（Gmax），s | 14.6 | $* 28$ | 6.7 | 51.4 | 18.8 | 23.3 | 27.5 | $* 31$ |
| Max Q Clear Time（g＿c $\mathbf{c}+1$ ），s | 11.1 | 11.6 | 5.7 | 40.8 | 16.9 | 21.4 | 18.9 | 28.5 |
| Green Ext Time（p＿c），s | 0.1 | 0.8 | 0.0 | 4.2 | 0.5 | 0.2 | 0.2 | 1.3 |

Intersection Summary

| HCM 6th Ctrl Delay | 51.9 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 8.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations |  |  | 1 | 个 | 个 |  |
| Traffic Vol, veh/h | 0 | 430 | 273 | 57 | 163 | 2 |
| Future Vol, veh/h | 0 | 430 | 273 | 57 | 163 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 150 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 430 | 273 | 57 | 163 | 2 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 8.1 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | Y |  |
| Traffic Vol, veh/h | 54 | 4 | 217 | 58 | 4 | 376 |
| Future Vol, veh/h | 54 | 4 | 217 | 58 | 4 | 376 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 54 | 4 | 217 | 58 | 4 | 376 |



River Oaks Marketplace 12:00 am 08/25/2020 AM Baseline Plus Project with Recommendations

|  | $\rightarrow$ | $\leftarrow$ | $\checkmark$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | SBL | SBR |
| Lane Group Flow (vph) | 468 | 311 | 765 | 96 |
| v/c Ratio | 0.65 | 0.43 | 0.90 | 0.06 |
| Control Delay | 19.7 | 15.4 | 29.5 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 19.7 | 15.4 | 29.5 | 0.1 |
| Queue Length 50th (ft) | 134 | 80 | 183 | 0 |
| Queue Length 95th (ft) | 208 | 129 | \#421 | 0 |
| Internal Link Dist (tt) | 294 | 252 | 765 |  |
| Turn Bay Length (t) |  |  |  | 800 |
| Base Capacity (vph) | 741 | 741 | 877 | 1583 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.63 | 0.42 | 0.87 | 0.06 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |

Queues
2: Eastbound I-80 Ramp \& West El Camino Avenue

|  | $\rightarrow$ |  | 4 | $p$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | NBL | NBR |
| Lane Group Flow (vph) | 1115 | 695 | 117 | 429 |
| v/c Ratio | 0.86 | 0.53 | 0.28 | 0.89 |
| Control Delay | 20.8 | 9.6 | 37.8 | 48.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 20.8 | 9.6 | 37.8 | 48.9 |
| Queue Length 50th ( t ) | 622 | 246 | 64 | 188 |
| Queue Length 95th (ft) | 670 | 248 | 127 | \#425 |
| Internal Link Dist (ft) | 249 | 128 | 477 |  |
| Turn Bay Length (ft) |  |  |  | 150 |
| Base Capacity (vph) | 1368 | 1373 | 413 | 483 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.82 | 0.51 | 0.28 | 0.89 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longerQueue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |

Queues
3: Orchard Lane \& West El Camino Avenue

|  | 7 | $\rightarrow$ | 7 | $\checkmark$ | 4 | 4 | 4 | $\dagger$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Group Flow (vph) | 260 | 1211 | 71 | 57 | 806 | 46 | 438 | 131 | 173 | 18 | 402 |
| v/c Ratio | 0.80 | 0.88 | 0.10 | 0.40 | 0.80 | 0.08 | 0.77 | 0.32 | 0.58 | 0.05 | 0.63 |
| Control Delay | 64.5 | 42.2 | 0.3 | 38.9 | 40.1 | 4.8 | 57.3 | 12.3 | 54.3 | 44.2 | 9.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 64.5 | 42.2 | 0.3 | 38.9 | 40.1 | 4.8 | 57.3 | 12.3 | 54.3 | 44.2 | 9.5 |
| Queue Length 50th (ft) | 195 | 448 | 0 | 42 | 344 | 2 | 165 | 6 | 127 | 12 | 0 |
| Queue Length 95th (ft) | 276 | 513 | 0 | 88 | 418 | 26 | \#245 | 66 | 192 | 34 | 96 |
| Internal Link Dist (ft) |  | 183 |  |  | 844 |  |  | 420 |  | 204 |  |
| Turn Bay Length (ft) | 295 |  | 240 | 295 |  | 135 | 155 |  | 70 |  | 240 |
| Base Capacity (vph) | 405 | 1520 | 767 | 143 | 1021 | 571 | 584 | 485 | 296 | 422 | 669 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.64 | 0.80 | 0.09 | 0.40 | 0.79 | 0.08 | 0.75 | 0.27 | 0.58 | 0.04 | 0.60 |

Intersection Summary
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Queues
4: West River Drive/River Oaks Way \& West El Camino Avenue

|  | $\rangle$ |  | $\dagger$ |  | 4 | 4 | $\dagger$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 15 | 1355 | 196 | 850 | 25 | 13 | 47 | 122 | 49 |
| v/c Ratio | 0.08 | 0.97 | 0.84 | 0.48 | 0.03 | 0.07 | 0.09 | 0.61 | 0.10 |
| Control Delay | 33.3 | 57.7 | 80.6 | 21.9 | 0.1 | 49.9 | 0.4 | 64.8 | 12.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 33.3 | 57.7 | 80.6 | 21.9 | 0.1 | 49.9 | 0.4 | 64.8 | 12.6 |
| Queue Length 50th (ft) | 9 | 570 | 149 | 189 | 0 | 9 | 0 | 91 | 2 |
| Queue Length 95th (ft) | m13 | \#712 | \#271 | 326 | 0 | 30 | 0 | \#158 | 35 |
| Internal Link Dist (ft) |  | 844 |  | 641 |  |  | 474 |  | 441 |
| Turn Bay Length (ft) |  |  | 155 |  | 165 | 100 |  | 100 |  |
| Base Capacity (vph) | 190 | 1391 | 243 | 1788 | 851 | 179 | 510 | 199 | 498 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.08 | 0.97 | 0.81 | 0.48 | 0.03 | 0.07 | 0.09 | 0.61 | 0.10 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |
| m Volume for 95th perc | queue | metere | by upstr | am sign |  |  |  |  |  |

Queues
6: Gateway Oaks Drive \& West El Camino Avenue

|  | 4 | $\rightarrow$ | 7 | 7 | - | 4 | 4 | $\dagger$ | p |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 324 | 767 | 445 | 351 | 602 | 574 | 220 | 117 | 127 | 130 | 34 | 44 |
| v/c Ratio | 0.58 | 0.62 | 0.62 | 0.62 | 0.69 | 0.70 | 0.30 | 0.18 | 0.32 | 0.25 | 0.05 | 0.12 |
| Control Delay | 36.2 | 29.4 | 6.9 | 36.5 | 31.6 | 7.4 | 31.1 | 29.2 | 8.5 | 32.5 | 29.4 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 36.2 | 29.4 | 6.9 | 36.5 | 31.6 | 7.4 | 31.1 | 29.2 | 8.5 | 32.5 | 29.4 | 0.6 |
| Queue Length 50th (tt) | 77 | 123 | 0 | 84 | 143 | 0 | 51 | 25 | 0 | 29 | 7 | 0 |
| Queue Length 95th (ft) | 129 | 168 | 69 | 135 | 196 | 77 | 90 | 52 | 46 | 59 | 21 | 0 |
| Internal Link Dist (ft) |  | 185 |  |  | 456 |  |  | 405 |  |  | 335 |  |
| Turn Bay Length (ft) | 175 |  | 150 | 190 |  | 190 | 140 |  | 140 | 230 |  | 230 |
| Base Capacity (vph) | 562 | 2032 | 899 | 649 | 1512 | 1005 | 734 | 1392 | 699 | 519 | 1343 | 674 |
| Starvation Cap Reductn | , | 0 | 0 | , | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.58 | 0.38 | 0.49 | 0.54 | 0.40 | 0.57 | 0.30 | 0.08 | 0.18 | 0.25 | 0.03 | 0.07 |

[^21]
## INTERSECTION ANALYSIS

## BASELINE PLUS PROJECT WITH RECOMMENDATIONS CONDITIONS

 PM PEAK HOUR|  | 4 | $\rightarrow$ | 7 | $\checkmark$ | 4 | 4 | 4 | 4 | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊ | 个4 | 「 | \％ | 个个 | F | ＊＊ | $\hat{\beta}$ |  | \％ | $\uparrow$ | F |
| Traffic Volume（veh／h） | 265 | 884 | 285 | 114 | 1074 | 47 | 221 | 5 | 97 | 134 | 0 | 176 |
| Future Volume（veh／h） | 265 | 884 | 285 | 114 | 1074 | 47 | 221 | 5 | 97 | 134 | 6 | 176 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 265 | 884 | 285 | 114 | 1074 | 47 | 221 | 5 | 97 | 134 | 6 | 176 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 293 | 1476 | 658 | 144 | 1153 | 514 | 281 | 8 | 154 | 409 | 481 | 408 |
| Arrive On Green | 0.16 | 0.42 | 0.42 | 0.08 | 0.32 | 0.32 | 0.08 | 0.10 | 0.10 | 0.23 | 0.26 | 0.26 |
| Sat Flow，veh／h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 3456 | 78 | 1519 | 1781 | 1870 | 1585 |
| Grp Volume（v），veh／h | 265 | 884 | 285 | 114 | 1074 | 47 | 221 | 0 | 102 | 134 | 6 | 176 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1728 | 0 | 1597 | 1781 | 1870 | 1585 |
| Q Serve（g＿s），s | 17.5 | 23.2 | 15.4 | 7.5 | 35.1 | 2.5 | 7.5 | 0.0 | 7.4 | 7.5 | 0.3 | 7.3 |
| Cycle Q Clear（g＿c），s | 17.5 | 23.2 | 15.4 | 7.5 | 35.1 | 2.5 | 7.5 | 0.0 | 7.4 | 7.5 | 0.3 | 7.3 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.95 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 293 | 1476 | 658 | 144 | 1153 | 514 | 281 | 0 | 162 | 409 | 481 | 408 |
| V／C Ratio（X） | 0.91 | 0.60 | 0.43 | 0.79 | 0.93 | 0.09 | 0.79 | 0.00 | 0.63 | 0.33 | 0.01 | 0.43 |
| Avail Cap（c＿a），veh／h | 379 | 1478 | 659 | 226 | 1173 | 523 | 343 | 0 | 309 | 409 | 481 | 408 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 0.40 | 0.40 | 0.40 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 49.2 | 27.3 | 25.0 | 54.1 | 39.2 | 28.2 | 54.1 | 0.0 | 51.7 | 38.5 | 33.2 | 16.1 |
| Incr Delay（d2），s／veh | 18.4 | 0.5 | 0.2 | 5.6 | 6.2 | 0.0 | 10.7 | 0.0 | 17.0 | 0.2 | 0.0 | 3.3 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 9.0 | 9.5 | 5.6 | 3.5 | 15.6 | 0.9 | 3.7 | 0.0 | 3.7 | 3.3 | 0.1 | 4.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 67.6 | 27.8 | 25.2 | 59.8 | 45.5 | 28.3 | 64.8 | 0.0 | 68.7 | 38.7 | 33.3 | 19.4 |
| LnGrp LOS | E | C | C | E | D | C | E | A | E | D | C | B |
| Approach Vol，veh／h |  | 1434 |  |  | 1235 |  |  | 323 |  |  | 316 |  |
| Approach Delay，s／veh |  | 34.6 |  |  | 46.1 |  |  | 66.0 |  |  | 27.9 |  |
| Approach LOS |  | C |  |  | D |  |  | E |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 32.9 | 17.6 | 14.2 | 55.2 | 14.3 | 36.3 | 25.1 | 44.3 |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ）， s | 5.4 | ＊ 5.4 | 4.5 | 5.4 | 4.5 | 5.4 | 5.4 | ＊ 5.4 |  |  |  |  |
| Max Green Setting（Gmax），s | 11.9 | ＊23 | 15.2 | 49.9 | 11.9 | 23.2 | 25.5 | ＊40 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 9.5 | 9.4 | 9.5 | 25.2 | 9.5 | 9.3 | 19.5 | 37.1 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 0.5 | 0.2 | 4.3 | 0.2 | 0.3 | 0.2 | 1.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 41.3 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |

## Notes

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 6 |  |  | -1 | Y |  |
| Traffic Vol, veh/h | 47 | 2 | 138 | 56 | 2 | 203 |
| Future Vol, veh/h | 47 | 2 | 138 | 56 | 2 | 203 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 47 | 2 | 138 | 56 | 2 | 203 |



|  | $\rightarrow$ | $\leftarrow$ | - | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | SBL | SBR |
| Lane Group Flow (vph) | 294 | 932 | 454 | 152 |
| v/c Ratio | 0.31 | 0.98 | 0.73 | 0.10 |
| Control Delay | 10.4 | 44.0 | 21.9 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 10.4 | 44.0 | 21.9 | 0.1 |
| Queue Length 50th (ft) | 51 | 274 | 124 | 0 |
| Queue Length 95th (ft) | 118 | \#591 | 172 | 0 |
| Internal Link Dist (tt) | 294 | 252 | 765 |  |
| Turn Bay Length (t) |  |  |  | 800 |
| Base Capacity (vph) | 953 | 953 | 852 | 1583 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.31 | 0.98 | 0.53 | 0.10 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |

Queues
2: Eastbound I-80 Ramp \& West El Camino Avenue

|  | $\rightarrow$ |  | 4 | 7 |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | NBL | NBR |
| Lane Group Flow (vph) | 674 | 747 | 646 | 759 |
| v/c Ratio | 0.75 | 0.82 | 0.82 | 0.96 |
| Control Delay | 30.2 | 34.4 | 36.1 | 46.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.2 | 34.4 | 36.1 | 46.5 |
| Queue Length 50th (ft) | 397 | 466 | 365 | 400 |
| Queue Length 95th (t) | 549 | \#694 | 529 | \#678 |
| Internal Link Dist (ft) | 249 | 128 | 477 |  |
| Turn Bay Length (ft) |  |  |  | 150 |
| Base Capacity (vph) | 905 | 910 | 831 | 828 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.74 | 0.82 | 0.78 | 0.92 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longerQueue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |

Queues
3: Orchard Lane \& West El Camino Avenue

|  | 7 | $\rightarrow$ | 1 | $\dagger$ | 4 | 4 | 4 | $\dagger$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Group Flow (vph) | 265 | 884 | 285 | 114 | 1074 | 47 | 221 | 102 | 134 | 6 | 176 |
| v/c Ratio | 0.84 | 0.59 | 0.34 | 0.56 | 0.83 | 0.07 | 0.64 | 0.29 | 0.63 | 0.02 | 0.40 |
| Control Delay | 70.1 | 28.0 | 3.6 | 26.4 | 36.0 | 2.0 | 60.7 | 13.4 | 62.9 | 43.8 | 9.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 70.1 | 28.0 | 3.6 | 26.4 | 36.0 | 2.0 | 60.7 | 13.4 | 62.9 | 43.8 | 9.4 |
| Queue Length 50th (ft) | 199 | 252 | 0 | 77 | 468 | 0 | 84 | 3 | 101 | 4 | 0 |
| Queue Length 95th (ft) | 288 | 341 | 51 | m91 | 534 | m0 | 128 | 57 | 161 | 17 | 63 |
| Internal Link Dist (ft) |  | 183 |  |  | 844 |  |  | 420 |  | 204 |  |
| Turn Bay Length (ft) | 295 |  | 240 | 295 |  | 135 | 155 |  | 70 |  | 240 |
| Base Capacity (vph) | 376 | 1543 | 851 | 237 | 1296 | 681 | 356 | 424 | 214 | 410 | 485 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 |  |  |  | 0 | 0 |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.70 | 0.57 | 0.33 | 0.48 | 0.83 | 0.07 | 0.62 | 0.24 | 0.63 | 0.01 | 0.36 |

Intersection Summary
m Volume for 95 th percentile queue is metered by upstream signal.

Queues
4: West River Drive/River Oaks Way \& West El Camino Avenue

|  | $\stackrel{ }{*}$ | $\rightarrow$ | 7 | 4 | 4 | 4 | $\uparrow$ | - | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 73 | 1074 | 64 | 1183 | 60 | 6 | 35 | 104 | 24 |
| v/c Ratio | 0.38 | 0.76 | 0.39 | 0.86 | 0.09 | 0.03 | 0.08 | 0.52 | 0.04 |
| Control Delay | 38.8 | 37.7 | 58.4 | 41.0 | 0.9 | 49.2 | 15.0 | 60.4 | 14.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 38.8 | 37.7 | 58.4 | 41.0 | 0.9 | 49.2 | 15.0 | 60.4 | 14.2 |
| Queue Length 50th (ft) | 54 | 410 | 47 | 426 | 0 | 4 | 2 | 77 | 1 |
| Queue Length 95th (ft) | m78 | 492 | 93 | 510 | 6 | 18 | 30 | 136 | 25 |
| Internal Link Dist (ft) |  | 844 |  | 641 |  |  | 474 |  | 441 |
| Turn Bay Length (ft) |  |  | 155 |  | 165 | 100 |  | 100 |  |
| Base Capacity (vph) | 190 | 1501 | 169 | 1462 | 715 | 179 | 434 | 199 | 620 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.38 | 0.72 | 0.38 | 0.81 | 0.08 | 0.03 | 0.08 | 0.52 | 0.04 |

Intersection Summary
m Volume for 95 th percentile queue is metered by upstream signal.

Queues
6: Gateway Oaks Drive \& West El Camino Avenue

|  | 4 | $\rightarrow$ | 7 | $\checkmark$ | - | 4 | 4 | $\uparrow$ | $>$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 84 | 862 | 223 | 245 | 575 | 102 | 387 | 60 | 371 | 450 | 117 | 288 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.16 | 0.72 | 0.42 | 0.50 | 0.59 | 0.19 | 0.65 | 0.09 | 0.72 | 0.71 | 0.16 | 0.53 |
| Control Delay | 35.8 | 34.2 | 7.7 | 40.1 | 32.1 | 4.9 | 39.8 | 30.2 | 19.7 | 40.2 | 29.2 | 9.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 35.8 | 34.2 | 7.7 | 40.1 | 32.1 | 4.9 | 39.8 | 30.2 | 19.7 | 40.2 | 29.2 | 9.0 |
| Queue Length 50th (t) | 19 | 146 | 4 | 59 | 141 | 0 | 96 | 13 | 53 | 111 | 26 | 8 |
| Queue Length 95th (tt) | 50 | 237 | 64 | 122 | 243 | 30 | 175 | 33 | 167 | 197 | 54 | 75 |
| Internal Link Dist (tt) |  | 185 |  |  | 456 |  |  | 405 |  |  | 335 |  |
| Turn Bay Length (ft) | 175 |  | 150 | 190 |  | 190 | 140 |  | 140 | 230 |  | 230 |
| Base Capacity (vph) | 531 | 1585 | 639 | 490 | 1130 | 589 | 739 | 1293 | 741 | 858 | 1411 | 793 |
| Starvation Cap Reductn | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | , | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.16 | 0.54 | 0.35 | 0.50 | 0.51 | 0.17 | 0.52 | 0.05 | 0.50 | 0.52 | 0.08 | 0.36 |

[^22]
[^0]:    ${ }^{1}$ California Code of Regulations, Title 14, Division 6, Chapter 3, Section 15064.3(c).
    ${ }^{2}$ Governor's Office of Planning and Research, Technical Advisory on Evaluating Transportation Impacts in CEQA. (New York: Free Press, December 2018), 15-16.
    ${ }^{3}$ A Primer on Retail Types and Urban Centers, Robert Steuteville, Congress for the New Urbanism, Public Square, September 1, 2007.

[^1]:    ${ }^{\text {a }}$ Limited data; building size out of range.
    ${ }^{\mathrm{b}}$ Limited data; limited time periods.
    ${ }^{\text {c }}$ Assumed land use for analysis purposes.
    Source: ITE Trip Generation, Tenth Edition, 2017 as updated; DKS Associates, 2020.

[^2]:    ${ }^{1}$ Buttke, Carl H. Unpublished studies of building employment densities, Portland, Oregon.

[^3]:    *Mr. Glenn Gebhardt - City Engineer, October 2019.

[^4]:    Source: Crane Transportation Group

[^5]:    Source: Crane Transportation Group

[^6]:    ${ }^{1}$ Although the car wash does not open prior to 10 AM , the traffic count worksheets (see Appendix B) show traffic volumes that could be employees/maintenance vehicles.

[^7]:    ${ }^{1}$ Although the car wash does not open prior to 10 AM, the traffic count worksheets (see Appendix B) show traffic volumes that
    could be employees/maintenance vehicles.

[^8]:    ${ }^{1}$ When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel outside the through lanes. $L=$ Left; $T=$ Through; $R=$ Right; $d=$ Defacto Right Turn

[^9]:    ${ }^{3}$ TS = Traffic Signal; CSS = Cross Street Stop

[^10]:    ${ }^{1}$ Source: Manual vehicle count of the existing Matt's Express Carwash facility located in the City of Rialto on January 16, 2014.

[^11]:    ${ }^{1}$ When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel outside the through lanes. $L=$ Left $; T=$ Through; $R=$ Right; $d=$ Defacto Right Turn' $\underline{\underline{1}}=$ Improvement

[^12]:    ${ }^{1}$ When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel outside the through lanes. $L=$ Left $; T=$ Through; $R=$ Right; $d=$ Defacto Right Turn' $\underline{\mathbf{1}}=$ Improvement
    ${ }^{2}$ Delay and level of service calculated using the following analysis software: Traffix, Version 7.9.0215. Per the Highway Capacity Manual, overall average intersection delay and level of service are shown for intersections with traffic signal or all way stop control. For intersections with cross street stop control, the delay and level of service for the worst individual movement (or movements sharing a single lane) are shown.

[^13]:    ${ }^{3}$ TS = Traffic Signal; CSS = Cross Street Stop

[^14]:    ${ }^{1}$ When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel outside the through lanes. $L=$ Left; $T=$ Through; $R=$ Right; $d=$ Defacto Right Turn' $\underline{\mathbf{1}}=$ Improvement

[^15]:    ${ }^{1}$ When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel
    outside the through lanes. $\mathrm{L}=$ Left $; \mathrm{T}=$ Through; $\mathrm{R}=$ Right; $\mathrm{d}=$ Defacto Right Turn $\underline{\mathbf{1}}=$ Improvement

[^16]:    ${ }^{2}$ Delay and level of service calculated using the following analysis software: Traffix, Version 7.9.0215. Per the Highway Capacity Manual, overall average intersection
    delay and level of service are shown for intersections with traffic signal or all way stop control. For intersections with cross street stop control, the delay and level of service for the worst individual movement (or movements sharing a single lane) are shown.

[^17]:    ${ }^{1}$ When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel outside the through lanes. L = Left; $T=$ Through; $R=$ Right; $d=$ Defacto Right Turn' $\underline{\mathbf{1}}=$ Improvement

[^18]:    ${ }^{3}$ TS $=$ Traffic Signal; CSS = Cross Street Stop
    ${ }^{4}$ Traffic signal improvements proposed.

[^19]:    Intersection Summary

[^20]:    Intersection Summary

[^21]:    Intersection Summary

[^22]:    Intersection Summary

