#### Volume III

Greenbriar Development Project Sacramento, California

Draft Environmental Impact Report









#### Appendices G-P

State Clearinghouse Number 2005062144

Prepared for:

City of Sacramento Environmental Planning Services

and

Sacramento Local Agency Formation Commission

July 2006



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Greenbriar Development Project Sacramento, California

#### Draft Environmental Impact Report



#### Appendices G-P

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> > July 2006



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RUN NAME: W. ELVERTA RD WEST OF POWERLINE RD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 7.38 1.20 0.91 H-TRUCKS 1.71 0.28 0.21 AUTOS

ADT: 460 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 56.50

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 0.0

DO YOU WANT A HARD COPY? (YM)RUN NAME: POWERLINE RD NORTH OF ELKHORN BLVD

RUN NAME: POWERLINE RD SOUTH OF W. ELVERTA RD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NICHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS 1.71 0.28 0.21 AUTOS

ADT: 390 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT PROM NEAR TRAVEL LANE CENTERLINE = 55.78
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL. \*\*
70 CNEL, 65 CNEL, 60 CNEL, 55 CNEL

0.0

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: W. ELVERTA RD EAST OF POWERLINE RD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES
DAY EVENING NIGHT AUTOS 68.82 11.20 8.49 M-TRUCKS 0.28 0.21 1.20 0.91 H-TRUCKS 17 ADT: 640 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT FROM NEAR TRAVEL LANE CENTERLINE = 57.93
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 87.5 0.0 0.0 DO YOU WANT A HARD COPY? (Y/N)

## Existing Conditions (2005)

RUN NAME: POWERLINE RD NORTH OF W. ELVERTA RD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

68.82 11.20 8.49 M-TRUCKS 1,20 0.91 0.28 0.21 7.38 1. H-TRUCKS AUTOS

ADT: 250 SPBED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT PROM NEAR TRAVEL LANE CENTERLINE = 53.85 \*\* DISTANCE (PEET) FROM ROADWAY CENTERLINE TO CNEL \*\* 70 CNEL 65 CNEL 66 CNEL 55 CNEL

0.0 0.0 0.0 0.0

RUN NAME: ELKHORN BLVD BTWN LONE TREE RD AND SR 99710 (TUST W) RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT AUTOS 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 7.38

ADT: 458 SPEED; 45 ACTIVE HALF WIDTH (FT); 6 SITE CHARACTERISTICS; SOFT GRADE (PERCENT); .5

0.28 0.21

7

H-TRUCKS

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 56.48
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 70.1

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: POWERLINE RD BTWN ELKHORN BLVD AND DEL PASO RD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTENG CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS AUTOS

ADT: 1160 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

0.28 0.21

1.71

CNEL AT 30 FT FROM NEAR TRAVEL LANE CENTERLINE = 60.51

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 60.3 129.9

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLYD BTWN POWERLINE RD AND LONE TREE RD (TUST W) RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES
DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS AUTOS

ADT: 210 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

0.28 0.21

1.7

CNEL AT 50 FT FROM NBAR TRAVEL LANG CENTERLINE = \$3.09
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 0.0 DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: POWERLING RD NORTH OF ELKHORN BLVD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NICHT

68.82 11.20 8.49 M-TRUCKS AUTOS

1,20 0,91 7.38 1 H-TRUCKS 1.71 0

0.28 0.21

ADT: 1250 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 30 FT FROM NEAR TRAVEL LANE CENTERLINE = 60.84

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL.\*\*
70 CNEL. 65 CNEL. 60 CNEL. 55 CNEL.

0.0 0.0 63.6 136.5

RUN NAME: POWERLINE RD SOUTH OF DEL PASO RD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES
DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS AUTOS

ADT; 930 SPEED; 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS; SOFT GRADE (PERCENT): .5

0.28 0.21

1.71

CNEL AT 50 FT PROM NEAR TRAVEL LANE CENTERLINE = 59.56
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 52.3 112.1

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLVD EAST OF E. COMMERCE PKWY RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M.TRUCKS 7.38 1.20 0.91 H-TRUCKS 0.28 0.21 1.71 AUTOS

ADT: 13670 SPRED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 71.23

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL. \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

67.5 144.9 311.9 671.7

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: E, COMMERCE PKWY BTWN ELKHORN BLYD AND DEL PASO RD RUN DATE: OCTOBER 3, 2035 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NICHT

AUTOS

68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS

0.28 0.21

ADT: 1730 SPEED: 40 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT PROM NEAR TRAVEL LANE CENTERLINE = 61.11
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 66 CNEL 55 CNEL

DO YOU WANT A HARD COPY? (Y/N)

0.0 0.0 66.3 142.2

RUN NAME: ELKHORN BLVD BTWN SR 99710 AND E. COMMERCE PKWY RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS AUTOS

0.28 0.21 7

ADT: 17276 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT PROM NEAR TRAVEL LANE CENTERLINE = 72.24 \*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL. \*\* 70 CNEL 65 CNEL 65 CNEL 55 CNEL

78.8 169.3 364.5 784.9

RUN NAME, SR9970 BTWN W ELVERTA RD AND ELKHORN BLVD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS 11.20 8.49 0.28 0.21 1.71 AUTOS

ADT: 40500 SPEED: 65 ACTIVE HALF WIDTH (FT): 40 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 30 FT FROM NEAR TRAVEL LANE CENTERLINE = 77.19
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

246.2 524.7 1127.7 2427.8

DO YOU WANT A HARD COPY? (YM)

RUN NAME: DEL PASO RD BTWN WYNDVIEW DR AND EL CENTRO RD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS 11.20 8.49 AUTOS

ADT: 40 SPBED: 25 ACTIVE HALF WIDTH (PT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): 5

0.28 0.21

1.7

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 40.37

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 0.0 DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: SR9970 NORTH OF W ELVERTA RD RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NICHT AUTOS 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 1.71 0.28 0.21 H-TRUCKS

ADT: 32000 SPEED; 65 ACTIVE HALF WIDTH (FT); 40 SITE CHARACTERISTICS; SOFT GRADE (PERCENT); .5

CNEL AT 50 PT PROM NEAR TRAVEL LANE CENTERLINE = 76.16
\*\* DISTANCE (FRET) FROM ROADWAY CENTERLINE TO CNEL. \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL.

211.4 448.9 964.0 2075.1

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME. DEL PASO RD BTWN POWERLINE RD AND WYNDVIEW DR RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M.TRUCKS AUTOS

7.38 1.20 0.91 H-TRUCKS 1.71 0.28 0.21

ADT: 40 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT PROM NEAR TRAVEL LANE CENTERLINE = 45.89
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0

RUN NAME: POWERLINE RD BTWN ELKHORN BLVD AND DEL PASO RD RUN DATE: OCT 3 SCENARIO: BASELINE NO PROJECT

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS 1.71 0.28 0.21 AUTOS

ADT: 1172 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 60.56

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 61.0 130.8

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME. INTERSTATE 5 WEST OF SR99710 1-5 SPLIT RUN DATE: OCTOBER 3, 2005 SCENARIO: EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 1.20 02.1 0.28 0.21 738 1. H-TRUCKS 1.71 0 AUTOS

ADT: 76000 SPEED: 65 ACTIVE HALF WIDTH (FT): 88 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 78.10
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL. \*
70 CNEL. 65 CNEL. 60 CNEL. 55 CNEL.

378,7 798.2 1711,0 3681,7

DO YOU WANT A HARD COPY? (Y/N)

## Baseline No Project Conditions

RUN NAME: W. ELVERTA RD EAST OF POWERLINE RD

RUN DATE: OCT 3 SCENARIO: BASELINE NO PROJECT

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

11.20 8.49 68.82 1 M-TRUCKS 7.38 1 H-TRUCKS AUTOS

1.20 0.91 0.28 0.21 1.7 ADT: 646 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT PROM NEAR TRAVEL LANE CENTERLINE = 57.97
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL.\*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 88.1

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: SR9970 BTWN ELKHORN BLVD AND 1-5 SPLIT RUN DATE: OCTOBER 3, 2005 SCENARIO; EXISTING CONDITIONS (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT AUTOS 68.82 11.20 8.49 M-TRUCKS 1.20 0.91

ADT: 47500 SPEED: 65 ACTIVE HALF WIDTH (FT): 40 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5 0.28 0.21 1.7

H-TRUCKS

CNEL AT 30 PT PROM NEAR TRAVEL LANE CENTERLINE = 77.88 \*\* DISTANCE (FRET) FROM ROADWAY CENTERLINE TO CNEL \*\* 70 CNEL 65 CNEL 60 CNEL 55 CNEL

273.1 583.2 1254.0 2700.0

RUN NAME. ELKHORN BLVD BTWN SR99/10 AND E COMMERCE PKWY RUN DATE. OCT 3 SCENARIO: BASELINE NO PROJECT

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT AUTOS 68.82 11.20 8.49 M-TRUCKS 1,20 0.91 0.28 0.21 H-TRUCKS

ADT: 20629 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 73.01

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

88.6 190.5 410.2 883.4

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME, ELKHORN BLVD BTWN LONE TREE RD AND SR99/70 (1UST W) RUN DATE: OCT 3 SCENARIO: BASELINE NO PROJECT

TRAPFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 0.28 0.21 7.38 E H-TRUCKS 1.71 0 AUTOS

ADT: 2103 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 STE CHARACTERISTICS: SOFT GRADE (PERCENT): ,5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 63.10
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLENE TO CNEL \*\*
70 CNEL 63 CNEL 60 CNEL 53 CNEL

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME. LONE TREE RD SOUTH OF BLKHORN BLVD RUN DATE: OCT 3 SCENARIO: BASELINE NO PROJECT

TRAPPIC DISTRIBUTION PERCENTAGES
DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 AUTOS

0.28 0.21 H-TRUCKS ADT: 1421 SPEED; 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 61.40
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL. \*\*
70 CNEL 63 CNEL 55 CNEL 55 CNEL

0.0 0.0 69.2 148.7

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLVD BTWN POWERLINE RD AND LONE TREE RD (JUST W) RUN DATE: OCT 3 SCENARIO: BASELINE NO PROJECT

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS AUTOS

0.28 0.21 1.73 ADT: 212 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT PROM NEAR TRAVEL LANE CENTERLINE = 53.13
\*\* DISTANCE (FRET) FROM ROADWAY CENTERLINE TO CNEL. \*\*
70 CNEL 65 CNEL 65 CNEL 55 CNEL.

# Baseline + Project + Meister Road Overpass

RUN NAME: W. ELVERTA RD EAST OF POWERLINE RD RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 11.20 8.49 1.20 0.91 0.28 0.21 68.82 11 M-TRUCKS 7.38 1. H-TRUCKS AUTOS 1.71 ADT: 760 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = \$8.68 \*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\* 70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 0.0 98.1

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLVD EAST OF E COMMERCE PKWY RUN DATE: OCT 3 SCENARIO: BASELINE NO PROJECT

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 H-TRUCKS 1.21 0.21 AUTOS

ADT: 6550 SPEED: 40 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 66.89

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 55 CNEL 60 CNEL 55 CNEL

0.0 74.6 160.4 345.2

DO YOU WANT A HARD COPY? (YAN)

RUN NAME, SR 9970 BTWN W ELYERTA RD AND ELKHORN BLVD RUN DATE: OCT 3 SCENARIO: BASELINE NO PROJECT

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NICHT

11.20 8.49 AUTOS 68.82 L M-TRUCKS

1.20 0.91

H-TRUCKS

0.28 0.21 1.71 ADT: 86675 SPEED: 65 ACTIVE HALF WIDTH (FT): 40 SITE CHARACTERISTICS: SOFT ORADE (PERCENT): .5

CNEL AT 50 FT PROM NEAR TRAVEL LANE CENTERLINE = 80.49
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

405.3 869.8 1871.9 4031.4

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: BLKHORN BLVD EAST OF B COMMERCE PKWY RUN DATE: OCT 3 SCENARIO: BASELINE NO PROJECT

68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS 1.71 0.28 0.21 11.20 8.49 AUTOS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

ADT: 15470 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT PROM NEAR TRAVEL LANE CENTERLINE = 71.76
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

73.2 157.3 338.7 729.4

RUN NAME: LONE TREE RD SOUTH OF ELKHORN BLVD RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING MIGHT 68.82 11,20 8,49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS 1.71 0.28 0.21 AUTOS

ADT: 8277 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT FROM NEAR TRAVEL LANE CENTERLINE = 69.05
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 103,8 223,3 480.8

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLYD BTWN POWERLINE RD AND LONE TREE RD (JUST W) RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT AUTOS 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS 0.28 0.21 1.71 ADT: 4690 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT ORADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANG CENTERLINE = 66.58

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 71.2 153.0 329.3

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLVD BTWN LONE TREE RD AND SR9970 (1UST W) RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS AUTOS

0.21 0.28 2 CNEL AT 50 PT FROM NEAR TRAVEL LANE CENTERLINE = 71.81

\*\* DISTANCE (FRET) FROM ROADWAY CENTERLINE TO CNEL. \*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

ADT: 15620 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

73.7 158.3 340.9 734.1

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: POWERLINE RD BTWN ELKHORN BLVD AND DEL PASO RD RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS 0.28 0.21 AUTOS

ADT: 4830 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT PROM NEAR TRAVEL LANE CENTERLINE = 66.71
70 CNEL 65 CNEL 60 CNEL 55 CNEL
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 72.6 156.0 335.8

RUN NAME: SR 99/10 BTWN W ELVERTA RD AND ELKHORN BLVD RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 11.20 8.49 16.0 0.28 0.21 1.20 68.62 I M-TRUCKS H-TRUCKS AUTOS

ADT: 100195 SPEED: 65 ACTIVE HALF WIDTH (FT): 40 STTE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 30 FT PROM NEAR TRAVEL LANE CENTERLINE = 8.1.12

\*\* DISTANCE (FEET) PROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

446.0 957.6 2061.2 4439.2

DO YOU WANT A HARD COPYT (Y/N)

RUN NAME: ELKHORN BLVD EAST OF E COMMERCE PKWY RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT AUTOS 68.62 11.20 8.49 M-TRUCKS 16'0 0.28 0.21 1.20 H-TRUCKS 1.71 0 ADT: 20290 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): 5

CNEL AT 30 FT FROM NEAR TRAVEL LANG CENTERLINE = 72.94

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

87.6 188.4 405.7 873.8

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: BLEHORN BLYD BAST OF E COMMERCE PKWY KUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

11.20 8.49 68.62 1 M-TRUCKS 7.38 1 AUTOS

1,20 0.91

0.21 0.28 H-TRUCKS

ADT: 14140 SPEED: 40 ACTIVE HALF WIDTH (FT): 6 STTE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT FROM NEAR TRAVEL LANE CENTERLINE = 70.23
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\* 70 CNEL 65 CNEL 60 CNEL 55 CNEL

58.0 124.4 267.6 576.3

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLVD BTWN SR99/70 AND E COMMERCE PKWY RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT + MEISTER RD OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

11.20 8.49 AUTOS

M-TRUCKS 68.62

7.38 1.20 0.91 H-TRUCKS 1.71 0.28 0.21

ADT: 25620 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 73.95 \*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL. \*\* 70 CNEL 65 CNEL 66 CNEL 55 CNEL

102.3 220.1 473.9 1020.8

RUN NAME: ELKHORN BLVD BTWN LONE TREE RD AND SR9970 (TUST W) RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 7.38 1 H-TRUCKS AUTOS

ADT: 22170 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

0.28 0.21

1.71

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 73.33

\*\* DISTANCE (FIET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 66 CNEL 55 CNEL

93.0 199.9 430.5 927.1

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: POWERLINE RD BTWN ELKHORN BLYD AND DEL PASO RD RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 7.38 1.20 0.91 H-TRUCKS AUTOS 68.82 11.20 8.49 M-TRUCKS

ADT: 11670 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

1.71 0.28 0.21

CNEL AT 50 FT FROM NEAR TRAVEL LANG CENTERLINE = 70.54

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL.\*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

60.8 130.4 280.7 604.5

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLVD BTWN POWERLINE RD AND LONE TREE RD (TUST W) RUN DATE: OCTOBER 3, 2005
SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 11,20 8.49 1.20 0.91 68.82 1 M-TRUCKS 7.38 1 H-TRUCKS 1.71 0 AUTOS

ADT: 13180 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

0.28 0.21

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 11.07
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

65.9 141.4 304.4 655.5

DO YOU WANT A HARD COPY? (Y/N)

## Baseline + Project No Overpass

RUN NAME. W. ELVERTA RD EAST OF POWERLINE RD RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 11,20 8,49 1.20 0.91 68.82 1 M-TRUCKS AUTOS

0.28 0.21 H-TRUCKS 1.71 (

ADT: 2440 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT PROM NEAR TRAVEL LANG CENTERLING = 63.74

\*\* DISTANCE (FBET) FROM ROADWAY CENTERLING TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

0.0 0.0 99.1 213.1

RUN NAME: ELKHORN BLVD EAST OF E COMMERCE PKWY RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT AUTOS 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 7.38 1 H-TRUCKS 1.71 0 ADT: 6710 SPEED: 40 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

0.28 0.21

CNEL AT 30 FT FROM NEAR TRAVEL LANG CENTERLINE = 66.99

\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

75.8 163.0 350.8

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLVD BTWN SR99/10 AND E COMMERCE PKWY RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 H-TRUCKS 0.21 AUTOS

ADT: 24150 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): 5

CNEL AT 50 FT PROM NEAR TRAVEL LANE CENTERLINE = 73,70
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

98,4 211.6 455.7 981.6

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: ELKHORN BLVD EAST OF E COMMERCE PKWY RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 68.82 11.20 8.49 M-TRUCKS 1.20 0.91 AUTOS

ADT: 18870 SPEED: 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5 0.28 0.21 H-TRUCKS

CNEL AT 30 FT FROM NEAR TRAVEL LANE CENTERLINE = 72.63 \*\* DISTANCE (FRET) FROM ROADWAY CENTERLINE TO CNEL \*\* 70 CNEL 65 CNEL 65 CNEL 55 CNEL

83.5 179.6 386.6 832.7

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: LONE TREE RD SOUTH OF ELKHORN BLVD RUN DATE: OCTOBER 1, 2005 SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT 11.20 8,49 16:0 1.20 68.82 I M-TRUCKS AUTOS

0.28 0.21 H-TRUCKS

ADT: 17128 SPEED; 45 ACTIVE HALF WIDTH (FT): 6 SITE CHARACTERISTICS; SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 72.21
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

78.3 168.4 362.5 780.6

RUN NAME: MEISTER WAY BTWN LONE TREE AND SR 99/70 (ON PROJECT SITE) RUN DATE: OCTOBER 3, 2005 SCENARIO: CUMULATIVE + PROPOSED PROJECT (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

11.06 8.38 8.24 1.34 1.02 H-TRUCKS 1.71 0.28 0.21 67.76 I M-TRUCKS AUTOS

ADT: 18900 SPEED: 35 ACTIVE HALF WIDTH (FT): 12 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 68.82 \*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\* 70 CNEL 65 CNEL 60 CNEL 55 CNEL

60.3 128.0 274.7 591.2

DO YOU WANT A HARD COPY? (YAN)

# Cumulative + Project Conditions (2005)

RUN NAME: ELKHORN BLVD BTWN LONE TREE RD AND SR 99/70 (JUST W) RUN DATE: OCTOBER 3, 2005 SCENARIO: CUMULATIVE + PROPOSED PROJECT (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

67.76 11.06 8.38 M-TRUCKS 8.24 1.34 1.02 H-TRUCKS 1.71 0.28 0.21 AUTOS

ADT: 60940 SPEED: 45 ACTIVE HALF WIDTH (FT): 36 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 75.68
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL. \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

190.3 404.0 867.6 1867.5

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: LONE TREE RD SOUTH OF ELKHORN BLVD RUN DATE: OCTOBER 3, 2005 SCENARIO: CUMULATIVE + PROPOSED PROJECT (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT AUTOS

67.76 11.06 8.38 M-TRUCKS 8.24 1.34 1.02 H-TRUCKS 1.71 0.28 0.21

ADT: 21870 SPEED: 45 ACTIVE HALF WIDTH (FT): 21 STTE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 30 PT PROM NEAR TRAVEL LANE CENTERLINE = 72.16
\*\*\* DISTANCE (FRET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 66 CNEL 55 CNEL

96.8 204.6 438.8 944.4

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: SR 9970 BTWN W ELVERTA RD AND ELKHORN BLVD RUN DATE: OCTOBER 3, 2005 SCENARIO: BASELINE + PROJECT NO OVERPASS

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT

68.82 11.20 8.49 M-TRUCKS 7.38 1.20 0.91 H-TRUCKS

0.28 0.21 1.7 ADT: 101325 SPEED: 65 ACTIVE HALF WIDTH (FT): 40 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 PT FROM NEAR TRAVEL LANE CENTERLINE = 81.17
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 45 CNEL 66 CNEL 55 CNEL

449.4 965.0 2077.2 4473.7

RUN NAME: DYTERSTATE 5 WEST OF SR 99/10 SPLIT RUN DATE: OCTOBER 3, 2005 SCENARIO: CUMULATIVE + PROPOSED PROJECT (2005)

TRAFFIC DISTRIBUTION PERCENTAGES
DAY EVENING NIGHT  ADT: 102739 SPEED: 65 ACTIVE HALF WIDTH (FT): 88 SITE CHARACTERISTICS: SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 79.60
\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\*
70 CNEL 65 CNEL 60 CNEL 55 CNEL

472.0 1002.7 2153.2 4635.0

DO YOU WANT A HARD COPY? (Y/N)

RUN NAME: SR 99/10 BTWN ELKHORN BLVD AND I-5 SPLIT RUN DATE: OCTOBER 3, 2005 SCENARIO: CUMULATIVE + PROPOSED PROJECT (2005)

TRAFFIC DISTRIBUTION PERCENTAGES DAY EVENING NIGHT AUTOS 67.76 11.06 8.38 M-TRUCKS 8.24 1.34 1.02 H-TRUCKS 1.71 0.28 0.21

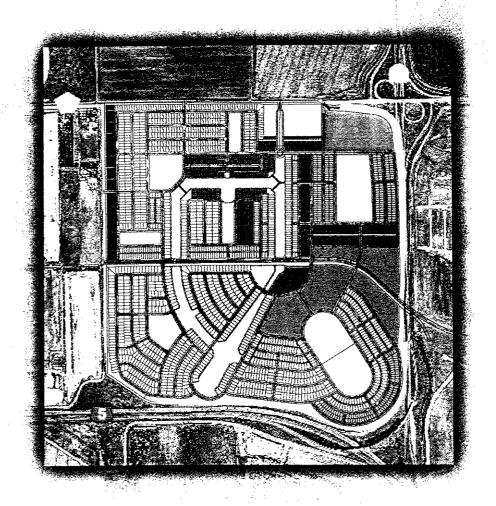
ADT: 64212 SPEED: 65 ACTIVE HALF WIDTH (FT): 40 SITE CHARACTERISTICS; SOFT GRADE (PERCENT): .5

CNEL AT 50 FT FROM NEAR TRAVEL LANE CENTERLINE = 79.38 \*\*\* DISTANCE (FEET) FROM ROADWAY CENTERLINE TO CNEL \*\* 70 CNEL 65 CNEL 60 CNEL 55 CNEL

342.5 733.7 1578.5 3399.3



## Greenbriar Water Study





July 2005

Prepared by

#### WOOD RODGERS

DEVELOPING INNOVATIVE DESIGN SOLUTIONS

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## Greenbriar

**Water Study** 

Sacramento, California

**Prepared For:** 

City of Sacramento

**July 2005** 

Prepared By:





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#### PURPOSE

This water analysis is intended to assist in properly sizing the domestic transmission and distribution system for the Greenbriar Property. This analysis will confirm that the proposed water lines will be sized appropriately to meet or exceed the City of Sacramento's Water Distribution System Design Criteria.

#### STUDY AREA

Greenbriar is located within the North Natomas Vision Area and is currently outside the Request Limits. Sacramento City annexation into the City is currently being processed. Greenbriar is located directly west of Highway 99 and north of Interstate 5. The development encompasses approximately 577 acres. The purpose of this study is to transmission the size adequately distribution mains within the Greenbriar development. Land use for the Plan Area will consist of low, medium and high density residential, elementary school, parks, and commercially zoned properties. The existing land use consists of open agricultural fields with relatively gentle slopes.

Refer to Figure 1 for the project location.

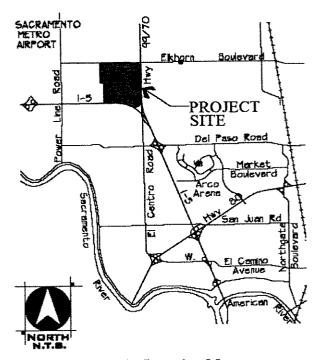


Figure 1 - Location Map.

#### ASSUMPTIONS

Assumptions used for this analysis are based on the proposed land use plan dated April 4, 2005 by Wood Rodgers, Inc.; the City of Sacramento's Department of Utilities staff; and the City of Sacramento's Water Distribution System Design Criteria.

#### Land Use

The Greenbriar development is proposed to consist of:

- 1,146 low density residential lots.
- 1.565 medium density residential lots.
- 1,012 high density residential lots.
- 26 acres of commercial.
- 49 acres of parks.

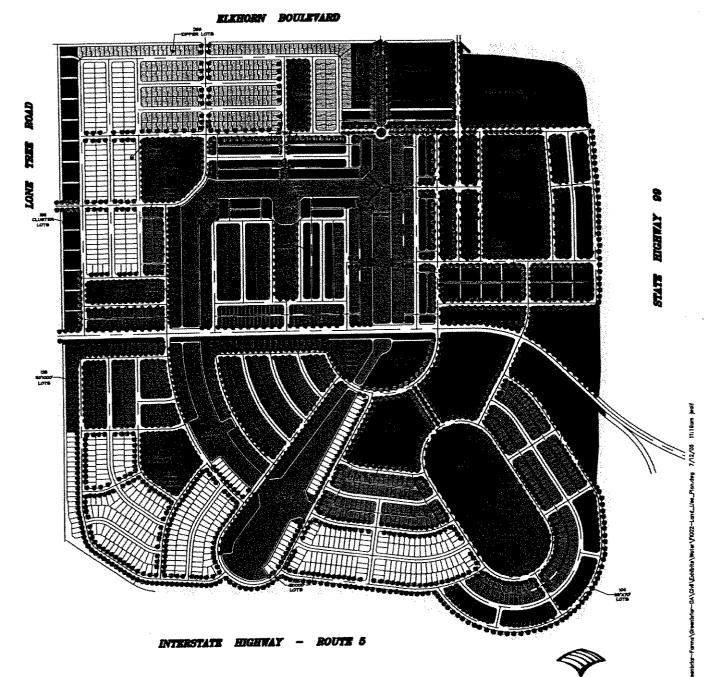
Figure 2 shows the proposed land use plan for Greenbriar.

#### FIGURE 2. LAND USE PLAN

### **GREENBRIAR**









#### **Demand and Peaking Factors**

The City's Water Distribution System Criteria were used to determine the proposed water use demands in the model. Peaking factors were used to simulate system-operating scenarios for the water distribution system analysis. Maximum Day Demands (MDD) were developed by applying a MDD factor of 1.8 to the Average Day Demand (ADD) estimates. The Peak Hour Demands (PHD) were developed by applying a PHD factor of 1.3 to the Maximum Day Demands (MDD). The demands were increased by 7.5% to account for system losses per City criteria. Table 1 shows the ADD, MDD, and PHD used for the hydraulic modeling scenarios. Refer to Appendix A for complete demand projections.

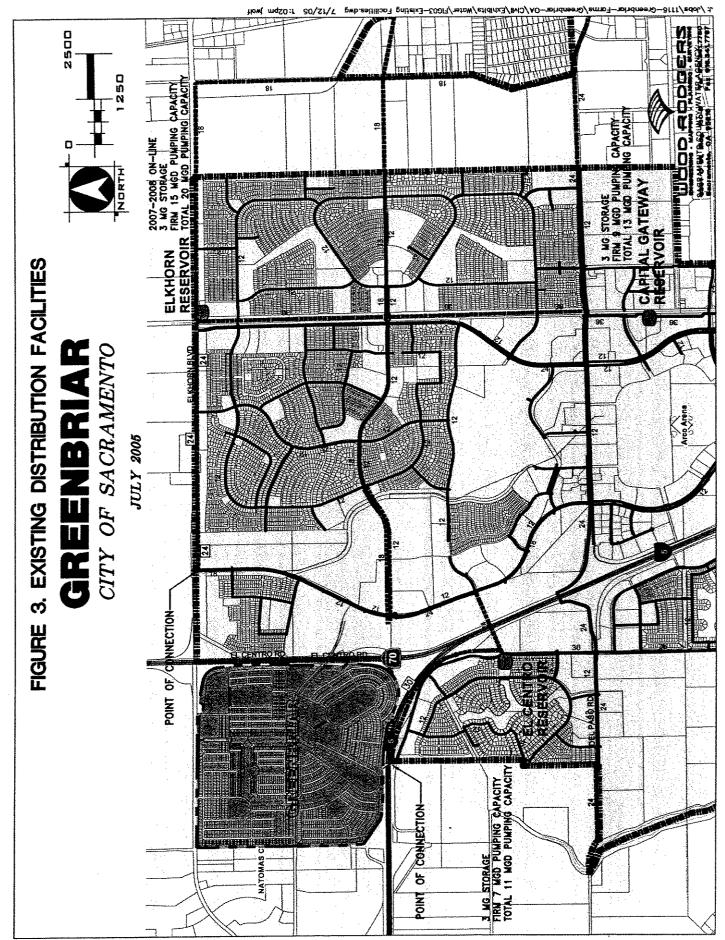
Table 1 - Potable Water Demand Projections for Greenbriar.

| A Company of the Comp | Total            |                   | ADD Unit Water Demand |        | Den  | p <b>m</b> ) |      |
|--|------------------|-------------------|-----------------------|--------|------|--------------|------|
| <b>Land Use Designation</b>  | Acres*.<br>(net) | Dwelling<br>Units | gpm/ac                | gpm/du | ADD  | MDD          | PHD  |
| Low Density Residential  | 128              | 1,146             |                       | 0.44   | 504  | 907          | 1179 |
| Medium Density Residential   | 106              | 1,565             |                       | 0.44   | 689  | 1240         | 1612 |
| High Density Residential   | 45               | 1,012             | 2.48                  |        | 112  | 202          | 262  |
| Commercial   | 26               |                   | 1.86                  |        | 48   | 86           | 112  |
| Parks/Landscape  | 84               |                   | 2.60                  |        | 217  | 391          | 508  |
| Schools  | 10               |                   | 1.55                  |        | 16   | 29           | 37   |
| Subtotal   | 399              | 3723              |                       |        | 1586 | 2855         | 3711 |
| 7.5% System Losses   |                  |                   |                       |        | 119  | 214          | 278  |
| Totals   |                  |                   |                       |        | 1705 | 3069         | 3989 |

<sup>\*</sup>Acreage does not include street right of way.

#### **Operational Requirements**

The City of Sacramento has developed water distribution system design criteria to be used in the planning of new water distribution systems. These criteria apply to water studies that analyze subdivision level developments. The criteria help ensure adequate pressure and flow are available to serve customers on a daily basis and also during emergency fire situations. The criteria used in this study are listed in **Table 2**.



**Table 3 - Boundary Conditions.** 

| Point of Connection<br>Location       | Point of<br>Connection<br>ID | Hydraulic<br>(1<br>MDD | U    | Pressu<br>MDD | re (psi)<br>PHD |
|---------------------------------------|------------------------------|------------------------|------|---------------|-----------------|
| Terminal End of<br>Airport Connection | PUMP-105                     | 91.4                   | 91.2 | 30.1          | 30.0            |
| Elkhorn Blvd and East Commerce Way    | PUMP-107                     | 96.7                   | 95.9 | 30.6          | 30.2            |

#### SUMMARY OF ANALYSIS

The water model was developed using MWH Soft, Inc. hydraulic modeling program, H<sub>2</sub>0NET version 6.0. An electronic copy of the water distribution model is available upon request.

The transmission and distribution system was laid out following the street centerline, creating a looped system. Pipe sizes range from 8-inch to 18-inch diameter with the larger diameter pipes looped around commercial and school sites to convey the higher fire flow requirements. Greenbriar was modeled independent of the surrounding developments. **Table 4** summarizes the model results for average day demands, maximum day demands, and peak hour demands.

Table 4 - System Hydraulic Modeling Scenario Results.

| IUVIC             |                               | <del></del>                         |                               |
|-------------------|-------------------------------|-------------------------------------|-------------------------------|
| Demand Scenario 7 | Greenbriar<br>Demand<br>(gpm) | Minimum System<br>Pressure<br>(psi) | Maximum System Velocity (fps) |
| Average Day       | 1,705                         | 34                                  | 1.2                           |
| Maximum Day       | 3,069                         | 31                                  | 2.2                           |
| Peak Hour         | 3,989                         | 30                                  | 2.5                           |

Figure 4 shows the layout of the proposed water system. A full size exhibit is located in Appendix C. Hardcopy results for the demand scenarios are located in Appendix D.

#### Fire Flow Results

Fire flow analyses were performed during maximum day demands. The fire flow demand requirements by land use are shown in **Table 2**. The fire flow analysis calculated the available fire flow at every required node in the system. **Table 5** lists the locations most sensitive to the fire flow demands.



Table 5 - Fire Flow Results During Maximum Day Demands.

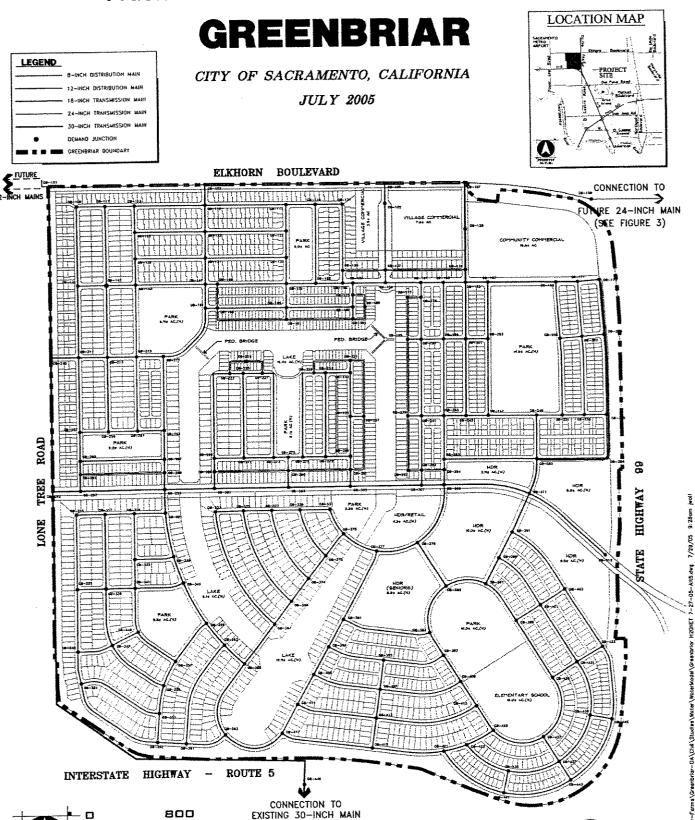
| Fire Flow |               | Total Plan  |          | Maximum 8            |
|-----------|---------------|-------------|----------|----------------------|
| Node      | 9             | Area Demand | Pressure | Velocity<br>(ft/sec) |
| GB-443    | (gpm) = 1,500 | 4,569       | 25       | 4.6                  |
| GB-313    | 2,000         | 5,069       | 23       | 5.8                  |
| GB-427    | 3,000         | 6,069       | 20       | 4.5                  |

Hardcopy results for all scenarios are located in Appendix D.

#### CONCLUSIONS

The City of Sacramento Water Distribution Design Criteria requirements were met for this water distribution system. There are several assumptions on which the hydraulic model is based. The model would require modification if any additional information becomes available that would affect the way water is delivered to the development.

#### FIGURE 4. DISTRIBUTION SYSTEM LAYOUT



(SEE FIGURE 3)

400

WOOD RODGERS

3301 C St, Bidg. 100-B Sacremento, CA 95816



## APPENDIX A GREENBRIAR DEMAND SPREADSHEET

|                  |               |  |                | mand Spreads                | neet                                    |                |                |                |  |
|------------------|---------------|--|----------------|-----------------------------|---|----------------|----------------|----------------|--|
|                  |               | L  | and Use Design | ation                       |   | Total Demand   |                |                |  |
| Model ID Label   | Commercial    | Parks/<br>Landscape                              | Schools        | High Density<br>Residential | Single Family<br>Residential            | ADD            | MDD            | PHD            |  |
|                  | (acres)       | (acres)  | (acres)        | (acres)                     | (units)                                 | (gpm)          | (gpm)          | (gpm)          |  |
|                  | 1.86 gpm/acre |  | 1.55 gpm/acre  | 2.48 gpm/acre               | 0.44 gpm/unit<br>0.44                   |                |                |                |  |
|                  | 1.86          | 2.600  | 1.55           | 2.48                        | 0.44                                    | 2.57           | 4.63           | 6.02           |  |
| GB-103           |               | 0.99   |                |                             |   | 2.57           | 4.63           | 6.02           |  |
| GB-105           |               | 0.99   |                |                             |   | 0.00           | 0.00           | 0.00           |  |
| GB-107<br>GB-108 | 7.81          |  |                |                             | *************************************** | 14.53          | 26.15          | 33.99          |  |
| GB-109           | 1             |  |                |                             | 36                                      | 15.84          | 28.51          | 37.07          |  |
| GB-111           | <u> </u>      |  |                |                             | 20                                      | 8.80           | 15.84          | 20.59          |  |
| GB-113           |               |  |                |                             | 18                                      | 7.92           | 14.26          | 18.53          |  |
| GB-115           |               |  |                |                             | 30<br>20                                | 13.20<br>8.80  | 23.76<br>15.84 | 30.89<br>20.59 |  |
| GB-117           |               | 440  |                |                             | 14                                      | 10.01          | 18.01          | 23.42          |  |
| GB-119           |               | 1.48   |                |                             | 18                                      | 7,92           | 14.26          | 18.53          |  |
| GB-121           | 6.32          | 1.15   |                |                             |   | 14.75          | 26.54          | 34.50          |  |
| GB-122<br>GB-123 | 0.32          | 1.19   |                | WIII                        | 17                                      | 7.48           | 13.46          | 17.50          |  |
| GB-125           |               |  |                |                             | 29                                      | 12.76          | 22.97          | 29.86          |  |
| GB-127           | <b>!</b>      |  |                |                             | 16                                      | 7.04           | 12.67          | 16.47          |  |
| GB-128           | 11.60         |  |                |                             |   | 21.58          | 38.84          | 50.49          |  |
| GB-129           |               |  | ļļ             |                             | 17<br>28                                | 7.48<br>12.32  | 13,46<br>22,18 | 17.50<br>28.83 |  |
| GB-131           | <b> </b>      |  |                |                             | 28<br>16                                | 7.04           | 12.67          | 16.47          |  |
| GB-133           | <u> </u>      |  |                |                             | 14                                      | 6.16           | 11.09          | 14.41          |  |
| GB-135           |               |  |                |                             | 20                                      | 8.80           | 15.84          | 20.59          |  |
| GB-137<br>GB-139 |               |  |                |                             | 20                                      | 8.80           | 15,84          | 20.59          |  |
| GB-141           |               |  |                |                             | 43                                      | 18.92          | 34.06          | 44.27          |  |
| GB-143           |               |  |                |                             | 26                                      | 11.44          | 20.59          | 26.77          |  |
| GB-145           |               |  |                |                             | 14                                      | 6.16           | 11.09          | 14.41<br>26.98 |  |
| GB-147           |               | 3.42   |                |                             | 6<br>19                                 | 11.53<br>8.36  | 20.76<br>15.05 | 19.56          |  |
| GB-149           |               | <u> </u>   |                |                             | 22                                      | 9.68           | 17.42          | 22.65          |  |
| GB-151           | <b></b>       | 1,48   |                |                             | 14                                      | 10.01          | 18.01          | 23.42          |  |
| GB-153<br>GB-155 |               | 1.40   |                |                             | 8                                       | 3.52           | 6.34           | 8.24           |  |
| GB-157           | <u> </u>      | ·····  |                | ····                        | 3                                       | 1.32           | 2.38           | 3.09           |  |
| GB-159           |               | 0.13   |                |                             | 6                                       | 2.98           | 5.36           | 6.97           |  |
| GB-161           |               |  |                |                             | 5                                       | 2.20           | 3.96           | 5.15           |  |
| GB-163           |               |  |                |                             | 11                                      | 4.84           | 8.71<br>9.50   | 11.33<br>12.36 |  |
| GB-165           |               |  |                |                             | 12<br>6                                 | 5.28<br>12.26  | 22.07          | 28.69          |  |
| GB-167           |               | 3.70   |                |                             | 5                                       | 2.20           | 3,96           | 5.15           |  |
| GB-169           | <u> </u>      | <u> </u>   |                |                             | 10                                      | 4.40           | 7.92           | 10.30          |  |
| GB-171<br>GB-173 |               | 4.81   |                |                             | 5                                       | 14.71          | 26.47          | 34.41          |  |
| GB-175           |               | 7.01   |                |                             | 2                                       | 0.88           | 1.58           | 2.06           |  |
| GB-177           | -             |  |                |                             | 7                                       | 3.08           | 5.54           | 7.21           |  |
| GB-179           |               |  |                |                             | 12                                      | 5.28           | 9,50           | 12.36          |  |
| GB-181           |               |  |                |                             | 7                                       | 3.08           | 5.54           | 7.21<br>24.71  |  |
| GB-183           |               | <u> </u>   | <b>_</b>       |                             | 24<br>40                                | 10.56<br>17.60 | 19.01<br>31.68 | 41.18          |  |
| GB-185           | <u> </u>      | <u> </u>   |                |                             | 22                                      | 9.68           | 17.42          | 22.65          |  |
| GB-187           |               |  |                |                             | 10                                      | 4.40           | 7.92           | 10.30          |  |
| GB-189<br>GB-191 |               | 0.13   |                |                             | 21                                      | 9.58           | 17.24          | 22.41          |  |
| GB-193           | 1             | 0.12   |                |                             | 13                                      | 6.03           | 10.86          | 14,11          |  |
| GB-195           | 1             | 0.12   |                |                             | 13                                      | 6.03           | 10.86          | 14.11          |  |
| GB-197           |               |  |                |                             | 24                                      | 10.56          | 19.01          | 24.71          |  |
| GB-199           |               |  |                |                             | 24                                      | 10.56          | 19.01          | 24.71<br>28.83 |  |
| GB-201           |               |  |                |                             | 28                                      | 12.32<br>15.78 | 22.18<br>28.40 | 36.93          |  |
| GB-203           | <u> </u>      | 3.70   |                |                             | 14                                      | 15.78          | 28.40          | 36.93          |  |
| GB-205           |               | 3.70   |                |                             | 28                                      | 12.32          | 22.18          | 28.83          |  |
| GB-207           | +             | <u> </u>   |                |                             | 14                                      | 6.16           | 11.09          | 14.41          |  |
| GB-209<br>GB-210 | -             | 3.70   | <u> </u>       |                             |   | 9.62           | 17.32          | 22.51          |  |
| GB-210<br>GB-211 | 1             | <del>                                     </del> |                |                             | 54                                      | 23.76          | 42.77          | 55.60          |  |
| GB-213           |               |  |                |                             | 26                                      | 11.44          | 20,59          | 26.77          |  |
| GB-215           |               | 3.42   |                |                             | 15                                      | 15.49          |                | 36.25          |  |
| GB-217           |               |  |                |                             | 14                                      | 6.16           | 11.09          | 14.41          |  |
| GB-219           |               |  |                | <b></b>                     | 15                                      | 6.60           | 11.88          | 15.44<br>20.96 |  |
| GB-221           |               | 0.23   |                |                             | 19<br>19                                | 8.96<br>9.53   | 16,12          | 22.30          |  |
| GB-223           |               | 0,45   |                |                             | 12                                      | 5.28           | 9.50           | 12.36          |  |

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| <u> </u>         | Tr   | tal Dema             | ınd  |  |                        |                |                |                |
|------------------|--|----------------------|--|--|------------------------|----------------|----------------|----------------|
|                  | Land Use Designation  Commercial Parks/ Schools High Density Single Family |                      |  |  |                        |                | ADD MDD        |                |
| Model ID Label   | Commercial<br>(acres)  | Landscape<br>(acres) | (acres)  | Residential (acres)                    | Residential<br>(units) |                |                | PHD            |
|                  | 1.86 gpm/acre  | 2.60 gpm/acre        | 1.55 gpm/acre                                    | 2.48 gpm/acre                          | 0.44 gpm/unit          | (gpm)          | (gpm)          | (gpm)          |
|                  | 1.86   | 2.600                | 1.55   | 2.48                                   | 0.44                   |                |                |                |
| GB-227           |  |                      |  |  | 13                     | 5.72           | 10.30          | 13.38          |
| GB-229           |  | 1.55                 |  |  | 13                     | 9.75           | 17.55          | 22.82          |
| GB-231           |  |                      |  |  | 22                     | 9.68           | 17.42          | 22.65          |
| GB-233           |  |                      |  |  | 14                     | 6.16           | 11.09          | 14.41          |
| GB-235           |  |                      |  |  | 22<br>14               | 9.68<br>6.47   | 17.42<br>11.65 | 22.65<br>15.14 |
| GB-237           |  | 0.12<br>0.12         |  |  | 14                     | 6.47           | 11.65          | 15.14          |
| GB-239<br>GB-241 |  | 0.12                 |  |  | 28                     | 12.32          | 22.18          | 28.83          |
| GB-241           |  |                      |  |  | 30                     | 13.20          | 23.76          | 30.89          |
| GB-245           |  |                      |  |  | 28                     | 12.32          | 22.18          | 28.83          |
| GB-247           |  |                      |  |  | 19                     | 8.36           | 15.05          | 19.56          |
| GB-249           |  | 3.70                 |  |  | 20                     | 18.42          | 33,16          | 43.10          |
| GB-251           |  |                      |  |  | 19                     | 8.36           | 15.05          | 19.56          |
| GB-253           |  |                      |  |  | 28                     | 12.32          | 22.18          | 28.83<br>38.53 |
| GB-255           |  | 4.81                 |  |  | 9<br>25                | 16.47<br>11.00 | 29.64<br>19.80 | 25.74          |
| GB-257<br>GB-259 |  |                      |  |  | 12                     | 5.28           | 9.50           | 12.36          |
| GB-259<br>GB-261 |  |                      |  |  | 13                     | 5.72           | 10.30          | 13.38          |
| GB-263           |  |                      |  |  | 15                     | 6.60           | 11.88          | 15.44          |
| GB-265           |  | 1.58                 |  |  | 20                     | 12.91          | 23.23          | 30.20          |
| GB-267           |  | 1.58                 |  |  | 14                     | 10.27          | 18.48          | 24.03          |
| GB-269           |  |                      |  |  | 22                     | 9.68           | 17.42          | 22.65          |
| GB-271           |  |                      |  |  | 21                     | 9.24           | 16.63          | 21.62<br>12.36 |
| GB-273           |  | 1.55                 |  |  | 12                     | 5.28<br>4.91   | 9.50<br>8.84   | 11.49          |
| GB-275           |  | 1.55                 |  |  | 12                     | 5.28           | 9.50           | 12.36          |
| GB-277<br>GB-279 |  |                      |  |  | 22                     | 9.68           | 17.42          | 22.65          |
| GB-279           |  |                      |  |  | 11                     | 4.84           | 8.71           | 11.33          |
| GB-283           |  | - <u> </u>           |  |  | 25                     | 11.00          | 19.80          | 25.74          |
| GB-285           |  |                      |  |  | 30                     | 13.20          | 23.76          | 30.89          |
| GB-286           |  |                      |  |  | 20                     | 8.80           | 15.84          | 20.59          |
| GB-287           |  |                      |  |  | 20                     | 8.80           | 15.84          | 20.59<br>11.33 |
| GB-288           |  |                      |  |  | 11<br>8                | 4.84<br>3.52   | 8.71<br>6.34   | 8.24           |
| GB-289           |  |                      |  |  | 13                     | 5.72           | 10.30          | 13.38          |
| GB-290<br>GB-291 |  |                      |  | ······································ | 19                     | 8.36           | 15.05          | 19.56          |
| GB-292           |  |                      |  |  | 9                      | 3.96           | 7.13           | 9,27           |
| GB-293           |  |                      |  |  | 16                     | 7.04           | 12.67          | 16.47          |
| GB-294           |  |                      |  | 2.2                                    |                        | 5.46           | 9.82           | 12.77          |
| GB-295           |  |                      |  |  |                        | 0.00           | 0.00           | 0.00           |
| GB-297           |  |                      |  |  |                        | 0.00           | 0.00           | 0.00           |
| GB-299           |  |                      |  |  |                        | 0.00           | 0.00           | 0.00           |
| GB-301           |  |                      |  | <b></b>                                |                        | 0.00           | 0.00           | 0.00           |
| GB-303<br>GB-305 |  |                      |  |  |                        | 0.00           | 0.00           | 0.00           |
| GB-307           |  |                      |  |  |                        | 0.00           | 0.00           | 0.00           |
| GB-309           |  |                      |  |  |                        | 0.00           | 0.00           | 0.00           |
| GB-311           |  |                      |  | 6.75                                   |                        | 16.74          | 30.13          | 39.17          |
| GB-313           |  |                      |  | 8.78                                   | ,                      | 21.77          | 39.19          | 50.95          |
| GB-315           |  |                      |  |  | 18                     | 7.92           | 14.26          | 18.53          |
| GB-317           |  |                      |  |  | 17                     | 7.48           | 13,46          | 17.50          |
| GB-319           |  |                      |  | <b></b>                                | 11                     | 4.84<br>4.84   | 8.71<br>8.71   | 11.33          |
| GB-321           |  |                      |  | I                                      | 26                     | 11.44          | 20,59          | 26.77          |
| GB-323<br>GB-325 |  |                      |  |  | 21                     | 9.24           | 16.63          | 21.62          |
| GB-327           |  |                      |  |  | 17                     | 7.48           | 13.46          | 17.50          |
| GB-329           |  |                      | <del>*************************************</del> |  | 12                     | 5.28           | 9.50           | 12.36          |
| GB-331           |  |                      |  |  | 5                      | 2.20           | 3.96           | 5,15           |
| GB-333           |  |                      |  |  | 14                     | 6.16           | 11.09          | 14.41          |
| GB-335           |  |                      |  |  | 12                     | 5.28           | 9,50           | 12.36          |
| GB-337           |  |                      |  |  | 22                     | 9.68           | 17.42          | 22.65          |
| GB-339           |  |                      |  |  | 19                     | 8.36           | 15.05          | 19.56          |
| GB-341           |  | 1.32                 |  |  | 8                      | 6.95           | 12.51          | 16.27          |
| GB-343           |  | 1.32                 |  | <b>_</b>                               | 5                      | 5.63           | 10.14          | 13.18          |
| GB-345           |  |                      |  | <b></b>                                | 17<br>20               | 7.48<br>8.80   | 13.46<br>15.84 | 17.50<br>20.59 |

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|                       |                      | Greenb              | riar - Water De | emand Spreads               | heet                         |              |                |                |
|-----------------------|----------------------|---------------------|-----------------|-----------------------------|------------------------------|--------------|----------------|----------------|
|                       | Land Use Designation |                     |                 |                             |                              |              |                | nd             |
| Model ID Label        | Commercial           | Parks/<br>Landscape | Schools         | High Density<br>Residential | Single Family<br>Residential | ADD          | MDD            | PHD            |
|                       | (acres)              | (acres)             | (acres)         | (acres)                     | (units)                      | (gpm)        | (gpm)          | (gpm)          |
|                       | 1.86 gpm/acre        | 2.60 gpm/acre       | 1.55 gpm/acre   | 2.48 gpm/acre               | 0.44 gpm/unit                | (Bhu)        | (Shue)         | (3)            |
|                       | 1.86                 | 2.600               | 1.55            | 2.48                        | 0.44                         |              |                |                |
| GB-349                |                      |                     |                 |                             | 8                            | 3.52         | 6.34           | 8.24           |
| GB-351                |                      |                     |                 |                             | 25                           | 11.00        | 19.80          | 25.74          |
| GB-352                |                      | 4.13                |                 |                             | 11                           | 15.58        | 28.04          | 36.45          |
| GB-353                |                      |                     |                 |                             | 19                           | 8.36         | 15.05          | 19.56          |
| GB-355                |                      |                     |                 |                             | 16                           | 7.04         | 12.67          | 16.47          |
| GB-357                |                      | 1.32                |                 |                             | 10                           | 7.83         | 14.10          | 18.33          |
| GB-359                |                      | 1.32                |                 |                             | 6                            | 6.07         | 10.93          | 14.21          |
| GB-361                |                      |                     |                 |                             | 19                           | 8.36         | 15.05          | 19.56          |
| GB-362                |                      |                     |                 | ····                        | 24                           | 10.56        | 19.01          | 24.71          |
| GB-363                |                      |                     |                 |                             | 13                           | 5.72         | 10,30          | 13.38          |
| GB-365                |                      | 0.11                |                 |                             | 16                           | 7.33         | 13,19          | 17.14          |
| GB-367                |                      | 0.10                |                 |                             | 22                           | 9.94         | 17.89          | 23.26          |
| GB-369                |                      |                     |                 |                             | 20                           | 8.80         | 15.84          | 20.59          |
| GB-371                |                      |                     |                 |                             | 16                           | 7.04         | 12.67          | 16.47          |
| GB-373                |                      |                     |                 |                             | 12<br>3                      | 5.28<br>7.61 | 9,50<br>13,70  | 12.36<br>17.81 |
| GB-375                |                      | 2.42                |                 | 2.22                        | 9                            | 9.47         | 17.04          | 22.15          |
| GB-377                |                      |                     |                 | 2.22<br>9.46                | <u> </u>                     | 23.46        | 42.23          | 54.90          |
| GB-379                |                      |                     |                 | 2.22                        | 18                           | 13.43        | 24.17          | 31.42          |
| GB-381                |                      |                     |                 | 2.22                        | 8                            | 9.03         | 16.25          | 21.12          |
| GB-383                |                      |                     |                 | 2.22                        | <u> </u>                     | 5.51         | 9,91           | 12.88          |
| GB-385                |                      |                     |                 | 2.49                        | 4                            | 7.94         | 14.28          | 18.57          |
| GB-387<br>GB-389      |                      |                     |                 | £. TV                       | 11                           | 4.84         | 8,71           | 11.33          |
| GB-391                |                      |                     |                 | 6.72                        | 7                            | 19.75        | 35.54          | 46.20          |
| GB-393                |                      | 0.11                |                 |                             | 17                           | 7.77         | 13.98          | 18.17          |
| GB-395                |                      | <u> </u>            |                 |                             | 18                           | 7.92         | 14.26          | 18.53          |
| GB-397                |                      | 5.09                |                 | ·······                     | 14                           | 19.39        | 34.91          | 45.38          |
| GB-399                |                      | 5.09                |                 |                             | 11                           | 18.07        | 32.53          | 42.29          |
| GB-401                |                      |                     |                 |                             | 23                           | 10.12        | 18,22          | 23.68          |
| GB-403                |                      |                     |                 |                             | 13                           | 5.72         | 10.30          | 13.38          |
| GB-405                |                      | 0.10                |                 |                             | 13                           | 5.98         | 10.76          | 13.99          |
| GB-407                |                      |                     |                 |                             | 26                           | 11.44        | 20.59          | 26.77          |
| GB-409                |                      |                     |                 |                             | 16                           | 7.04         | 12.67          | 16.47          |
| GB-411                |                      |                     |                 |                             | 20                           | 8.80         | 15.84          | 20.59          |
| GB-413                |                      |                     |                 |                             | 31                           | 13.64        | 24.55          | 31.92          |
| GB-415                |                      |                     |                 |                             | 16                           | 7.04         | 12.67          | 16.47          |
| GB-417                |                      | 4.13                |                 |                             | 17                           | 18.22        | 32.79          | 42.63          |
| GB-419                |                      |                     |                 |                             | 13                           | 5.72         | 10.30          | 13.38          |
| GB-421                |                      | 4.1                 |                 |                             | 15                           | 17.26        | 31.07          | 40.39          |
| GB-423                |                      |                     |                 |                             | 13                           | 5.72         | 10.30          | 13.38          |
| GB-425                |                      |                     | 5.09            |                             | 8                            | 11.41        | 20,54          | 26.70          |
| GB-427                |                      |                     |                 |                             | 13                           | 5.72         | 10.30          | 13.38          |
| GB-429                |                      |                     | 5,09            |                             | 14                           | 14.05        | 25.29          | 32.88          |
| GB-431                |                      |                     |                 |                             | 26                           | 11.44        | 20.59          | 26.77          |
| GB-433                |                      | 4.1                 |                 |                             | 16                           | 17.70        | 31.86          | 41.42          |
| GB-435                |                      |                     |                 |                             | 20                           | 8.80         | 15.84          | 20.59<br>21.62 |
| GB-437                |                      |                     |                 |                             | 21                           | 9.24         | 16.63<br>16.63 | 21.62          |
| GB-439                |                      |                     |                 |                             | 21                           | 9.24         | 10.30          | 13.38          |
| GB-441                |                      |                     |                 |                             | 13<br>14                     | 5.72<br>6.16 | 11.09          | 14,41          |
| GB-443                |                      |                     |                 |                             | 13                           | 5.72         | 10.30          | 13.38          |
| GB-445                |                      |                     | 10              | #E                          |                              | 1 9.72       | 10.30          | 10.00          |
| TOTAL<br>DEMAND (gpm) | 26<br>48             | 83<br>217           | 10<br>16        | 45<br>112                   | 2,711<br>1,193               | 1586         | 2855           | 3711           |
|                       |                      |                     | 7.5% l          | Jnaccounted For L           | _08 <b>868</b>               | 119          | 214            | 278            |
|                       |                      |                     |                 | Total C                     | Demand                       | 1705         | 3069           | 3989           |



#### APPENDIX B

EXHIBITS - DISTRIBUTION SYSTEM CONNECTIONS

#### ALTERNATIVE 1 DISTRIBUTION SYSTEM CONNECTIONS

### **GREENBRIAR**

B-INCH DISTRIBUTION MAIN

12-INCH DISTRIBUTION MAIN

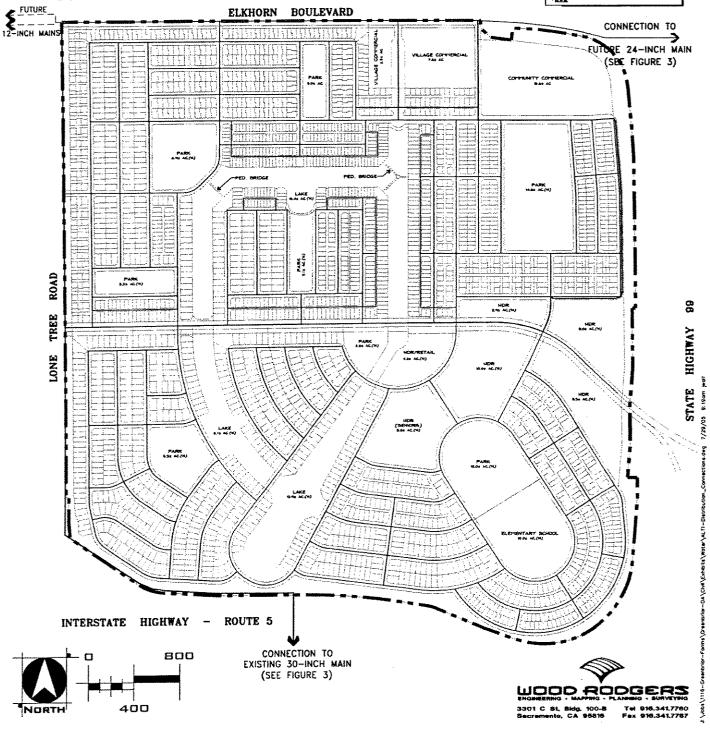
18-INCH TRANSMISSION MAIN

24-INCH TRANSMISSION MAIN

30-INCH TRANSMISSION MAIN

GREENBRAR BOUNDARY



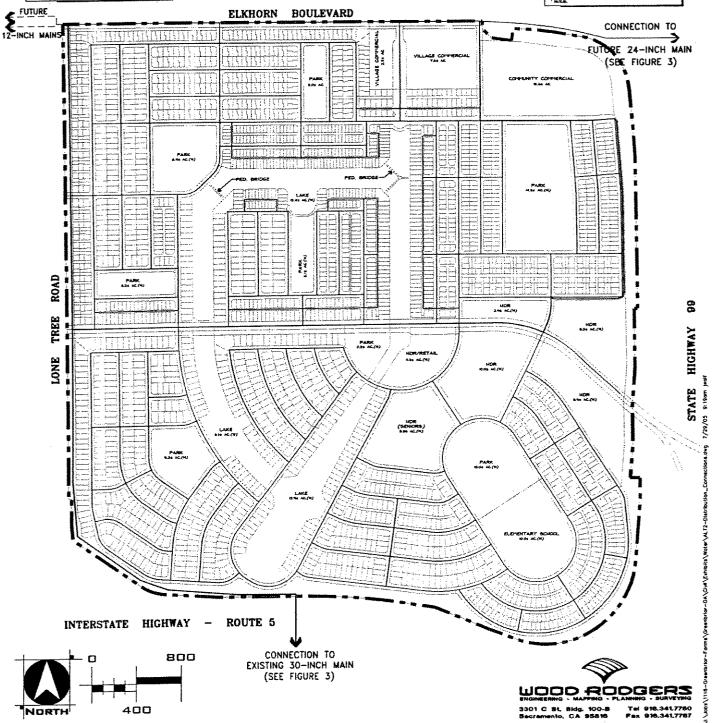


#### ALTERNATIVE 2 DISTRIBUTION SYSTEM CONNECTIONS

## **GREENBRIAR**

8-INCH DISTRIBUTION MAIN
12-INCH DISTRIBUTION MAIN
18-INCH TRANSISSION MAIN
24-INCH TRANSISSION MAIN
30-INCH TRANSISSION MAIN
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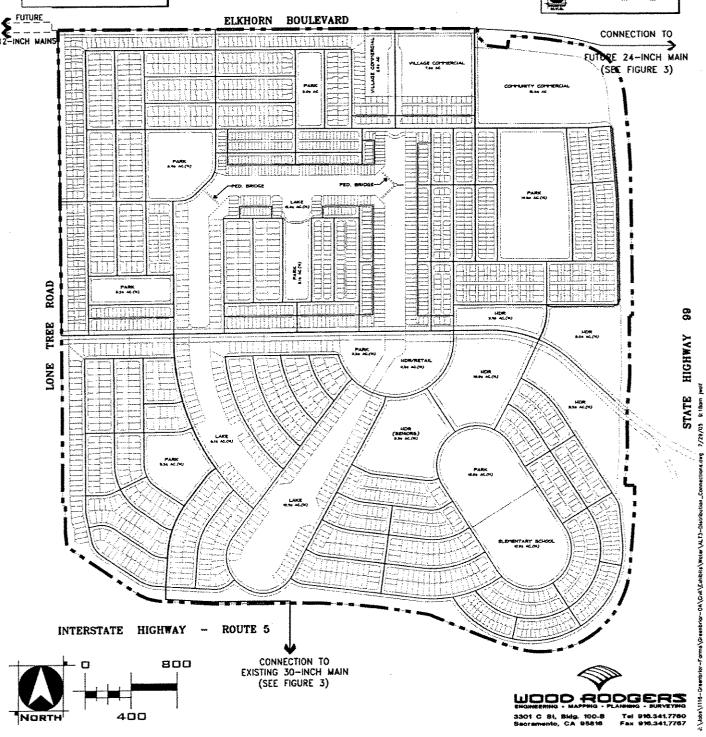


#### ALTERNATIVE 3 DISTRIBUTION SYSTEM CONNECTIONS

### **GREENBRIAR**

8-INCH DISTRIBUTION MAIN
12-INCH DISTRIBUTION MAIN
18-INCH TRANSSISSOM MAIN
24-INCH TRANSMISSION MAIN
30-INCH TRANSMISSION MAIN
GREENBRAR ROUNDARY







# APPENDIX C EXHIBIT - WATER DISTRIBUTION SYSTEM



#### APPENDIX D

#### HZONET ANALYSIS RESULTS

- AVERAGE DAY DEMANDS
- MAXIMUM DAY DEMANDS
- PEAK HOUR DEMANDS
- FIRE FLOW SUMMARY
- MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443
- MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313
- MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427



## AVERAGE DAY DEMANDS

**AVERAGE DAY DEMANDS - JUNCTION REPORT - GREENBRIAR** Head Pressure Demand Elevation ID (ft) (psi) (ft) (gpm) 20.00 104.30 36.53 0.00 **GB-101** 38.71 104.35 15.00 2.76 **GB-103** 104,44 37.02 19.00 2.76 **GB-105** 104.50 36.61 0.00 20.00 **GB-107** 36.29 104.75 21.00 15.62 **GB-108** 104.25 36.51 17.03 20.00 **GB-109** 36.51 20.00 104.25 9.46 **GB-111** 104.26 36.69 19.59 8.51 **GB-113** 18.97 104.32 36.98 14.19 **GB-115** 37.00 18.87 104.27 9.46 **GB-117** 37.02 18.84 104.27 10.76 **GB-119** 104.27 37.03 18.80 8.51 **GB-121** 37.11 18.80 104.44 15.86 **GB-122** 36.94 104.26 8.04 19.02 **GB-123** 18.39 104.27 37.21 13.72 **GB-125** 37.26 104.26 7.57 18.28 **GB-127** 37.23 104.41 23.20 18.50 **GB-128** 37.15 8.04 18.53 104.26 **GB-129** 104.26 37.46 17.81 13.24 **GB-131** 17.67 104.26 37.52 7.57 **GB-133** 17.23 104.27 37.71 6.62 **GB-135** 37.76 9.46 17.16 104.30 **GB-137** 37.48 17.85 104.34 9.46 **GB-139** 104.25 36.98 18.91 20.34 **GB-141** 18.52 104.25 37.15 12.30 **GB-143** 104.25 37.34 18.08 6.62 **GB-145** 104.25 37.70 17.24 12.39 **GB-147** 37.72 104.25 8.99 17.21 **GB-149** 104.26 37.81 16.99 10.41 GB-151 104.26 37.81 10.76 16.99 **GB-153** 104.27 37.84 3.78 16.94 **GB-155** 104.27 37.83 16.96 1.42 **GB-157** 104.28 37.98 16.62 3.20 GB-159 37.75 104.27 2.37 17.14 **GB-161** 5.20 17.39 104.28 37.65 **GB-163** 104.33 37.50 17.79 5.68 **GB-165** 18.26 104.31 37.28 13.18 **GB-167** 104.27 36.62 2.37 19.75 **GB-169** 

20.27

104.26

36.39

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**GB-171** 

4.73

AVERAGE DAY DEMANDS - JUNCTION REPORT - GREENBRIAR

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-173 | 15.81           | 20.84             | 104.25       | 36.14             |
| GB-175 | 0.95            | 16.69             | 104.26       | 37.94             |
| GB-177 | 3.31            | 16.45             | 104.25       | 38.04             |
| GB-179 | 5.68            | 16.82             | 104.25       | 37.88             |
| GB-181 | 3.31            | 16.63             | 104.25       | 37.97             |
| GB-183 | 11.35           | 16.54             | 104.25       | 38.01             |
| GB-185 | 18.92           | 16.64             | 104.25       | 37.96             |
| GB-187 | 10.41           | 16.47             | 104.26       | 38.04             |
| GB-189 | 4.73            | 16.36             | 104.26       | 38.08             |
| GB-191 | 10.30           | 16.28             | 104.25       | 38.12             |
| GB-193 | 6.48            | 16.24             | 104.26       | 38.14             |
| GB-195 | 6.48            | 16.38             | 104.24       | 38.07             |
| GB-197 | 11.35           | 16.75             | 104.24       | 37.91             |
| GB-199 | 11.35           | 17.29             | 104.24       | 37.68             |
| GB-201 | 13.24           | 17.77             | 104.25       | 37.47             |
| GB-203 | 16.96           | 18.25             | 104.25       | 37.26             |
| GB-205 | 16.96           | 19.83             | 104.23       | 36.57             |
| GB-207 | 13.24           | 20.34             | 104.23       | 36.35             |
| GB-209 | 6.62            | 20.85             | 104.23       | 36.13             |
| GB-210 | 10.34           | 15.00             | 104.28       | 38.69             |
| GB-211 | 25.54           | 18.60             | 104.27       | 37.12             |
| GB-213 | 12.30           | 17.80             | 104.25       | 37.46             |
| GB-215 | 16.65           | 17.16             | 104.25       | 37.73             |
| GB-217 | 6.62            | 16.45             | 104.25       | 38.04             |
| GB-219 | 7.09            | 16.33             | 104.18       | 38.07             |
| GB-221 | 9.63            | 16.30             | 104.18       | 38.08             |
| GB-223 | 10.24           | 16.58             | 104.18       | 37.96             |
| GB-225 | 5.68            | 16.63             | 104.18       | 37.93             |
| GB-227 | 6.15            | 16.52             | 104.18       | 37.98             |
| GB-229 | 10.48           | 16.65             | 104.18       | 37.92             |
| GB-231 | 10.41           | 16.65             | 104.18       | 37.92             |
| GB-233 | 6.62            | 16.59             | 104.18       | 37.95             |
| GB-235 | 10.41           | 17.04             | 104.18       | 37.76             |
| GB-237 | 6.96            | 16.54             | 104.18       | 37.98             |
| GB-239 | 6.96            | 16.37             | 104.21       | 38.06             |
| GB-241 | 13.24           | 16.74             | 104.21       | 37.90             |
| GB-243 | 14.19           | 17.28             | 104.21       | 37.67             |
| GB-245 | 13.24           | 17.76             | 104.21       | 37.46             |
| GB-247 | 8.99            | 18.25             | 104.22       | 37.25             |

**AVERAGE DAY DEMANDS - JUNCTION REPORT - GREENBRIAR** Head Pressure Elevation Demand ID (ft) (psi) (ft) (gpm) 19.30 104.21 36.79 19.80 **GB-249** 19.87 104.21 36.55 8.99 **GB-251** 20.36 104.21 36.33 13.24 GB-253 104.21 36.12 17.71 20.86 GB-255 104.25 37.31 18.14 11.82 **GB-257** 37.46 104.24 5.68 17.78 GB-259 104.24 37.74 6.15 17.15 **GB-261** 104.24 38.03 7.09 16.46 **GB-263** 37.37 104.24 13.88 18.00 **GB-265** 16.46 104.22 38.03 11.04 **GB-267** 37.99 16.52 104.19 10.41 **GB-269** 37.58 9.93 17.44 104.18 **GB-271** 37.34 104.18 5.68 18.00 **GB-273** 104.18 37.34 18.00 5.28 **GB-275** 5.68 18.00 104.18 37.34 **GB-277** 104.18 37.45 17.76 10.41 **GB-279** 104.18 37.76 5.20 17.04 **GB-281** 104.19 37.66 17.28 11.82 GB-283 104.19 36.69 19.52 14.19 GB-285 36.11 9.46 20.86 104.21 **GB-286** 104.25 37.37 9.46 18.00 **GB-287** 104.21 38.03 5.20 16.45 **GB-288** 104.19 37.99 3.78 16.52 **GB-289** 104.19 37.35 18.00 6.15 **GB-290** 37.76 8.99 17.04 104.18 **GB-291** 38.05 16.37 104.19 4.26 **GB-292** 37.89 7.57 16.74 104.18 **GB-293** 104.18 37.66 17.28 5.87 GB-294 15.00 104.27 38.68 0.00 **GB-295** 37.37 18.00 104.25 0.00 **GB-297** 104.21 38.02 16.45 0.00 **GB-299** 104.20 37.99 0.00 16.53 **GB-301** 37.35 18.00 104.19 0.00 GB-303 37.76 17.05 104.18 0.00 **GB-305** 37.84 104.18 0.00 16.86 **GB-307** 104.18 37.65 17.28 0.00 **GB-309** 36.85 19.13 104.18

20.80

18.00

104.18

104.10

36.13

37.31

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**GB-311** 

**GB-313** 

**GB-315** 

18.00

23.40

8.51

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-317 | 8.04            | 17.77             | 104.11       | 37.41             |
| GB-319 | 5.20            | 17.24             | 104.12       | 37.65             |
| GB-321 | 5.20            | 16.45             | 104.17       | 38.01             |
| GB-323 | 12.30           | 16.54             | 104.08       | 37.93             |
| GB-325 | 9.93            | 17.42             | 104.08       | 37.55             |
| GB-327 | 8.04            | 18.00             | 104.08       | 37.30             |
| GB-329 | 5.68            | 18.00             | 104.08       | 37.30             |
| GB-331 | 2.37            | 17.39             | 104.09       | 37.56             |
| GB-333 | 6.62            | 17.35             | 104.12       | 37.60             |
| GB-335 | 5.68            | 16.42             | 104.13       | 38.00             |
| GB-337 | 10.41           | 18.00             | 104.10       | 37.31             |
| GB-339 | 8.99            | 18.00             | 104.10       | 37.31             |
| GB-341 | 7.47            | 17.49             | 104.10       | 37.53             |
| GB-343 | 6.05            | 16.16             | 104.11       | 38.11             |
| GB-345 | 8.04            | 18.00             | 104.09       | 37.30             |
| GB-347 | 9.46            | 18.00             | 104.09       | 37.30             |
| GB-349 | 3.78            | 17.75             | 104.09       | 37.41             |
| GB-351 | 11.82           | 18.00             | 104.08       | 37.30             |
| GB-352 | 16.75           | 17.35             | 104.08       | 37.58             |
| GB-353 | 8.99            | 17.91             | 104.08       | 37.34             |
| GB-355 | 7.57            | 17.82             | 104.09       | 37.38             |
| GB-357 | 8.42            | 17.40             | 104.09       | 37.56             |
| GB-359 | 6.53            | 16.14             | 104.09       | 38.11             |
| GB-361 | 8.99            | 17.26             | 104.08       | 37.62             |
| GB-362 | 11.35           | 16.38             | 104.09       | 38.00             |
| GB-363 | 6.15            | 16.29             | 104.08       | 38.04             |
| GB-365 | 7.88            | 16.32             | 104.08       | 38.03             |
| GB-367 | 10.69           | 16.59             | 104.08       | 37.91             |
| GB-369 | 9.46            | 17.03             | 104.08       | 37.72             |
| GB-371 | 7.57            | 16.87             | 104.08       | 37.79             |
| GB-373 | 5.68            | 16.73             | 104.08       | 37.85             |
| GB-375 | 8.18            | 16.59             | 104.09       | 37.92             |
| GB-377 | 10.18           | 16.34             | 104.10       | 38.02             |
| GB-379 | 25.22           | 17.08             | 104.11       | 37.71             |
| GB-381 | 14.44           | 16.42             | 104.08       | 37.98             |
| GB-383 | 9.71            | 18.29             | 104.08       | 37.17             |
| GB-385 | 5.92            | 18.09             | 104.10       | 37.27             |
| GB-387 | 8.54            | 18.82             | 104.10       | 36.95             |
| GB-389 | 5.20            | 18.79             | 104.11       | 36.97             |

AVERAGE DAY DEMANDS - JUNCTION REPORT - GREENBRIAR

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-391 | 21.23           | 18.77             | 104.13       | 36.99             |
| GB-393 | 8.35            | 16.43             | 104.07       | 37.98             |
| GB-395 | 8,51            | 17.71             | 104.07       | 37.42             |
| GB-397 | 20.84           | 18.80             | 104.08       | 36.95             |
| GB-399 | 19.43           | 19.79             | 104.09       | 36.53             |
| GB-401 | 10.88           | 20.09             | 104.09       | 36.40             |
| GB-403 | 6.15            | 20.39             | 104.09       | 36.27             |
| GB-405 | 6.43            | 16.13             | 104.07       | 38.11             |
| GB-407 | 12.30           | 17.95             | 104.07       | 37.32             |
| GB-409 | 7.57            | 19.40             | 104.08       | 36.69             |
| GB-411 | 9.46            | 16.46             | 104.07       | 37.96             |
| GB-413 | 14.66           | 18.20             | 104.07       | 37.21             |
| GB-415 | 7.57            | 19.96             | 104.07       | 36.45             |
| GB-417 | 19.59           | 16.45             | 104.07       | 37.97             |
| GB-419 | 6.15            | 18.63             | 104.07       | 37.02             |
| GB-421 | 18.55           | 19.83             | 104.07       | 36.50             |
| GB-423 | 6.15            | 20.20             | 104.07       | 36.34             |
| GB-425 | 12.27           | 20.56             | 104.07       | 36.19             |
| GB-427 | 6.15            | 21.58             | 104.08       | 35.75             |
| GB-429 | 15.10           | 21.13             | 104.08       | 35.94             |
| GB-431 | 12.30           | 21.45             | 104.08       | 35.80             |
| GB-433 | 19.03           | 22.00             | 104.08       | 35.56             |
| GB-435 | 9.46            | 21.27             | 104.07       | 35.88             |
| GB-437 | 9.93            | 22.00             | 104.07       | 35.56             |
| GB-439 | 9.93            | 22.00             | 104.07       | 35.56             |
| GB-441 | 6.15            | 21.27             | 104.07       | 35.88             |
| GB-443 | 6.62            | 22.00             | 104.07       | 35.56             |
| GB-445 | 6.15            | 21.00             | 104.07       | 36.00             |
| GB-446 | 0.00            | 22.00             | 104.27       | 35.65             |
| GB-447 | 0.00            | 26.00             | 105.48       | 34.44             |

AVERAGE DAY DEMANDS - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos: |
|------|----------------|------------------|-----------|---------------|--------------------|----------|
| P101 | 117.50         | 8.00             | 130.00    | 32.23         | 0.21               | 0.00     |
| P102 | 117.50         | 8.00             | 130.00    | -60.42        | 0.39               | 0.01     |
| P103 | 739.21         | 8.00             | 130.00    | 40.96         | 0.26               | 0.04     |
| P104 | 117.50         | 8.00             | 130.00    | 39.01         | 0.25               | 0.01     |
| P105 | 117.50         | 8.00             | 130.00    | 47.12         | 0.30               | 0.01     |
| P106 | 436.40         | 12.00            | 130.00    | 21.90         | 0.06               | 0.000    |
| P107 | 650.57         | 8.00             | 130.00    | 17.22         | 0.11               | 0.01     |
| P108 | 535,27         | 8.00             | 130.00    | 14.47         | 0.09               | 0.00     |
| P109 | 357.35         | 18.00            | 130.00    | -723.26       | 0.91               | 0.07     |
| P110 | 243.09         | 12.00            | 130.00    | -65.63        | 0.19               | 0.00     |
| P111 | 253.19         | 8.00             | 130.00    | -17.22        | 0.11               | 0.00     |
| P112 | 380.98         | 8.00             | 130.00    | 35.81         | 0.23               | 0.01     |
| P113 | 904.24         | 8.00             | 130.00    | 5.40          | 0.03               | 0.00     |
| P114 | 693.26         | 8.00             | 130.00    | -30.28        | 0.19               | 0.02     |
| P115 | 105.50         | 8.00             | 130.00    | -5.22         | 0.03               | 0.000    |
| P116 | 147.51         | 12.00            | 130.00    | 44.63         | 0.13               | 0.00     |
| P117 | 132.50         | 12.00            | 130.00    | -49.10        | 0.14               | 0.00     |
| P118 | 226.54         | 8.00             | 130.00    | 30.42         | 0.19               | 0.01     |
| P119 | 193.01         | 8.00             | 130.00    | 8.31          | 0.05               | 0.000    |
| P120 | 193.01         | 8.00             | 130.00    | -8.73         | 0.06               | 0.000    |
| P121 | 713.00         | 8.00             | 130.00    | 6.72          | 0.04               | 0.00     |
| P122 | 615.89         | 8.00             | 130.00    | -6.48         | 0.04               | 0.000    |
| P123 | 713.00         | 8.00             | 130.00    | -50.80        | 0.32               | 0.05     |
| P124 | 677.66         | 8.00             | 130.00    | -38.32        | 0.24               | 0.03     |
| P125 | 476.65         | 8.00             | 130.00    | -35.69        | 0.23               | 0.02     |
| P126 | 117.50         | 8.00             | 130.00    | -31.43        | 0.20               | 0.00     |
| P127 | 677.66         | 8.00             | 130.00    | 40.74         | 0.26               | 0.03     |
| P128 | 193.00         | 8.00             | 130.00    | -8.76         | 0.06               | 0.000    |
| P129 | 117.50         | 8.00             | 130.00    | -33.43        | 0.21               | 0.00     |
| P130 | 633.34         | 8.00             | 130.00    | 16.67         | 0.11               | 0.01     |
| P131 | 232.72         | 8.00             | 130.00    | 24.89         | 0.16               | 0.00     |
| P132 | 233.02         | 8.00             | 130.00    | 26.45         | 0.17               | 0.01     |
| P133 | 618.66         | 8.00             | 130.00    | 20.17         | 0.13               | 0.01     |
| P134 | 713.00         | 8.00             | 130.00    | -14.89        | 0.10               | 0.01     |
| P135 | 195.00         | 8.00             | 130.00    | 18.12         | 0.12               | 0.00     |
| P136 | 193.00         | 8.00             | 130.00    | 33.89         | 0.22               | 0.01     |
| P137 | 112.20         | 18.00            | 130.00    | 666.03        | 0.84               | 0.02     |
| P138 | 701.50         | 8.00             | 130.00    | -47.77        | 0.30               | 0.05     |
| P139 | 378.03         | 8.00             | 130.00    | -53.11        | 0.34               | 0.03     |

AVERAGE DAY DEMANDS - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlo:<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|-----------------|
| P140 | 586.50         | 8.00             | 130.00    | -13.30        | 0.08               | 0.00            |
| P141 | 253.00         | 8.00             | 130.00    | 18.97         | 0.12               | 0.00            |
| P142 | 233.00         | 8.00             | 130.00    | -22.37        | 0.14               | 0.00            |
| P143 | 233.00         | 8.00             | 130.00    | -29.69        | 0.19               | 0.01            |
| P144 | 232.70         | 8.00             | 130.00    | -17.56        | 0.11               | 0.00            |
| P145 | 574.54         | 8.00             | 130.00    | 11.80         | 0.08               | 0.00            |
| P146 | 105.50         | 8.00             | 130.00    | 46.31         | 0.30               | 0.01            |
| P147 | 126.23         | 8.00             | 130.00    | 25.67         | 0.16               | 0.00            |
| P148 | 126.78         | 8.00             | 130.00    | -8.06         | 0.05               | 0.000           |
| P149 | 388.16         | 8.00             | 130.00    | 8.80          | 0.06               | 0.00            |
| P150 | 117.50         | 8.00             | 130.00    | 3.96          | 0.03               | 0.0000          |
| P151 | 611.16         | 8.00             | 130.00    | -7.22         | 0.05               | 0.00            |
| P152 | 418.00         | 8.00             | 130.00    | -0.05         | 0.000              | O.0000          |
| P153 | 97.50          | 8.00             | 130.00    | -0.23         | 0.00               | 0.00            |
| P154 | 261.76         | 8.00             | 130.00    | -4.68         | 0.03               | 0.000           |
| P155 | 839.51         | 8.00             | 130.00    | -7.06         | 0.05               | 0.00            |
| P156 | 170.40         | 8.00             | 130.00    | 2.31          | 0.01               | O.0000          |
| P157 | 116.20         | 8.00             | 130.00    | 0.00          | 0.000              | 0.00            |
| P158 | 248.92         | 8.00             | 130.00    | -5.49         | 0.04               | 0.000           |
| P159 | 247.10         | 8.00             | 130.00    | 8.50          | 0.05               | 0.000           |
| P160 | 247.67         | 8.00             | 130.00    | 18.41         | 0.12               | 0.00            |
| P161 | 247.82         | 8.00             | 130.00    | 28.53         | 0.18               | 0.01            |
| P162 | 247.00         | 8.00             | 130.00    | -17.68        | 0.11               | 0.00            |
| P163 | 249.87         | 8.00             | 130.00    | -11.98        | 0.08               | 0.00            |
| P164 | 1,149.31       | 8.00             | 130.00    | 5.72          | 0.04               | 0.00            |
| P165 | 710.72         | 12.00            | 130.00    | -35.85        | 0.10               | 0.00            |
| P166 | 369.00         | 8.00             | 130.00    | 13.48         | 0.09               | 0.00            |
| P167 | 253.00         | 8.00             | 130.00    | 9.69          | 0.06               | 0.000           |
| P168 | 918.21         | 8.00             | 130.00    | 9.22          | 0.06               | 0.00            |
| P169 | 282.81         | 8.00             | 130.00    | 24.29         | 0.16               | 0.01            |
| P170 | 333.36         | 12.00            | 130.00    | -57.99        | 0.16               | 0.00            |
| P171 | 253.00         | 8.00             | 130.00    | 41.19         | 0.26               | 0.01            |
| P172 | 234.54         | 8.00             | 130.00    | 27.59         | 0.18               | 0.01            |
| P173 | 253.00         | 8.00             | 130.00    | 19.68         | 0.13               | 0.00            |
| P174 | 657.99         | 8.00             | 130.00    | 16.52         | 0.11               | 0.01            |
| P175 | 633.34         | 8.00             | 130.00    | 6.36          | 0.04               | 0.000           |
| P176 | 253.02         | 8.00             | 130.00    | 5.50          | 0.04               | 0.000           |
| P177 | 633.34         | 8.00             | 130.00    | 27.27         | 0.17               | 0.01            |
| P178 | 242.02         | 12.00            | 130.00    | 132.25        | 0.38               | 0.01            |

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>(ft) |
|------|----------------|---------------|-----------|---------------|--------------------|------------------|
| P179 | 253.00         | 8.00          | 130.00    | 49.48         | 0.32               | 0.02             |
| P180 | 273.00         | 8.00          | 130.00    | -23.28        | 0.15               | 0.00             |
| P181 | 628.13         | 12.00         | 130.00    | 6.61          | 0.02               | 0.000            |
| P182 | 797.55         | 12.00         | 130.00    | 14.96         | 0.04               | 0.000            |
| P183 | 578.83         | 12.00         | 130.00    | 43.19         | 0.12               | 0.00             |
| P184 | 193.00         | 8.00          | 130.00    | -4.39         | 0.03               | 0.000            |
| P185 | 653.19         | 8.00          | 130.00    | 6.10          | 0.04               | 0.000            |
| P186 | 193.00         | 8.00          | 130.00    | -0.65         | 0.00               | O.00000          |
| P187 | 193.00         | 8.00          | 130.00    | 0.16          | 0.000              | 0.00             |
| P188 | 437.56         | 8.00          | 130.00    | 4.25          | 0.03               | 0.000            |
| P189 | 203.57         | 12.00         | 130.00    | -14.06        | 0.04               | 0.000            |
| P190 | 596.95         | 8.00          | 130.00    | 24.63         | 0.16               | 0.01             |
| P191 | 292.91         | 8.00          | 130.00    | -3.17         | 0.02               | 0.000            |
| P192 | 695.05         | 8.00          | 130.00    | -2.35         | 0.01               | 0.000            |
| P193 | 253.00         | 8.00          | 130.00    | 4.72          | 0.03               | 0.000            |
| P194 | 656.00         | 8.00          | 130.00    | -18.21        | 0.12               | 0.01             |
| P195 | 504.88         | 8.00          | 130.00    | -20.86        | 0.13               | 0.01             |
| P196 | 313.32         | 8.00          | 130.00    | -12.75        | 80.0               | 0.00             |
| P197 | 549.00         | 8.00          | 130.00    | 19.58         | 0.13               | 0.01             |
| P198 | 253.00         | 8.00          | 130.00    | 15.28         | 0.10               | 0.00             |
| P199 | 253.00         | 8.00          | 130.00    | 26.91         | 0.17               | 0.01             |
| P200 | 253.00         | 8.00          | 130.00    | 43.03         | 0.27               | 0.01             |
| P201 | 403.00         | 8.00          | 130.00    | 20.51         | 0.13               | 0.01             |
| P202 | 276.11         | 8.00          | 130.00    | 75.19         | 0.48               | 0.04             |
| P203 | 253.02         | 8.00          | 130.00    | -46.85        | 0.30               | 0.02             |
| P204 | 253.02         | 8.00          | 130.00    | -24.39        | 0.16               | 0.00             |
| P205 | 236.90         | 8.00          | 130.00    | -10.35        | 0.07               | 0.000            |
| P206 | 636.18         | 8.00          | 130.00    | 16.97         | 0.11               | 0.01             |
| P207 | 211.30         | 8.00          | 130.00    | 10.28         | 0.07               | 0.000            |
| P208 | 232.70         | 8.00          | 130.00    | 27.39         | 0.17               | 0.01             |
| P209 | 233.00         | 8.00          | 130.00    | 42.55         | 0.27               | 0.01             |
| P210 | 233.00         | 8.00          | 130.00    | 91.33         | 0.58               | 0.05             |
| P211 | 621.42         | 8.00          | 130.00    | -57.44        | 0.37               | 0.06             |
| P212 | 253.02         | 8.00          | 130.00    | -34.60        | 0.22               | 0.01             |
| P213 | 699.07         | 8.00          | 130.00    | -9.54         | 0.06               | 0.00             |
| P214 | 253.02         | 8.00          | 130.00    | 3.61          | 0.02               | 0.000            |
| P215 | 613.13         | 8.00          | 130.00    | 2.01          | 0.01               | 0.000            |
| P216 | 253.00         | 8.00          | 130.00    | 25.96         | 0.17               | 0.01             |
| P217 | 233.00         | 8.00          | 130.00    | 23.72         | 0.15               | 0.00             |

**AVERAGE DAY DEMANDS - PIPE REPORT - GREENBRIAR** Headloss Velocity Flow Length Diameter Roughness ID (ft) (ft/s) (in) (gpm) (ft) 42.05 0.01 8.00 130.00 0.27 289.50 P218 0.22 0.01 130.00 -34.56 8.00 P219 313.50 0.49 0.04 12.00 130.00 172.59 391.14 P220 0.00 130.00 12.57 0.08 590.71 8.00 P221 0.00 13.92 0.09 253.00 8.00 130.00 P222 0.01 390.32 8.00 130.00 30.54 0.19 P223 0.01 130.00 21.89 0.14 430.55 8.00 P224 130.00 137.77 0.39 0.02 248.33 12.00 P225 0.00 8.00 130.00 13.54 0.09430.73 P226 0.31 0.02 12.00 130.00 109.83 412.22 P227 14.35 0.04 0.000262.25 12.00 130.00 P228 130.00 27,32 80.0 0.000 12.00 253.00 P229 0.12 0.00 12.00 130.00 42.62 273.31 P230 0.01 0.22 130.00 75.93 P231 234,73 12.00 130.00 -76.56 0.22 0.01 422.16 12.00 P232 0.01 0.19 130.00 -66.14 596.34 12.00 P233 0.12 0.00 130.00 -41.77 591.74 12.00 P234 0.07 0.56 587.67 12.00 130.00 -197.91 P235 0.01 0.22 130.00 -76.88 457.95 12.00 P236 12.00 130.00 24.76 0.07 0.000 359.68 P237 0.0000 -2.02 0.01 8.00 130.00 193.00 P238 0.27 0.03 487.33 8.00 130.00 42.82 P239 0.02 0.23 8.00 130.00 -35.68 486.84 P240 0.19 0.02 -30.378.00 130.00 708.39 P241 0.02 617.10 8.00 130.00 -28.35 0.18 P242 0.01 -276.07 0.35 18.00 130.00 P243 319.69 0.00 130.00 -23.40 0.07 861.88 12.00 P244 0.00 -120.42 0.15 18.00 130.00 534.05 P245 -75.79 0.10 0.00 130.00 18.00 627.02 P246 0.00 0.16 195.01 18.00 130.00 -124.89 P247 0.03 0.000 21.66 18.00 130.00 751.91 P248 0.05 -213.01 0.60 370.87 12.00 130.00 P249 -26.06 0.17 0.01 602.79 8.00 130.00 P250 0.00 -12.90 80.0 8.00 130.00 656.30 P251 0.04 0.32 501.81 8.00 130.00 -50.07 P252 0.02 95.72 0.27 464.05 12.00 130.00 P253 0.01 130.00 89.76 0.25 12.00 P254 250.56 -12.84 80.0 0.00 8.00 130.00 423.72 P255 -17.96 0.11 0.00 235.04 8.00 130.00 P256

**AVERAGE DAY DEMANDS - PIPE REPORT - GREENBRIAR** Velocity Headloss **Length** Diameter Flow ID Roughness (ft/s) (in) (gpm) (ft) (ft) 0.01 8.00 130.00 29.15 0.19 344.48 P257 130.00 14.71 0.09 0.00 8.00 656.00 P258 130.00 8.00 15.72 0.10 0.00 P259 497.14 0.000 8.00 130.00 -6.44 0.04 494.52 P260 8.00 130.00 -5.37 0.03 0.000 P261 466.36 0.000 8.00 130.00 -3.87 0.02 616.00 P262 130.00 2.12 0.01 0.000 651.25 8.00 P263 0.00 8.00 130.00 22.96 0.15 246.49 P264 0.27 0.01 12.00 130.00 -95.80 375.42 P265 0.02 665.79 8.00 130.00 27.63 0.18 P266 8.00 130.00 -8.64 0.06 0.000 285.98 P267 0.00 8.00 130.00 10.48 0.07 272.69 P268 130.00 8.01 0.05 0.00 8.00 P269 744.21 8.00 130.00 2.37 0.02 O.0000 105.50 P270 14.09 0.090.01 8.00 130.00 892.22 P271 0.04 0.000 8.00 130.00 6.55 193.00 P272 0.000 8.00 130.00 10.00 0.06 105.50 P273 O.0000 130.00 -1.430.01 8.00 698.75 P274 181.50 12.00 130.00 -213.76 0.61 0.03 P275 0.21 0.00 130.00 -33.19 8.00 P276 112.20 80.0 0.00 698.70 8.00 130.00 -12.99 P277 0.03 0.0008.00 130.00 -4.56 713.00 P278 0.16 0.01 130.00 -25.20 422.00 8.00 P279 O.0000 117.50 8.00 130.00 4.32 0.03 P280 0.60 0.14 8.00 130.00 -94.61 589.97 P281 8.00 130.00 -73.84 0.47 0.02 130.50 P282 80.0 18.00 130.00 -746.46 0.94 410.65 P283 130.00 -66.46 0.42 0.06 8.00 500.49 P284 130.00 12.16 80.0 0.00 807.99 8.00 P285 0.0000 130.00 1.31 0.01 8.00 193.00 P286 0.0000 8.00 130.00 -2.19 0.01 263.00 P287 8.00 130.00 10.37 0.07 0.00 738.30 P288 130.00 -14.32 0.09 0.00 8.00 P289 233.02 -30.27 0.19 0.02 739.64 8.00 130.00 P290 0.000 8.00 130.00 -8.84 0.06 252.00 P291 262.03 8.00 130.00 -22.63 0.14 0.00 P292 8.00 130.00 -4.53 0.03 0.000 924.17 P293 -3.25 0.02 0.000 8.00 130.00 770.75 P294 12.78 80.0 0.01 956.68 8.00 130.00 P295

**AVERAGE DAY DEMANDS - PIPE REPORT - GREENBRIAR** Headloss Lenath Diameter Flow Velocity Roughness ID (ft) (in) (gpm) (ft/s) (ft) 693.81 8.00 130.00 -42.91 0.27 0.04 P296 678.13 8.00 130.00 31.09 0.20 0.02 P297 8.00 130.00 10.76 0.07 00.0 837.42 P298 8.00 557.94 130.00 -33.81 0.22 0.02 P299 -2.34 8.00 130.00 0.01 0.000 696.14 P300 468.04 8.00 130.00 -4.45 0.03 0.000 P301 130.00 -18.91 0.12 0.00 255.36 8.00 P302 130.00 21.27 0.00 8.00 0.14 247.32 P303 12.00 130.00 -252.98 0.72 0.04 208.11 P304 0.04 0.000 8.00 130.00 5.68 P305 88.53 130.00 -97.85 193.00 8.00 0.62 0.05 P306 0.12 0.01 8.00 130.00 18.13 P307 582.27 130.00 -41.12 0.26 0.03 677.66 8.00 P308 195.00 8.00 130.00 -41.64 0.27 0.01 P309 12.00 0.15 130.00 -51.36 0.00 132.50 P310 8.00 130.00 -42.70 0.27 0.02 380.98 P311 8.00 130.00 -39.42 0.25 0.02 475.68 P312 8.00 130.00 -14.06 0.09 0.00 655.89 P313 8.00 130.00 -20.70 0.13 0.01 P314 653.93 0.19 0.00 O.00000 8.00 130.00 215.00 P315 195.01 8.00 130.00 9.24 0.06 0.000 P316 8.00 130.00 -11.54 0.07 0.00 214.88 P317 252.22 8.00 130.00 3.23 0.02 0.000 P318 0.02 0.000 00.8 130.00 3.87 P319 245.38 130.00 0.05 0.00 8.00 -7.69 607.50 P320 0.08 130.00 0.00 574.53 8.00 -11.94 P321 8.00 130.00 -28.97 0.18 0.00 105.50 P322 212.18 8.00 130.00 11.66 0.07 0.00 P323 0.04 0.000 8.00 130.00 6.62 P324 105.50 8.00 130.00 -6.95 0.04 0.000 211.00 P325 8.00 130.00 -19.88 0.13 0.00 211.30 P326 8.00 130.00 -16.39 0.10 0.00 209.82 P327 130.00 -7.73 0.05 0.00 728.60 8.00 P328 0.01 8.00 130.00 0.89 0.00 594.64 P329 8.00 130.00 -8.40 0.05 0.000 258.06 P330 0.03 130.00 4.45 0.000 499.01 8.00 P331 80.0 130.00 -12.47 0.00 545.88 8.00 P332 783.02 8.00 130.00 -10.08 0.06 0.00 P333

130.00

-24.46

0.07

0.000

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12.00

260.55

P334

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm)  | Velocity<br>(ft/s) | Headloss (ft) |
|------|----------------|------------------|-----------|----------------|--------------------|---------------|
| P335 | 255.00         | 8.00             | 130.00    | 13.25          | 0.08               | 0.00          |
| P336 | 255.00         | 8.00             | 130.00    | 9.26           | 0.06               | 0.000         |
| P337 | 255.07         | 8.00 -           | 130.00    | 5.87           | 0.04               | 0.000         |
| P338 | 255.00         | 12.00            | 130.00    | 148.88         | 0.42               | 0.02          |
| P339 | 255.00         | 12.00            | 130.00    | -109.86        | 0.31               | 0.01          |
| P340 | 255.00         | 8.00             | 130.00    | -9.00          | 0.06               | 0.000         |
| P341 | 255.00         | 8.00             | 130.00    | -10.70         | 0.07               | 0.00          |
| P342 | 246.98         | 8.00             | 130.00    | -6.58          | 0.04               | 0.000         |
| P343 | 253.00         | 8.00             | 130.00    | -23.23         | 0.15               | 0.00          |
| P344 | 147.50         | 12.00            | 130.00    | 42.41          | 0.12               | 0.00          |
| P345 | 147.37         | 12.00            | 130.00    | 68.13          | 0.19               | 0.00          |
| P346 | 147.50         | 12.00            | 130.00    | 82.65          | 0.23               | 0.00          |
| P347 | 147.59         | 12.00            | 130.00    | -96.18         | 0.27               | 0.00          |
| P348 | 381.04         | 8.00             | 130.00    | -21.39         | 0.14               | 0.01          |
| P349 | 190.72         | 18.00            | 130.00    | -306.17        | 0.39               | 0.01          |
| P350 | 253.02         | 8.00             | 130.00    | 15.60          | 0.10               | 0.00          |
| P351 | 233.00         | 8.00             | 130.00    | -4.78          | 0.03               | 0.000         |
| P352 | 1,365.42       | 24.00            | 130.00    | 613.00         | 0.43               | 0.05          |
| P353 | 1,505.76       | 30.00            | 130.00    | -613.00        | 0.28               | 0.02          |
| P354 | 369.99         | 8.00             | 130.00    | -30.12         | 0.19               | 0.01          |
| P355 | 369.99         | 8.00             | 130.00    | -34.73         | 0.22               | 0.01          |
| P356 | 117.50         | 8.00             | 130.00    | -14.68         | 0.09               | 0.000         |
| P357 | 195.00         | 8.00             | 130.00    | -30.17         | 0.19               | 0.01          |
| P358 | 193.00         | 8.00             | 130.00    | -31.63         | 0.20               | 0.01          |
| P359 | 500.49         | 8.00             | 130.00    | -51.01         | 0.33               | 0.04          |
| P360 | 500.78         | 8.00             | 130.00    | -76.70         | 0.49               | 0.08          |
| P361 | 677.66         | 8.00             | 130.00    | -40.58         | 0.26               | 0.03          |
| P362 | 482.45         | 12.00            | 130.00    | -22.37         | 0.06               | 0.00          |
| P363 | 677.66         | 8.00             | 130.00    | -38.86         | 0.25               | 0.03          |
| P364 | 1,180.18       | 30.00            | 130.00    | -470.41        | 0.21               | 0.01          |
| P365 | 1,577.01       | 24.00            | 130.00    | -829.52        | 0.59               | 0.10          |
| P366 | 701.50         | 24.00            | 130.00    | <b>-942.75</b> | 0.67               | 0.05          |
| P367 | 242.00         | 18.00            | 130.00    | 470.41         | 0.59               | 0.02          |
| P368 | 738.68         | 18.00            | 130.00    | 387.76         | 0.49               | 0.04          |
| P369 | 253.00         | 8.00             | 130.00    | -11.92         | 0.08               | 0.00          |
| P370 | 660.09         | 8.00             | 130.00    | -32.58         | 0.21               | 0.02          |
| P371 | 193.00         | 18.00            | 130.00    | 485.80         | 0.61               | 0.02          |
| P372 | 595.91         | 18.00            | 130.00    | 406.16         | 0.51               | 0.04          |
| P373 | 191.34         | 18.00            | 130.00    | 353.72         | 0.45               | 0.01          |

AVERAGE DAY DEMANDS - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(în) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss (ft) |
|------|----------------|------------------|-----------|---------------|--------------------|---------------|
| P374 | 105.50         | 8.00             | 130.00    | 2.70          | 0.02               | 0.0000        |
| P375 | 607.50         | 8.00             | 130.00    | -13.23        | 0.08               | 0.00          |
| P376 | 438.00         | 18.00            | 130.00    | 230.96        | 0.29               | 0.01          |
| P377 | 650.57         | 18.00            | 130.00    | 162.83        | 0.21               | 0.01          |
| P378 | 112.20         | 8.00             | 130.00    | -79.81        | 0.51               | 0.02          |
| P379 | 117.50         | 8.00             | 130.00    | 31.99         | 0.20               | 0.00          |
| P380 | 348.36         | 8.00             | 130.00    | 15.25         | 0.10               | 0.00          |
| P381 | 178.10         | 12.00            | 130.00    | -110.47       | 0.31               | 0.01          |
| P382 | 1,122.42       | 24.00            | 130.00    | -1,689.21     | 1.20               | 0.26          |
| P383 | 93.09          | 8.00             | 130.00    | -43.04        | 0.27               | 0.01          |
| P384 | 195.01         | 8.00             | 130.00    | 14.19         | 0.09               | 0.00          |
| P385 | 4,416.05       | 30.00            | 130.00    | 0.00          | 0.00               | 0.00          |
| P386 | 3,100.00       | 24.00            | 130.00    | -1,704.83     | 1.21               | 0.72          |
| P388 | 1,581.75       | 18.00            | 130.00    | 254.68        | 0.32               | 0.04          |
| P389 | 621.96         | 18.00            | 130.00    | 238.26        | 0.30               | 0.02          |
| P990 | 235.86         | 99.00            | 130.00    | 0.00          | 0.00               | 0.00          |
| P991 | 377.34         | 99.00            | 130.00    | 0.00          | 0.00               | 0.00          |
| P992 | 233.99         | 99.00            | 130.00    | 1,704.83      | 0.07               | 0.0000        |
| P993 | 232.72         | 99.00            | 130.00    | 1,704.83      | 0.07               | 0.0000        |

AVERAGE DAY DEMANDS - PUMP REPORT - GREENBRIAR

| ID      | Elevation<br>(ft) | Downstream Pressure (psi) | Flow<br>(gpm) | Head Gain<br>(ft) |
|---------|-------------------|---------------------------|---------------|-------------------|
| PUMP105 | 22.00             | 35.65                     | 0.00          | 0.00              |
| PUMP107 | 26.00             | 34.44                     | 1,704.83      | 105.48            |



### MAXIMUM DAY DEMANDS

**MAXIMUM DAY DEMANDS - JUNCTION REPORT - GREENBRIAR** Demand Elevation Head Pressure ID (ft) (ft) (gpm) (psi) 93.16 31.70 0.00 20.00 **GB-101** 93.30 33.93 4.98 15.00 **GB-103** 93.59 32.32 19.00 4.98 **GB-105** 0.00 20.00 93.75 31.96 **GB-107** 94.51 31.85 28.11 21.00 **GB-108** 93.02 31.64 30.65 20.00 GB-109 93.03 17.03 20.00 31.64 **GB-111** 93.06 19.59 31.83 15.33 **GB-113** 93.23 32.17 25.54 18.97 **GB-115** 93.07 32.15 17.03 18.87 **GB-117** 18.84 93.06 32.16 19.36 **GB-119** 32.18 93.06 15.33 18.80 **GB-121** 93.57 32.40 28.53 18.80 **GB-122** 32.08 14.47 19.02 93.05 **GB-123** 32.36 18.39 93.08 24.69 GB-125 13.62 18.28 93.06 32.40 **GB-127** 93.50 32.50 41.75 18.50 **GB-128** 14.47 18.53 93.04 32.29 **GB-129** 93.04 32.60 17.81 23.84 **GB-131** 93.04 32.66 13.62 17.67 **GB-133** 93.07 32.86 11.92 17.23 **GB-135** 17.16 93.16 32.93 17.03 **GB-137** 17.85 93.30 32.69 17.03 **GB-139** 18.91 93.02 32.11 36.61 **GB-141** 18.52 93.02 32.28 22.13 **GB-143** 93.02 32.47 18.08 11.92 **GB-145** 32.84 17.24 93.02 22.32 **GB-147** 32.85 17.21 93.02 16.18 **GB-149** 32.95 16.99 93.03 18.73 **GB-151** 19.36 16.99 93.05 32.96 **GB-153** 93.06 32.98 6.82 16.94 **GB-155** 93.06 32.97 16.96 2.56 **GB-157** 16.62 93.11 33.14 5.76 **GB-159** 93.07 32.90 4.26 17.14 **GB-161** 9.36 17.39 93.10 32.81 **GB-163** 93.24 32.69 17.79 10.21 GB-165 93.19 32.47 18.26 23.73 GB-167 93.07 31.77 4.26 19.75 GB-169 31.53 20.27 93.04 8.51 **GB-171** 

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-173 | 28.46           | 20.84             | 93.02        | 31.28             |
| GB-175 | 1.70            | 16.69             | 93.04        | 33.08             |
| GB-177 | 5.96            | 16.45             | 93.00        | 33.17             |
| GB-177 | 10.21           | 16.82             | 93.02        | 33.02             |
| GB-173 | 5.96            | 16.63             | 93.02        | 33.10             |
| GB-183 | 20.44           | 16.54             | 93.02        | 33.14             |
| GB-185 | 34.06           | 16.64             | 93.03        | 33.10             |
| GB-187 | 18.73           | 16.47             | 93.03        | 33.17             |
| GB-189 | 8.51            | 16.36             | 93.04        | 33.22             |
| GB-191 | 18.53           | 16.28             | 93.02        | 33.26             |
| GB-193 | 11.67           | 16.24             | 93.03        | 33.27             |
| GB-195 | 11.67           | 16.38             | 92.97        | 33.19             |
| GB-197 | 20.44           | 16.75             | 92.98        | 33.03             |
| GB-199 | 20.44           | 17.29             | 92.99        | 32.80             |
| GB-201 | 23.84           | 17.77             | 93.01        | 32.60             |
| GB-203 | 30.53           | 18,25             | 93.01        | 32.39             |
| GB-205 | 30.53           | 19.83             | 92.97        | 31.69             |
| GB-207 | 23.84           | 20.34             | 92.97        | 31.47             |
| GB-209 | 11.92           | 20.85             | 92.97        | 31.25             |
| GB-210 | 18.62           | 15.00             | 93.11        | 33.84             |
| GB-211 | 45.98           | 18.60             | 93.07        | 32.27             |
| GB-213 | 22.13           | 17.80             | 93.02        | 32.59             |
| GB-215 | 29.98           | 17.16             | 93.00        | 32.86             |
| GB-217 | 11.92           | 16.45             | 93.00        | 33.17             |
| GB-219 | 12.77           | 16.33             | 92.81        | 33.14             |
| GB-221 | 17.33           | 16.30             | 92.80        | 33.15             |
| GB-223 | 18.44           | 16.58             | 92.81        | 33.03             |
| GB-225 | 10.21           | 16.63             | 92.81        | 33.01             |
| GB-227 | 11.07           | 16.52             | 92.81        | 33.06             |
| GB-229 | 18.87           | 16.65             | 92.80        | 32.99             |
| GB-231 | 18.73           | 16.65             | 92.80        | 32.99             |
| GB-233 | 11.92           | 16.59             | 92.80        | 33.02             |
| GB-235 | 18.73           | 17.04             | 92.80        | 32.83             |
| GB-237 | 12.52           | 16.54             | 92.80        | 33.05             |
| GB-239 | 12.52           | 16.37             | 92.89        | 33.15             |
| GB-241 | 23.84           | 16.74             | 92.89        | 32.99             |
| GB-243 | 25.54           | 17.28             | 92.89        | 32.76             |
| GB-245 | 23.84           | 17.76             | 92.91        | 32.56             |
| GB-247 | 16.18           | 18.25             | 92.91        | 32.35             |

| ID               | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure (psi) |
|------------------|-----------------|-------------------|--------------|----------------|
| GB-249           | 35.65           | 19.30             | 92.89        | 31.89          |
|                  | 16.18           | 19.87             | 92.91        | 31.65          |
| GB-251<br>GB-253 | 23.84           | 20.36             | 92.91        | 31.44          |
|                  | 31.86           | 20.86             | 92.91        | 31.22          |
| GB-255           | 21.28           | 18.14             | 93.00        | 32.44          |
| GB-257           | 10.21           | 17.78             | 93.00        | 32.59          |
| GB-259           | 11.07           | 17.15             | 92.99        | 32.86          |
| GB-261           | 12.77           | 16.46             | 92.97        | 33.16          |
| GB-263           | 24.97           | 18.00             | 93.00        | 32.50          |
| GB-265           | 19.87           | 16.46             | 92.94        | 33.14          |
| GB-267           | 18.73           | 16.52             | 92.83        | 33.06          |
| GB-269           | 17.88           | 17.44             | 92.81        | 32.66          |
| GB-271           | 10.21           | 18.00             | 92.81        | 32.42          |
| GB-273           | <u></u>         | 18.00             | 92.82        | 32.42          |
| GB-275           | 9.50            | 18.00             | 92.81        | 32.41          |
| GB-277           | 10.21           | 17.76             | 92.81        | 32.52          |
| GB-279           | 18.73<br>9.36   | 17.04             | 92.81        | 32.83          |
| GB-281           |                 | 17.28             | 92.83        | 32.74          |
| GB-283           | 21.28           |                   | 92.84        | <del></del>    |
| GB-285           | 25.54           | 19.52             | 92.89        | 31.77<br>31.21 |
| GB-286           | 17.03           | 20.86<br>18.00    | 93.01        | 32.50          |
| GB-287           | 17.03           | 16.45             | 92.90        | ·              |
| GB-288           | 9.36            |                   |              | 33.13          |
| GB-289           | 6.82            | 16.52             | 92.85        | 33.07          |
| GB-290           | 11.07           | 18.00             | 92.83        | 32.42          |
| GB-291           | 16.18           | 17.04             | 92.82        | 32.84          |
| GB-292           | 7.66            | 16.37             | 92.83        | 33.13          |
| GB-293           | 13.62           | 16.74             | 92.82        | 32.97          |
| GB-294           | 10.56           | 17.28             | 92.82        | 32.73          |
| GB-295           | 0.00            | 15.00             | 93.08        | 33.83          |
| GB-297           | 0.00            | 18.00             | 93.02        | 32.51          |
| GB-299           | 0.00            | 16.45             | 92.89        | 33.12          |
| GB-301           | 0.00            | 16.53             | 92.86        | 33.07          |
| GB-303           | 0.00            | 18.00             | 92.83        | 32.43          |
| GB-305           | 0.00            | 17.05             | 92.82        | 32.83          |
| GB-307           | 0.00            | 16.86             | 92.82        | 32.91          |
| GB-309           | 0.00            | 17.28             | 92.81        | 32.73          |
| GB-311           | 32.39           | 19.13             | 92.81        | 31.93          |
| GB-313           | 42.13           | 20.80             | 92.81        | 31.20          |
| GB-315           | 15.33           | 18.00             | 92.58        | 32.31          |

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure (psi) |
|--------|-----------------|-------------------|--------------|----------------|
| GB-317 | 14.47           | 17.77             | 92.59        | 32.42          |
| GB-319 | 9.36            | 17.24             | 92.64        | 32.67          |
| GB-321 | 9.36            | 16.45             | 92.77        | 33.07          |
| GB-323 | 22.13           | 16.54             | 92.51        | 32.92          |
| GB-325 | 17.88           | 17.42             | 92.51        | 32.54          |
| GB-327 | 14.47           | 18.00             | 92.52        | 32.29          |
| GB-329 | 10.21           | 18.00             | 92.52        | 32.29          |
| GB-331 | 4.26            | 17.39             | 92.53        | 32.56          |
| GB-333 | 11.92           | 17.35             | 92.62        | 32.62          |
| GB-335 | 10.21           | 16.42             | 92.65        | 33.03          |
| GB-337 | 18.73           | 18.00             | 92.56        | 32.31          |
| GB-339 | 16.18           | 18.00             | 92.57        | 32.31          |
| GB-341 | 13.45           | 17.49             | 92.58        | 32.54          |
| GB-343 | 10.90           | 16.16             | 92.60        | 33.12          |
| GB-345 | 14.47           | 18.00             | 92.54        | 32.30          |
| GB-347 | 17.03           | 18.00             | 92.55        | 32.30          |
| GB-349 | 6.82            | 17.75             | 92.55        | 32.41          |
| GB-351 | 21.28           | 18.00             | 92.52        | 32.29          |
| GB-352 | 30.14           | 17.35             | 92.52        | 32.57          |
| GB-353 | 16.18           | 17.91             | 92.52        | 32.33          |
| GB-355 | 13.62           | 17.82             | 92.54        | 32.38          |
| GB-357 | 15.16           | 17.40             | 92.54        | 32.56          |
| GB-359 | 11.75           | 16.14             | 92.55        | 33.11          |
| GB-361 | 16.18           | 17.26             | 92.51        | 32.61          |
| GB-362 | 20.44           | 16.38             | 92.53        | 33.00          |
| GB-363 | 11.07           | 16.29             | 92.51        | 33.03          |
| GB-365 | 14.18           | 16.32             | 92.52        | 33.02          |
| GB-367 | 19.23           | 16.59             | 92.52        | 32.90          |
| GB-369 | 17.03           | 17.03             | 92.51        | 32.71          |
| GB-371 | 13.62           | 16.87             | 92.52        | 32.78          |
| GB-373 | 10.21           | 16.73             | 92.52        | 32.84          |
| GB-375 | 14.73           | 16.59             | 92.54        | 32.91          |
| GB-377 | 18.32           | 16.34             | 92.56        | 33.02          |
| GB-379 | 45.40           | 17.08             | 92.59        | 32.72          |
| GB-381 | 25.98           | 16.42             | 92.51        | 32.97          |
| GB-383 | 17.47           | 18.29             | 92.52        | 32.16          |
| GB-385 | 10.65           | 18.09             | 92.56        | 32.27          |
| GB-387 | 15.35           | 18.82             | 92.57        | 31.95          |
| GB-389 | 9.36            | 18.79             | 92.60        | 31.98          |

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-391 | 38.21           | 18.77             | 92.65        | 32.01             |
| GB-393 | 15.03           | 16.43             | 92.50        | 32.96             |
| GB-395 | 15.33           | 17.71             | 92.49        | 32.40             |
| GB-397 | 37.53           | 18.80             | 92.50        | 31.94             |
| GB-399 | 34.97           | 19.79             | 92.54        | 31.52             |
| GB-401 | 19.59           | 20.09             | 92.54        | 31.39             |
| GB-403 | 11.07           | 20.39             | 92.54        | 31.26             |
| GB-405 | 11.57           | 16.13             | 92.49        | 33.09             |
| GB-407 | 22.13           | 17.95             | 92.49        | 32.30             |
| GB-409 | 13.62           | 19.40             | 92.50        | 31.67             |
| GB-411 | 17.03           | 16.46             | 92.49        | 32.95             |
| GB-413 | 26.39           | 18.20             | 92.49        | 32.19             |
| GB-415 | 13.62           | 19.96             | 92.49        | 31.43             |
| GB-417 | 35.25           | 16.45             | 92.49        | 32.95             |
| GB-419 | 11.07           | 18.63             | 92.49        | 32.00             |
| GB-421 | 33.40           | 19.83             | 92.49        | 31.48             |
| GB-423 | 11.07           | 20.20             | 92.49        | 31.32             |
| GB-425 | 22.08           | 20.56             | 92.49        | 31.17             |
| GB-427 | 11.07           | 21.58             | 92.50        | 30.73             |
| GB-429 | 27.19           | 21.13             | 92.51        | 30.93             |
| GB-431 | 22.13           | 21.45             | 92.51        | 30.79             |
| GB-433 | 34.25           | 22.00             | 92.51        | 30.55             |
| GB-435 | 17.03           | 21.27             | 92.49        | 30.86             |
| GB-437 | 17.88           | 22.00             | 92.49        | 30.54             |
| GB-439 | 17.88           | 22.00             | 92.49        | 30.55             |
| GB-441 | 11.07           | 21.27             | 92.49        | 30.86             |
| GB-443 | 11.92           | 22.00             | 92.49        | 30.54             |
| GB-445 | 11.07           | 21.00             | 92.49        | 30.98             |
| GB-446 | 0.00            | 22.00             | 93.08        | 30.80             |
| GB-447 | 0.00            | 26.00             | 96.66        | 30.62             |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|------------------|
| P101 | 117.50         | 8.00             | 130.00    | 58.01         | 0.37               | 0.01             |
| P102 | 117.50         | 8.00             | 130.00    | -108.76       | 0.69               | 0.04             |
| P103 | 739.21         | 8.00 ·           | 130.00    | 73.73         | 0.47               | 0.11             |
| P104 | 117.50         | 8.00             | 130.00    | 70.21         | 0.45               | 0.02             |
| P105 | 117.50         | 8.00             | 130.00    | 84.81         | 0.54               | 0.02             |
| P106 | 436.40         | 12.00            | 130.00    | 39.40         | 0.11               | 0.00             |
| P107 | 650.57         | 8.00             | 130.00    | 31.00         | 0.20               | 0.02             |
| P108 | 535.27         | 8.00             | 130.00    | 26.05         | 0.17               | 0.01             |
| P109 | 357.35         | 18.00            | 130.00    | -1,301.83     | 1.64               | 0.20             |
| P110 | 243.09         | 12.00            | 130.00    | -118.11       | 0.34               | 0.01             |
| P111 | 253.19         | 8.00             | 130.00    | -31.00        | 0.20               | 0.01             |
| P112 | 380.98         | 8.00             | 130.00    | 64.45         | 0.41               | 0.04             |
| P113 | 904.24         | 8.00             | 130.00    | 9.75          | 0.06               | 0.00             |
| P114 | 693.26         | 8.00             | 130.00    | -54.51        | 0.35               | 0.06             |
| P115 | 105.50         | 8.00             | 130.00    | -9.39         | 0.06               | 0.000            |
| P116 | 147.51         | 12.00            | 130.00    | 80.32         | 0.23               | 0.00             |
| P117 | 132.50         | 12.00            | 130.00    | -88.37        | 0.25               | 0.00             |
| P118 | 226.54         | 8.00             | 130.00    | 54.75         | 0.35               | 0.02             |
| P119 | 193.01         | 8.00             | 130.00    | 14.96         | 0.10               | 0.00             |
| P120 | 193.01         | 8.00             | 130.00    | -15.70        | 0.10               | 0.00             |
| P121 | 713.00         | 8.00             | 130.00    | 12.10         | 80.0               | 0.00             |
| P122 | 615.89         | 8.00             | 130.00    | -11.66        | 0.07               | 0.00             |
| P123 | 713.00         | 8.00             | 130.00    | -91.44        | 0.58               | 0.16             |
| P124 | 677.66         | 8.00             | 130.00    | -68.98        | 0.44               | 0.09             |
| P125 | 476.65         | 8.00             | 130.00    | -64.24        | 0.41               | 0.05             |
| P126 | 117.50         | 8.00             | 130.00    | -56.57        | 0.36               | 0.01             |
| P127 | 677.66         | 8.00             | 130.00    | 73.32         | 0.47               | 0.10             |
| P128 | 193.00         | 8.00             | 130.00    | -15.78        | 0.10               | 0.00             |
| P129 | 117.50         | 8.00             | 130.00    | -60.18        | 0.38               | 0.01             |
| P130 | 633.34         | 8.00             | 130.00    | 30.01         | 0.19               | 0.02             |
| P131 | 232.72         | 8.00             | 130.00    | 44.80         | 0.29               | 0.01             |
| P132 | 233.02         | 8.00             | 130.00    | 47.61         | 0.30               | 0.02             |
| P133 | 618.66         | 8.00             | 130.00    | 36.31         | 0.23               | 0.02             |
| P134 | 713.00         | 8.00             | 130.00    | -26.80        | 0.17               | 0.02             |
| P135 | 195.00         | 8.00             | 130.00    | 32.62         | 0.21               | 0.01             |
| P136 | 193.00         | 8.00             | 130.00    | 61.01         | 0.39               | 0.02             |
| P137 | 112.20         | 18.00            | 130.00    | 1,198.83      | 1.51               | 0.06             |
| P138 | 701.50         | 8.00             | 130.00    | -85.98        | 0.55               | 0.14             |
| P139 | 378.03         | 8.00             | 130.00    | -95.59        | 0.61               | 0.09             |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|-----------------|
| P140 | 586.50         | 8.00             | 130.00    | -23.94        | 0.15               | 0.01            |
| P141 | 253.00         | 8.00             | 130.00    | 34.14         | 0.22               | 0.01            |
| P142 | 233.00         | 8.00             | 130.00    | -40.26        | 0.26               | 0.01            |
| P143 | 233.00         | 8.00             | 130.00    | -53.44        | 0.34               | 0.02            |
| P144 | 232.70         | 8.00             | 130.00    | -31.60        | 0.20               | 0.01            |
| P145 | 574.54         | 8.00             | 130.00    | 21.24         | 0.14               | 0.01            |
| P146 | 105.50         | 8.00             | 130.00    | 83.35         | 0.53               | 0.02            |
| P147 | 126.23         | 8.00             | 130.00    | 46.20         | 0.29               | 0.01            |
| P148 | 126.78         | 8.00             | 130.00    | -14.50        | 0.09               | 0.000           |
| P149 | 388.16         | 8.00             | 130.00    | 15.87         | 0.10               | 0.00            |
| P150 | 117.50         | 8.00             | 130.00    | 7.15          | 0.05               | 0.000           |
| P151 | 611.16         | 8.00             | 130.00    | -12.95        | 0.08               | 0.00            |
| P152 | 418.00         | 8.00             | 130.00    | -1.21         | 0.01               | O.0000          |
| P153 | 97.50          | 8.00             | 130.00    | 0.71          | 0.00               | 0.00000         |
| P154 | 261.76         | 8.00             | 130.00    | -8.43         | 0.05               | O.000           |
| P155 | 839.51         | 8.00             | 130.00    | -12.71        | 0.08               | 0.00            |
| P156 | 170.40         | 8.00             | 130.00    | 4.16          | 0.03               | 0.000           |
| P157 | 116.20         | 8.00             | 130.00    | -0.05         | 0.000              | 0.00            |
| P158 | 248.92         | 8.00             | 130.00    | -9.87         | 0.06               | O.000           |
| P159 | 247.10         | 8.00             | 130.00    | 15.31         | 0.10               | 0.00            |
| P160 | 247.67         | 8.00             | 130.00    | 33.14         | 0.21               | 0.01            |
| P161 | 247.82         | 8.00             | 130.00    | 51.35         | 0.33               | 0.02            |
| P162 | 247.00         | 8.00             | 130.00    | -31.82        | 0.20               | 0.01            |
| P163 | 249.87         | 8.00             | 130.00    | -21.56        | 0.14               | 0.00            |
| P164 | 1,149.31       | 8.00             | 130.00    | 10.30         | 0.07               | 0.00            |
| P165 | 710.72         | 12.00            | 130.00    | -64.53        | 0.18               | 0.01            |
| P166 | 369.00         | 8.00             | 130.00    | 24.27         | 0.15               | 0.01            |
| P167 | 253.00         | 8.00             | 130.00    | 17.44         | 0.11               | 0.00            |
| P168 | 918.21         | 8.00             | 130.00    | 16.59         | 0.11               | 0.01            |
| P169 | 282.81         | 8.00             | 130.00    | 43.72         | 0.28               | 0.02            |
| P170 | 333.36         | 12.00            | 130.00    | -104.37       | 0.30               | 0.01            |
| P171 | 253.00         | 8.00             | 130.00    | 74.14         | 0.47               | 0.04            |
| P172 | 234.54         | 8.00             | 130.00    | 49.65         | 0.32               | 0.02            |
| P173 | 253.00         | 8.00             | 130.00    | 35.42         | 0.23               | 0.01            |
| P174 | 657.99         | 8.00             | 130.00    | 29.72         | 0.19               | 0.02            |
| P175 | 633.34         | 8.00             | 130.00    | 11.45         | 0.07               | 0.00            |
| P176 | 253.02         | 8.00             | 130.00    | 9.91          | 0.06               | 0.000           |
| P177 | 633.34         | 8.00             | 130.00    | 49.09         | 0.31               | 0.04            |
| P178 | 242.02         | 12.00            | 130.00    | 238.04        | 0.68               | 0.04            |

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos (ft) |
|------|----------------|---------------|-----------|---------------|--------------------|--------------|
| P179 | 253.00         | 8.00          | 130.00    | 89.06         | 0.57               | 0.05         |
| P180 | 273.00         | 8.00          | 130.00    | -41.89        | 0.27               | 0.01         |
| P181 | 628.13         | 12.00         | 130.00    | . 11.89       | 0.03               | 0.000        |
| P182 | 797.55         | 12.00         | 130.00    | 27.08         | 0.08               | 0.00         |
| P183 | 578.83         | 12.00         | 130.00    | 77.73         | 0.22               | 0.01         |
| P184 | 193.00         | 8.00          | 130.00    | -7.89         | 0.05               | 0.000        |
| P185 | 653.19         | 8.00          | 130.00    | 10.99         | 0.07               | 0.00         |
| P186 | 193.00         | 8.00          | 130.00    | -1.17         | 0.01               | O.00000      |
| P187 | 193.00         | 8.00          | 130.00    | 0.30          | 0.00               | O.00000      |
| P188 | 437.56         | 8.00          | 130.00    | 7.66          | 0.05               | 0.000        |
| P189 | 203.57         | 12.00         | 130.00    | -25.32        | 0.07               | 0.000        |
| P190 | 596.95         | 8.00          | 130.00    | 44.33         | 0.28               | 0.03         |
| P191 | 292.91         | 8.00          | 130.00    | -5.55         | 0.04               | O.000        |
| P192 | 695.05         | 8.00          | 130.00    | -3.92         | 0.03               | O.000        |
| P193 | 253.00         | 8.00          | 130.00    | 8.61          | 0.05               | O.000        |
| P194 | 656.00         | 8.00          | 130.00    | -32.78        | 0.21               | 0.02         |
| P195 | 504.88         | 8.00          | 130.00    | -37.54        | 0.24               | 0.02         |
| P196 | 313.32         | 8.00          | 130.00    | -22.94        | 0.15               | 0.01         |
| P197 | 549.00         | 8.00          | 130.00    | 35.25         | 0.22               | 0.02         |
| P198 | 253.00         | 8.00          | 130.00    | 27.50         | 0.18               | 0.01         |
| P199 | 253.00         | 8.00          | 130.00    | 48.43         | 0.31               | 0.02         |
| P200 | 253.00         | 8.00          | 130.00    | 77.45         | 0.49               | O.04         |
| P201 | 403.00         | 8.00          | 130.00    | 36.91         | 0.24               | O.02         |
| P202 | 276.11         | 8.00          | 130.00    | 135.34        | 0.86               | O.12         |
| P203 | 253.02         | 8.00          | 130.00    | -84.32        | 0.54               | <b>O</b> .05 |
| P204 | 253.02         | 8.00          | 130.00    | -43.91        | 0.28               | <b>O.</b> 01 |
| P205 | 236.90         | 8.00          | 130.00    | -18.64        | 0.12               | <b>O</b> .00 |
| P206 | 636.18         | 8.00          | 130.00    | 30.54         | 0.19               | O.02         |
| P207 | 211.30         | 8.00          | 130.00    | 18.50         | 0.12               | <b>O.</b> 00 |
| P208 | 232.70         | 8.00          | 130.00    | 49.30         | 0.31               | O.02         |
| P209 | 233.00         | 8.00          | 130.00    | 76.59         | 0.49               | <b>O</b> .04 |
| P210 | 233.00         | 8.00          | 130.00    | 164.40        | 1.05               | <b>O</b> .15 |
| P211 | 621.42         | 8.00          | 130.00    | -103.38       | 0.66               | <b>O</b> .17 |
| P212 | 253.02         | 8.00          | 130.00    | -62.29        | 0.40               | O.03         |
| P213 | 699.07         | 8.00          | 130.00    | -17.18        | 0.11               | O.01         |
| P214 | 253.02         | 8.00          | 130.00    | 6.49          | 0.04               | O.000        |
| P215 | 613.13         | 8.00          | 130.00    | 3.62          | 0.02               | O-000        |
| P216 | 253.00         | 8.00          | 130.00    | 46.73         | 0.30               | O.02         |
| P217 | 233.00         | 8.00          | 130.00    | 42.70         | 0.27               | <b>Q.</b> 01 |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss (ft) |
|------|----------------|------------------|-----------|---------------|--------------------|---------------|
| P218 | 289.50         | 8.00             | 130.00    | 75.68         | 0.48               | 0.04          |
| P219 | 313.50         | 8.00             | 130.00    | -62.21        | 0.40               | 0.03          |
| P220 | 391.14         | 12.00            | 130.00    | 310.66        | 0.88               | 0.11          |
| P221 | 590.71         | 8.00             | 130.00    | 22.62         | 0.14               | 0.01          |
| P222 | 253.00         | 8.00             | 130.00    | 25.05         | 0.16               | 0.01          |
| P223 | 390.32         | 8.00             | 130.00    | 54.97         | 0.35               | 0.03          |
| P224 | 430.55         | 8.00             | 130.00    | 39.39         | 0.25               | 0.02          |
| P225 | 248.33         | 12.00            | 130.00    | 247.98        | 0.70               | 0.05          |
| P226 | 430.73         | 8.00             | 130.00    | 24.38         | 0.16               | 0.01          |
| P227 | 412.22         | 12.00            | 130.00    | 197.68        | 0.56               | 0.05          |
| P228 | 262.25         | 12.00            | 130.00    | 25.85         | 0.07               | 0.000         |
| P229 | 253.00         | 12.00            | 130.00    | 49.22         | 0.14               | 0.00          |
| P230 | 273.31         | 12.00            | 130.00    | 76.75         | 0.22               | 0.01          |
| P231 | 234.73         | 12.00            | 130.00    | 136.70        | 0.39               | 0.01          |
| P232 | 422.16         | 12.00            | 130.00    | -137.83       | 0.39               | 0.03          |
| P233 | 596.34         | 12.00            | 130.00    | -119.06       | 0.34               | 0.03          |
| P234 | 591.74         | 12.00            | 130.00    | -75.20        | 0.21               | 0.01          |
| P235 | 587.67         | 12.00            | 130.00    | -356.22       | 1.01               | 0.22          |
| P236 | 457.95         | 12.00            | 130.00    | -138.39       | 0.39               | 0.03          |
| P237 | 359.68         | 12.00            | 130.00    | 44.56         | 0.13               | 0.00          |
| P238 | 193.00         | 8.00             | 130.00    | -3.63         | 0.02               | 0.000         |
| P239 | 487.33         | 8.00             | 130.00    | 77.07         | 0.49               | 0.08          |
| P240 | 486.84         | 8.00             | 130.00    | -64.22        | 0.41               | 0.06          |
| P241 | 708.39         | 8.00             | 130.00    | -54.66        | 0.35               | 0.06          |
| P242 | 617.10         | 8.00             | 130.00    | -51.03        | 0.33               | 0.05          |
| P243 | 319.69         | 18.00            | 130.00    | -496.90       | 0.63               | 0.03          |
| P244 | 861.88         | 12.00            | 130.00    | -42.13        | 0.12               | 0.01          |
| P245 | 534.05         | 18.00            | 130.00    | -216.76       | 0.27               | 0.01          |
| P246 | 627.02         | 18.00            | 130.00    | -136.43       | 0.17               | 0.01          |
| P247 | 195.01         | 18.00            | 130.00    | -224.80       | 0.28               | 0.00          |
| P248 | 751.91         | 18.00            | 130.00    | 38.97         | 0.05               | 0.000         |
| P249 | 370.87         | 12.00            | 130.00    | -383.41       | 1.09               | 0.16          |
| P250 | 602.79         | 8.00             | 130.00    | -46.91        | 0.30               | 0.04          |
| P251 | 656.30         | 8.00             | 130.00    | -23.23        | 0.15               | 0.01          |
| P252 | 501.81         | 8.00             | 130.00    | -90.13        | 0.58               | 0.11          |
| P253 | 464.05         | 12.00            | 130.00    | 172.30        | 0.49               | 0.05          |
| P254 | 250.56         | 12.00            | 130.00    | 161.55        | 0.46               | 0.02          |
| P255 | 423.72         | 8.00             | 130.00    | -23.11        | 0.15               | 0.01          |
| P256 | 235.04         | 8.00             | 130.00    | -32.33        | 0.21               | 0.01          |

| MAXIMUM DAY | Y DEMANDS - | PIPE REPORT - | GREENBRIAR |
|-------------|-------------|---------------|------------|
|             |             |               |            |

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | H eadlo       |
|------|----------------|---------------|-----------|---------------|--------------------|---------------|
| P257 | 344.48         | 8.00          | 130.00    | 52.46         | 0.33               | 0.03          |
| P258 | 656.00         | 8.00          | 130.00    | 26.48         | 0.17               | 0.01          |
| P259 | 497.14         | 8.00 .        | 130.00    | 28.30         | 0.18               | 0.01          |
| P260 | 494.52         | 8.00          | 130.00    | -11.59        | 0.07               | 0.00          |
| P261 | 466.36         | 8.00          | 130.00    | -9.67         | 0.06               | 0.00          |
| P262 | 616.00         | 8.00          | 130.00    | -6.96         | 0.04               | 0.00          |
| P263 | 651.25         | 8.00          | 130.00    | 3.81          | 0.02               | 0.000         |
| P264 | 246.49         | 8.00          | 130.00    | 41.32         | 0.26               | 0.01          |
| P265 | 375.42         | 12.00         | 130.00    | -172.42       | 0.49               | 0.04          |
| P266 | 665.79         | 8.00          | 130.00    | 49.74         | 0.32               | 0.05          |
| P267 | 285.98         | 8.00          | 130.00    | -15.40        | 0.10               | 0.00          |
| P268 | 272.69         | 8.00          | 130.00    | 18.77         | 0.12               | 0.00          |
| P269 | 744.21         | 8.00          | 130.00    | 14.42         | 0.09               | 0.01          |
| P270 | 105.50         | 8.00          | 130.00    | 3.17          | 0.02               | <b>⊘.0000</b> |
| P271 | 892.22         | 8.00          | 130.00    | 25.35         | 0.16               | 0.02          |
| P272 | 193.00         | 8.00          | 130.00    | 11.80         | 0.08               | €0.000        |
| P273 | 105.50         | 8.00          | 130.00    | 18.00         | 0.11               | 0.00          |
| P274 | 698.75         | 8.00          | 130.00    | -2.57         | 0.02               | €0.000        |
| P275 | 181.50         | 12.00         | 130.00    | -384.76       | 1.09               | 0.08          |
| P276 | 112.20         | 8.00          | 130.00    | -59.74        | 0.38               | 0.01          |
| P277 | 698.70         | 8.00          | 130.00    | -23.39        | 0.15               | 0.01          |
| P278 | 713.00         | 8.00          | 130.00    | -8.22         | 0.05               | 0.00          |
| P279 | 422.00         | 8.00          | 130.00    | -45.35        | 0.29               | 0.03          |
| P280 | 117.50         | 8.00          | 130.00    | 7.78          | 0.05               | €0.000        |
| P281 | 589.97         | 8.00          | 130.00    | -170.30       | 1.09               | 0.41          |
| P282 | 130.50         | 8.00          | 130.00    | -132.90       | 0.85               | 0.06          |
| P283 | 410.65         | 18.00         | 130.00    | -1,343.58     | 1.69               | 0.25          |
| P284 | 500.49         | 8.00          | 130.00    | -119.63       | 0.76               | 0.18          |
| P285 | 807.99         | 8.00          | 130.00    | 21.89         | 0.14               | 0.01          |
| P286 | 193.00         | 8.00          | 130.00    | 2.35          | 0.02               | O.0000        |
| P287 | 263.00         | 8.00          | 130.00    | -4.11         | 0.03               | <b>O.000</b>  |
| P288 | 738.30         | 8.00          | 130.00    | 18.66         | 0.12               | 0.01          |
| P289 | 233.02         | 8.00          | 130.00    | -25.77        | 0.16               | 0.00          |
| P290 | 739.64         | 8.00          | 130.00    | -54.49        | 0.35               | 0.06          |
| P291 | 252.00         | 8.00          | 130.00    | -15.91        | 0.10               | 0.00          |
| P292 | 262.03         | 8.00          | 130.00    | -40.73        | 0.26               | 0.01          |
| P293 | 924.17         | 8.00          | 130.00    | -8.15         | 0.05               | 0.00          |
| P294 | 770.75         | 8.00          | 130.00    | -5.85         | 0.04               | 0.00          |
| P295 | 956.68         | 8.00          | 130.00    | 23.01         | 0.15               | 0.02          |

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>(ft) |
|------|----------------|---------------|-----------|---------------|--------------------|------------------|
| P296 | 693.81         | 8.00          | 130.00    | -77.23        | 0.49               | 0.11             |
| P297 | 678.13         | 8.00          | 130.00    | 55.97         | 0.36               | 0.06             |
| P298 | 837.42         | 8.00          | 130.00    | . 19.36       | 0.12               | 0.01             |
| P299 | 557.94         | 8.00          | 130.00    | -60.86        | 0.39               | 0.06             |
| P300 | 696.14         | 8.00          | 130.00    | -4.21         | 0.03               | O.000            |
| P301 | 468.04         | 8.00          | 130.00    | -8.00         | 0.05               | 0.00             |
| P302 | 255.36         | 8.00          | 130.00    | -34.03        | 0.22               | 0.01             |
| P303 | 247.32         | 8.00          | 130.00    | 38.29         | 0.24               | 0.01             |
| P304 | 208.11         | 12.00         | 130.00    | -455.36       | 1.29               | 0.12             |
| P305 | 88.53          | 8.00          | 130.00    | 10.22         | 0.07               | O.000            |
| P306 | 193.00         | 8.00          | 130.00    | -176.13       | 1.12               | 0.14             |
| P307 | 582.27         | 8.00          | 130.00    | 32.62         | 0.21               | 0.02             |
| P308 | 677.66         | 8.00          | 130.00    | -74.01        | 0.47               | 0.10             |
| P309 | 195.00         | 8.00          | 130.00    | -74.95        | 0.48               | 0.03             |
| P310 | 132.50         | 12.00         | 130.00    | -92.44        | 0.26               | 0.00             |
| P311 | 380.98         | 8.00          | 130.00    | -76.86        | 0.49               | 0.06             |
| P312 | 475.68         | 8.00          | 130.00    | -70.95        | 0.45               | 0.06             |
| P313 | 655.89         | 8.00          | 130.00    | -25.30        | 0.16               | 0.01             |
| P314 | 653.93         | 8.00          | 130.00    | -37.26        | 0.24               | 0.03             |
| P315 | 215.00         | 8.00          | 130.00    | -0.78         | 0.00               | O.0000           |
| P316 | 195.01         | 8.00          | 130.00    | 16.63         | 0.11               | 0.00             |
| P317 | 214.88         | 8.00          | 130.00    | -20.76        | 0.13               | 0.00             |
| P318 | 252.22         | 8.00          | 130.00    | 5.80          | 0.04               | <b>O.000</b>     |
| P319 | 245.38         | 8.00          | 130.00    | 6.97          | 0.04               | O.000            |
| P320 | 607.50         | 8.00          | 130.00    | -13.84        | 0.09               | 0.00             |
| P321 | 574.53         | 8.00          | 130.00    | -21.50        | 0.14               | 0.01             |
| P322 | 105.50         | 8.00          | 130.00    | -52.15        | 0.33               | 0.01             |
| P323 | 212.18         | 8.00          | 130.00    | 20.99         | 0.13               | 0.00             |
| P324 | 105.50         | 8.00          | 130.00    | 11.93         | 0.08               | 0.000            |
| P325 | 211.00         | 8.00          | 130.00    | -12.50        | 0.08               | 0.00             |
| P326 | 211.30         | 8.00          | 130.00    | -35.79        | 0.23               | 0.01             |
| P327 | 209.82         | 8.00          | 130.00    | -29.50        | 0.19               | 0.01             |
| P328 | 728.60         | 8.00          | 130.00    | -13.91        | 0.09               | 0.00             |
| P329 | 594.64         | 8.00          | 130.00    | 1.65          | 0.01               | O.0000           |
| P330 | 258.06         | 8.00          | 130.00    | -15.18        | 0.10               | 0.00             |
| P331 | 499.01         | 8.00          | 130.00    | 8.09          | 0.05               | 0.00             |
| P332 | 545.88         | 8.00          | 130.00    | -22.42        | 0.14               | 0.01             |
| P333 | 783.02         | 8.00          | 130.00    | -18.13        | 0.12               | 0.01             |
| P334 | 260.55         | 12.00         | 130.00    | -44.05        | 0.12               | 0.00             |

| Maximum day | <b>DEMANDS - PI</b> | PE REPORT - 0    | REENBRIAR |
|-------------|---------------------|------------------|-----------|
| ID          | Length<br>(ft)      | Diameter<br>(in) | Roughness |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|-----------------|
| P335 | 255.00         | 8.00             | 130.00    | 23.85         | 0.15               | 0.00            |
| P336 | 255.00         | 8.00             | 130.00    | 16.68         | 0.11               | 0.00            |
| P337 | 255.07         | 8.00             | 130.00    | 10.57         | 0.07               | 0.00            |
| P338 | 255.00         | 12.00            | 130.00    | 267.97        | 0.76               | 0.06            |
| P339 | 255.00         | 12.00            | 130.00    | -197.74       | 0.56               | 0.03            |
| P340 | 255.00         | 8.00             | 130.00    | -16.20        | 0.10               | 0.00            |
| P341 | 255.00         | 8.00             | 130.00    | -19.25        | 0.12               | 0.00            |
| P342 | 246.98         | 8.00             | 130.00    | -11.84        | 0.08               | 0.00            |
| P343 | 253.00         | 8.00             | 130.00    | -41.81        | 0.27               | 0.01            |
| P344 | 147.50         | 12.00            | 130.00    | 76.33         | 0.22               | 0.00            |
| P345 | 147.37         | 12.00            | 130.00    | 122.62        | 0.35               | 0.01            |
| P346 | 147.50         | 12.00            | 130.00    | 148.76        | 0.42               | 0.01            |
| P347 | 147.59         | 12.00            | 130.00    | -173.12       | 0.49               | 0.01            |
| P348 | 381.04         | 8.00             | 130.00    | -38.50        | 0.25               | 0.02            |
| P349 | 190.72         | 18.00            | 130.00    | -551.09       | 0.69               | 0.02            |
| P350 | 253.02         | 8.00             | 130.00    | 28.08         | 0.18               | 0.01            |
| P351 | 233.00         | 8.00             | 130.00    | -8.61         | 0.05               | O.000           |
| P352 | 1,365.42       | 24.00            | 130.00    | 1,103.36      | 0.78               | 0.14            |
| P353 | 1,505.76       | 30.00            | 130.00    | -1,103.36     | 0.50               | 0.05            |
| P354 | 369.99         | 8.00             | 130.00    | -54.22        | 0.35               | 0.03            |
| P355 | 369.99         | 8.00             | 130.00    | -62.51        | 0.40               | 0.04            |
| P356 | 117.50         | 8.00             | 130.00    | -26.43        | 0.17               | 0.00            |
| P357 | 195.00         | 8.00             | 130.00    | -54.31        | 0.35               | 0.02            |
| P358 | 193.00         | 8.00             | 130.00    | -56.94        | 0.36               | 0.02            |
| P359 | 500.49         | 8.00             | 130.00    | -91.82        | 0.59               | 0.11            |
| P360 | 500.78         | 8.00             | 130.00    | -138.05       | 0.88               | 0.23            |
| P361 | 677.66         | 8.00             | 130.00    | -73.05        | 0.47               | 0.10            |
| P362 | 482.45         | 12.00            | 130.00    | -40.28        | 0.11               | 0.00            |
| P363 | 677.66         | 8.00             | 130.00    | -69.95        | 0.45               | 0.09            |
| P364 | 1,180.18       | 30.00            | 130.00    | -846.70       | 0.38               | 0.03            |
| P365 | 1,577.01       | 24.00            | 130.00    | -1,493.09     | 1.06               | 0.29            |
| P366 | 701.50         | 24.00            | 130.00    | -1,696.90     | 1.20               | 0.16            |
| P367 | 242.00         | 18.00            | 130.00    | 846.70        | 1.07               | 0.06            |
| P368 | 738.68         | 18.00            | 130.00    | 697.94        | 0.88               | 0.13            |
| P369 | 253.00         | 8.00             | 130.00    | -21.45        | 0.14               | 0.00            |
| P370 | 660.09         | 8.00             | 130.00    | <b>-58.65</b> | 0.37               | 0.06            |
| P371 | 193.00         | 18.00            | 130.00    | 874.42        | 1.10               | 0.05            |
| P372 | 595.91         | 18.00            | 130.00    | 731.07        | 0.92               | 0.12            |
| P373 | 191.34         | 18.00            | 130.00    | 636.68        | 0.80               | 0.03            |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss (ft) |
|------|----------------|------------------|-----------|---------------|--------------------|---------------|
| P374 | 105.50         | 8.00             | 130.00    | 4.87          | 0.03               | 0.0000        |
| P375 | 607.50         | 8.00             | 130.00    | -23.81        | 0.15               | 0.01          |
| P376 | 438.00         | 18.00°           | 130.00    | 415.71        | 0.52               | 0.03          |
| P377 | 650.57         | 18.00            | 130.00    | 293.09        | 0.37               | 0.02          |
| P378 | 112.20         | 8.00             | 130.00    | -143.66       | 0.92               | 0.06          |
| P379 | 117.50         | 8.00             | 130.00    | 57.57         | 0.37               | 0.01          |
| P380 | 348.36         | 8.00             | 130.00    | 27.44         | 0.18               | 0.01          |
| P381 | 178.10         | 12.00            | 130.00    | -198.83       | 0.56               | 0.02          |
| P382 | 1,122.42       | 24.00            | 130.00    | -3,040.48     | 2.16               | 0.76          |
| P383 | 93.09          | 8.00             | 130.00    | -77.47        | 0.49               | 0.01          |
| P384 | 195.01         | 8.00             | 130.00    | 25.53         | 0.16               | 0.00          |
| P385 | 4,416.05       | 30.00            | 130.00    | 0.00          | 0.00               | 0.00          |
| P386 | 3,100.00       | 24.00            | 130.00    | -3,068.59     | 2.18               | 2.14          |
| P388 | 1,581.75       | 18.00            | 130.00    | 458.41        | 0.58               | 0.13          |
| P389 | 621.96         | 18.00            | 130.00    | 428.85        | 0.54               | 0.05          |
| P990 | 235.86         | 99.00            | 130.00    | 0.00          | 0.00               | 0.00          |
| P991 | 377.34         | 99.00            | 130.00    | 0.00          | 0.00               | 0.00          |
| P992 | 233.99         | 99.00            | 130.00    | 3,068.59      | 0.13               | 0.000         |
| P993 | 232.72         | 99.00            | 130.00    | 3,068.59      | 0.13               | 0.000         |

| ID      | Elevation<br>(ft) | Downstream Pressure<br>(psi) | Flow<br>(gpm) | Head Gain<br>(ft) |
|---------|-------------------|------------------------------|---------------|-------------------|
| PUMP105 | 22.00             | 30.80                        | 0.00          | 0.00              |
| PUMP107 | 26.00             | 30.62                        | 3,068.59      | 96.66             |



## PEAK HOUR DEMANDS

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-101 | 0.00            | 20.00             | 91.31        | 30.90             |
| GB-103 | 6.47            | 15.00             | 91.47        | 33.13             |
| GB-105 | 6.47            | 19.00             | 91.82        | 31.55             |
| GB-107 | 0.00            | 20.00             | 92.02        | 31.21             |
| GB-108 | 36.54           | 21.00             | 93.03        | 31.21             |
| GB-109 | 39.85           | 20.00             | 91.06        | 30.79             |
| GB-111 | 22.13           | 20.00             | 91.06        | 30.79             |
| GB-113 | 19.92           | 19.59             | 91.10        | 30.98             |
| GB-115 | 33.21           | 18.97             | 91.35        | 31.36             |
| GB-117 | 22.13           | 18.87             | 91.11        | 31.30             |
| GB-119 | 25.18           | 18.84             | 91.09        | 31.31             |
| GB-121 | 19.92           | 18.80             | 91.09        | 31.32             |
| GB-122 | 37.09           | 18.80             | 91.79        | 31.62             |
| GB-123 | 18.81           | 19.02             | 91.09        | 31.23             |
| GB-125 | 32.10           | 18.39             | 91.12        | 31.51             |
| GB-127 | 17.71           | 18.28             | 91.09        | 31.55             |
| GB-128 | 54.28           | 18.50             | 91.66        | 31.70             |
| GB-129 | 18.81           | 18.53             | 91.07        | 31.43             |
| GB-131 | 30.99           | 17.81             | 91.07        | 31.74             |
| GB-133 | 17.71           | 17.67             | 91.07        | 31.80             |
| GB-135 | 15.49           | 17.23             | 91.10        | 32.01             |
| GB-137 | 22.13           | 17.16             | 91.21        | 32.08             |
| GB-139 | 22.13           | 17.85             | 91.37        | 31.86             |
| GB-141 | 47.59           | 18.91             | 91.06        | 31.26             |
| GB-143 | 28.78           | 18.52             | 91.06        | 31.43             |
| GB-145 | 15.49           | 18.08             | 91.05        | 31.62             |
| GB-147 | 29.00           | 17.24             | 91.05        | 31.98             |
| GB-149 | 21.03           | 17.21             | 91.04        | 31.99             |
| GB-151 | 24.35           | 16.99             | 91.05        | 32.09             |
| GB-153 | 25.18           | 16.99             | 91.07        | 32.10             |
| GB-155 | 8.86            | 16.94             | 91.08        | 32.13             |
| GB-157 | 3.32            | 16.96             | 91.08        | 32.12             |
| GB-159 | 7.49            | 16.62             | 91.13        | 32.28             |
| GB-161 | 5.54            | 17.14             | 91.06        | 32.03             |
| GB-163 | 12.18           | 17.39             | 91.10        | 31.94             |
| GB-165 | 13.29           | 17.79             | 91.29        | 31.85             |
| GB-167 | 30.84           | 18.26             | 91.22        | 31.61             |
| GB-169 | 5.54            | 19.75             | 91.05        | 30.89             |
| GB-171 | 11.07           | 20.27             | 91.00        | 30.65             |

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-173 | 36.99           | 20.84             | 90.97        | 30.39             |
|        | 2.21            | 16.69             | 91.06        | 32.22             |
| GB-175 | 7.75            | 16.45             | 90.95        | 32.28             |
| GB-177 | 13.29           | 16.82             | 90.97        | 32.13             |
| GB-179 |                 | 16.63             | 91.04        | 32.24             |
| GB-181 | 7.75            | 16.54             | 91.04        | 32.28             |
| GB-183 | 26.56           | 16.64             | 91.04        | 32.24             |
| GB-185 | 44.27           | 16.47             | 91.05        | 32.31             |
| GB-187 | 24.35           | <u> </u>          | 91.05        | 32.36             |
| GB-189 | 11.07           | 16.36             | 91.04        | 32.40             |
| GB-191 | 24.09           | 16.28             |              | 32.41             |
| GB-193 | 15.17           | 16.24             | 91.05        | 32.29             |
| GB-195 | 15.17           | 16.38             | 90.91        | 32.29             |
| GB-197 | 26.56           | 16.75             | 90.91        | <u> </u>          |
| GB-199 | 26.56           | 17.29             | 90.93        | 31.91             |
| GB-201 | 30.99           | 17.77             | 90.95        | 31.71             |
| GB-203 | 39.70           | 18.25             | 90.96        | 31.50             |
| GB-205 | 39.70           | 19.83             | 90.89        | 30.79             |
| GB-207 | 30.99           | 20.34             | 90.89        | 30.57             |
| GB-209 | 15.49           | 20.85             | 90.89        | 30.35             |
| GB-210 | 24.20           | 15.00             | 91.25        | 33.04             |
| GB-211 | 59.77           | 18.60             | 91.16        | 31.44             |
| GB-213 | 28.78           | 17.80             | 91.06        | 31.74             |
| GB-215 | 38.97           | 17.16             | 91.03        | 32.01             |
| GB-217 | 15.49           | 16.45             | 91.03        | 32.31             |
| GB-219 | 16.60           | 16.33             | 90.70        | 32.23             |
| GB-221 | 22.53           | 16.30             | 90.67        | 32.22             |
| GB-223 | 23.97           | 16.58             | 90.70        | 32.12             |
| GB-225 | 13.29           | 16.63             | 90.70        | 32.09             |
| GB-227 | 14.38           | 16.52             | 90.70        | 32.14             |
| GB-229 | 24.53           | 16.65             | 90.67        | 32.07             |
| GB-231 | 24.35           | 16.65             | 90.67        | 32.07             |
| GB-233 | 15.49           | 16.59             | 90.67        | 32.10             |
| GB-235 | 24.35           | 17.04             | 90.68        | 31.91             |
| GB-237 | 16.28           | 16.54             | 90.68        | 32.13             |
| GB-239 | 16.28           | 16.37             | 90.78        | 32.24             |
| GB-241 | 30.99           | 16.74             | 90.78        | 32.08             |
| GB-243 | 33.21           | 17.28             | 90.79        | 31.85             |
| GB-245 | 30.99           | 17.76             | 90.82        | 31.65             |
| GB-247 | 21.03           | 18.25             | 90.82        | 31.44             |

| ID     | Demand<br>(gpm) | Elevation (ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|----------------|--------------|-------------------|
| GB-249 | 46.33           | 19.30          | 90.78        | 30.97             |
| GB-251 | 21.03           | 19.87          | 90.81        | 30.74             |
| GB-253 | 30.99           | 20.36          | 90.81        | 30.53             |
| GB-255 | 41.42           | 20.86          | 90.81        | 30.31             |
| GB-257 | 27.67           | 18.14          | 91.05        | 31.59             |
| GB-259 | 13.29           | 17.78          | 91.04        | 31.74             |
| GB-261 | 14.38           | 17.15          | 91.02        | 32.01             |
| GB-263 | 16.60           | 16.46          | 90.99        | 32.30             |
| GB-265 | 32.47           | 18.00          | 91.05        | 31.65             |
| GB-267 | 25.83           | 16.46          | 90.94        | 32.27             |
| GB-269 | 24.35           | 16.52          | 90.73        | 32.16             |
| GB-271 | 23.24           | 17.44          | 90.71        | 31.74             |
| GB-273 | 13.29           | 18.00          | 90.71        | 31.50             |
| GB-275 | 12.35           | 18.00          | 90.71        | 31.50             |
| GB-277 | 13.29           | 18.00          | 90.69        | 31.50             |
| GB-279 | 24.35           | 17.76          | 90.69        | 31.60             |
| GB-281 | 12.18           | 17.04          | 90.69        | 31.91             |
| GB-283 | 27.67           | 17.28          | 90.71        | 31.82             |
| GB-285 | 33.21           | 19.52          | 90.72        | 30.85             |
| GB-286 | 22.13           | 20.86          | 90.79        | 30.30             |
| GB-287 | 22.13           | 18.00          | 91.08        | 31.67             |
| GB-288 | 12.18           | 16.45          | 90.88        | 32.25             |
| GB-289 | 8.86            | 16.52          | 90.77        | 32.17             |
| GB-290 | 14.38           | 18.00          | 90.73        | 31.51             |
| GB-291 | 21.03           | 17.04          | 90.71        | 31.92             |
| GB-292 | 9.97            | 16.37          | 90.71        | 32.21             |
| GB-293 | 17.71           | 16.74          | 90.70        | 32.05             |
| GB-294 | 13.73           | 17.28          | 90.69        | 31.81             |
| GB-295 | 0.00            | 15.00          | 91.23        | 33.03             |
| GB-297 | 0.00            | 18.00          | 91.10        | 31.68             |
| GB-299 | 0.00            | 16.45          | 90.85        | 32.24             |
| GB-301 | 0.00            | 16.53          | 90.79        | 32.18             |
| GB-303 | 0.00            | 18.00          | 90.74        | 31.52             |
| GB-305 | 0.00            | 17.05          | 90.71        | 31.92             |
| GB-307 | 0.00            | 16.86          | 90.69        | 31.99             |
| GB-309 | 0.00            | 17.28          | 90.68        | 31.81             |
| GB-311 | 42.11           | 19.13          | 90.68        | 31.00             |
| GB-313 | 54.77           | 20.80          | 90.67        | 30.28             |
| GB-315 | 19.92           | 18.00          | 90.32        | 31.34             |

PEAK HOUR DEMANDS - JUNCTION REPORT - GREENBRIAR Pressure Elevation Head Demand ID (ft) (psi) (ft) (gpm) 31.45 17.77 90.35 18.81 **GB-317** 90.43 31.71 17.24 12.18 **GB-319** 32.15 90.64 12.18 16.45 **GB-321** 90.21 31.92 16.54 28.78 **GB-323** 31.54 90.21 23.24 17.42 **GB-325** 31.29 90.22 18.00 18.81 **GB-327** 90.23 31.30 18.00 13.29 GB-329 31.56 17.39 90.24 5.54 GB-331 17.35 31.65 90.41 15.49 **GB-333** 32.08 16.42 90.45 13.29 **GB-335** 90.30 31.33 18.00 24.35 **GB-337** 31.33 18.00 90.31 21.03 **GB-339** 90.34 31.56 17.49 17.49 GB-341 90.37 32.15 16.16 14.17 **GB-343** 90.26 31.31 18.00 18.81 **GB-345** 90.27 31.32 18.00 22.13 **GB-347** 31.43 90.28 17.75 8.86 **GB-349** 31.30 90.24 18.00 27.67 **GB-351** 31.58 17.35 90.22 39.18 **GB-352** 90.23 31.34 17.91 21.03 GB-353 90.26 31.39 17.82 17.71 **GB-355** 31.57 90.27 19.70 17.40 **GB-357** 32.13 90.28 16.14 15.28 GB-359 31.61 17.26 90.22 21.03 **GB-361** 90.24 32.00 16.38 26.56 GB-362 32.03 16.29 90.20 14.38 **GB-363** 32.02 90.22 16.32 18.43 GB-365 90.22 31.90 16.59 25.00 **GB-367** 90.21 31.71 22.13 17.03 GB-369 90.22 31.78 16.87 17.71 **GB-371** 31.85 90.23 16.73 13.29 **GB-373** 31.92 90.26 16.59 19.15 **GB-375** 90.28 32.04 23.81 16.34 **GB-377** 31.74 90.33 59.02 17.08 **GB-379** 90.20 31.97 16.42 33.78 **GB-381** 18.29 90.21 31.16 22.70 **GB-383** 18.09 90.29 31.28 13.85 GB-385 90.29 30.97 18.82 19.96 **GB-387** 90.34 31.00 18.79 12.18 **GB-389** 

PEAK HOUR DEMANDS - JUNCTION REPORT - GREENBRIAR

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-391 | 49.67           | 18.77             | 90.43        | 31.05             |
| GB-393 | 19.53           | 16.43             | 90.18        | 31.95             |
| GB-395 | 19.92           | 17.71             | 90.18        | 31.40             |
| GB-397 | 48.78           | 18.80             | 90.19        | 30.93             |
| GB-399 | 45.46           | 19.79             | 90.25        | 30.53             |
| GB-401 | 25.46           | 20.09             | 90.25        | 30.40             |
| GB-403 | 14.38           | 20.39             | 90.25        | 30.27             |
| GB-405 | 15.04           | 16.13             | 90.17        | 32.08             |
| GB-407 | 28.78           | 17.95             | 90.17        | 31.29             |
| GB-409 | 17.71           | 19.40             | 90.18        | 30.67             |
| GB-411 | 22.13           | 16.46             | 90.17        | 31.94             |
| GB-413 | 34.31           | 18.20             | 90.17        | 31.19             |
| GB-415 | 17.71           | 19.96             | 90.18        | 30.42             |
| GB-417 | 45.83           | 16.45             | 90.18        | 31.95             |
| GB-419 | 14.38           | 18.63             | 90.17        | 31.00             |
| GB-421 | 43.42           | 19.83             | 90.17        | 30.48             |
| GB-423 | 14.38           | 20.20             | 90.17        | 30.32             |
| GB-425 | 28.70           | 20.56             | 90.18        | 30.16             |
| GB-427 | 14.38           | 21.58             | 90.18        | 29.72             |
| GB-429 | 35.35           | 21.13             | 90.20        | 29.93             |
| GB-431 | 28.78           | 21.45             | 90.20        | 29.79             |
| GB-433 | 44.53           | 22.00             | 90.19        | 29.55             |
| GB-435 | 22.13           | 21.27             | 90.17        | 29.85             |
| GB-437 | 23.24           | 22.00             | 90.17        | 29.54             |
| GB-439 | 23.24           | 22.00             | 90.18        | 29.54             |
| GB-441 | 14.38           | 21.27             | 90.17        | 29.85             |
| GB-443 | 15.49           | 22.00             | 90.17        | 29.54             |
| GB-445 | 14.38           | 21.00             | 90.18        | 29.97             |
| GB-446 | 0.00            | 22.00             | 91.25        | 30.01             |
| GB-447 | 0.00            | 26.00             | 95.89        | 30.28             |

PEAK HOUR DEMANDS - PIPE REPORT - GREENBRIAR **Flow** Velocity **Headloss** Diameter Length Roughness ID (in) (gpm) (ft/s) (ft) (ft) 130.00 97.95 0.63 0.03 8.00 P101 117.50 130.00 -143.32 0.91 0.06 8.00 117.50 P102 104.14 0.20 130.00 0.66 739.21 8.00 -P103 130.00 90.76 0.58 0.03 8.00 117.50 P104 117.36 0.75 0.04 8.00 130.00 117.50 P105 130.00 55.91 0.16 0.01 12.00 436.40 P106 47.22 0.04 130.00 0.30 8.00 650.57 P107 0.03 40.47 0.26 8.00 130.00 535.27 P108 0.29 130.00 -1,577.09 1.99 18.00 357.35 P109 0.02 -161.72 0.46 243.09 12.00 130.00 P110 0.01 8.00 130.00 -42.63 0.27 253.19 P111 73.75 0.47 0.06 8.00 130.00 380.98 P112 11.72 0.00 130.00 0.07 8.00 P113 904.24 8.00 130.00 -65.85 0.42 80.0 693.26 P114 0.000 130.00 -10.86 0.07 8.00 105.50 P115 91.26 0.26 0.00 12.00 130.00 147.51 P116 -92.68 0.26 0.00 130.00 132.50 12.00 P117 64.64 0.41 0.03 130.00 8.00 P118 226.54 18.08 0.12 0.00 8.00 130.00 193.01 P119 0.00 -16.79 0.11 130.00 8.00 193.01 P120 0.000 130.00 5.43 0.03 713.00 8.00 P121 -5.34 0.03 0.000 8.00 130.00 615.89 P122 -116.56 0.74 0.24 8.00 130.00 713.00 P123 0.13 -83.78 0.53 677.66 8.00 130.00 P124 0.07 130.00 -74.93 0.48 8.00 476.65 P125 0.01 8.00 130.00 -64.97 0.41 117.50 P126 89.01 0.57 0.14 130.00 8.00 677.66 P127 0.00 130.00 -17.14 0.11 8.00 193.00 P128 0.02 130.00 -75.87 0.48 117.50 8.00 P129 130.00 32.71 0.21 0.02 8.00 P130 633.34 0.01 45.99 0.29 8.00 130.00 232.72 P131 59.47 0.38 0.02 8.00 130.00 233.02 P132 41.93 0.03 130.00 0.27 8.00 618.66 P133 0.03 -36.88 0.24 130.00 713.00 8.00 P134 130.00 36.01 0.23 0.01 8.00 195.00 P135

130.00

130.00

130.00

130.00

70.28

1,459.29

-95.67

-106.66

0.45

1.84

0.61

0.68

0.03

80.0

0.17

0.11

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193.00

112.20

701.50

378.03

P136

P137

P138

P139

8.00

18.00

8.00

8.00

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|------------------|
| P140 | 586.50         | 8.00             | 130.00    | -22.29        | 0.14               | 0.01             |
| P141 | 253.00         | 8.00             | 130.00    | 51.12         | 0.33               | 0.02             |
| P142 | 233.00         | 8.00             | 130.00    | -43.31        | 0.28               | 0.01             |
| P143 | 233.00         | 8.00             | 130.00    | -62.49        | 0.40               | 0.03             |
| P144 | 232.70         | 8.00             | 130.00    | -44.86        | 0.29               | 0.01             |
| P145 | 574.54         | 8.00             | 130.00    | 18.66         | 0.12               | 0.01             |
| P146 | 105.50         | 8.00             | 130.00    | 90.33         | 0.58               | 0.02             |
| P147 | 126.23         | 8.00             | 130.00    | 66.65         | 0.43               | 0.02             |
| P148 | 126.78         | 8.00             | 130.00    | -11.76        | 0.08               | 0.000            |
| P149 | 388.16         | 8.00             | 130.00    | 19.46         | 0.12               | 0.00             |
| P150 | 117.50         | 8.00             | 130.00    | 8.51          | 0.05               | 0.000            |
| P151 | 611.16         | 8.00             | 130.00    | -15.91        | 0.10               | 0.01             |
| P152 | 418.00         | 8.00             | 130.00    | -1.64         | 0.01               | O.0000           |
| P153 | 97.50          | 8.00             | 130.00    | -0.56         | 0.00               | <b>(3).0000</b>  |
| P154 | 261.76         | 8.00             | 130.00    | -16.33        | 0.10               | 0.00             |
| P155 | 839.51         | 8.00             | 130.00    | -14.81        | 0.09               | 0.01             |
| P156 | 170.40         | 8.00             | 130.00    | 6.72          | 0.04               | €0.000           |
| P157 | 116.20         | 8.00             | 130.00    | 1.60          | 0.01               | OD.000O          |
| P158 | 248.92         | 8.00             | 130.00    | -16.52        | 0.11               | 0.00             |
| P159 | 247.10         | 8.00             | 130.00    | 16.81         | 0.11               | 0.00             |
| P160 | 247.67         | 8.00             | 130.00    | 40.55         | 0.26               | 0.01             |
| P161 | 247.82         | 8.00             | 130.00    | 64.00         | 0.41               | 0.03             |
| P162 | 247.00         | 8.00             | 130.00    | -39.21        | 0.25               | 0.01             |
| P163 | 249.87         | 8.00             | 130.00    | -26.44        | 0.17               | 0.01             |
| P164 | 1,149.31       | 8.00             | 130.00    | 14.39         | 0.09               | 0.01             |
| P165 | 710.72         | 12.00            | 130.00    | -87.39        | 0.25               | 0.02             |
| P166 | 369.00         | 8.00             | 130.00    | 35.58         | 0.23               | 0.01             |
| P167 | 253.00         | 8.00             | 130.00    | 26.35         | 0.17               | 0.01             |
| P168 | 918.21         | 8.00             | 130.00    | 22.90         | 0.15               | 0.02             |
| P169 | 282.81         | 8.00             | 130.00    | 58.88         | 0.38               | 0.03             |
| P170 | 333.36         | 12.00            | 130.00    | -131.02       | 0.37               | 0.02             |
| P171 | 253.00         | 8.00             | 130.00    | 92.24         | 0.59               | 0.06             |
| P172 | 234.54         | 8.00             | 130.00    | 66.34         | 0.42               | 0.03             |
| P173 | 253.00         | 8.00             | 130.00    | 55.78         | 0.36               | 0.02             |
| P174 | 657.99         | 8.00             | 130.00    | 29.09         | 0.19               | 0.02             |
| P175 | 633.34         | 8.00             | 130.00    | -9.93         | 0.06               | 0.00             |
| P176 | 253.02         | 8.00             | 130.00    | 20.83         | 0.13               | 0.00             |
| P177 | 633.34         | 8.00             | 130.00    | 78.20         | 0.50               | 0.10             |
| P178 | 242.02         | 12.00            | 130.00    | 346.27        | 0.98               | 0.09             |

PEAK HOUR DEMANDS - PIPE REPORT - GREENBRIAR **Headloss** Flow Velocity Diameter Length ID Roughness (ft/s) (ft) (gpm) (ft) (in) 0.09 0.75 117.92 253.00 8.00 130.00 P179 0.02 0.34 -53.51 273.00 8.00 130.00 P180 0.00 0.06 12.00 130.00 19.49 628.13 P181 0.01 40.00 0.11 12.00 130.00 797.55 P182 0.02 0.31 12.00 130.00 108.58 578.83 P183 0.000 0.06 130.00 -10.07 193.00 8.00 P184 0.09 0.00 13.61 8.00 130.00 653.19 P185 -1.49 0.01 O.0000 8.00 130.00 193.00 P186 0.00 0.000 130.00 0.05 P187 193.00 8.00 0.00 130.00 10.52 0.07 8.00 437.56 P188 0.09 0.000-30.07 130.00 203.57 12.00 P189 0.05 56.81 0.36 130.00 8.00 596.95 P190 O.000 -5.39 0.03 292.91 8.00 130.00 P191 0.04 O.000 -6.01 130.00 695.05 8.00 P192 O.000 0.07 130.00 10.45 253.00 8.00 P193 0.04 -43.77 0.28 130.00 8.00 656.00 P194 0.04 0.32 -50.27 8.00 130.00 504.88 P195 0.01 0.19 -30.39 313.32 8.00 130.00 P196 0.04 47.30 0.30 8.00 130.00 549.00 P197 0.01 0.23 36,22 253.00 8.00 130.00 P198 0.03 130.00 63.75 0.41 8.00 253.00 P199 0.07 0.66 8.00 130.00 102.92 253.00 P200 0.03 0.31 49.26 130.00 P201 403.00 8.00 0.21 130.00 179.36 1.14 8.00 276.11 P202 0.10 -129.21 0.82 130.00 253.02 00.8 P203 0.03 -61.41 0.39 130.00 253,02 8.00 P204 0.01 0.19 -30.21 8.00 130.00 236.90 P205 0.18 0.02 27.77 130.00 P206 636,18 8.00 0.00 0.17 130.00 27.35 211.30 8.00 P207 0.02 0.37 58.14 130.00 232.70 8.00 P208 0.05 94.54 0.60 130.00 233.00 8.00 P209 0.23 1.31 205.45 233.00 8.00 130.00 P210 0.81 0.25 -127.32 8.00 130.00 621.42 P211 0.03 0.45 8.00 130.00 -71.05 253.02 P212 0.01 0.12 130.00 -18.85 8.00 699.07 P213 0.00 130.00 -20.83 0.13 8.00 253.02 P214 -18.63 0.12 0.01 130.00 8.00 613.13 P215 0.29 0.02 45.67 130.00 P216 253.00 8.00 0.27 0.01 130.00 42.54 233.00 8.00 P217

PEAK HOUR DEMANDS - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|-----------------|
| P218 | 289.50         | 8.00             | 130.00    | 76.16         | 0.49               | 0.04            |
| P219 | 313.50         | 8.00             | 130.00    | -89.73        | 0.57               | 0.07            |
| P220 | 391.14         | 12.00            | 130.00    | . 412.63      | 1.17               | 0.19            |
| P221 | 590.71         | 8.00             | 130.00    | 30.58         | 0.20               | 0.02            |
| P222 | 253.00         | 8.00             | 130.00    | 32.84         | 0.21               | 0.01            |
| P223 | 390.32         | 8.00             | 130.00    | 73.19         | 0.47               | 0.06            |
| P224 | 430.55         | 8.00             | 130.00    | 51.51         | 0.33               | 0.03            |
| P225 | 248.33         | 12.00            | 130.00    | 330.19        | 0.94               | 0.08            |
| P226 | 430.73         | 8.00             | 130.00    | 30.69         | 0.20               | 0.01            |
| P227 | 412.22         | 12.00            | 130.00    | 264.51        | 0.75               | 0.09            |
| P228 | 262.25         | 12.00            | 130.00    | 33.51         | 0.10               | O.00            |
| P229 | 253.00         | 12.00            | 130.00    | 62.94         | 0.18               | 0.00            |
| P230 | 273.31         | 12.00            | 130.00    | 97.91         | 0.28               | O.01            |
| P231 | 234.73         | 12.00            | 130.00    | 175.03        | 0.50               | 0.02            |
| P232 | 422.16         | 12.00            | 130.00    | -177.45       | 0.50               | 0.04            |
| P233 | 596.34         | 12.00            | 130.00    | -152.46       | 0.43               | O.05            |
| P234 | 591.74         | 12.00            | 130.00    | -95.25        | 0.27               | 0.02            |
| P235 | 587.67         | 12.00            | 130.00    | -457.04       | 1.30               | <b>O.</b> 35    |
| P236 | 457.95         | 12.00            | 130.00    | -178.87       | 0.51               | O.05            |
| P237 | 359.68         | 12.00            | 130.00    | 55.68         | 0.16               | O.00            |
| P238 | 193.00         | 8.00             | 130.00    | -3.47         | 0.02               | O.0000          |
| P239 | 487.33         | 8.00             | 130.00    | 95.04         | 0.61               | 0.11            |
| P240 | 486.84         | 8.00             | 130.00    | -79.68        | 0.51               | 0.08            |
| P241 | 708.39         | 8.00             | 130.00    | -65.86        | 0.42               | O.08            |
| P242 | 617.10         | 8.00             | 130.00    | -60.72        | 0.39               | 0.06            |
| P243 | 319.69         | 18.00            | 130.00    | -585.83       | 0.74               | 0.04            |
| P244 | 861.88         | 12.00            | 130.00    | -54.77        | 0.16               | <b>O.</b> 01    |
| P245 | 534.05         | 18.00            | 130.00    | -346.68       | 0.44               | 0.03            |
| P246 | 627.02         | 18.00            | 130.00    | -255.42       | 0.32               | 0.02            |
| P247 | 195.01         | 18.00            | 130.00    | -348.10       | 0.44               | <b>O.</b> 01    |
| P248 | 751.91         | 18.00            | 130.00    | -3.24         | 0.00               | 000000          |
| P249 | 370.87         | 12.00            | 130.00    | -492.19       | 1.40               | 0.25            |
| P250 | 602.79         | 8.00             | 130.00    | -60.13        | 0.38               | 0.06            |
| P251 | 656.30         | 8.00             | 130.00    | -29.48        | 0.19               | 0.02            |
| P252 | 501.81         | 8.00             | 130.00    | -110.76       | 0.71               | 0.16            |
| P253 | 464.05         | 12.00            | 130.00    | 220.70        | 0.63               | 0.07            |
| P254 | 250.56         | 12.00            | 130.00    | 218.55        | 0.62               | <b>O</b> .04    |
| P255 | 423.72         | 8.00             | 130.00    | -31.49        | 0.20               | 0.01            |
| P256 | 235.04         | 8.00             | 130.00    | -42.48        | 0.27               | 0.01            |

PEAK HOUR DEMANDS - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|---------------|-----------|---------------|--------------------|-----------------|
| P257 | 344.48         | 8.00          | 130.00    | 69.15         | 0.44               | 0.04            |
| P258 | 656.00         | 8.00          | 130.00    | 35.42         | 0.23               | 0.02            |
| P259 | 497.14         | 8-00          | 130.00    | 36.01         | 0.23               | 0.02            |
| P260 | 494.52         | 8.00          | 130.00    | -14.26        | 0.09               | 0.00            |
| P261 | 466.36         | 8.00          | 130.00    | -11.66        | 0.07               | 0.00            |
| P262 | 616.00         | 8.00          | 130.00    | -8.18         | 0.05               | 0.00            |
| P263 | 651.25         | 8.00          | 130.00    | 6.14          | 0.04               | O.000           |
| P264 | 246.49         | 8.00          | 130.00    | 55.35         | 0.35               | 0.02            |
| P265 | 375.42         | 12.00         | 130.00    | -219.15       | 0.62               | 0.06            |
| P266 | 665.79         | 8.00          | 130.00    | 64.32         | 0.41               | 0.08            |
| P267 | 285.98         | 8.00          | 130.00    | -22.76        | 0.15               | O.00            |
| P268 | 272.69         | 8.00          | 130.00    | 23.52         | 0.15               | O.00            |
| P269 | 744.21         | 8.00          | 130.00    | 18.41         | 0.12               | O.01            |
| P270 | 105.50         | 8.00          | 130.00    | 4.99          | 0.03               | 0-0000          |
| P271 | 892.22         | 8.00          | 130.00    | 35.03         | 0.22               | O.03            |
| P272 | 193.00         | 8.00          | 130.00    | 12.55         | 0.08               | <b>O.00</b>     |
| P273 | 105.50         | 8.00          | 130.00    | 8.17          | 0.05               | O.000           |
| P274 | 698.75         | 8.00          | 130.00    | -9.78         | 0.06               | O.00            |
| P275 | 181.50         | 12.00         | 130.00    | -482.55       | 1.37               | 0.12            |
| P276 | 112.20         | 8.00          | 130.00    | -68.88        | 0.44               | <b>O</b> .01    |
| P277 | 698.70         | 8.00          | 130.00    | -28.31        | 0.18               | 0.02            |
| P278 | 713.00         | 8.00          | 130.00    | 80.0          | 0.000              | 0_00000         |
| P279 | 422.00         | 8.00          | 130.00    | -55.44        | 0.35               | 0.04            |
| P280 | 117.50         | 8.00          | 130.00    | 7.43          | 0.05               | ©.000           |
| P281 | 589.97         | 8.00          | 130.00    | -206.51       | 1.32               | 0.58            |
| P282 | 130.50         | 8.00          | 130.00    | -168.13       | 1.07               | 0.09            |
| P283 | 410.65         | 18.00         | 130.00    | -1,631.37     | 2.06               | 0.36            |
| P284 | 500.49         | 8.00          | 130.00    | -145.85       | 0.93               | 0.26            |
| P285 | 807.99         | 8.00          | 130.00    | 25.67         | 0.16               | 0.02            |
| P286 | 193.00         | 8.00          | 130.00    | 1.66          | 0.01               | OD_0000         |
| P287 | 263.00         | 8.00          | 130.00    | -6.12         | 0.04               | €0.000          |
| P288 | 738.30         | 8.00          | 130.00    | 24.81         | 0.16               | 0.01            |
| P289 | 233.02         | 8.00          | 130.00    | -36.35        | 0.23               | 0.01            |
| P290 | 739.64         | 8.00          | 130.00    | -76.92        | 0.49               | 0.12            |
| P291 | 252.00         | 8.00          | 130.00    | -39.98        | 0.26               | 0.01            |
| P292 | 262.03         | 8.00          | 130.00    | -57.99        | 0.37               | 0.02            |
| P293 | 924.17         | 8.00          | 130.00    | -11.20        | 0.07               | 0.00            |
| P294 | 770.75         | 8.00          | 130.00    | -8.31         | 0.05               | 0.00            |
| P295 | 956.68         | 8.00          | 130.00    | 30.26         | 0.19               | 0.03            |

PEAK HOUR DEMANDS - PIPE REPORT - GREENBRIAR Headloss Velocity Lenath Diameter Flow Roughness ID (ft) (gpm) (ft/s) (ft) (in) -99.09 0.63 0.18 693.81 8.00 130.00 P296 0.43 0.08 130.00 67.59 678.13 8.00 P297 0.02 26.73 0.17 8.00 130.00 837.42 P298 -78.16 0.09 557.94 8.00 130.00 0.50 P299 O.000 8.00 130.00 -6.040.04 696.14 P300 130.00 -10.16 0.06 0.00 468.04 8.00 P301 -42.34 0.27 O.01 8.00 130.00 255.36 P302 47.88 0.31 O.028.00 130.00 247.32 P303 130.00 -604.17 1.71 O.21 12.00 208.11 P304 O.000 130.00 17.49 0.11 8.00 P305 88.53 O.20 8.00 130.00 -210.11 1.34 193.00 P306 40.69 0.26  $\mathbf{O}.03$ 8.00 130.00 P307 582.27 130.00 -89.77 0.57 O.14 8.00 677.66 P308 O.04 -83.94 0.54 195.00 8.00 130.00 P309 -112.18 0.32 O.01 12.00 130.00 132.50 P310 O.08 0.58 8.00 130.00 -90.83 380.98 P311 -82.50 0.53 O.09 8.00 130.00 475.68 P312 O.01 8.00 130.00 -24.94 0.16 655.89 P313 O.03 -42.49 0.27 8.00 130.00 653.93 P314 8.00 130.00 1.02 0.01 0..0000 215.00 P315 O.00 130.00 26.63 0.17 195.01 8.00 P316 8.00 130.00 -22.53 0.14 **O.00** 214.88 P317 7.15 0.05 O.000 252.22 8.00 130.00 P318 9.45 0.06 O.000 8.00 130.00 P319 245.38 8.00 130.00 -7.51 0.05 0.00 607.50 P320 0.01 130.00 -18.87 0.12 8.00 574.53 P321 -55.77 0.36 0.01 8.00 130.00 105.50 P322 21.28 0.00 130.00 0.14 212.18 8.00 P323 O.000 12.55 0.08 130,00 105.50 8.00 P324 0.008.00 130.00 -21.80 0.14 211.00 P325 0.28 0.01 130.00 -43.77 8.00 211.30 P326 -32.35 0.21 0.01 8.00 130.00 209.82 P327 -17.26 0.01 130.00 0.11 728.60 8.00 P328 O.000 130.00 3.09 0.02 8.00 594.64 P329 O.00 8.00 130.00 -18.88 0.12 258.06 P330 10.46 0.07 0.00 130.00 8.00 499.01 P331 130.00 -28.34 0.18 0.01 545.88 8.00 P332 0.15 0.01 -22.96 783.02 8.00 130.00 P333 0.00 0.16 130.00 -54.97 260.55 12.00 P334

PEAK HOUR DEMANDS - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|-----------------|
| P335 | 255.00         | 8.00             | 130.00    | 30.71         | 0.20               | 0.01            |
| P336 | 255.00         | 8.00             | 130.00    | 21.86         | 0.14               | 0.00            |
| P337 | 255.07         | 8.00             | 130.00    | . 13.88       | 0.09               | 0.00            |
| P338 | 255.00         | 12.00            | 130.00    | 343.43        | 0.97               | 0.09            |
| P339 | 255.00         | 12.00            | 130.00    | -253.09       | 0.72               | 0.05            |
| P340 | 255.00         | 8.00             | 130.00    | -20.47        | 0.13               | 0.00            |
| P341 | 255.00         | 8.00             | 130.00    | -24.58        | 0.16               | 0.00            |
| P342 | 246.98         | 8.00             | 130.00    | -14.39        | 0.09               | 0.00            |
| P343 | 253.00         | 8.00             | 130.00    | -55.34        | 0.35               | 0.02            |
| P344 | 147.50         | 12.00            | 130.00    | 98.39         | 0.28               | 0.01            |
| P345 | 147.37         | 12.00            | 130.00    | 173.44        | 0.49               | 0.01            |
| P346 | 147.50         | 12.00            | 130.00    | 224.22        | 0.64               | 0.02            |
| P347 | 147.59         | 12.00            | 130.00    | -235.28       | 0.67               | 0.03            |
| P348 | 381.04         | 8.00             | 130.00    | -41.22        | 0.26               | 0.02            |
| P349 | 190.72         | 18.00            | 130.00    | -668.54       | 0.84               | 0.03            |
| P350 | 253.02         | 8.00             | 130.00    | 30.07         | 0.19               | 0.01            |
| P351 | 233.00         | 8.00             | 130.00    | -2.37         | 0.02               | O.0000          |
| P352 | 1,365.42       | 24.00            | 130.00    | 1,175.44      | 0.83               | 0.16            |
| P353 | 1,505.76       | 30.00            | 130.00    | -1,175.44     | 0.53               | 0.06            |
| P354 | 369.99         | 8.00             | 130.00    | -68.12        | 0.43               | 0.05            |
| P355 | 369.99         | 8.00             | 130.00    | -78.97        | 0.50               | 0.06            |
| P356 | 117.50         | 8.00             | 130.00    | -30.82        | 0.20               | 0.00            |
| P357 | 195.00         | 8.00             | 130.00    | -63.33        | 0.40               | 0.02            |
| P358 | 193.00         | 8.00             | 130.00    | -65.67        | 0.42               | 0.02            |
| P359 | 500.49         | 8.00             | 130.00    | -113.99       | 0.73               | 0.16            |
| P360 | 500.78         | 8.00             | 130.00    | -168.25       | 1.07               | 0.34            |
| P361 | 677.66         | 8.00             | 130.00    | -88.73        | 0.57               | 0.14            |
| P362 | 482.45         | 12.00            | 130.00    | -50.16        | 0.14               | 0.00            |
| P363 | 677.66         | 8.00             | 130.00    | -84.91        | 0.54               | 0.13            |
| P364 | 1,180.18       | 30.00            | 130.00    | -804.97       | 0.37               | 0.02            |
| P365 | 1,577.01       | 24.00            | 130.00    | -1,664.46     | 1.18               | 0.35            |
| P366 | 701.50         | 24.00            | 130.00    | -1,914.52     | 1.36               | 0.20            |
| P367 | 242.00         | 18.00            | 130.00    | 1,211.61      | 1.53               | 0.12            |
| P368 | 738.68         | 18.00            | 130.00    | 987.40        | 1.24               | 0.25            |
| P369 | 253.00         | 8.00             | 130.00    | -11.44        | 0.07               | 0.00            |
| P370 | 660.09         | 8.00             | 130.00    | -79.09        | 0.50               | 0.11            |
| P371 | 193.00         | 18.00            | 130.00    | 1,067.64      | 1.35               | 0.08            |
| P372 | 595.91         | 18.00            | 130.00    | 890.95        | 1.12               | 0.17            |
| P373 | 191.34         | 18.00            | 130.00    | 774.65        | 0.98               | 0.04            |

PEAK HOUR DEMANDS - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos (ft) |
|------|----------------|------------------|-----------|---------------|--------------------|--------------|
| P374 | 105.50         | 8.00             | 130.00    | 20.41         | 0.13               | 0.00         |
| P375 | 607.50         | 8.00             | 130.00    | -22.41        | 0.14               | 0.01         |
| P376 | 438.00         | 18.00 ·          | 130.00    | 618.51        | 0.78               | 0.06         |
| P377 | 650.57         | 18.00            | 130.00    | 445.07        | 0.56               | 0.05         |
| P378 | 112.20         | 8.00             | 130.00    | -173.38       | 1.11               | 0.08         |
| P379 | 117.50         | 8.00             | 130.00    | 70.01         | 0.45               | 0.02         |
| P380 | 348.36         | 8.00             | 130.00    | 35.30         | 0.23               | 0.01         |
| P381 | 178.10         | 12.00            | 130.00    | -243.60       | 0.69               | 0.03         |
| P382 | 1,122.42       | 24.00            | 130.00    | -3,545.90     | 2.51               | 1.01         |
| P383 | 93.09          | 8.00             | 130.00    | -88.83        | 0.57               | 0.02         |
| P384 | 195.01         | 8.00             | 130.00    | 37.08         | 0.24               | 0.01         |
| P385 | 4,416.05       | 30.00            | 130.00    | 406.65        | 0.18               | 0.02         |
| P386 | 3,100.00       | 24.00            | 130.00    | -3,582.44     | 2.54               | 2.85         |
| P388 | 1,581.75       | 18.00            | 130.00    | 551.87        | 0.70               | 0.19         |
| P389 | 621.96         | 18.00            | 130.00    | 510.24        | 0.64               | 0.06         |
| P990 | 235.86         | 99.00            | 130.00    | 406.65        | 0.02               | 0.00000      |
| P991 | 377.34         | 99.00            | 130.00    | 406.65        | 0.02               | 0.00000      |
| P992 | 233.99         | 99.00            | 130.00    | 3,582.44      | 0.15               | 0.000        |
| P993 | 232.72         | 99.00            | 130.00    | 3,582.44      | 0.15               | 0.000        |

### PEAK HOUR DEMANDS - PUMP REPORT - GREENBRIAR

| D       | Elevation<br>(ft) | Downstream Pressure<br>(psi) | Flow<br>(gpm) | Head Gain<br>(ft) |
|---------|-------------------|------------------------------|---------------|-------------------|
| PUMP105 | 22.00             | 30.01                        | 406.65        | 91.25             |
| PUMP107 | 26.00             | 30.28                        | 3,582.44      | 95.89             |



## FIRE FLOW SUMMARY

FIRE FLOW SUMMARY - GREENBRIAR Available **Available Flow** Available Flow Residual Static Fire-Flow Static Flow Head @Hydrant **Pressure** Pressure Pressure Demand ID Demand (ft) (psi) (gpm) (psi) (psi) (gpm) (gpm) 62.03 30.83 6,159.42 20.38 1,500.00 4.98 33.93 **GB-103** 65.88 26.14 5,607.58 20.31 4.98 32.32 3,000.00 **GB-105** 20.30 66.86 25.81 5,517.28 31.96 3,000.00 0.00 **GB-107** 67.86 25.73 5,561.93 20.31 28.11 31.85 3,000.00 **GB-108** 20.05 66.28 2,345.20 1,500.00 25.47 30.65 31.64 **GB-109** 2,841.32 20.08 66.34 26.71 31.64 1,500.00 17.03 **GB-111** 65.98 27.42 3,191.37 20.10 31.83 1,500.00 15.33 **GB-113** 20.23 65.65 28.83 4,775.91 1,500.00 32.17 25.54 **GB-115** 65.26 1,500.00 27.66 3,203.48 20.10 17.03 32.15 **GB-117** 2,953.26 20.09 65.19 1,500.00 27.27 32.16 19.36 **GB-119** 65.10 1,500.00 26.33 2,511.07 20.06 32.18 15.33 **GB-121** 20.21 65.45 3,000.00 25.08 4,639.70 28.53 32.40 **GB-122** 27.73 3,288.68 20.11 65.42 1,500.00 14.47 32.08 **GB-123** 20.15 64.89 28.48 3,862.46 1,500.00 24.69 32.36 **GB-125** 27.96 64.68 3,282.36 20.11 1,500.00 13.62 32.40 **GB-127** 65.32 5,416.21 20.29 25.95 41.75 32.50 3,000.00 **GB-128** 64.94 3,379,10 20.11 27.98 14.47 32.29 1,500.00 **GB-129** 64.29 28.59 3,780.26 20.14 32.60 1,500.00 23.84 **GB-131** 64.09 3,371.23 20.11 28.25 13.62 32.66 1,500.00 **GB-133** 20.12 63.67 1,500.00 28.55 3,493.10 11.92 32.86 **GB-135** 63.69 20.16 24.20 4,056.59 17.03 32.93 3,000.00 **GB-137** 20.28 64.66 26.00 5,318.00 32.69 3,000.00 **GB-139** 17.03 65.28 32.11 1,500.00 27.36 3,047.64 20.09 36.61 **GB-141** 64.96 20.12 28.13 3,544.15 32.28 1,500.00 22.13 **GB-143** 64.56 1,500.00 28.48 3.746.30 20.14 32.47 11.92 **GB-145** 63.73 28.84 3,857.34 20.15 32.84 1,500.00 22.32 **GB-147** 28.59 3,567.37 20.13 63.66 1.500.00 32.85 16.18 **GB-149** 63.47 20.14 32.95 1,500.00 28.87 3.787.15 18.73 **GB-151** 20.11 63.41 28.49 3.393.38 1,500.00 19.36 32.96 **GB-153** 20.14 63.42 28.89 3.751.25 6.82 32.98 1,500.00 **GB-155** 63.44 28.89 3,751.56 20.14 2.56 32.97 1,500.00 **GB-157** 63.14 29.22 3,946.16 20.16 33,14 1,500.00 5.76 **GB-159** 63.64 20.15 4.26 32.90 1,500.00 28.91 3,832.71 **GB-161** 20.15 63.89 3,874.29 1,500.00 28.86 32.81 9.36 **GB-163** 64.59 25.96 5,267.08 20.28 32.69 3,000.00 10.21 **GB-165** 65.01 25.62 5,107.67 20.26 3,000.00 23.73 32.47 **GB-167** 4,622.24 20.21 66.40 24.67 31.77 3,000.00 4.26 **GB-169** 20.20 66.89 31.53 3,000.00 24.37 4.498.42 8.51 **GB-171** 

| ID     | Static<br>Demand<br>(gpm) | Static<br>Pressure<br>(psi) | Fire-Flow<br>Demand<br>(gpm) | Residual<br>Pressure<br>(psi) | Available Flow<br>@Hydrant<br>(gpm) | Available Flow<br>Pressure<br>(psi) | Available<br>Flow Head<br>(ft) |
|--------|---------------------------|-----------------------------|------------------------------|-------------------------------|-------------------------------------|-------------------------------------|--------------------------------|
| GB-173 | 28.46                     | 31.28                       | 3,000.00                     | 24.06                         | 4,403.34                            | 20.19                               | 67.44                          |
| GB-175 | 1.70                      | 33.08                       | 1,500.00                     | 28.54                         | 3,338.28                            | 20.11                               | 63.10                          |
| GB-177 | 5.96                      | 33.17                       | 1,500.00                     | 28.27                         | 3,095.23                            | 20.10                               | 62.83                          |
| GB-179 | 10.21                     | 33.02                       | 1,500.00                     | 28.73                         | 3,562.26                            | 20.13                               | 63.27                          |
| GB-181 | 5.96                      | 33.10                       | 1,500.00                     | 28.86                         | 3,622.67                            | 20.13                               | 63.09                          |
| GB-183 | 20.44                     | 33.14                       | 1,500.00                     | 28.96                         | 3,718.53                            | 20.14                               | 63.01                          |
| GB-185 | 34.06                     | 33.10                       | 1,500.00                     | 28.80                         | 3,619.14                            | 20.13                               | 63.10                          |
| GB-187 | 18.73                     | 33.17                       | 1,500.00                     | 28.46                         | 3,241.56                            | 20.10                               | 62.87                          |
| GB-189 | 8.51                      | 33.22                       | 1,500.00                     | 27.73                         | 2,805.68                            | 20.08                               | 62.70                          |
| GB-191 | 18.53                     | 33.26                       | 1,500.00                     | 28.61                         | 3,307.49                            | 20.11                               | 62.68                          |
| GB-193 | 11.67                     | 33.27                       | 1,500.00                     | 28.38                         | 3,133.40                            | 20.10                               | 62.62                          |
| GB-195 | 11.67                     | 33.19                       | 1,500.00                     | 28.79                         | 3,497.85                            | 20.12                               | 62.82                          |
| GB-197 | 20.44                     | 33.03                       | 1,500.00                     | 29.00                         | 3,862.83                            | 20.15                               | 63.24                          |
| GB-199 | 20.44                     | 32.80                       | 1,500.00                     | 28.91                         | 3,985.22                            | 20.16                               | 63.81                          |
| GB-201 | 23.84                     | 32.60                       | 1,500.00                     | 28.71                         | 3,935.49                            | 20.15                               | 64.28                          |
| GB-203 | 30.53                     | 32.39                       | 1,500.00                     | 28.07                         | 3,420.76                            | 20.11                               | 64.67                          |
| GB-205 | 30.53                     | 31.69                       | 1,500.00                     | 27.19                         | 3,164.05                            | 20.10                               | 66.21                          |
| GB-207 | 23.84                     | 31.47                       | 1,500.00                     | 27.33                         | 3,442.70                            | 20.12                               | 66.77                          |
| GB-209 | 11.92                     | 31.25                       | 1,500.00                     | 26.75                         | 3,060.29                            | 20.09                               | 67.22                          |
| GB-210 | 18.62                     | 33.84                       | 1,500.00                     | 30.77                         | 6,181.89                            | 20.38                               | 62.03                          |
| GB-211 | 45.98                     | 32.27                       | 1,500.00                     | 28.92                         | 4,738.69                            | 20.22                               | 65.27                          |
| GB-213 | 22.13                     | 32.59                       | 1,500.00                     | 28.75                         | 3,945.91                            | 20.15                               | 64.31                          |
| GB-215 | 29.98                     | 32.86                       | 1,500.00                     | 28.87                         | 3,836.14                            | 20.14                               | 63.65                          |
| GB-217 | 11.92                     | 33.17                       | 1,500.00                     | 28.67                         | 3,369.67                            | 20.11                               | 62.87                          |
| GB-219 | 12.77                     | 33.14                       | 1,500.00                     | 25.76                         | 2,214.02                            | 20.05                               | 62.60                          |
| GB-221 | 17.33                     | 33.15                       | 1,500.00                     | 27.63                         | 2,828.01                            | 20.08                               | 62.64                          |
| GB-223 | 18.44                     | 33.03                       | 1,500.00                     | 26.56                         | 2,440.04                            | 20.06                               | 62.87                          |
| GB-225 | 10.21                     | 33.01                       | 1,500.00                     | 26.65                         | 2,465.51                            | 20.06                               | 62.93                          |
| GB-227 | 11.07                     | 33.06                       | 1,500.00                     | 26.51                         | 2,413.77                            | 20.06                               | 62.81                          |
| GB-229 | 18.87                     | 32.99                       | 1,500.00                     | 27.51                         | 2,822.52                            | 20.08                               | 62.99                          |
| GB-231 | 18.73                     | 32.99                       | 1,500.00                     | 27.60                         | 2,864.81                            | 20.08                               | 63.00                          |
| GB-233 | 11.92                     | 33.02                       | 1,500.00                     | 27.65                         | 2,872.07                            | 20.08                               | 62.94                          |
| GB-235 | 18.73                     | 32.83                       | 1,500.00                     | 27.81                         | 3,033.46                            | 20.09                               | 63.41                          |
| GB-237 | 12.52                     | 33.05                       | 1,500.00                     | 27.95                         | 3,014.38                            | 20.09                               | 62.90                          |
| GB-239 | 12.52                     | 33.15                       | 1,500.00                     | 28.89                         | 3,637.50                            | 20.13                               | 62.84                          |
| GB-241 | 23.84                     | 32.99                       | 1,500.00                     | 29.08                         | 4,021.44                            | 20.16                               | 63.27                          |
| GB-243 | 25.54                     | 32.76                       | 1,500.00                     | 28.87                         | 4,000.00                            | 20.16                               | 63.80                          |
| GB-245 | 23.84                     | 32.56                       | 1,500.00                     | 28.31                         | 3,533.45                            | 20.12                               | 64.21                          |

| FIRE FLOW | SUMMARY | - GHEENBI | HIAH |
|-----------|---------|-----------|------|
|           | Static  | Static    | Fire |

| ID     | Static<br>Demand<br>(gpm) | Static<br>Pressure<br>(psi) | Fire-Flow<br>Demand<br>(gpm) | Residual<br>Pressure<br>(psi) | Available Flow<br>@Hydrant<br>(gpm) | Available Flow<br>Pressure<br>(psi) | Available<br>Flow Head<br>(ft) |
|--------|---------------------------|-----------------------------|------------------------------|-------------------------------|-------------------------------------|-------------------------------------|--------------------------------|
| GB-247 | 16.18                     | 32.35                       | 1,500.00                     | 27.92                         | 3,301.79                            | 20.11                               | 64.65                          |
| GB-249 | 35.65                     | 31.89                       | 1,500.00                     | 27.55                         | 3,335.70                            | 20.11                               | 65.71                          |
| GB-251 | 16.18                     | 31.65                       | 1,500.00                     | 27.20                         | 3,173.60                            | 20.10                               | 66.26                          |
| GB-253 | 23.84                     | 31.44                       | 1,500.00                     | 26.94                         | 3,108.70                            | 20.10                               | 66.74                          |
| GB-255 | 31.86                     | 31.22                       | 1,500.00                     | 26.71                         | 3,065.55                            | 20.09                               | 67.23                          |
| GB-257 | 21.28                     | 32.44                       | 1,500.00                     | 28.30                         | 3,549.74                            | 20.12                               | 64.59                          |
| GB-259 | 10.21                     | 32.59                       | 1,500.00                     | 28.32                         | 3,438.90                            | 20.12                               | 64.21                          |
| GB-261 | 11.07                     | 32.86                       | 1,500.00                     | 28.54                         | 3,459.40                            | 20.12                               | 63.58                          |
| GB-263 | 12.77                     | 33.16                       | 1,500.00                     | 28.92                         | 3,605.26                            | 20.13                               | 62.91                          |
| GB-265 | 24.97                     | 32.50                       | 1,500.00                     | 28.68                         | 3,945.26                            | 20.15                               | 64.51                          |
| GB-267 | 19.87                     | 33.14                       | 1,500.00                     | 29.29                         | 4,054.85                            | 20.16                               | 62.99                          |
| GB-269 | 18.73                     | 33.06                       | 1,500.00                     | 28.60                         | 3,453.27                            | 20.12                               | 62.95                          |
| GB-271 | 17.88                     | 32.66                       | 1,500.00                     | 27.62                         | 2,983.15                            | 20.09                               | 63.81                          |
| GB-273 | 10.21                     | 32.42                       | 1,500.00                     | 27.75                         | 3,168.16                            | 20.10                               | 64.39                          |
| GB-275 | 9.50                      | 32.42                       | 1,500.00                     | 28.39                         | 3,777.39                            | 20.14                               | 64.49                          |
| GB-277 | 10.21                     | 32.41                       | 1,500.00                     | 27.94                         | 3,315.85                            | 20.11                               | 64.41                          |
| GB-279 | 18.73                     | 32.52                       | 1,500.00                     | 27.81                         | 3,171.40                            | 20.10                               | 64.15                          |
| GB-281 | 9.36                      | 32.83                       | 1,500.00                     | 28.56                         | 3,604.35                            | 20.13                               | 63.50                          |
| GB-283 | 21.28                     | 32.74                       | 2,000.00                     | 27.11                         | 3,883.79                            | 20.15                               | 63.78                          |
| GB-285 | 25.54                     | 31.77                       | 2,000.00                     | 27.04                         | 4,555.76                            | 20.21                               | 66.15                          |
| GB-286 | 17.03                     | 31.21                       | 2,000.00                     | 26.46                         | 4,328.61                            | 20.19                               | 67.45                          |
| GB-287 | 17.03                     | 32.50                       | 1,500.00                     | 29.17                         | 4,874.71                            | 20.24                               | 64.70                          |
| GB-288 | 9.36                      | 33.13                       | 1,500.00                     | 29.73                         | 4,955.80                            | 20.24                               | 63.17                          |
| GB-289 | 6.82                      | 33.07                       | 1,500.00                     | 29.50                         | 4,597.56                            | 20.21                               | 63.16                          |
| GB-290 | 11.07                     | 32.42                       | 1,500.00                     | 28.88                         | 4,508.35                            | 20.20                               | 64.62                          |
| GB-291 | 16.18                     | 32.84                       | 1,500.00                     | 29.21                         | 4,493.08                            | 20.20                               | 63.66                          |
| GB-292 | 7.66                      | 33.13                       | 1,500.00                     | 28.65                         | 3,412.75                            | 20.12                               | 62.79                          |
| GB-293 | 13.62                     | 32.97                       | 1,500.00                     | 29.43                         | 4,719.17                            | 20.22                               | 63.41                          |
| GB-294 | 10.56                     | 32.73                       | 1,500.00                     | 29.17                         | 4,603.72                            | 20.21                               | 63.92                          |
| GB-295 | 0.00                      | 33.83                       | 1,500.00                     | 30.77                         | 6,188.37                            | 20.38                               | 62.04                          |
| GB-297 | 0.00                      | 32.51                       | 1,500.00                     | 29.36                         | 5,481.34                            | 20.30                               | 64.85                          |
| GB-299 | 0.00                      | 33.12                       | 1,500.00                     | 29.84                         | 5,391.14                            | 20.29                               | 63.28                          |
| GB-301 | 0.00                      | 33.07                       | 1,500.00                     | 29.72                         | 5,177.82                            | 20.27                               | 63.31                          |
| GB-303 | 0.00                      | 32.43                       | 1,500.00                     | 29.02                         | 4,848.96                            | 20.24                               | 64.70                          |
| GB-305 | 0.00                      | 32.83                       | 1,500.00                     | 29.41                         | 4,974.29                            | 20.25                               | 63.78                          |
| GB-307 | 0.00                      | 32.91                       | 3,000.00                     | 25.77                         | 5,019.08                            | 20.25                               | 63.60                          |
| GB-309 | 0.00                      | 32.73                       | 3,000.00                     | 25.57                         | 4,952.25                            | 20.25                               | 64.00                          |
| GB-311 | 32.39                     | 31.93                       | 2,000.00                     | 27.19                         | 4,616.43                            | 20.21                               | 65.77                          |

| ID     | Static<br>Demand<br>(gpm) | Static<br>Pressure<br>(psi) | Fire-Flow<br>Demand<br>(gpm) | Residual<br>Pressure<br>(psi) | Available Flow<br>@Hydrant<br>(gpm) | Available Flow<br>Pressure<br>(psi) | Available<br>Flow Head<br>(ft) |
|--------|---------------------------|-----------------------------|------------------------------|-------------------------------|-------------------------------------|-------------------------------------|--------------------------------|
| GB-313 | 42.13                     | 31.20                       | 2,000.00                     | 22.91                         | 2,513.26                            | 20.06                               | 67.10                          |
| GB-315 | 15.33                     | 32.31                       | 1,500.00                     | 25.48                         | 2,258.49                            | 20.05                               | 64.27                          |
| GB-317 | 14.47                     | 32.42                       | 1,500.00                     | 26.87                         | 2,720.56                            | 20.07                               | 64.10                          |
| GB-319 | 9.36                      | 32.67                       | 1,500.00                     | 27.90                         | 3,172.76                            | 20.10                               | 63.63                          |
| GB-321 | 9.36                      | 33.07                       | 1,500.00                     | 29.36                         | 4,483.37                            | 20.20                               | 63.07                          |
| GB-323 | 22.13                     | 32.92                       | 1,500.00                     | 25.35                         | 2,172.41                            | 20.05                               | 62.80                          |
| GB-325 | 17.88                     | 32.54                       | 1,500.00                     | 26.26                         | 2,467.43                            | 20.06                               | 63.72                          |
| GB-327 | 14.47                     | 32.29                       | 1,500.00                     | 26.48                         | 2,603.25                            | 20.07                               | 64.31                          |
| GB-329 | 10.21                     | 32.29                       | 1,500.00                     | 26.67                         | 2,676.70                            | 20.07                               | 64.32                          |
| GB-331 | 4.26                      | 32.56                       | 1,500.00                     | 26.63                         | 2,573.60                            | 20.07                               | 63.70                          |
| GB-333 | 11.92                     | 32.62                       | 1,500.00                     | 27.82                         | 3,158.86                            | 20.10                               | 63.74                          |
| GB-335 | 10.21                     | 33.03                       | 1,500.00                     | 29.03                         | 4,037.36                            | 20.16                               | 62.95                          |
| GB-337 | 18.73                     | 32.31                       | 1,500.00                     | 26.60                         | 2,639.88                            | 20.07                               | 64.32                          |
| GB-339 | 16.18                     | 32.31                       | 1,500.00                     | 27.29                         | 2,987.14                            | 20.09                               | 64.36                          |
| GB-341 | 13.45                     | 32.54                       | 1,500.00                     | 27.91                         | 3,281.56                            | 20.11                               | 63.89                          |
| GB-343 | 10.90                     | 33.12                       | 1,500.00                     | 29.01                         | 3,933.79                            | 20.15                               | 62.67                          |
| GB-345 | 14.47                     | 32.30                       | 1,500.00                     | 26.69                         | 2,685.95                            | 20.07                               | 64.32                          |
| GB-347 | 17.03                     | 32.30                       | 1,500.00                     | 27.21                         | 2,951.87                            | 20.09                               | 64.36                          |
| GB-349 | 6.82                      | 32.41                       | 1,500.00                     | 27.16                         | 2,861.15                            | 20.08                               | 64.10                          |
| GB-351 | 21.28                     | 32.29                       | 1,500.00                     | 26.16                         | 2,478.62                            | 20.06                               | 64.30                          |
| GB-352 | 30.14                     | 32.57                       | 1,500.00                     | 26.95                         | 2,741.14                            | 20.07                               | 63.68                          |
| GB-353 | 16.18                     | 32.33                       | 1,500.00                     | 26.67                         | 2,667.15                            | 20.07                               | 64.23                          |
| GB-355 | 13.62                     | 32.38                       | 1,500.00                     | 26.96                         | 2,788.57                            | 20.08                               | 64.15                          |
| GB-357 | 15.16                     | 32.56                       | 1,500.00                     | 27.34                         | 2,912.95                            | 20.08                               | 63.76                          |
| GB-359 | 11.75                     | 33.11                       | 1,500.00                     | 28.90                         | 3,841.42                            | 20.15                               | 62.64                          |
| GB-361 | 16.18                     | 32.61                       | 1,500.00                     | 27.34                         | 2,899.48                            | 20.08                               | 63.61                          |
| GB-362 | 20.44                     | 33.00                       | 1,500.00                     | 28.75                         | 3,791.25                            | 20.14                               | 62.87                          |
| GB-363 | 11.07                     | 33.03                       | 1,500.00                     | 28.65                         | 3,667.14                            | 20.13                               | 62.75                          |
| GB-365 | 14.18                     | 33.02                       | 1,500.00                     | 28.74                         | 3,769.26                            | 20.14                               | 62.80                          |
| GB-367 | 19.23                     | 32.90                       | 1,500.00                     | 28.19                         | 3,323.12                            | 20.11                               | 63.00                          |
| GB-369 | 17.03                     | 32.71                       | 1,500.00                     | 27.24                         | 2,825.30                            | 20.08                               | 63.37                          |
| GB-371 | 13.62                     | 32.78                       | 1,500.00                     | 27.18                         | 2,773.44                            | 20.08                               | 63.20                          |
| GB-373 | 10.21                     | 32.84                       | 1,500.00                     | 27.49                         | 2,894.56                            | 20.08                               | 63.08                          |
| GB-375 | 14.73                     | 32.91                       | 1,500.00                     | 28.28                         | 3,388.22                            | 20.11                               | 63.01                          |
| GB-377 | 18.32                     | 33.02                       | 3,000.00                     | 23.28                         | 3,770.82                            | 20.14                               | 62.82                          |
| GB-379 | 45.40                     | 32.72                       | 3,000.00                     | 24.15                         | 4,164.60                            | 20.17                               | 63.63                          |
| GB-381 | 25.98                     | 32.97                       | 2,000.00                     | 25.20                         | 2,943.97                            | 20.09                               | 62.77                          |
| GB-383 | 17.47                     | 32.16                       | 2,000.00                     | 26.18                         | 3,611.27                            | 20.13                               | 64.75                          |

FIRE FLOW SUMMARY - GREENBRIAR

| ID     | Static<br>Demand<br>(gpm) | Static<br>Pressure<br>(psi) | Fire-Flow<br>Demand<br>(gpm) | Residual<br>Pressure<br>(psi) | Available Flow<br>@Hydrant<br>(gpm) | Available Flow<br>Pressure<br>(psi) | Available<br>Flow Head<br>(ft) |
|--------|---------------------------|-----------------------------|------------------------------|-------------------------------|-------------------------------------|-------------------------------------|--------------------------------|
| GB-385 | 10.65                     | 32.27                       | 2,000.00                     | 26.68                         | 3,905.49                            | 20.15                               | 64.60                          |
| GB-387 | 15.35                     | 31.95                       | 2,000.00                     | 26.35                         | 3,817.00                            | 20.14                               | 65.31                          |
| GB-389 | 9.36                      | 31.98                       | 2,000.00                     | 26.40                         | 3,822.78                            | 20.15                               | 65.28                          |
| GB-391 | 38.21                     | 32.01                       | 2,000.00                     | 26.62                         | 3,996.05                            | 20.16                               | 65.29                          |
| GB-393 | 15.03                     | 32.96                       | 1,500.00                     | 27.73                         | 2,991.29                            | 20.09                               | 62.79                          |
| GB-395 | 15.33                     | 32.40                       | 1,500.00                     | 27.14                         | 2,883.41                            | 20.08                               | 64.05                          |
| GB-397 | 37.53                     | 31.94                       | 1,500.00                     | 27.61                         | 3,517.00                            | 20.12                               | 65.24                          |
| GB-399 | 34.97                     | 31.52                       | 1,500.00                     | 27.26                         | 3,461.10                            | 20.12                               | 66.22                          |
| GB-401 | 19.59                     | 31.39                       | 1,500.00                     | 26.79                         | 3,102.97                            | 20.10                               | 66.47                          |
| GB-403 | 11.07                     | 31.26                       | 2,000.00                     | 23.78                         | 2,726.93                            | 20.07                               | 66.72                          |
| GB-405 | 11.57                     | 33.09                       | 1,500.00                     | 27.82                         | 2,984.60                            | 20.09                               | 62.49                          |
| GB-407 | 22.13                     | 32.30                       | 1,500.00                     | 27.43                         | 3,110.22                            | 20.10                               | 64.33                          |
| GB-409 | 13.62                     | 31.67                       | 3,000.00                     | 21.70                         | 3,387.61                            | 20.11                               | 65.82                          |
| GB-411 | 17.03                     | 32.95                       | 1,500.00                     | 27.78                         | 3,024.39                            | 20.09                               | 62.82                          |
| GB-413 | 26.39                     | 32.19                       | 1,500.00                     | 27.39                         | 3,140.88                            | 20.10                               | 64.58                          |
| GB-415 | 13.62                     | 31.43                       | 3,000.00                     | 21.44                         | 3,323.05                            | 20.11                               | 66.37                          |
| GB-417 | 35.25                     | 32.95                       | 1,500.00                     | 28.50                         | 3,616.19                            | 20.13                               | 62.90                          |
| GB-419 | 11.07                     | 32.00                       | 1,500.00                     | 27.50                         | 3,324.01                            | 20.11                               | 65.04                          |
| GB-421 | 33.40                     | 31.48                       | 1,500.00                     | 26.97                         | 3,238.24                            | 20.10                               | 66.23                          |
| GB-423 | 11.07                     | 31.32                       | 1,500.00                     | 26.87                         | 3,228.65                            | 20.10                               | 66.60                          |
| GB-425 | 22.08                     | 31.17                       | 3,000.00                     | 21.29                         | 3,300.42                            | 20.11                               | 66.97                          |
| GB-427 | 11.07                     | 30.73                       | 3,000.00                     | 20.49                         | 3,099.96                            | 20.10                               | 67.96                          |
| GB-429 | 27.19                     | 30.93                       | 3,000.00                     | 20.75                         | 3,173.73                            | 20.10                               | <b>6</b> 7.52                  |
| GB-431 | 22.13                     | 30.79                       | 1,500.00                     | 25.95                         | 2,846.20                            | 20.08                               | 67.79                          |
| GB-433 | 34.25                     | 30.55                       | 1,500.00                     | 25.09                         | 2,479.40                            | 20.06                               | 68.30                          |
| GB-435 | 17.03                     | 30.86                       | 1,500.00                     | 25.50                         | 2,570.60                            | 20.07                               | 67.58                          |
| GB-437 | 17.88                     | 30.54                       | 1,500.00                     | 25.58                         | 2,726.65                            | 20.07                               | 68.33                          |
| GB-439 | 17.88                     | 30.55                       | 1,500.00                     | 25.05                         | 2,449.12                            | 20.06                               | 68.29                          |
| GB-441 | 11.07                     | 30.86                       | 1,500.00                     | 25.33                         | 2,487.09                            | 20.06                               | 67.57                          |
| GB-443 | 11.92                     | 30.54                       | 1,500.00                     | 25.00                         | 2,423.28                            | 20.06                               | 68.29                          |
| GB-445 | 11.07                     | 30.98                       | 1,500.00                     | 25.33                         | 2,452.15                            | 20.06                               | 67.29                          |



## MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - JUNCTION REPORT - GREENBRIAR

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-101 | 0.00            | 20.00             | 86.23        | 28.70             |
| GB-103 | 4.98            | 15.00             | 86.41        | 30.94             |
| GB-105 | 4.98            | 19.00             | 86.78        | 29.37             |
| GB-107 | 0.00            | 20.00             | 87.00        | 29.03             |
| GB-108 | 28.11           | 21.00             | 88.16        | 29.10             |
| GB-109 | 30.65           | 20.00             | 86.00        | 28.60             |
| GB-111 | 17.03           | 20.00             | 86.00        | 28.60             |
| GB-113 | 15.33           | 19.59             | 86.04        | 28.79             |
| GB-115 | 25.54           | 18.97             | 86.29        | 29.17             |
| GB-117 | 17.03           | 18.87             | 86.04        | 29.11             |
| GB-119 | 19.36           | 18.84             | 86.02        | 29.11             |
| GB-121 | 15.33           | 18.80             | 86.02        | 29.12             |
| GB-122 | 28.53           | 18.80             | 86.75        | 29.44             |
| GB-123 | 14.47           | 19.02             | 86.03        | 29.04             |
| GB-125 | 24.69           | 18.39             | 86.07        | 29.32             |
| GB-127 | 13.62           | 18.28             | 86.03        | 29.36             |
| GB-128 | 41.75           | 18.50             | 86.55        | 29.48             |
| GB-129 | 14.47           | 18.53             | 86.01        | 29.24             |
| GB-131 | 23.84           | 17.81             | 86.01        | 29.55             |
| GB-133 | 13.62           | 17.67             | 86.01        | 29.61             |
| GB-135 | 11.92           | 17.23             | 86.02        | 29.80             |
| GB-137 | 17.03           | 17.16             | 86.09        | 29.87             |
| GB-139 | 17.03           | 17.85             | 86.17        | 29.60             |
| GB-141 | 36.61           | 18.91             | 86.00        | 29.07             |
| GB-143 | 22.13           | 18.52             | 85.99        | 29.23             |
| GB-145 | 11.92           | 18.08             | 85.99        | 29.42             |
| GB-147 | 22.32           | 17.24             | 85.98        | 29.79             |
| GB-149 | 16.18           | 17.21             | 85.98        | 29.80             |
| GB-151 | 18.73           | 16.99             | 85.99        | 29.90             |
| GB-153 | 19.36           | 16.99             | 86.00        | 29.90             |
| GB-155 | 6.82            | 16.94             | 86.00        | 29.92             |
| GB-157 | 2.56            | 16.96             | 86.00        | 29.91             |
| GB-159 | 5.76            | 16.62             | 86.00        | 30.06             |
| GB-161 | 4.26            | 17.14             | 85.82        | 29.76             |
| GB-163 | 9.36            | 17.39             | 85.85        | 29.66             |
| GB-165 | 10.21           | 17.79             | 86.06        | 29.58             |
| GB-167 | 23.73           | 18.26             | 85.95        | 29.33             |
| GB-169 | 4.26            | 19.75             | 85.70        | 28.58             |
| GB-171 | 8.51            | 20.27             | 85.64        | 28.32             |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - JUNCTION REPORT - GREENBRIAR Elevation Head Pressure Demand ID (gpm) (ft) (ft) (psi) 28.46 20.84 85.58 28.05 **GB-173** 16.69 85.98 30.03 1.70 **GB-175** 85.65 29.98 5.96 16.45 **GB-177** 16.82 85.68 29.84 10.21 **GB-179** 85.97 30.05 5.96 16.63 **GB-181** 85.98 30.09 20.44 16.54 **GB-183** 30.04 16.64 85.98 34.06 **GB-185** 85.98 30.12 18.73 16.47 **GB-187** 16.36 30.17 8.51 85.98 **GB-189** 85.98 30.20 18.53 16.28 **GB-191** 16.24 30.22 11.67 85.98 **GB-193** 29.98 11.67 16.38 85.56 GB-195 29.82 16.75 85.57 20.44 **GB-197** 20.44 17.29 85.60 29.60 **GB-199** 29.40 17.77 85.62 23.84 **GB-201** 18.25 85.63 29.19 30.53 **GB-203** 85.49 28.45 19.83 30.53 **GB-205** 85.49 28.23 20.34 23.84 **GB-207** 85.49 28.01 11.92 20.85 **GB-209** 30.83 15.00 86.16 18.62 **GB-210** 18.60 86.08 29.24 45.98 GB-211 17.80 85.98 29.54 22.13 GB-213 17.16 85.94 29.80 29.98 **GB-215** 30.11 85.93 11.92 16.45 **GB-217** 85.23 29.85 12.77 16.33 **GB-219** 29.84 17.33 16.30 85.16 **GB-221** 85.23 29.74 16.58 18.44 **GB-223** 16.63 85.23 29.72 10.21 **GB-225** 16.52 85.23 29.77 11.07 **GB-227** 16.65 85.16 29.69 18.87 GB-229 85.16 29.69 18.73 16.65 **GB-231** 85.16 29.71 11.92 16.59 GB-233 85.16 29.52 18.73 17.04 **GB-235** 29.74 85.16 16.54 12.52 **GB-237** 

16.37

16.74

17.28

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29.72

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29.10

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**GB-239** 

**GB-241** 

**GB-243** 

**GB-245** 

**GB-247** 

12.52

23.84

25.54

23.84

16.18

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - JUNCTION REPORT - GREENBRIAT Head Pressure Elevation Demand ID (gpm) (ft) (ft) (psi) 85.31 28.60 19.30 35.65 **GB-249** 85.36 28.38 19.87 16.18 **GB-251** 28.17 20.36 85,36 23.84 **GB-253** 85.35 27.94 20.86 31.86 **GB-255** 29.37 18.14 85.92 21.28 **GB-257** 85.92 29.52 17.78 10.21 **GB-259** 29.79 85.89 17.15 11.07 **GB-261** 30.06 16.46 85.84 12.77 **GB-263** 85.89 29.42 18.00 24.97 **GB-265** 85.68 29.99 19.87 16.46 **GB-267** 16.52 85.27 29.79 18.73 **GB-269** 29.37 17.44 85.23 17.88 GB-271 29.13 85.22 18.00 10.21 GB-273 18.00 85,22 29.13 9.50 **GB-275** 85.19 29.11 18.00 10.21 **GB-277** 85.17 29.21 17.76 18.73 **GB-279** 29.52 85.17 9.36 17.04 GB-281 85.12 29.40 17.28 21.28 GB-283 28.43 19.52 85.14 25.54 **GB-285** 27.91 85.26 20.86 17.03 **GB-286** 85.91 29.42 17.03 18.00 **GB-287** 85.52 29.93 16.45 9.36 **GB-288** 85.32 29.81 16.52 6.82 **GB-289** 29.13 85.24 11.07 18.00 **GB-290** 29.52 85.17 17.04 16.18 **GB-291** 29.80 16.37 85.14 7.66 **GB-292** 85.10 29.62 16.74 13.62 GB-293 29.37 17.28 85.07 10.56 GB-294 86.13 30.82 0.00 15.00 GB-295 85.93 29.43 18.00 0.00 **GB-297** 85.46 29.90 16.45 0.00 **GB-299** 85.34 29.82 16.53 0.00 **GB-301** 29.13 18.00 85.24 0.00 GB-303 29.52 85.17 0.00 17.05 **GB-305** 85.09 29.56 16.86 0.00 **GB-307** 29.36 17.28 85.05 0.00 **GB-309** 28.56 19.13 85.04 32.39 **GB-311** 85.04 27.83 20.80 42.13 **GB-313** 84.42 28.78 15.33 18.00 **GB-315** 

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - JUNCTION REPORT - GREENBRIAR

| ID     | Demand | Elevation | Head  | Pressure |
|--------|--------|-----------|-------|----------|
| ***    | (gpm)  | (ft)      | (ft)  | (psi)    |
| GB-317 | 14.47  | 17.77     | 84.46 | 28.90    |
| GB-319 | 9.36   | 17.24     | 84.63 | 29.20    |
| GB-321 | 9.36   | 16.45     | 85.04 | 29.72    |
| GB-323 | 22.13  | 16.54     | 83.89 | 29.18    |
| GB-325 | 17.88  | 17.42     | 83.89 | 28.80    |
| GB-327 | 14.47  | 18.00     | 83.89 | 28.55    |
| GB-329 | 10.21  | 18.00     | 83.89 | 28.55    |
| GB-331 | 4.26   | 17.39     | 83.89 | 28.81    |
| GB-333 | 11.92  | 17.35     | 84.56 | 29.12    |
| GB-335 | 10.21  | 16.42     | 84.63 | 29.55    |
| GB-337 | 18.73  | 18.00     | 84.35 | 28.75    |
| GB-339 | 16.18  | 18.00     | 84.37 | 28.76    |
| GB-341 | 13.45  | 17.49     | 84.41 | 28.99    |
| GB-343 | 10.90  | 16.16     | 84.44 | 29.58    |
| GB-345 | 14.47  | 18.00     | 84.24 | 28.70    |
| GB-347 | 17.03  | 18.00     | 84.26 | 28.71    |
| GB-349 | 6.82   | 17.75     | 84.27 | 28.82    |
| GB-351 | 21.28  | 18.00     | 84.16 | 28.67    |
| GB-352 | 30.14  | 17.35     | 84.06 | 28.91    |
| GB-353 | 16.18  | 17.91     | 84.13 | 28.70    |
| GB-355 | 13.62  | 17.82     | 84.19 | 28.76    |
| GB-357 | 15.16  | 17.40     | 84.20 | 28.94    |
| GB-359 | 11.75  | 16.14     | 84.19 | 29.48    |
| GB-361 | 16.18  | 17.26     | 83.95 | 28.90    |
| GB-362 | 20.44  | 16.38     | 84.02 | 29.31    |
| GB-363 | 11.07  | 16.29     | 83.70 | 29.21    |
| GB-365 | 14.18  | 16.32     | 83.91 | 29.29    |
| GB-367 | 19.23  | 16.59     | 83.90 | 29.16    |
| GB-369 | 17.03  | 17.03     | 83.89 | 28.97    |
| GB-371 | 13.62  | 16.87     | 83.89 | 29.04    |
| GB-373 | 10.21  | 16.73     | 83.89 | 29.10    |
| GB-375 | 14.73  | 16.59     | 83.90 | 29.17    |
| GB-377 | 18.32  | 16.34     | 83.90 | 29.28    |
| GB-379 | 45.40  | 17.08     | 83.99 | 28.99    |
| GB-381 | 25.98  | 16.42     | 83.38 | 29.01    |
| GB-383 | 17.47  | 18.29     | 83.37 | 28.20    |
| GB-385 | 10.65  | 18.09     | 83.64 | 28.40    |
| GB-387 | 15.35  | 18.82     | 83.64 | 28.09    |
| GB-389 | 9.36   | 18.79     | 83.81 | 28.17    |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - JUNCTION REPORT - GREENBRIAR

| ID     | Demand Elevation (gpm) (ft) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------------------|-------------------|--------------|-------------------|
| GB-391 | 38.21                       | 18.77             | 84.15        | 28.33             |
| GB-393 | 15.03                       | 16.43             | 83.26        | 28.96             |
| GB-395 | 15.33                       | 17.71             | 83.21        | 28.38             |
| GB-397 | 37.53                       | 18.80             | 83.23        | 27.92             |
| GB-399 | 34.97                       | 19.79             | 83.30        | 27.52             |
| GB-401 | 19.59                       | 20.09             | 83.30        | 27.39             |
| GB-403 | 11.07                       | 20.39             | 83.30        | 27.26             |
| GB-405 | 11.57                       | 16.13             | 83.23        | 29.08             |
| GB-407 | 22.13                       | 17.95             | 83.16        | 28.25             |
| GB-409 | 13.62                       | 19.40             | 83.12        | 27.61             |
| GB-411 | 17.03                       | 16.46             | 83.23        | 28.93             |
| GB-413 | 26.39                       | 18.20             | 83.11        | 28.13             |
| GB-415 | 13.62                       | 19.96             | 83.00        | 27.31             |
| GB-417 | 35.25                       | 16.45             | 83.33        | 28.98             |
| GB-419 | 11.07                       | 18.63             | 83.07        | 27.92             |
| GB-421 | 33.40                       | 19.83             | 82.80        | 27.28             |
| GB-423 | 11.07                       | 20.20             | 82.79        | 27.12             |
| GB-425 | 22.08                       | 20.56             | 82.84        | 26.99             |
| GB-427 | 11.07                       | 21.58             | 82.77        | 26.52             |
| GB-429 | 27.19                       | 21.13             | 82.91        | 26.77             |
| GB-431 | 22.13                       | 21.45             | 82.72        | 26.55             |
| GB-433 | 34.25                       | 22.00             | 82.68        | 26.29             |
| GB-435 | 17.03                       | 21.27             | 81.87        | 26.26             |
| GB-437 | 17.88                       | 22.00             | 81.63        | 25.84             |
| GB-439 | 17.88                       | 22.00             | 81.82        | 25.92             |
| GB-441 | 11.07                       | 21.27             | 81.77        | 26.22             |
| GB-443 | 1,511.92                    | 22.00             | 79.69        | 25.00             |
| GB-445 | 11.07                       | 21.00             | 81.73        | 26.31             |
| GB-446 | 0.00                        | 22.00             | 86.20        | 27.82             |
| GB-447 | 0.00                        | 26.00             | 91,43        | 28.35             |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|------------------|
| P101 | 117.50         | 8.00             | 130.00    | 66.26         | 0.42               | 0.01             |
| P102 | 117.50         | 8.00             | 130.00    | -244.58       | 1.56               | 0.16             |
| P103 | 739.21         | 8.00 -           | 130.00    | 145.59        | 0.93               | 0.38             |
| P104 | 117.50         | 8.00             | 130.00    | 72.47         | 0.46               | 0.02             |
| P105 | 117.50         | 8.00             | 130.00    | 133.10        | 0.85               | 0.05             |
| P106 | 436.40         | 12.00            | 130.00    | 75.22         | 0.21               | 0.01             |
| P107 | 650.57         | 8.00             | 130.00    | 70.40         | 0.45               | 0.09             |
| P108 | 535.27         | 8.00             | 130.00    | 66.24         | 0.42               | 0.06             |
| P109 | 357.35         | 18.00            | 130.00    | -1,805.71     | 2.28               | 0.38             |
| P110 | 243.09         | 12.00            | 130.00    | -405.12       | 1.15               | 0.12             |
| P111 | 253.19         | 8.00             | 130.00    | -104.49       | 0.67               | 007              |
| P112 | 380.98         | 8.00             | 130.00    | 137.52        | 0.88               | 0.18             |
| P113 | 904.24         | 8.00             | 130.00    | -67.73        | 0.43               | 0.11             |
| P114 | 693.26         | 8.00             | 130.00    | -83.97        | 0.54               | 0.13             |
| P115 | 105.50         | 8.00             | 130.00    | -12.86        | 0.08               | O.000            |
| P116 | 147.51         | 12.00            | 130.00    | -10.42        | 0.03               | O.0000           |
| P117 | 132.50         | 12.00            | 130.00    | -161.29       | 0.46               | 0.01             |
| P118 | 226.54         | 8.00             | 130.00    | 88.18         | 0.56               | 0.05             |
| P119 | 193.01         | 8.00             | 130.00    | 18.26         | 0.12               | 0.00             |
| P120 | 193.01         | 8.00             | 130.00    | -41.87        | 0.27               | 0.01             |
| P121 | 713.00         | 8.00             | 130.00    | 5.99          | 0.04               | O.000            |
| P122 | 615.89         | 8.00             | 130.00    | -7.63         | 0.05               | 0.00             |
| P123 | 713.00         | 8.00             | 130.00    | -117.30       | 0.75               | 0.25             |
| P124 | 677.66         | 8.00             | 130.00    | -120.30       | 0.77               | 0.25             |
| P125 | 476.65         | 8.00             | 130.00    | -122.71       | 0.78               | 0.18             |
| P126 | 117.50         | 8.00             | 130.00    | -115.05       | 0.73               | 0.04             |
| P127 | 677.66         | 8.00             | 130.00    | 116.50        | 0.74               | 0.23             |
| P128 | 193.00         | 8.00             | 130.00    | -18.60        | 0.12               | 0.00             |
| P129 | 117.50         | 8.00             | 130.00    | -100.05       | 0.64               | 0.03             |
| P130 | 633.34         | 8.00             | 130.00    | 48.41         | 0.31               | 0.04             |
| P131 | 232.72         | 8.00             | 130.00    | 57.33         | 0.37               | 0.02             |
| P132 | 233.02         | 8.00             | 130.00    | 64.17         | 0.41               | 0.03             |
| P133 | 618.66         | 8.00             | 130.00    | 42.56         | 0.27               | 0.03             |
| P134 | 713.00         | 8.00             | 130.00    | -38.91        | 0.25               | 0.03             |
| P135 | 195.00         | 8.00             | 130.00    | 54.38         | 0.35               | 0.02             |
| P136 | 193.00         | 8.00             | 130.00    | 107.80        | 0.69               | 0.06             |
| P137 | 112.20         | 18.00            | 130.00    | 1,723.58      | 2.17               | 0.11             |
| P138 | 701.50         | 8.00             | 130.00    | -65.10        | 0.42               | 0.08             |
| P139 | 378.03         | 8.00             | 130.00    | -85.87        | 0.55               | 0.07             |

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos:<br>(ft) |
|------|----------------|---------------|-----------|---------------|--------------------|------------------|
| P140 | 586.50         | 8.00          | 130.00    | -3.09         | 0.02               | 0.000            |
| P141 | 253.00         | 8.00          | 130.00    | 61.87         | 0.39               | 0.03             |
| P142 | 233.00         | 8.00          | 130.00    | -38.40        | 0.25               | 0.01             |
| P143 | 233.00         | 8.00          | 130.00    | -63.69        | 0.41               | 0.03             |
| P144 | 232.70         | 8.00          | 130.00    | -52.60        | 0.34               | 0.02             |
| P145 | 574.54         | 8.00          | 130.00    | 11.66         | 0.07               | 0.00             |
| P146 | 105.50         | 8.00          | 130.00    | 63.25         | 0.40               | 0.01             |
| P147 | 126.23         | 8.00          | 130.00    | 96.76         | 0.62               | 0.03             |
| P148 | 126.78         | 8.00          | 130.00    | 33.79         | 0.22               | 0.00             |
| P149 | 388.16         | 8.00          | 130.00    | 8.35          | 0.05               | 0.000            |
| P150 | 117.50         | 8.00          | 130.00    | 1.71          | 0.01               | O.0000           |
| P151 | 611.16         | 8.00          | 130.00    | -6.85         | 0.04               | 0.00             |
| P152 | 418.00         | 8.00          | 130.00    | -6.53         | 0.04               | O.000            |
| P153 | 97.50          | 8.00          | 130.00    | -6.40         | 0.04               | O.000            |
| P154 | 261.76         | 8.00          | 130.00    | -37.21        | 0.24               | 0.01             |
| P155 | 839.51         | 8.00          | 130.00    | 6.79          | 0.04               | 0.00             |
| P156 | 170.40         | 8.00          | 130.00    | 16.12         | 0.10               | 0.00             |
| P157 | 116.20         | 8.00          | 130.00    | 8.55          | 0.05               | O.000            |
| P158 | 248.92         | 8.00          | 130.00    | -36.88        | 0.24               | 0.01             |
| P159 | 247.10         | 8.00          | 130.00    | -9.44         | 0.06               | O.000            |
| P160 | 247.67         | 8.00          | 130.00    | 12.57         | 0.08               | 0.00             |
| P161 | 247.82         | 8.00          | 130.00    | 29.91         | 0.19               | 0.01             |
| P162 | 247.00         | 8.00          | 130.00    | -16.57        | 0.11               | 0.00             |
| P163 | 249.87         | 8.00          | 130.00    | -10.49        | 0.07               | O.000            |
| P164 | 1,149.31       | 8.00          | 130.00    | 19.11         | 0.12               | 0.01             |
| P165 | 710.72         | 12.00         | 130.00    | -315.72       | 0.90               | 0.21             |
| P166 | 369.00         | 8.00          | 130.00    | 170.57        | 1.09               | 0.25             |
| P167 | 253.00         | 8.00          | 130.00    | 134.53        | 0.86               | 0.11             |
| P168 | 918.21         | 8.00          | 130.00    | 60.18         | 0.38               | 0.09             |
| P169 | 282.81         | 8.00          | 130.00    | 111.63        | 0.71               | 0.09             |
| P170 | 333.36         | 12.00         | 130.00    | -68.55        | 0.19               | 0.01             |
| P171 | 253.00         | 8.00          | 130.00    | 159.30        | 1.02               | 0.15             |
| P172 | 234.54         | 8.00          | 130.00    | 97.98         | 0.63               | 0.06             |
| P173 | 253.00         | 8.00          | 130.00    | 57.97         | 0.37               | 0.02             |
| P174 | 657.99         | 8.00          | 130.00    | 56.70         | 0.36               | 0.06             |
| P175 | 633.34         | 8.00          | 130.00    | 22.57         | 0.14               | 0.01             |
| P176 | 253.02         | 8.00          | 130.00    | 33.27         | 0.21               | 0.01             |
| P177 | 633.34         | 8.00          | 130.00    | 69.25         | 0.44               | 0.08             |
| P178 | 242.02         | 12.00         | 130.00    | 338.84        | 0.96               | 0.08             |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Hi eadios<br>(ft) |
|------|----------------|---------------|-----------|---------------|--------------------|-------------------|
| P179 | 253.00         | 8.00          | 130.00    | 165.98        | 1.06               | 0.17              |
| P180 | 273.00         | 8.00          | 130.00    | -136.40       | 0.87               | 0.12              |
| P181 | 628.13         | 12.00         | 130.00    | . 386.81      | 1.10               | 0.27              |
| P182 | 797.55         | 12.00         | 130.00    | 325.51        | 0.92               | 0.25              |
| P183 | 578.83         | 12.00         | 130.00    | 475.22        | 1.35               | 0.37              |
| P184 | 193.00         | 8.00          | 130.00    | -724.30       | 4.62               | 1.94              |
| P185 | 653.19         | 8.00          | 130.00    | 385.35        | 2.46               | 2.04              |
| P186 | 193.00         | 8.00          | 130.00    | 142.07        | 0.91               | 0.09              |
| P187 | 193.00         | 8.00          | 130.00    | 146.99        | 0.94               | 0.10              |
| P188 | 437.56         | 8.00          | 130.00    | 311.15        | 1.99               | 0.92              |
| P189 | 203.57         | 12.00         | 130.00    | 87.05         | 0.25               | 10.0              |
| P190 | 59 <b>6.95</b> | 8.00          | 130.00    | 205.52        | 1.31               | 0.58              |
| P191 | 292.91         | 8.00          | 130.00    | 16.20         | 0.10               | 0.00              |
| P192 | 695.05         | 8.00          | 130.00    | -81.23        | 0.52               | 0.12              |
| P193 | 253.00         | 8.00          | 130.00    | 85.26         | 0.54               | 0.05              |
| P194 | 656.00         | 8.00          | 130.00    | -74.03        | 0.47               | 0.10              |
| P195 | 504.88         | 8.00          | 130.00    | -90.50        | 0.58               | 0.11              |
| P196 | 313.32         | 8.00          | 130.00    | -39.37        | 0.25               | 0.01              |
| P197 | 549.00         | 8.00          | 130.00    | 86.73         | 0.55               | 0.11              |
| P198 | 253.00         | 8.00          | 130.00    | 43.30         | 0.28               | 0.01              |
| P199 | 253.00         | 8.00          | 130.00    | 75.95         | 0.48               | 0.04              |
| P200 | 253.00         | 8.00          | 130.00    | 158.03        | 1.01               | 0.15              |
| P201 | 403.00         | 8.00          | 130.00    | 82.16         | 0.52               | 0.07              |
| P202 | 276.11         | 8.00          | 130.00    | 257.51        | 1.64               | 0.41              |
| P203 | 253.02         | 8.00          | 130.00    | -126.99       | 0.81               | 0.10              |
| P204 | 253.02         | 8.00          | 130.00    | -70.73        | 0.45               | 0.03              |
| P205 | 236.90         | 8.00          | 130.00    | -38.07        | 0.24               | 0.01              |
| P206 | 636.18         | 8.00          | 130.00    | 47.94         | 0.31               | 0.04              |
| P207 | 211.30         | 8.00          | 130.00    | 33.85         | 0.22               | 0.01              |
| P208 | 232.70         | 8.00          | 130.00    | 63.98         | 0.41               | 0.03              |
| P209 | 233.00         | 8.00          | 130.00    | 97.98         | 0.63               | 0.06              |
| P210 | 233.00         | 8.00          | 130.00    | 204.14        | 1.30               | 0.22              |
| P211 | 621.42         | 8.00          | 130.00    | -126.86       | 0.81               | 0.25              |
| P212 | 253.02         | 8.00          | 130.00    | -75.45        | 0.48               | 0.04              |
| P213 | 699.07         | 8.00          | 130.00    | -27.14        | 0.17               | 0.02              |
| P214 | 253.02         | 8.00          | 130.00    | -15.71        | 0.10               | 0.00              |
| P215 | 613.13         | 8.00          | 130.00    | -12.71        | 0.08               | 0.00              |
| P216 | 253.00         | 8.00          | 130.00    | 32.21         | 0.21               | 0.01              |
| P217 | 233.00         | 8.00          | 130.00    | 21.30         | 0.14               | 0.00              |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|------------------|
| P218 | 289.50         | 8.00             | 130.00    | 23.06         | 0.15               | 0.00             |
| P219 | 313.50         | 8.00             | 130.00    | -154.18       | 0.98               | 0.18             |
| P220 | 391.14         | 12.00            | 130.00    | 621.80        | 1.76               | 0.41             |
| P221 | 590.71         | 8.00             | 130.00    | 67.00         | 0.43               | 0.07             |
| P222 | 253.00         | 8.00             | 130.00    | 32.90         | 0.21               | 0.01             |
| P223 | 390.32         | 8.00             | 130.00    | 119.08        | 0.76               | 0.14             |
| P224 | 430.55         | 8.00             | 130.00    | 50.45         | 0.32               | 0.03             |
| P225 | 248.33         | 12.00            | 130.00    | 523.79        | 1.49               | 0.19             |
| P226 | 430.73         | 8.00             | 130.00    | -27.09        | 0.17               | 0.01             |
| P227 | 412.22         | 12.00            | 130.00    | 462.44        | 1.31               | 0.25             |
| P228 | 262.25         | 12.00            | 130.00    | 461.53        | 1.31               | 0.16             |
| P229 | 253.00         | 12.00            | 130.00    | 407.42        | 1.16               | 0.12             |
| P230 | 273.31         | 12.00            | 130.00    | 377.76        | 1.07               | 0.11             |
| P231 | 234.73         | 12.00            | 130.00    | 455.29        | 1.29               | 0.14             |
| P232 | 422.16         | 12.00            | 130.00    | -534.14       | 1.52               | 0.33             |
| P233 | 596.34         | 12.00            | 130.00    | -482.14       | 1.37               | 0.39             |
| P234 | 591.74         | 12.00            | 130.00    | -275.65       | 0.78               | 0.14             |
| P235 | 587.67         | 12.00            | 130.00    | -833.40       | 2.36               | 1.06             |
| P236 | 457.95         | 12.00            | 130.00    | -518.64       | 1.47               | 0.34             |
| P237 | 359.68         | 12.00            | 130.00    | -55.34        | 0.16               | 0.00             |
| P238 | 193.00         | 8.00             | 130.00    | -12.43        | 80.0               | 0.00             |
| P239 | 487.33         | 8.00             | 130.00    | 107.66        | 0.69               | 0.14             |
| P240 | 486.84         | 8.00             | 130.00    | -85.67        | 0.55               | 0.09             |
| P241 | 708.39         | 8.00             | 130.00    | -86.03        | 0.55               | 0.14             |
| P242 | 617.10         | 8.00             | 130.00    | -87.61        | 0.56               | 0.12             |
| P243 | 319.69         | 18.00            | 130.00    | -912.17       | 1.15               | 0.09             |
| P244 | 861.88         | 12.00            | 130.00    | -42.13        | 0.12               | 0.01             |
| P245 | 534.05         | 18.00            | 130.00    | -575.97       | 0.73               | 0.07             |
| P246 | 627.02         | 18.00            | 130.00    | -586.39       | 0.74               | 0.08             |
| P247 | 195.01         | 18.00            | 130.00    | -747.68       | 0.94               | 0.04             |
| P248 | 751.91         | 18.00            | 130.00    | -135.27       | 0.17               | 0.01             |
| P249 | 370.87         | 12.00            | 130.00    | -972.92       | 2.76               | 0.89             |
| P250 | 602.79         | 8.00             | 130.00    | -212.04       | 1.35               | 0.62             |
| P251 | 656.30         | 8.00             | 130.00    | -254.35       | 1.62               | 0.95             |
| P252 | 501.81         | 8.00             | 130.00    | -129.05       | 0.82               | 0.21             |
| P253 | 464.05         | 12.00            | 130.00    | 452.65        | 1.28               | 0.27             |
| P254 | 250.56         | 12.00            | 130.00    | 477.78        | 1.36               | 0.16             |
| P255 | 423.72         | 8.00             | 130.00    | -79.36        | 0.51               | 0.07             |
| P256 | 235.04         | 8.00             | 130.00    | -37.12        | 0.24               | 0.01             |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - PIPE REPORT - GREENBRIAR Velocity **H**eadloss Flow Diameter Length Roughness ID (gpm) (ft/s) (ft) (in) (ft) 0.07 87.79 0.56 8.00 130.00 344.48 P257 0.40 0.07 62.15 8.00 130.00 P258 656.00 286.13 1.83 0.89 497.14 8.00 130.00 P259 0.20 0.81 130.00 -126.19 494.52 8.00 P260 0.24 147.14 0.94 466.36 8.00 130.00 P261 2.08 402.28 8.00 130.00 2.57 616.00 P262 1.70 1.03 8.00 130.00 266.36 651.25 P263 130.00 90.50 0.58 0.05 246.49 8.00 P264 80.0 -269.36 0.76 12.00 130.00 375.42 P265 0.52 8.00 130.00 182.49 1.16 665.79 P266 -114.46 0.73 0.09 8.00 130.00 285.98 P267 8.00 130.00 61.25 0.39 0.03 272.69 P268 0.01 130.00 17.79 0.11 P269 744,21 8.00 8.00 3.95 0.03 O.0000 130.00 105.50 P270 0.04 41.50 0.26 8.00 130.00 P271 892.22 15.33 0.10 0.00 8.00 130.00 193.00 P272 0.13 0.00 130.00 20.04 105.50 8.00 P273 0.64 0.00 0.0000 8.00 130.00 P274 698.75 130.00 -473.85 1.34 0.12 181.50 12.00 P275 -70.86 0.45 0.02 112.20 8.00 130.00 P276 0.02 8.00 130.00 -30.27 0.19 698.70 P277 0.000 2.53 0.02 713.00 8.00 130.00 P278 80.0 0.54 8.00 130.00 -84.99 P279 422.00 117.50 8.00 130.00 14.93 0.10 0.000 P280 0.66 -220.81 1.41 8.00 130.00 589.97 P281 -218.54 1.39 0.14 8.00 130,00 130.50 P282 -1,847.47 2.33 0.45 130.00 18.00 410.65 P283 1.06 0.33 -165.63 130.00 8.00 P284 500.49 0.01 8.00 130.00 23.65 0.15 807.99 P285 12.28 0.08 0.00 130.00 8.00 193.00 P286 72.37 0.46 0.04 8.00 130.00 263.00 P287 19.85 0.13 0.01 130.00 738.30 8.00 P288 -36.08 0.23 0.01 130.00 233.02 8.00 P289 0.21 739.64 8.00 130.00 -105.140.67 P290 0.00 -11.48 8.00 130.00 0.07 252.00 P291 130.00 -72.88 0.47 0.04 8.00 262.03 P292 -10.41 0.07 0.00 8.00 130.00 924.17 P293 0.02 -30.17 0.19 130.00 8.00 P294 770.75 0.07 8.00 130.00 52.22 0.33 956.68 P295

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - PIPE REPORT - GREENBRIAR Velocity **Headloss** Diameter Flow Length Roughness ID (ft/s) (in) (gpm) **(ft)** (ft) -232.17 1.48 0.85 8.00 130.00 693.81 P296 86.09 0.55 0.13 8.00 130.00 678.13 P297 0.03 8.00 130.00 31.79 0.20 837.42 P298 -199.02 1.27 0.51 130.00 8.00 557.94 P299 0.05 0.00 8.00 130.00 -8.39 696.14 P300 0.05 O.000 130.00 -7.13 468.04 8.00 P301 0.00 130.00 -19.65 0.13 8.00 255.36 P302 0.00 8.00 130.00 23.91 0.15 247.32 P303 0.42 2.52 12.00 130.00 -888.67 208.11 P304 0.00 0.27 88.53 8.00 130.00 42.75 P305 0.22 130.00 -221.43 1.41 8.00 193.00 P306 0.13 0.01 8.00 130.00 21.09 582.27 P307 0.26 130.00 -124.16 0.79 8.00 P308 677.66 130.00 -68.62 0.44 0.02 8.00 195.00 P309 0.020.63 130.00 -220.98 132.50 12.00 P310 0.97 0.21 8.00 130.00 -152.04 380.98 P311 0.22 130.00 -137.00 0.87 475.68 8.00 P312 0.33 0.05 130.00 -51.08 8.00 P313 655.89 0.47 0.10 8.00 130.00 -74.09 653.93 P314 **O.000** 7.52 0.05 130.00 215.00 8.00 P315 54.76 0.35 0.02 195.01 8.00 130.00 P316 0.10 0.00 16.18 130.00 214.88 8.00 P317 0.01 O.0000 130.00 -1.758.00 252.22 P318 0.00 245.38 8.00 130.00 14.52 0.09 P319 0.00 -8.48 0.05 8.00 130.00 607.50 P320 0.00 130.00 -10.980.07 574.53 8.00 P321 0.25 0.00 130.00 -38.72 8.00 105.50 P322 130.00 14.32 0.090.00 8.00 212.18 P323 O.000 9.01 0.06 105.50 8.00 130.00 P324 0.17 0.00 130.00 -26.02 8.00 P325 211.00 0.28 0.01 8.00 130.00 -44.41 P326 211.30 0.00 130.00 -22.84 0.15 8.00 P327 209.82 0.04 130.00 43.27 0.28 8.00 728.60 P328 65.89 0.42 0.07 594.64 8.00 130.00 P329 -84.79 0.54 0.05 130.00 8.00 258.06 P330 0.05 8.00 130.00 60.12 0.38 499.01 P331 130.00 -39.99 0.26 0.038.00 545.88 P332 20.10 0.13 0.01 130.00 8.00 783.02 P333 0.67 0.05 12.00 130.00 -235.18 260.55

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P334

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|---------------|-----------|---------------|--------------------|-----------------|
| P335 | 255.00         | 8.00          | 130.00    | 468.85        | 2.99               | 1.15            |
| P336 | 255.00         | 8.00          | 130.00    | 179.31        | 1.14               | 0.19            |
| P337 | 255.07         | 8.00          | 130.00    | 76.56         | 0.49               | 0.04            |
| P338 | 255.00         | 12.00         | 130.00    | 702.54        | 1.99               | 0.34            |
| P339 | 255.00         | 12.00         | 130.00    | -494.15       | 1.40               | 0.18            |
| P340 | 255.00         | 8.00          | 130.00    | 17.03         | 0.11               | 0.00            |
| P341 | 255.00         | 8.00          | 130.00    | -9.06         | 0.06               | O.000           |
| P342 | 246.98         | 8.00          | 130.00    | -3.02         | 0.02               | 0.0000          |
| P343 | 253.00         | 8.00          | 130.00    | -77.48        | 0.49               | 0.04            |
| P344 | 147.50         | 12.00         | 130.00    | 79.38         | 0.23               | 0.00            |
| P345 | 147.37         | 12.00         | 130.00    | 210.32        | 0.60               | 0.02            |
| P346 | 147.50         | 12.00         | 130.00    | 228.89        | 0.65               | 0.02            |
| P347 | 147.59         | 12.00         | 130.00    | -380.81       | 1.08               | 0.06            |
| P348 | 381.04         | 8.00          | 130.00    | -96.03        | 0.61               | <b>O</b> .09    |
| P349 | 190.72         | 18.00         | 130.00    | -858.97       | 1.08               | <b>O</b> .05    |
| P350 | 253.02         | 8.00          | 130.00    | 31.29         | 0.20               | <b>O</b> .01    |
| P351 | 233.00         | 8.00          | 130.00    | 12.24         | 0.08               | <b>O.00</b>     |
| P352 | 1,365.42       | 24.00         | 130.00    | 1,247.74      | 0.88               | <b>O</b> .18    |
| P353 | 1,505.76       | 30.00         | 130.00    | -1,247.74     | 0.57               | <b>O</b> .07    |
| P354 | 369.99         | 8.00          | 130.00    | -94.10        | 0.60               | 0.08            |
| P355 | 369.99         | 8.00          | 130.00    | -108.28       | 0.69               | 0.11            |
| P356 | 117.50         | 8.00          | 130.00    | -37.88        | 0.24               | <b>O</b> .01    |
| P357 | 195.00         | 8.00          | 130.00    | -71.43        | 0.46               | 0.03            |
| P358 | 193.00         | 8.00          | 130.00    | -72.58        | 0.46               | 0.03            |
| P359 | 500.49         | 8.00          | 130.00    | -143.45       | 0.92               | 0.25            |
| P360 | 500.78         | 8.00          | 130.00    | -194.14       | 1.24               | 0.44            |
| P361 | 677.66         | 8.00          | 130.00    | -116.32       | 0.74               | 0.23            |
| P362 | 482.45         | 12.00         | 130.00    | 204.27        | 0.58               | 0.06            |
| P363 | 677.66         | 8.00          | 130.00    | -121.39       | 0.77               | 0.25            |
| P364 | 1,180.18       | 30.00         | 130.00    | -890.27       | 0.40               | 0.03            |
| P365 | 1,577.01       | 24.00         | 130.00    | -1,726.57     | 1.22               | 0.38            |
| P366 | 701.50         | 24.00         | 130.00    | -1,980.88     | 1.40               | 0.22            |
| P367 | 242.00         | 18.00         | 130.00    | 1,602.41      | 2.02               | 0.20            |
| P368 | 738.68         | 18.00         | 130.00    | 1,373.52      | 1.73               | 0.47            |
| P369 | 253.00         | 8.00          | 130.00    | -63.85        | 0.41               | 0.03            |
| P370 | 660.09         | 8.00          | 130.00    | -96.62        | 0.62               | 0.16            |
| P371 | 193.00         | 18.00         | 130.00    | 1,297.80      | 1.64               | 0.11            |
| P372 | 595.91         | 18.00         | 130.00    | 1,108.45      | 1.40               | 0.25            |
| P373 | 191.34         | 18.00         | 130.00    | 975.14        | 1.23               | 0.06            |

#### MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm)   | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|------------------|-----------|-----------------|--------------------|-----------------|
| P374 | 105.50         | 8.00             | 130.00    | 20.52           | 0.13               | 0.00            |
| P375 | 607.50         | 8.00             | 130.00    | -21.67          | 0.14               | 0.01            |
| P376 | 438.00         | 18.00 -          | 130.00    | 865.67          | 1.09               | 0.12            |
| P377 | 650.57         | 18.00            | 130.00    | 655.35          | 0.83               | 0.10            |
| P378 | 112.20         | 8.00             | 130.00    | -183 <b>.01</b> | 1.17               | 0.09            |
| P379 | 117.50         | 8.00             | 130.00    | 18.55           | 0.12               | 0.00            |
| P380 | 348.36         | 8.00             | 130.00    | 25.37           | 0.16               | 0.01            |
| P381 | 178.10         | 12.00            | 130.00    | -249.34         | 0.71               | 0.03            |
| P382 | 1,122.42       | 24.00            | 130.00    | -3,828.35       | 2.72               | 1.17            |
| P383 | 93.09          | 8.00             | 130.00    | -154.40         | 0.99               | 0.05            |
| P384 | 195.01         | 8.00             | 130.00    | 77.13           | 0.49               | 0.03            |
| P385 | 4,416.05       | 30.00            | 130.00    | 712.14          | 0.32               | 0.07            |
| P386 | 3,100.00       | 24.00            | 130.00    | -3,856.46       | 2.73               | 3.27            |
| P388 | 1,581.75       | 18.00            | 130.00    | 744.84          | 0.94               | 0.32            |
| P389 | 621.96         | 18.00            | 130.00    | 736.23          | 0.93               | 0.12            |
| P990 | 235.86         | 99.00            | 130.00    | 712.14          | 0.03               | 0.0000          |
| P991 | 377.34         | 99.00            | 130.00    | 712.14          | 0.03               | 0.0000          |
| P992 | 233.99         | 99.00            | 130.00    | 3,856.46        | 0.16               | 0.000           |
| P993 | 232.72         | 99.00            | 130.00    | 3,856.46        | 0.16               | 0.000           |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-443 - PUMP REPORT - GREENBRIAR

| ID      | Elevation<br>(ft) | Downstream Pressure<br>(psi) | Flow<br>(gpm) | Head Gain<br>(ft) |
|---------|-------------------|------------------------------|---------------|-------------------|
| PUMP105 | 22.00             | 27.82                        | 712.14        | 86.20             |
| PUMP107 | 26.00             | 28.35                        | 3,856.46      | 91.44             |



# MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - JUNCTION REPORT - GREENBRIAR

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft)      | Pressure<br>(psi) |
|--------|-----------------|-------------------|-------------------|-------------------|
| GB-101 | 0.00            | 20.00             | 83.84             | 27.66             |
| GB-103 | 4.98            | 15.00             | 84.00             | 29.90             |
| GB-105 | 4.98            | 19.00             | 84.35             | 28.32             |
| GB-107 | 0.00            | 20.00             | 84.56             | 27.98             |
| GB-108 | 28.11           | 21.00             | 85.85             | 28.10             |
| GB-109 | 30.65           | 20.00             | 83.55             | 27.53             |
| GB-111 | 17.03           | 20.00             | 83.55             | 27.54             |
| GB-113 | 15.33           | 19.59             | 83.5 <del>9</del> | 27.73             |
| GB-115 | 25.54           | 18.97             | 83.86             | 28.12             |
| GB-117 | 17.03           | 18.87             | 83.56             | 28.03             |
| GB-119 | 19.36           | 18.84             | 83.51             | 28.03             |
| GB-121 | 15.33           | 18.80             | 83.51             | 28.04             |
| GB-122 | 28.53           | 18.80             | 84.31             | 28.39             |
| GB-123 | 14.47           | 19.02             | 83.57             | 27.97             |
| GB-125 | 24.69           | 18.39             | 83.60             | 28.26             |
| GB-127 | 13.62           | 18.28             | 83.55             | 28.28             |
| GB-128 | 41.75           | 18.50             | 84.01             | 28.39             |
| GB-129 | 14.47           | 18.53             | 83.54             | 28.17             |
| GB-131 | 23.84           | 17.81             | 83.53             | 28.48             |
| GB-133 | 13.62           | 17.67             | 83.52             | 28.53             |
| GB-135 | 11.92           | 17.23             | 83.50             | 28.72             |
| GB-137 | 17.03           | 17.16             | 83.54             | 28.76             |
| GB-139 | 17.03           | 17.85             | 83.54             | 28.47             |
| GB-141 | 36.61           | 18.91             | 83.55             | 28.01             |
| GB-143 | 22.13           | 18.52             | 83.53             | 28.17             |
| GB-145 | 11.92           | 18.08             | 83.52             | 28.35             |
| GB-147 | 22.32           | 17.24             | 83.50             | 28.71             |
| GB-149 | 16.18           | 17.21             | 83.49             | 28.72             |
| GB-151 | 18.73           | 16.99             | 83.49             | 28.82             |
| GB-153 | 19.36           | 16.99             | 83.49             | 28.82             |
| GB-155 | 6.82            | 16.94             | 83.49             | 28.84             |
| GB-157 | 2.56            | 16.96             | 83.48             | 28.82             |
| GB-159 | 5.76            | 16.62             | 83.46             | 28.96             |
| GB-161 | 4.26            | 17.14             | 83.15             | 28.60             |
| GB-163 | 9.36            | 17.39             | 83.17             | 28.50             |
| GB-165 | 10.21           | 17.79             | 83.40             | 28.43             |
| GB-167 | 23.73           | 18.26             | 83.25             | 28.16             |
| GB-169 | 4.26            | 19.75             | 82.89             | 27.36             |
| GB-171 | 8.51            | 20.27             | 82.80             | 27.09             |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - JUNCTION REPORT - GREENBRIAR

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-173 | 28.46           | 20.84             | 82.72        | 26.81             |
| GB-175 | 1.70            | 16.69             | 83.48        | 28.94             |
| GB-177 | 5.96            | 16.45             | 82.91        | 28.80             |
| GB-179 | 10.21           | 16.82             | 82.96        | 28.66             |
| GB-181 | 5.96            | 16.63             | 83.48        | 28.97             |
| GB-183 | 20.44           | 16.54             | 83.48        | 29.01             |
| GB-185 | 34.06           | 16.64             | 83.48        | 28.96             |
| GB-187 | 18.73           | 16.47             | 83.48        | 29.03             |
| GB-189 | 8.51            | 16.36             | 83.48        | 29.08             |
| GB-191 | 18.53           | 16.28             | 83.48        | 29.12             |
| GB-193 | 11.67           | 16.24             | 83.48        | 29.13             |
| GB-195 | 11.67           | 16.38             | 82.80        | 28.78             |
| GB-197 | 20.44           | 16.75             | 82.80        | 28.62             |
| GB-199 | 20.44           | 17.29             | 82.83        | 28.40             |
| GB-201 | 23.84           | 17.77             | 82.86        | 28.20             |
| GB-203 | 30.53           | 18.25             | 82.86        | 27.99             |
| 3B-205 | 30.53           | 19.83             | 82.61        | 27.20             |
| GB-207 | 23.84           | 20.34             | 82.61        | 26.98             |
| GB-209 | 11.92           | 20.85             | 82.61        | 26.76             |
| GB-210 | 18.62           | 15,00             | 83.78        | 29.80             |
| GB-211 | 45.98           | 18.60             | 83.67        | 28.20             |
| GB-213 | 22.13           | 17.80             | 83.53        | 28.48             |
| GB-215 | 29.98           | 17.16             | 83.48        | 28.74             |
| GB-217 | 11.92           | 16.45             | 83.47        | 29.04             |
| GB-219 | 12.77           | 16.33             | 82.54        | 28.69             |
| GB-221 | 17.33           | 16.30             | 82.40        | 28.64             |
| GB-223 | 18.44           | 16.58             | 82.55        | 28.58             |
| GB-225 | 10.21           | 16.63             | 82.54        | 28.56             |
| GB-227 | 11.07           | 16.52             | 82.54        | 28.61             |
| GB-229 | 18.87           | 16.65             | 82.40        | 28.49             |
| GB-231 | 18.73           | 16.65             | 82.40        | 28.49             |
| GB-233 | 11.92           | 16.59             | 82.40        | 28.51             |
| GB-235 | 18.73           | 17.04             | 82.40        | 28.32             |
| GB-237 | 12.52           | 16.54             | 82.40        | 28.54             |
| GB-239 | 12.52           | 16.37             | 82.47        | 28.64             |
| GB-241 | 23.84           | 16.74             | 82.47        | 28.48             |
| GB-243 | 25.54           | 17.28             | 82.48        | 28.25             |
| GB-245 | 23.84           | 17.76             | 82.54        | 28.07             |
| GB-247 | 16.18           | 18.25             | 82.54        | 27.86             |

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure (psi) |
|--------|-----------------|-------------------|--------------|----------------|
| GB-249 | 35.65           | 19.30             | 82.37        | 27.33          |
| GB-251 | 16.18           | 19.87             | 82.43        | 27.11          |
| GB-253 | 23.84           | 20.36             | 82.43        | 26.90          |
| GB-255 | 31.86           | 20.86             | 82.41        | 26.67          |
| GB-257 | 21.28           | 18.14             | 83.48        | 28.31          |
| GB-259 | 10.21           | 17.78             | 83.48        | 28.47          |
| GB-261 | 11.07           | 17.15             | 83.44        | 28.72          |
| GB-263 | 12.77           | 16.46             | 83.38        | 29.00          |
| GB-265 | 24.97           | 18.00             | 83.46        | 28.36          |
| GB-267 | 19.87           | 16.46             | 83.21        | 28.92          |
| GB-269 | 18.73           | 16.52             | 82.62        | 28.64          |
| GB-271 | 17.88           | 17.44             | 82.55        | 28.21          |
| GB-273 | 10.21           | 18.00             | 82.53        | 27.96          |
| GB-275 | 9.50            | 18.00             | 82.51        | 27.95          |
| GB-277 | 10.21           | 18.00             | 82.45        | 27.93          |
| GB-279 | 18.73           | 17.76             | 82.41        | 28.01          |
| GB-281 | 9.36            | 17.04             | 82.40        | 28.32          |
| GB-283 | 21.28           | 17.28             | 82.16        | 28.11          |
| GB-285 | 25.54           | 19.52             | 82.05        | 27.10          |
| GB-286 | 17.03           | 20.86             | 82.24        | 26.60          |
| GB-287 | 17.03           | 18.00             | 83.48        | 28.37          |
| GB-288 | 9.36            | 16.45             | 83.03        | 28.85          |
| GB-289 | 6.82            | 16.52             | 82.70        | 28.68          |
| GB-290 | 11.07           | 18.00             | 82.53        | 27.96          |
| GB-291 | 16.18           | 17.04             | 82.40        | 28.32          |
| GB-292 | 7.66            | 16.37             | 82.25        | 28.55          |
| GB-293 | 13.62           | 16.74             | 82.21        | 28.37          |
| GB-294 | 10.56           | 17.28             | 82.14        | 28.10          |
| GB-295 | 0.00            | 15.00             | 83.76        | 29.79          |
| GB-297 | 0.00            | 18.00             | 83.51        | 28.39          |
| GB-299 | 0.00            | 16.45             | 82.96        | 28.82          |
| GB-301 | 0.00            | 16.53             | 82.74        | 28.69          |
| GB-303 | 0.00            | 18.00             | 82.53        | 27.96          |
| GB-305 | 0.00            | 17.05             | 82.39        | 28.31          |
| GB-307 | 0.00            | 16.86             | 82.20        | 28.31          |
| GB-309 | 0.00            | 17.28             | 82.12        | 28.09          |
| GB-311 | 32.39           | 19.13             | 81.88        | 27.19          |
| GB-313 | 2,042.13        | 20.80             | 73.68        | 22.91          |
| GB-315 | 15.33           | 18.00             | 82.28        | 27.85          |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - JUNCTION REPORT - GREENBRIAR

| ID               | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure (psi) |
|------------------|-----------------|-------------------|--------------|----------------|
| GB-317           | 14.47           | 17.77             | 82.31        | 27.96          |
| GB-317<br>GB-319 | 9.36            | 17.24             | 82.42        | 28.24          |
| GB-321           | 9.36            | 16.45             | 82.68        | 28.70          |
| GB-323           | 22.13           | 16.54             | 81.92        | 28.33          |
| GB-325           | 17.88           | 17.42             | 81.91        | 27.94          |
| GB-327           | 14.47           | 18.00             | 81.91        | 27.69          |
| GB-329           | 10.21           | 18.00             | 81.91        | 27.69          |
| GB-331           | 4.26            | 17.39             | 81.91        | 27.95          |
| GB-333           | 11.92           | 17.35             | 82.37        | 28.17          |
| GB-335           | 10.21           | 16.42             | 82.42        | 28.60          |
| GB-337           | 18.73           | 18.00             | 82.24        | 27.84          |
| GB-339           | 16.18           | 18.00             | 82.25        | 27.84          |
| GB-341           | 13.45           | 17.49             | 82.28        | 28.07          |
| GB-343           | 10.90           | 16.16             | 82.30        | 28.66          |
| GB-345           | 14.47           | 18.00             | 82.18        | 27.81          |
| GB-347           | 17.03           | 18.00             | 82.19        | 27.81          |
| GB-349           | 6.82            | 17.75             | 82.19        | 27.92          |
| GB-351           | 21.28           | 18.00             | 82.13        | 27.79          |
| GB-352           | 30.14           | 17.35             | 82.08        | 28.05          |
| GB-353           | 16.18           | 17.91             | 82.12        | 27.82          |
| GB-355           | 13.62           | 17.82             | 82.15        | 27.87          |
| GB-357           | 15.16           | 17.40             | 82.16        | 28.06          |
| GB-359           | 11.75           | 16.14             | 82.16        | 28.60          |
| GB-361           | 16.18           | 17.26             | 82.04        | 28.07          |
| GB-362           | 20.44           | 16.38             | 82.07        | 28.46          |
| GB-363           | 11.07           | 16.29             | 81.96        | 28.45          |
| GB-365           | 14.18           | 16.32             | 82.00        | 28.46          |
| GB-367           | 19.23           | 16.59             | 81.97        | 28.33          |
| GB-369           | 17.03           | 17.03             | 81.93        | 28.12          |
| GB-371           | 13.62           | 16.87             | 81.91        | 28.18          |
| GB-373           | 10.21           | 16.73             | 81.91        | 28.24          |
| GB-375           | 14.73           | 16.59             | 81.91        | 28.30          |
| GB-377           | 18.32           | 16.34             | 81.91        | 28.41          |
| GB-379           | 45.40           | 17.08             | 81.92        | 28.09          |
| GB-381           | 25.98           | 16.42             | 81.83        | 28.34          |
| GB-383           | 17.47           | 18.29             | 81.83        | 27.53          |
| GB-385           | 10.65           | 18.09             | 81.85        | 27.63          |
| GB-387           | 15.35           | 18.82             | 81.84        | 27.31          |
| GB-389           | 9.36            | 18.79             | 81.84        | 27.32          |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - JUNCTION REPORT - GREENBRIAR

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-391 | 38.21           | 18.77             | 81.85        | 27.33             |
| GB-393 | 15.03           | 16.43             | 81.83        | 28.33             |
| 3B-395 | 15.33           | 17.71             | 81.82        | 27.78             |
| 3B-397 | 37.53           | 18.80             | 81.82        | 27.31             |
| 3B-399 | 34.97           | 19.79             | 81.82        | 26.88             |
| GB-401 | 19.59           | 20.09             | 81.82        | 26.75             |
| 3B-403 | 11.07           | 20.39             | 81.82        | 26.62             |
| GB-405 | 11.57           | 16.13             | 81.83        | 28.47             |
| GB-407 | 22.13           | 17.95             | 81.82        | 27.67             |
| GB-409 | 13.62           | 19.40             | 81.82        | 27.05             |
| GB-411 | 17.03           | 16.46             | 81.83        | 28.33             |
| GB-413 | 26.39           | 18.20             | 81.82        | 27.57             |
| GB-415 | 13.62           | 19.96             | 81.82        | 26.80             |
| GB-417 | 35.25           | 16.45             | 81.87        | 28.35             |
| GB-419 | 11.07           | 18.63             | 81.83        | 27.38             |
| GB-421 | 33.40           | 19.83             | 81.81        | 26.86             |
| GB-423 | 11.07           | 20.20             | 81.81        | 26.70             |
| GB-425 | 22.08           | 20.56             | 81.81        | 26.54             |
| GB-427 | 11.07           | 21.58             | 81.81        | 26.10             |
| GB-429 | 27.19           | 21.13             | 81.81        | 26.29             |
| GB-431 | 22.13           | 21.45             | 81.81        | 26.15             |
| GB-433 | 34.25           | 22.00             | 81.81        | 25.91             |
| GB-435 | 17.03           | 21.27             | 81.81        | 26.23             |
| GB-437 | 17.88           | 22.00             | 81.81        | 25.91             |
| GB-439 | 17.88           | 22.00             | 81.81        | 25.91             |
| GB-441 | 11.07           | 21.27             | 81.81        | 26.23             |
| GB-443 | 11.92           | 22.00             | 81.81        | 25.91             |
| GB-445 | 11.07           | 21.00             | 81.81        | 26.35             |
| GB-446 | 0.00            | 22.00             | 83.89        | 26.82             |
| GB-447 | 0.00            | 26.00             | 89.44        | 27.49             |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - PIPE REPORT - GREENBRIAR Headloss Flow Velocity Diameter Length ID Roughness (ft/s) (ft) (in) (gpm) (ft) 0.54 0.02 130.00 84.55 117.50 8.00 P101 0.18 8.00 130.00 -261.64 1.67 117.50 P102 0.45 8.00 130.00 159.79 1.02 739.21 P103 0.02 0.50 8.00 130.00 78.86 117.50 P104 171.50 0.08 117.50 8.00 130.00 1.09 P105 0.03 130.00 143.26 0.41 12.00 436.40 P106 0.17 130.00 101.55 0.65 8.00 650.57 P107 97.68 0.62 0.13 8.00 130.00 535.27 P108 2.56 0.47 130.00 -2,028.25 18.00 357.35 P109 12.00 130.00 -295.09 0.84 0.06 243.09 P110 0.45 0.03 130.00 -70.41 8.00 253.19 P111 189.90 1.21 0.32 130.00 8.00 380.98 P112 0.01 -13.92 0.09 904.24 8.00 130.00 P113 -99.79 0.64 0.18 130.00 8.00 693.26 P114 0.000 0.09 8.00 130.00 -13.97 105.50 P115 0.00 0.25 130.00 -86.65 147.51 12.00 P116 0.01 130.00 -145.18 0.41 12.00 132.50 P117 0.06 0.64 99.84 226.54 8.00 130.00 P118 13.96 0.09 0.00 8.00 130.00 193.01 P119 0.02 0.40 8.00 130.00 -61.98 193.01 P120 0.00 130.00 -12.62 80.0 8.00 713.00 P121 0.00 11.33 0.07 8.00 130.00 615.89 P122 0.30 130.00 -131.03 0.84 8.00 713.00 P123 8.00 130.00 -140.49 0.90 0.33 677.66 P124 0.22 -135.59 0.87 130.00 476.65 8.00 P125 0.82 0.05 8.00 130.00 -127.93117.50 P126 0.32 130.00 138.27 0.88 8.00 677.66 P127 0.00 -13.88 0.09 130.00 8.00 193.00 P128 0.04 130.00 -118.36 0.76 117.50 8.00 P129 0.28 0.04 44.29 130.00 633.34 8.00 P130 48.93 0.31 0.02 130.00 232.72 8.00 P131 74.73 0.48 0.03 130.00 233.02 8.00 P132 0.26 0.03 41.03 8.00 130.00 P133 618.66 0.05 8.00 130.00 -48.54 0.31 713.00 P134 0.26 0.01 130.00 41.06 8.00 195.00 P135 130.00 110.49 0.71 0.06 8.00 193.00 P136 2.53 0.14 130.00 2,003.62 18.00 112.20 P137 0.00 -7.60 0.05 8.00 130.00 701.50 P138

130.00

-60.49

0.39

0.04

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8.00

378.03

P139

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|---------------|-----------|---------------|--------------------|-----------------|
| P140 | 586.50         | 8.00          | 130.00    | 15.02         | 0.10               | 0.00            |
| P141 | 253.00         | 8.00          | 130.00    | 82.22         | 0.52               | 0.05            |
| P142 | 233.00         | 8.00 -        | 130.00    | -31.78        | 0.20               | 0.01            |
| P143 | 233.00         | 8.00          | 130.00    | -66.70        | 0.43               | 0.03            |
| P144 | 232.70         | 8.00          | 130.00    | -71.60        | 0.46               | 0.03            |
| P145 | 574.54         | 8.00          | 130.00    | -8.06         | 0.05               | 0.00            |
| P146 | 105.50         | 8.00          | 130.00    | 22.70         | 0.14               | 0.00            |
| P147 | 126.23         | 8.00          | 130.00    | 141.55        | 0.90               | 0.06            |
| P148 | 126.78         | 8.00          | 130.00    | 72.19         | 0.46               | 0.02            |
| P149 | 388.16         | 8.00          | 130.00    | -0.74         | 0.00               | O.0000          |
| P150 | 117.50         | 8.00          | 130.00    | 0.30          | 0.00               | O.0000          |
| P151 | 611.16         | 8.00          | 130.00    | 1.64          | 0.01               | O-00000         |
| P152 | 418.00         | 8.00          | 130.00    | -14.06        | 0.09               | 0.00            |
| P153 | 97.50          | 8.00          | 130.00    | -12.67        | 80.0               | 0.000           |
| P154 | 261.76         | 8.00          | 130.00    | -60.30        | 0.38               | 0.03            |
| P155 | 839.51         | 8.00          | 130.00    | 22.10         | 0.14               | 0.01            |
| P156 | 170.40         | 8.00          | 130.00    | 24.83         | 0.16               | 0.00            |
| P157 | 116.20         | 8.00          | 130.00    | 14.86         | 0.09               | 0.000           |
| P158 | 248.92         | 8.00          | 130.00    | -83.33        | 0.53               | 0.05            |
| P159 | 247.10         | 8.00          | 130.00    | -45.42        | 0.29               | 0.01            |
| P160 | 247.67         | 8.00          | 130.00    | -22.79        | 0.15               | 0.00            |
| P161 | 247.82         | 8.00          | 130.00    | -10.21        | 0.07               | 0.000           |
| P162 | 247.00         | 8.00          | 130.00    | 16.11         | 0.10               | 0.00            |
| P163 | 249.87         | 8.00          | 130.00    | 21.56         | 0.14               | 0.00            |
| P164 | 1,149.31       | 8.00          | 130.00    | 40.70         | 0.26               | 0.06            |
| P165 | 710.72         | 12.00         | 130.00    | -137.65       | 0.39               | 0.05            |
| P166 | 369.00         | 8.00          | 130.00    | 93.90         | 0.60               | 80.0            |
| P167 | 253.00         | 8.00          | 130.00    | 80.52         | 0.51               | 0.04            |
| P168 | 918.21         | 8.00          | 130.00    | 40.24         | 0.26               | 0.04            |
| P169 | 282.81         | 8.00          | 130.00    | 81.20         | 0.52               | 0.05            |
| P170 | 333.36         | 12.00         | 130.00    | -0.51         | 0.00               | 0.00            |
| P171 | 253.00         | 8.00          | 130.00    | 165.28        | 1.05               | 0.16            |
| P172 | 234.54         | 8.00          | 130.00    | 106.70        | 0.68               | 0.07            |
| P173 | 253.00         | 8.00          | 130.00    | 71.43         | 0.46               | 0.03            |
| P174 | 657.99         | 8.00          | 130.00    | 53.71         | 0.34               | 0.05            |
| P175 | 633.34         | 8.00          | 130.00    | 8.54          | 0.05               | 0.00            |
| P176 | 253.02         | 8.00          | 130.00    | 44.27         | 0.28               | 0.01            |
| P177 | 633.34         | 8.00          | 130.00    | 86.75         | 0.55               | 0.13            |
| P178 | 242.02         | 12.00         | 130.00    | 390.59        | 1.11               | 0.11            |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss (ft) |
|------|----------------|------------------|-----------|---------------|--------------------|---------------|
| P179 | 253.00         | 8.00             | 130.00    | 132.62        | 0.85               | 0.11          |
| P180 | 273.00         | 8.00             | 130.00    | -29.25        | 0.19               | 0.01          |
| P181 | 628.13         | 12.00            | 130.00    | 79.27         | 0.22               | 0.01          |
| P182 | 797.55         | 12.00            | 130.00    | 118.51        | 0.34               | 0.04          |
| P183 | 578.83         | 12.00            | 130.00    | 220.47        | 0.63               | 0.09          |
| P184 | 193.00         | 8.00             | 130.00    | -8.54         | 0.05               | 0.000         |
| P185 | 653.19         | 8.00             | 130.00    | -3.34         | 0.02               | 0.000         |
| P186 | 193.00         | 8.00             | 130.00    | 1.12          | 0.01               | 0.0000        |
| P187 | 193.00         | 8.00             | 130.00    | -0.69         | 0.00               | 0.00          |
| P188 | 437.56         | 8.00             | 130.00    | 21.78         | 0.14               | 0.01          |
| P189 | 203.57         | 12.00            | 130.00    | 27.39         | 0.08               | 0.000         |
| P190 | 596.95         | 8.00             | 130.00    | 25.47         | 0.16               | 0.01          |
| P191 | 292.91         | 8.00             | 130.00    | 27.82         | 0.18               | 0.01          |
| P192 | 695.05         | 8.00             | 130.00    | -21.86        | 0.14               | 0.01          |
| P193 | 253.00         | 8.00             | 130.00    | -9.72         | 0.06               | 0.000         |
| P194 | 656.00         | 8.00             | 130.00    | -56.17        | 0.36               | 0.06          |
| P195 | 504.88         | 8.00             | 130.00    | -67.56        | 0.43               | 0.06          |
| P196 | 313.32         | 8.00             | 130.00    | -31.40        | 0.20               | 0.01          |
| P197 | 549.00         | 8.00             | 130.00    | 64.27         | 0.41               | 0.06          |
| P198 | 253.00         | 8.00             | 130.00    | 36.34         | 0.23               | 0.01          |
| P199 | 253.00         | 8.00             | 130.00    | 63.91         | 0.41               | 0.03          |
| P200 | 253.00         | 8.00             | 130.00    | 123.11        | 0.79               | 0.10          |
| P201 | 403.00         | 8.00             | 130.00    | 62.73         | 0.40               | 0.04          |
| P202 | 276.11         | 8.00             | 130.00    | 204.72        | 1.31               | 0.27          |
| P203 | 253.02         | 8.00             | 130.00    | -151.99       | 0.97               | 0.14          |
| P204 | 253.02         | 8.00             | 130.00    | -84.69        | 0.54               | 0.05          |
| P205 | 236.90         | 8.00             | 130.00    | -52.66        | 0.34               | 0.02          |
| P206 | 636.18         | 8.00             | 130.00    | 30.62         | 0.20               | 0.02          |
| P207 | 211.30         | 8.00             | 130.00    | 46.55         | 0.30               | 0.01          |
| P208 | 232.70         | 8.00             | 130.00    | 76.31         | 0.49               | 0.04          |
| P209 | 233.00         | 8.00             | 130.00    | 107.33        | 0.69               | 0.07          |
| P210 | 233.00         | 8.00             | 130.00    | 221.60        | 1.41               | 0.26          |
| P211 | 621.42         | 8.00             | 130.00    | -134.48       | 0.86               | 0.28          |
| P212 | 253.02         | 8.00             | 130.00    | -70.99        | 0.45               | 0.03          |
| P213 | 699.07         | 8.00             | 130.00    | -29.17        | 0.19               | 0.02          |
| P214 | 253.02         | 8.00             | 130.00    | -42.77        | 0.27               | 0.01          |
| P215 | 613.13         | 8.00             | 130.00    | -35.49        | 0.23               | 0.02          |
| P216 | 253.00         | 8.00             | 130.00    | 1.34          | 0.01               | 0.0000        |
| P217 | 233.00         | 8.00             | 130.00    | -11.80        | 0.08               | 0.00          |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - PIPE REPORT - GREENBRIAR **Headloss** Diameter Flow Velocity Length ID Roughness (in) (gpm) (ft/s) (ft) (ft) 0.02 8.00 130.00 -43.32 0.28 289.50 P218 0.31 8.00 130.00 -208.55 1.33 313.50 P219 0.26 130.00 487.88 1.38 P220 391.14 12.00 0.30 0.04 130.00 47.66 590.71 8.00 P221 0.01 8.00 130.00 28.53 0.18 P222 253.00 0.08 130.00 91.31 0.58 390.32 8.00 P223 45.56 0.29 0.03 430.55 8.00 130.00 P224 12.00 130.00 405.37 1.15 0.12 P225 248.33 0.00 130.00 -7.92 0.05 430.73 8.00 P226 0.15 412.22 12.00 130.00 348.91 0.99 P227 130.00 52.76 0.15 0.00 262.25 12.00 P228 0.00 12.00 130.00 52.47 0.15 253.00 P229 56.81 0.16 0.00 12.00 130.00 P230 273.31 12.00 130.00 100.89 0.29 0.01 234.73 P231 0.31 0.02 12.00 130.00 -110.56 422.16 P232 0.01 12.00 130.00 -63.45 0.18 596.34 P233 0.000 0.04 591.74 12.00 130.00 -13.16 P234 0.20 -339.68 0.96 12.00 130.00 587.67 P235 0.07 12.00 130.00 -211.88 0.60 457.95 P236 0.01 -91.22 0.26 12.00 130.00 P237 359.68 0.00 193.00 8.00 130.00 -18.63 0.12 P238 0.19 0.79 130.00 124.46 487.33 8.00 P239 0.62 0.12 -96.39 486.84 8.00 130.00 P240 0.20 708.39 8.00 130.00 -103.93 0.66 P241 0.19 130.00 -110.72 0.71 617.10 8.00 P242 130.00 -1.275.341.61 0.18 319.69 18.00 P243 8.20 -2.042.13 5.79 12.00 130.00 861.88 P244 -852.04 1.07 0.14 18.00 130.00 534.05 P245 0.20 627.02 18.00 130.00 -938.69 1.18 P246 0.08 -1,083.88 1.37 18.00 130.00 195.01 P247 0.24 130.00 -952.52 1.20 751.91 18.00 P248 0.03 -153.34 0.43 370.87 12.00 130.00 P249 130.00 -27.09 0.17 0.01 8.00 602.79 P250 0.00 0.04 656.30 8.00 130.00 -6.61 P251 0.28 -151.22 0.97 501.81 8.00 130.00 P252 0.02 464.05 12.00 130.00 110.00 0.31 P253 130.00 345.08 0.98 0.09 250.56 12.00

130.00

130.00

0.36

0.21

-55.96

-32.88

0.04

0.01

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8.00

8.00

423,72

235.04

P254

P255

P256

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocit <del>y</del><br>(ft/s) | Headloss<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------------------|------------------|
| P257 | 344.48         | 8.00             | 130.00    | 72.29         | 0.46                           | 0.05             |
| P258 | 656.00         | 8.00             | 130.00    | 46.66         | 0.30                           | 0.04             |
| P259 | 497.14         | 8.00             | 130.00    | 12.67         | 0.08                           | 0.00             |
| P260 | 494.52         | 8.00             | 130.00    | 6.33          | 0.04                           | 0.000            |
| P261 | 466.36         | 8.00             | 130.00    | 5.44          | 0.03                           | 0.000            |
| P262 | 616.00         | 8.00             | 130.00    | 6.72          | 0.04                           | 0.00             |
| P263 | 651.25         | 8.00             | 130.00    | 18.49         | 0.12                           | 0.01             |
| P264 | 246.49         | 8.00             | 130.00    | 66.92         | 0.43                           | 0.03             |
| P265 | 375.42         | 12.00            | 130.00    | -82.41        | 0.23                           | 0.01             |
| P266 | 665.79         | 8.00             | 130.00    | 63.58         | 0.41                           | 0.07             |
| P267 | 285.98         | 8.00             | 130.00    | -66.71        | 0.43                           | 0.03             |
| P268 | 272.69         | 8.00             | 130.00    | -1.34         | 0.01                           | O.000O           |
| P269 | 744,21         | 8.00             | 130.00    | 20.18         | 0.13                           | 0.01             |
| P270 | 105.50         | 8.00             | 130.00    | 4.91          | 0.03                           | O.000O           |
| P271 | 892.22         | 8.00             | 130.00    | 54.42         | 0.35                           | 0.07             |
| P272 | 193.00         | 8.00             | 130.00    | -3.61         | 0.02                           | O.000O           |
| P273 | 105.50         | 8.00             | 130.00    | -9.97         | 0.06                           | 0.000            |
| P274 | 698.75         | 8.00             | 130.00    | -5.86         | 0.04                           | 0.000            |
| P275 | 181.50         | 12.00            | 130.00    | -512.65       | 1.45                           | 0.13             |
| P276 | 112.20         | 8.00             | 130.00    | -63.59        | 0.41                           | 0.01             |
| P277 | 698.70         | 8.00             | 130.00    | -32.51        | 0.21                           | 0.02             |
| P278 | 713.00         | 8.00             | 130.00    | 18.52         | 0.12                           | 0.01             |
| P279 | 422.00         | 8.00             | 130.00    | -125.71       | 0.80                           | 0.17             |
| P280 | 117.50         | 8.00             | 130.00    | 7.62          | 0.05                           | 0.000            |
| P281 | 589.97         | 8.00             | 130.00    | -240.92       | 1.54                           | 0.77             |
| P282 | 130.50         | 8.00             | 130.00    | -258.25       | 1.65                           | 0.19             |
| P283 | 410.65         | 18.00            | 130.00    | -2,070.00     | 2.61                           | 0.56             |
| P284 | 500.49         | 8.00             | 130.00    | -182.68       | 1.17                           | 0.39             |
| P285 | 807.99         | 8.00             | 130.00    | -69.89        | 0.45                           | 0.11             |
| P286 | 193.00         | 8.00             | 130.00    | 19.46         | 0.12                           | 0.00             |
| P287 | 263.00         | 8.00             | 130.00    | -28.16        | 0.18                           | 0.01             |
| P288 | 738.30         | 8.00             | 130.00    | 23.63         | 0.15                           | 0.01             |
| P289 | 233.02         | 8.00             | 130.00    | -48.17        | 0.31                           | 0.02             |
| P290 | 739.64         | 8.00             | 130.00    | -116.23       | 0.74                           | 0.25             |
| P291 | 252.00         | 8.00             | 130.00    | -27.94        | 0.18                           | 0.01             |
| P292 | 262.03         | 8.00             | 130.00    | -98.36        | 0.63                           | 0.07             |
| P293 | 924.17         | 8.00             | 130.00    | -20.88        | 0.13                           | 0.01             |
| P294 | 770.75         | 8.00             | 130.00    | -19.67        | 0.13                           | 0.01             |
| P295 | 956.68         | 8.00             | 130.00    | 29.56         | 0.19                           | 0.03             |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - PIPE REPORT - GREENBRIAR **Headloss** Velocity Flow Diameter Length Roughness ID (ft) (gpm) (ft/s) (in) (ft) 0.23 0.03 8.00 130.00 -35.87 693.81 P296 0.18 130.00 102.06 0.65 678.13 8.00 P297 0.05 8.00 130.00 45.60 0.29 837.42 P298 0.02 -35.20 0.22 130.00 557.94 8.00 P299 0.00 8.00 130.00 -9.01 0.06 696.14 P300 0.000 -2.37 0.02 8.00 130.00 468.04 P301 0.000 8.26 0.05 8.00 130.00 255.36 P302 0.03 0.000 8.00 130.00 -4.01 247.32 P303 0.27 130.00 -701.96 1.99 208.11 12.00 P304 130.00 68.58 0.44 0.01 8.00 88.53 P305 0.23 -231.47 1.48 130.00 193.00 8.00 P306 130.00 11.18 0.07 0.00 582.27 8.00 P307 0.35 -145.75 8.00 130.00 0.93 677.66 P308 0.34 0.02 130.00 -53.95 8.00 195.00 P309 0.59 0.02 130.00 -208.32 132.50 12.00 P310 1.21 0.32 -189.63 8.00 130.00 380.98 P311 0.26 -151.29 0.978.00 130.00 475.68 P312 0.04 0.30 -46.34 655.89 8.00 130.00 P313 -71.36 0.46 0.09 130.00 8.00 653.93 P314 0.00 0.11 8.00 130.00 17.57 215.00 P315 85.74 0.55 0.04 8.00 130.00 195.01 P316 0.28 0.01 130.00 43.39 8.00 214.88 P317 **0.000** -8.35 0.05 130.00 252.22 8.00 P318 130.00 21.12 0.13 0.00 8.00 245,38 P319 12.24 80.0 0.00 130.00 8.00 607.50 P320 0.00 130.00 9.86 0.06 8.00 574.53 P321 0.000 -12.21 80.0 130.00 105.50 8.00 P322 0.00000 0.28 0.00 130.00 212.18 8.00 P323 O.0000 130.00 3.33 0.02 8.00 105.50 P324 0.01 -35.32 0.23 8.00 130.00 211.00 P325 0.29 0.01 -45.648.00 130.00 211.30 P326 0.000 -8.80 0.06 209.82 8.00 130.00 P327 0.00 9.28 130.00 0.06 8.00 728.60 P328 130.00 14.92 0.10 0.00 8.00 594.64 P329 0.000 -6.77 0.04 130.00 8.00 258.06 P330 15.55 0.10 0.00 130.00 8.00 499.01 P331 0.000 -6.55 0.04 130.00 8.00 545.88 P332 0.00 8.35 0.05 130.00 783.02 8.00 P333 -5.47 0.02 O.0000 12.00 130.00 260.55 P334

| Œ    | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|------------------|
| P335 | 255.00         | 8.00             | 130.00    | 27.31         | 0.17               | 0.01             |
| P336 | 255.00         | 8.00             | 130.00    | 23.11         | 0.15               | 0.00             |
| P337 | 255.07         | 8.00             | 130.00    | 13.77         | 0.09               | 0.00             |
| P338 | 255.00         | 12.00            | 130.00    | 79.26         | 0.22               | 0.01             |
| P339 | 255.00         | 12.00            | 130.00    | -34.70        | 0.10               | 0.00             |
| P340 | 255.00         | 8.00             | 130.00    | 12.14         | 0.08               | 0.00             |
| P341 | 255.00         | 8.00             | 130.00    | 2.29          | 0.01               | 0.0000           |
| P342 | 246.98         | 8.00             | 130.00    | 18.56         | 0.12               | 0.00             |
| P343 | 253.00         | 8.00             | 130.00    | -61.99        | 0.40               | 0.03             |
| P344 | 147.50         | 12.00            | 130.00    | 86.06         | 0.24               | 0.00             |
| P345 | 147.37         | 12.00            | 130.00    | 279.87        | 0.79               | 0.04             |
| P346 | 147.50         | 12.00            | 130.00    | 261.37        | 0.74               | 0.03             |
| P347 | 147.59         | 12.00            | 130.00    | -412.07       | 1.17               | 0.07             |
| P348 | 381.04         | 8.00             | 130.00    | -134.05       | 0.86               | 0.17             |
| P349 | 190.72         | 18.00            | 130.00    | -1,048.92     | 1.32               | 0.07             |
| P350 | 253.02         | 8.00             | 130.00    | 24.79         | 0.16               | 0.00             |
| P351 | 233.00         | 8.00             | 130.00    | 30.35         | 0.19               | 0.01             |
| P352 | 1,365.42       | 24.00            | 130.00    | 1,165.89      | 0.83               | 0.16             |
| P353 | 1,505.76       | 30.00            | 130.00    | -1,165.89     | 0.53               | 0.06             |
| P354 | 369.99         | 8.00             | 130.00    | -112.40       | 0.72               | 0.12             |
| P355 | 369.99         | 8.00             | 130.00    | -129.68       | 0.83               | 0.15             |
| P356 | 117.50         | 8.00             | 130.00    | -39.76        | 0.25               | 0.01             |
| P357 | 195.00         | 8.00             | 130.00    | -72.22        | 0.46               | 0.03             |
| P358 | 193.00         | 8.00             | 130.00    | -70.24        | 0.45               | 0.03             |
| P359 | 500.49         | 8.00             | 130.00    | -168.16       | 1.07               | 0.34             |
| P360 | 500.78         | 8.00             | 130.00    | -218.15       | 1.39               | 0.55             |
| P361 | 677.66         | 8.00             | 130.00    | -137.95       | 0.88               | 0.32             |
| P362 | 482.45         | 12.00            | 130.00    | 25.22         | 0.07               | 0.00             |
| P363 | 677.66         | 8.00             | 130.00    | -141.70       | 0.90               | 0.33             |
| P364 | 1,180.18       | 30.00            | 130.00    | -756.68       | 0.34               | 0.02             |
| P365 | 1,577.01       | 24.00            | 130.00    | -1,683.52     | 1.19               | 0.36             |
| P366 | 701.50         | 24.00            | 130.00    | -1,957.95     | 1.39               | 0.21             |
| P367 | 242.00         | 18.00            | 130.00    | 1,769.22      | 2.23               | 0.24             |
| P368 | 738.68         | 18.00            | 130.00    | 1,507.86      | 1.90               | 0.56             |
| P369 | 253.00         | 8.00             | 130.00    | -56.65        | 0.36               | 0.02             |
| P370 | 660.09         | 8.00             | 130.00    | -105.87       | 0.68               | 0.19             |
| P371 | 193.00         | 18.00            | 130.00    | 1,543.78      | 1.95               | 0.15             |
| P372 | 595.91         | 18.00            | 130.00    | 1,337.37      | 1.69               | 0.36             |
| P373 | 191.34         | 18.00            | 130.00    | 1,181.90      | 1.49               | 0.09             |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|-----------------|
| P374 | 105.50         | 8.00             | 130.00    | 42.93         | 0.27               | 0.01            |
| P375 | 607.50         | 8.00             | 130.00    | -8.57         | 0.05               | 0.00            |
| P376 | 438.00         | 18.00            | 130.00    | 1,217.97      | 1.54               | 0.22            |
| P377 | 650.57         | 18.00            | 130.00    | 938.10        | 1.18               | 0.20            |
| P378 | 112.20         | 8.00             | 130.00    | -171.00       | 1.09               | 0.08            |
| P379 | 117.50         | 8.00             | 130.00    | -16.33        | 0.10               | 0.00            |
| P380 | 348.36         | 8.00             | 130.00    | 17.69         | 0.11               | 0.00            |
| P381 | 178.10         | 12.00            | 130.00    | -269.45       | 0.76               | 0.04            |
| P382 | 1,122.42       | 24.00            | 130.00    | -4,027.95     | 2.86               | 1.28            |
| P383 | 93.09          | 8.00             | 130.00    | -98.46        | 0.63               | 0.02            |
| P384 | 195.01         | 8.00             | 130.00    | 120.42        | 0.77               | 0.07            |
| P385 | 4,416.05       | 30.00            | 130.00    | 1,012.54      | 0.46               | 0.13            |
| P386 | 3,100.00       | 24.00            | 130.00    | -4,056.06     | 2.88               | 3.59            |
| P388 | 1,581.75       | 18.00            | 130.00    | 924.07        | 1.17               | 0.48            |
| P389 | 621.96         | 18.00            | 130.00    | 930.38        | 1.17               | 0.19            |
| P990 | 235.86         | 99.00            | 130.00    | 1,012.54      | 0.04               | 0.0000          |
| P991 | 377.34         | 99.00            | 130.00    | 1,012.54      | 0.04               | 0.0000          |
| P992 | 233.99         | 99.00            | 130.00    | 4,056.06      | 0.17               | 0.000           |
| P993 | 232.72         | 99.00            | 130.00    | 4,056.06      | 0.17               | 0.000           |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-313 - PUMP REPORT - GREENBRIAR

| ID      | Elevation<br>(ft) | Downstream Pressure<br>(psi) | Flow<br>(gpm) | Head Gain<br>(ft) |
|---------|-------------------|------------------------------|---------------|-------------------|
| PUMP105 | 22.00             | 26.82                        | 1,012.54      | 83.89             |
| PUMP107 | 26.00             | 27.49                        | 4,056.06      | 89.44             |



### MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427 - JUNCTION REPORT - GREENBRIAR

| ID               | Demand (gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure (psi) |
|------------------|--------------|-------------------|--------------|----------------|
| GB-101           | 0.00         | 20.00             | 79.25        | 25.67          |
| GB-101           | 4.98         | 15.00             | 79.43        | 27.92          |
| GB-105           | 4.98         | 19.00             | 79.85        | 26.37          |
| GB-103<br>GB-107 | 0.00         | 20.00             | 80.10        | 26.04          |
| GB-107<br>GB-108 | 28.11        | 21.00             | 81.66        | 26.28          |
| GB-108<br>GB-109 | 30.65        | 20.00             | 78.87        | 25.51          |
| GB-103<br>GB-111 | 17.03        | 20.00             | 78.88        | 25.51          |
| GB-1113          | 15.33        | 19.59             | 78.92        | 25.71          |
| GB-115           | 25.54        | 18.97             | 79.27        | 26.13          |
| GB-117           | 17.03        | 18.87             | 78.89        | 26.01          |
| GB-119           | 19.36        | 18.84             | 78.83        | 26.00          |
| GB-121           | 15.33        | 18.80             | 78.82        | 26.01          |
| GB-122           | 28.53        | 18.80             | 79.81        | 26.43          |
| GB-123           | 14.47        | 19.02             | 78.90        | 25.95          |
| GB-125           | 24.69        | 18.39             | 78.94        | 26.24          |
| GB-127           | 13.62        | 18.28             | 78.88        | 26.26          |
| GB-128           | 41.75        | 18.50             | 79.42        | 26.40          |
| GB-129           | 14.47        | 18.53             | 78.86        | 26.14          |
| GB-131           | 23.84        | 17.81             | 78.85        | 26.45          |
| GB-133           | 13.62        | 17.67             | 78.84        | 26.51          |
| GB-135           | 11.92        | 17.23             | 78.81        | 26.68          |
| GB-137           | 17.03        | 17.16             | 78.84        | 26.73          |
| GB-139           | 17.03        | 17.85             | 78.84        | 26.43          |
| GB-141           | 36.61        | 18.91             | 78.87        | 25.98          |
| GB-143           | 22.13        | 18.52             | 78.85        | 26.14          |
| GB-145           | 11.92        | 18.08             | 78.83        | 26.32          |
| GB-147           | 22.32        | 17.24             | 78.80        | 26.68          |
| GB-149           | 16.18        | 17.21             | 78.80        | 26.69          |
| GB-151           | 18.73        | 16.99             | 78.80        | 26.78          |
| GB-153           | 19.36        | 16.99             | 78.80        | 26.78          |
| GB-155           | 6.82         | 16.94             | 78.80        | 26.80          |
| GB-157           | 2.56         | 16.96             | 78.78        | 26.79          |
| GB-159           | 5.76         | 16.62             | 78.75        | 26.92          |
| GB-161           | 4.26         | 17.14             | 78.33        | 26.51          |
| GB-163           | 9.36         | 17.39             | 78.35        | 26.41          |
| GB-165           | 10.21        | 17.79             | 78.66        | 26.37          |
| GB-167           | 23.73        | 18.26             | 78.47        | 26.09          |
| GB-169           | 4.26         | 19.75             | 78.02        | 25.25          |
| GB-171           | 8.51         | 20.27             | 77.91        | 24.97          |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427 - JUNCTION REPORT - GREENBRIAR

| <b>ID</b> | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|-----------|-----------------|-------------------|--------------|-------------------|
| GB-173    | 28.46           | 20.84             | 77.82        | 24.69             |
| GB-175    | 1.70            | 16.69             | 78.78        | 26.90             |
| GB-177    | 5.96            | 16.45             | 78.01        | 26.68             |
| GB-179    | 10.21           | 16.82             | 78.07        | 26.54             |
| GB-181    | 5.96            | 16.63             | 78.79        | 26.93             |
| GB-183    | 20.44           | 16.54             | 78.79        | 26.97             |
| GB-185    | 34.06           | 16.64             | 78.78        | 26.92             |
| GB-187    | 18.73           | 16.47             | 78.78        | 27.00             |
| GB-189    | 8.51            | 16.36             | 78.78        | 27.05             |
| GB-191    | 18.53           | 16.28             | 78.78        | 27.08             |
| GB-193    | 11.67           | 16.24             | 78.78        | 27.10             |
| GB-195    | 11.67           | 16.38             | 77.85        | 26.64             |
| GB-197    | 20.44           | 16.75             | 77.86        | 26.48             |
| GB-199    | 20.44           | 17.29             | 77.90        | 26.26             |
| GB-201    | 23.84           | 17.77             | 77.94        | 26.07             |
| GB-203    | 30.53           | 18.25             | 77.95        | 25.87             |
| GB-205    | 30.53           | 19.83             | 77.68        | 25.07             |
| GB-207    | 23.84           | 20.34             | 77.68        | 24.84             |
| GB-209    | 11.92           | 20.85             | 77.67        | 24.62             |
| GB-210    | 18.62           | 15.00             | 79.18        | 27.81             |
| GB-211    | 45.98           | 18.60             | 79.03        | 26.19             |
| GB-213    | 22.13           | 17.80             | 78.84        | 26.45             |
| GB-215    | 29.98           | 17.16             | 78.77        | 26.69             |
| GB-217    | 11.92           | 16.45             | 78.74        | 26.99             |
| GB-219    | 12.77           | 16.33             | 77.31        | 26.42             |
| GB-221    | 17.33           | 16.30             | 77.13        | 26.36             |
| GB-223    | 18.44           | 16.58             | 77.31        | 26.31             |
| GB-225    | 10.21           | 16.63             | 77.31        | 26.29             |
| GB-227    | 11.07           | 16.52             | 77.30        | 26.34             |
| GB-229    | 18.87           | 16.65             | 77.14        | 26.21             |
| GB-231    | 18.73           | 16.65             | 77.14        | 26.21             |
| GB-233    | 11.92           | 16.59             | 77.13        | 26.23             |
| GB-235    | 18.73           | 17.04             | 77.13        | 26.04             |
| GB-237    | 12.52           | 16.54             | 77.13        | 26.26             |
| GB-239    | 12.52           | 16.37             | 77.38        | 26.43             |
| GB-241    | 23.84           | 16.74             | 77.38        | 26.27             |
| GB-243    | 25.54           | 17.28             | 77.41        | 26.05             |
| GB-245    | 23.84           | 17.76             | 77.52        | 25.89             |
| GB-247    | 16.18           | 18.25             | 77.53        | 25.69             |

| ID     | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft)  | Pressure<br>(psi) |
|--------|-----------------|-------------------|---------------|-------------------|
| GB-249 | 35.65           | 19.30             | 77.36         | 25.16             |
| GB-251 | 16.18           | 19.87             | 77.45         | 24.95             |
| GB-253 | 23.84           | 20.36             | 77.45         | 24.74             |
| GB-255 | 31.86           | 20.86             | 77.43         | 24.51             |
| GB-257 | 21.28           | 18.14             | 78.73         | 26.25             |
| GB-259 | 10.21           | 17.78             | 78.73         | 26.41             |
| GB-261 | 11.07           | 17.15             | 78.68         | 26.66             |
| GB-263 | 12.77           | 16.46             | 78.56         | 26.91             |
| GB-265 | 24.97           | 18.00             | 78.67         | 26.29             |
| GB-267 | 19.87           | 16.46             | 78.25         | 26.77             |
| GB-269 | 18.73           | 16.52             | 77.39         | 26.38             |
| GB-271 | 17.88           | 17.44             | 77.32         | 25.94             |
| GB-273 | 10.21           | 18.00             | 77.29         | 25.69             |
| GB-275 | 9.50            | 18.00             | 77.27         | 25.68             |
| GB-277 | 10.21           | 18.00             | 77.20         | 25.65             |
| GB-279 | 18.73           | 17.76             | <i>7</i> 7.15 | 25.73             |
| GB-281 | 9.36            | 17.04             | 77.14         | 26.04             |
| GB-283 | 21.28           | 17.28             | 76.95         | 25.86             |
| GB-285 | 25.54           | 19.52             | 76.97         | 24.89             |
| GB-286 | 17.03           | 20.86             | 77.21         | 24.42             |
| GB-287 | 17.03           | 18.00             | 78.70         | 26.30             |
| GB-288 | 9.36            | 16.45             | 77.91         | 26.63             |
| GB-289 | 6.82            | 16.52             | 77.48         | 26.41             |
| GB-290 | 11.07           | 18.00             | 77.29         | 25.69             |
| GB-291 | 16.18           | 17.04             | 77.14         | 26.04             |
| GB-292 | 7.66            | 16.37             | 77.01         | 26.27             |
| GB-293 | 13.62           | 16.74             | 76.92         | 26.08             |
| GB-294 | 10.56           | 17.28             | 76.84         | 25.81             |
| GB-295 | 0.00            | 15.00             | 79.16         | 27.80             |
| GB-297 | 0.00            | 18.00             | 78.74         | 26.32             |
| GB-299 | 0.00            | 16.45             | 77.77         | 26.57             |
| GB-301 | 0.00            | 16.53             | 77.52         | 26.43             |
| GB-303 | 0.00            | 18.00             | 77.29         | 25.69             |
| GB-305 | 0.00            | 17.05             | 77.13         | 26.03             |
| GB-307 | 0.00            | 16.86             | 76.90         | 26.02             |
| GB-309 | 0.00            | 17.28             | 76.80         | 25.79             |
| GB-311 | 32.39           | 19.13             | 76.77         | 24.98             |
| GB-313 | 42.13           | 20.80             | 76.76         | 24.25             |

|        | Demand<br>(gpm) | Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|-------------------|--------------|-------------------|
| GB-317 | 14.47           | 17.77             | 75.73        | 25.11             |
| GB-319 | 9.36            | 17.24             | 76.06        | 25.49             |
| GB-321 | 9.36            | 16.45             | 76.89        | 26.19             |
| GB-323 | 22.13           | 16.54             | 74.22        | 24.99             |
| GB-325 | 17.88           | 17.42             | 74.22        | 24.61             |
| GB-327 | 14.47           | 18.00             | 74.22        | 24.36             |
| GB-329 | 10.21           | 18.00             | 74.22        | 24.36             |
| GB-331 | 4.26            | 17.39             | 74.22        | 24.62             |
| GB-333 | 11.92           | 17.35             | 75.90        | 25.37             |
| GB-335 | 10.21           | 16.42             | 76.03        | 25.83             |
| GB-337 | 18.73           | 18.00             | 75.49        | 24.91             |
| GB-339 | 16.18           | 18.00             | 75.52        | 24.92             |
| GB-341 | 13.45           | 17.49             | 75.58        | 25.17             |
| GB-343 | 10.90           | 16.16             | 75.62        | 25.76             |
| GB-345 | 14.47           | 18.00             | 75.25        | 24.81             |
| GB-347 | 17.03           | 18.00             | 75.27        | 24.82             |
| GB-349 | 6.82            | 17.75             | 75.29        | 24.93             |
| GB-351 | 21.28           | 18.00             | 75.04        | 24.72             |
| GB-352 | 30.14           | 17.35             | 74.80        | 24.89             |
| GB-353 | 16.18           | 17.91             | 74.98        | 24.73             |
| GB-355 | 13.62           | 17.82             | 75.09        | 24.82             |
| GB-357 | 15.16           | 17.40             | 75.10        | 25.00             |
| GB-359 | 11.75           | 16.14             | 75.03        | 25.52             |
| GB-361 | 16.18           | 17.26             | 74.46        | 24.79             |
| GB-362 | 20.44           | 16.38             | 74.62        | 25.23             |
| GB-363 | 11.07           | 16.29             | 73.72        | 24.88             |
| GB-365 | 14.18           | 16.32             | 74.30        | 25.13             |
| GB-367 | 19.23           | 16.59             | 74.27        | 24.99             |
| GB-369 | 17.03           | 17.03             | 74.23        | 24.79             |
| GB-371 | 13.62           | 16.87             | 74.22        | 24.85             |
| GB-373 | 10.21           | 16.73             | 74.22        | 24.91             |
| GB-375 | 14.73           | 16.59             | 74.22        | 24.97             |
| GB-377 | 18.32           | 16.34             | 74.22        | 25.08             |
| GB-379 | 45.40           | 17.08             | 74.35        | 24.81             |
| GB-381 | 25.98           | 16.42             | 72.74        | 24.41             |
| GB-383 | 17.47           | 18.29             | 72.66        | 23.56             |
| GB-385 | 10.65           | 18.09             | 73.36        | 23.95             |
| GB-387 | 15.35           | 18.82             | 73.33        | 23.62             |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427 - JUNCTION REPORT - GREENBRIAR

| ID     | Demand<br>(gpm) | OW AT GB-427 - JUNC<br>Elevation<br>(ft) | Head<br>(ft) | Pressure<br>(psi) |
|--------|-----------------|--|--------------|-------------------|
| GB-391 | 38.21           | 18.77                                    | 74.60        | 24.19             |
| GB-393 | 15.03           | 16.43                                    | 72.41        | 24.26             |
| GB-395 | 15.33           | 17.71                                    | 72.24        | 23.63             |
| GB-397 | 37.53           | 18.80                                    | 72.27        | 23.17             |
| GB-399 | 34.97           | 19.79                                    | 72.37        | 22.78             |
| GB-401 | 19.59           | 20.09                                    | 72.41        | 22.67             |
| GB-403 | 11.07           | 20.39                                    | 72.44        | 22.55             |
| GB-405 | 11.57           | 16.13                                    | 72.35        | 24.36             |
| GB-407 | 22.13           | 17.95                                    | 72.10        | 23.46             |
| GB-409 | 13.62           | 19.40                                    | 71.89        | 22.74             |
| GB-411 | 17.03           | 16.46                                    | 72.36        | 24.22             |
| GB-413 | 26.39           | 18.20                                    | 71.98        | 23.30             |
| GB-415 | 13.62           | 19.96                                    | 71.45        | 22.31             |
| GB-417 | 35.25           | 16.45                                    | 72.66        | 24.35             |
| GB-419 | 11.07           | 18.63                                    | 71.89        | 23.08             |
| GB-421 | 33.40           | 19.83                                    | 71.08        | 22.21             |
| GB-423 | 11.07           | 20.20                                    | 70.93        | 21.98             |
| GB-425 | 22.08           | 20.56                                    | 70.84        | 21.79             |
| GB-427 | 3,011.07        | 21.58                                    | 68.88        | 20.49             |
| GB-429 | 27.19           | 21.13                                    | 70.90        | 21.56             |
| GB-431 | 22.13           | 21.45                                    | 71.17        | 21.54             |
| GB-433 | 34.25           | 22.00                                    | 71.24        | 21.34             |
| GB-435 | 17.03           | 21.27                                    | 70.72        | 21.42             |
| GB-437 | 17.88           | 22.00                                    | 70.40        | 20.97             |
| GB-439 | 17.88           | 22.00                                    | 70.81        | 21.15             |
| GB-441 | 11.07           | 21.27                                    | 70.73        | 21.43             |
| GB-443 | 11.92           | 22.00                                    | 70.58        | 21.05             |
| GB-445 | 11.07           | 21.00                                    | 70.82        | 21.59             |
| GB-446 | 0.00            | 22.00                                    | 79.45        | 24.89             |
| GB-447 | 0.00            | 26.00                                    | 86.01        | 26.00             |

| ID   | Length<br>(ft) | Diameter (in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | H eadloss<br>(ft) |
|------|----------------|---------------|-----------|---------------|--------------------|-------------------|
| P101 | 117.50         | 8.00          | 130.00    | 84.33         | 0.54               | 0.02              |
| P102 | 117.50         | 8.00          | 130.00    | -370.26       | 2.36               | 0.34              |
| P103 | 739.21         | 8.00 -        | 130.00    | 216.10        | 1.38               | 0.79              |
| P104 | 117.50         | 8.00          | 130.00    | 80.24         | 0.51               | 0.02              |
| P105 | 117.50         | 8.00          | 130.00    | 180.23        | 1.15               | 0.09              |
| P106 | 436.40         | 12.00         | 130.00    | 137.96        | 0.39               | 0.03              |
| P107 | 650.57         | 8.00          | 130.00    | 108.80        | 0.69               | 0.20              |
| P108 | 535.27         | 8.00          | 130.00    | 104.83        | 0.67               | 0.15              |
| P109 | 357.35         | 18.00         | 130.00    | -2,279.77     | 2.87               | 0.58              |
| P110 | 243.09         | 12.00         | 130.00    | -697.21       | 1.98               | 0.32              |
| P111 | 253.19         | 8.00          | 130.00    | -172.60       | 1.10               | 0.18              |
| P112 | 380.98         | 8.00          | 130.00    | 212.79        | 1.36               | 0.40              |
| P113 | 904.24         | 8.00          | 130.00    | -155.78       | 0.99               | 0.53              |
| P114 | 693.26         | 8.00          | 130.00    | -113.98       | 0.73               | 0.23              |
| P115 | 105.50         | 8.00          | 130.00    | -17.06        | 0.11               | 0.00              |
| P116 | 147.51         | 12.00         | 130.00    | -103.92       | 0.29               | 0.01              |
| P117 | 132.50         | 12.00         | 130.00    | -234.96       | 0.67               | 0.02              |
| P118 | 226.54         | 8.00          | 130.00    | 123.26        | 0.79               | 0.09              |
| P119 | 193.01         | 8.00          | 130.00    | 22.44         | 0.14               | 0.00              |
| P120 | 193.01         | 8.00          | 130.00    | -67.69        | 0.43               | 0.02              |
| P121 | 713.00         | 8.00          | 130.00    | -12.47        | 0.08               | 0.00              |
| P122 | 615.89         | 8.00          | 130.00    | 11.38         | 0.07               | 0.00              |
| P123 | 713.00         | 8.00          | 130.00    | -147.72       | 0.94               | 0.38              |
| P124 | 677.66         | 8.00          | 130.00    | -171.79       | 1.10               | 0.47              |
| P125 | 476.65         | 8.00          | 130.00    | -181.60       | 1.16               | 0.37              |
| P126 | 117.50         | 8.00          | 130.00    | -173.94       | 1.11               | 80.0              |
| P127 | 677.66         | 8.00          | 130.00    | 160.87        | 1.03               | 0.42              |
| P128 | 193.00         | 8.00          | 130.00    | -21.98        | 0.14               | 0.00              |
| P129 | 117.50         | 8.00          | 130.00    | -139.19       | 0.89               | 0.06              |
| P130 | 633.34         | 8.00          | 130.00    | 60.27         | 0.38               | 0.06              |
| P131 | 232.72         | 8.00          | 130.00    | 61.32         | 0.39               | 0.02              |
| P132 | 233.02         | 8.00          | 130.00    | 87.18         | 0.56               | 0.05              |
| P133 | 618.66         | 8.00          | 130.00    | 46.49         | 0.30               | 0.04              |
| P134 | 713.00         | 8.00          | 130.00    | -55.22        | 0.35               | 0.06              |
| P135 | 195.00         | 8.00          | 130.00    | 76.64         | 0.49               | 0.03              |
| P136 | 193.00         | 8.00          | 130.00    | 156.42        | 1.00               | 0.11              |
| P137 | 112.20         | 18.00         | 130.00    | 2,273.38      | 2.87               | 0.18              |
| P138 | 701.50         | 8.00          | 130.00    | 10.64         | 0.07               | 0.00              |
| P139 | 378.03         | 8.00          | 130.00    | -55.92        | 0.36               | 0.03              |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm)  | Velocity<br>(ft/s) | Headlos:<br>(ft) |
|------|----------------|------------------|-----------|----------------|--------------------|------------------|
| P140 | 586.50         | 8.00             | 130.00    | 22.66          | 0.14               | 0.01             |
| P141 | 253.00         | 8.00             | 130.00    | 95.30          | 0.61               | 0.06             |
| P142 | 233.00         | 8.00             | 130.00    | -35. <b>39</b> | 0.23               | 0.01             |
| P143 | 233.00         | 8.00             | 130.00    | -76.99         | 0.49               | 0.04             |
| P144 | 232.70         | 8.00             | 130.00    | -84.33         | 0.54               | 0.04             |
| P145 | 574.54         | 8.00             | 130.00    | -10.99         | 0.07               | 0.00             |
| P146 | 105.50         | 8.00             | 130.00    | 16.52          | 0.11               | 0.000            |
| P147 | 126.23         | 8.00             | 130.00    | 151.66         | 0.97               | 0.07             |
| P148 | 126.78         | 8.00             | 130.00    | 80.92          | 0.52               | 0.02             |
| P149 | 388.16         | 8.00             | 130.00    | -4.19          | 0.03               | O.00O            |
| P150 | 117.50         | 8.00             | 130.00    | -2.01          | 0.01               | 0.00             |
| P151 | 611.16         | 8.00             | 130.00    | 2.99           | 0.02               | <b>©.000</b>     |
| P152 | 418.00         | 8.00             | 130.00    | -16.06         | 0.10               | 0.00             |
| P153 | 97.50          | 8.00             | 130.00    | -14.04         | 0.09               | O.000            |
| P154 | 261.76         | 8.00             | 130.00    | -65.78         | 0.42               | 0.03             |
| P155 | 839.51         | 8.00             | 130.00    | 25.35          | 0.16               | 0.02             |
| P156 | 170.40         | 8.00             | 130.00    | 26.70          | 0.17               | 0.00             |
| P157 | 116.20         | 8.00             | 130.00    | 16.39          | 0.10               | 0.00             |
| P158 | 248.92         | 8.00             | 130.00    | -79.69         | 0.51               | 0.04             |
| P159 | 247.10         | 8.00             | 130.00    | -42.64         | 0.27               | 0.01             |
| P160 | 247.67         | 8.00             | 130.00    | -20.30         | 0.13               | 0.00             |
| P161 | 247.82         | 8.00             | 130.00    | -7.39          | 0.05               | <b>©.000</b>     |
| P162 | 247.00         | 8.00             | 130.00    | 13.30          | 0.08               | 0.00             |
| P163 | 249.87         | 8.00             | 130.00    | 19.05          | 0.12               | 0.00             |
| P164 | 1,149.31       | 8.00             | 130.00    | 39.04          | 0.25               | 0.05             |
| P165 | 710.72         | 12.00            | 130.00    | -545.07        | 1.55               | 0.59             |
| P166 | 369.00         | 8.00             | 130.00    | 304.93         | 1.95               | 0.75             |
| P167 | 253.00         | 8.00             | 130.00    | 243.34         | 1.55               | 0.34             |
| P168 | 918.21         | 8.00             | 130.00    | 100.89         | 0.64               | 0.24             |
| P169 | 282.81         | 8.00             | 130.00    | 175.14         | 1.12               | 0.21             |
| P170 | 333.36         | 12.00            | 130.00    | -5.81          | 0.02               | CD.0000          |
| P171 | 253.00         | 8.00             | 130.00    | 235.03         | 1.50               | 0.32             |
| P172 | 234.54         | 8.00             | 130.00    | 144.72         | 0.92               | 0.12             |
| P173 | 253.00         | 8.00             | 130.00    | 86.35          | 0.55               | 0.05             |
| P174 | 657.99         | 8.00             | 130.00    | 77.94          | 0.50               | 0.11             |
| P175 | 633.34         | 8.00             | 130.00    | 23.60          | 0.15               | 0.01             |
| P176 | 253.02         | 8.00             | 130.00    | 58.17          | 0.37               | 0.02             |
| P177 | 633.34         | 8.00             | 130.00    | 98.96          | 0.63               | 0.16             |
| P178 | 242.02         | 12.00            | 130.00    | 461.38         | 1.31               | 0.15             |

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|------------------|-----------|---------------|--------------------|-----------------|
| P179 | 253.00         | 8.00             | 130.00    | 241.02        | 1.54               | 0.33            |
| P180 | 273.00         | 8.00             | 130.00    | -230.87       | 1.47               | 0.33            |
| P181 | 628.13         | 12.00            | 130.00    | 694.07        | 1.97               | 0.81            |
| P182 | 797.55         | 12.00            | 130.00    | 591.97        | 1.68               | 0.77            |
| P183 | 578.83         | 12.00            | 130.00    | 838.93        | 2.38               | 1.06            |
| P184 | 193.00         | 8.00             | 130.00    | 204.04        | 1.30               | 0.19            |
| P185 | 653.19         | 8.00             | 130.00    | 120.36        | 0.77               | 0.24            |
| P186 | 193.00         | 8.00             | 130.00    | -32.89        | 0.21               | 0.01            |
| P187 | 193.00         | 8.00             | 130.00    | -43.82        | 0.28               | 0.01            |
| P188 | 437.56         | 8.00             | 130.00    | 143.35        | 0.91               | 0.22            |
| P189 | 203.57         | 12.00            | 130.00    | 510.18        | 1.45               | 0.15            |
| P190 | 596.95         | 8.00             | 130.00    | 309.06        | 1.97               | 1.24            |
| P191 | 292.91         | 8.00             | 130.00    | 43.05         | 0.27               | 0.02            |
| P192 | 695.05         | 8.00             | 130.00    | -151.64       | 0.97               | 0.39            |
| P193 | 253.00         | 8.00             | 130.00    | 143.71        | 0.92               | 0.13            |
| P194 | 656.00         | 8.00             | 130.00    | -114.38       | 0.73               | 0.22            |
| P195 | 504.88         | 8.00             | 130.00    | -140.60       | 0.90               | 0.24            |
| P196 | 313.32         | 8.00             | 130.00    | -54.35        | 0.35               | 0.03            |
| P197 | 549.00         | 8.00             | 130.00    | 135.26        | 0.86               | 0.25            |
| P198 | 253.00         | 8.00             | 130.00    | 57.15         | 0.36               | 0.02            |
| P199 | 253.00         | 8.00             | 130.00    | 99.55         | 0.64               | 0.06            |
| P200 | 253.00         | 8.00             | 130.00    | 237.16        | 1.51               | 0.32            |
| P201 | 403.00         | 8.00             | 130.00    | 127.11        | 0.81               | 0.16            |
| P202 | 276.11         | 8.00             | 130.00    | 377.49        | 2.41               | 0.83            |
| P203 | 253.02         | 8.00             | 130.00    | -180.79       | 1.15               | 0.19            |
| P204 | 253.02         | 8.00             | 130.00    | -104.32       | 0.67               | 0.07            |
| P205 | 236.90         | 8.00             | 130.00    | -65.17        | 0.42               | 0.03            |
| P206 | 636.18         | 8.00             | 130.00    | 49.83         | 0.32               | 0.04            |
| P207 | 211.30         | 8.00             | 130.00    | 56.61         | 0.36               | 0.02            |
| P208 | 232.70         | 8.00             | 130.00    | 89.50         | 0.57               | 0.05            |
| P209 | 233.00         | 8.00             | 130.00    | 122.92        | 0.78               | 0.09            |
| P210 | 233.00         | 8.00             | 130.00    | 249.32        | 1.59               | 0.32            |
| P211 | 621.42         | 8.00             | 130.00    | -151.27       | 0.97               | 0.34            |
| P212 | 253.02         | 8.00             | 130.00    | -80.79        | 0.52               | 0.04            |
| P213 | 699.07         | 8.00             | 130.00    | -37.28        | 0.24               | 0.03            |
| P214 | 253.02         | 8.00             | 130.00    | -49.72        | 0.32               | 0.02            |
| P215 | 613.13         | 8.00             | 130.00    | -38.84        | 0.25               | 0.03            |
| P216 | 253.00         | 8.00             | 130.00    | -2.55         | 0.02               | O.0000          |
| P217 | 233.00         | 8.00             | 130.00    | -21.15        | 0.13               | 0.00            |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427 - PIPE REPORT - GREENBRIAR Headloss Flow Velocity Length Diameter Roughness ID (gpm) (ft/s) (ft) (in) (ft) 130.00 -61.91 0.40 0.03 8.00 289.50 P218 8.00 130.00 -244.04 1.56 0.42 313.50 P219 12.00 0.86 130.00 928.27 2.63 391.14 P220 0.18 8.00 130.00 109.84 0.70 590.71 P221 40.62 0.26 0.01 130.00 8.00 P222 253.00 179.41 1.15 0.30 8.00 130.00 390.32 P223 0.35 0.04 8.00 130.00 55.25 430.55 P224 796.08 2.26 0.41 130.00 248.33 12.00 P225 -77.23 0.07 430.73 8.00 130.00 0.49 P226 729.94 0.58 12.00 130.00 2.07 412.22 P227 956.79 0.61 12.00 130.00 2.71 262.25 P228 814.64 0.4412.00 130.00 2.31 253.00 P229 273.31 12.00 130.00 720.12 2.04 0.38 P230 0.39 130.00 799.64 2.27 234.73 12.00 P231 12.00 130.00 -942.95 2.67 0.96 422.16 P232 -985.57 2.80 1.47 596.34 12.00 130.00 P233 -1,174.57 3.33 2.02 12.00 130.00 P234 591.74 12.00 130.00 -1,307.88 3.71 2.45 587.67 P235 2.61 0.99 130.00 -918.58 12.00 457.95 P236 -153.75 0.440.03 12.00 130.00 359.68 P237 0.00 -21.78 0.14 130.00 P238 193.00 8.00 0.89 0.23 139.01 8.00 130.00 487.33 P239 0.14 486.84 8.00 130.00 -107.07 0.68 P240 0.25 0.75 130.00 -118.13 708.39 8.00 P241 -126.0608.0 0.24 617.10 8.00 130.00 P242 0.20 -1,352.05 1.70 18.00 130.00 319.69 P243 0.12 10.0 12.00 130.00 -42.13861.88 P244 0.16 534.05 18.00 130.00 -916.36 1.16 P245 0.23 130.00 -1.020.281.29 18.00 627.02 P246 0.10 18.00 130,00 -1.255.24 1.58 195.01 P247 130.00 -294.45 0.37 0.03 18.00 751.91 P248 12.00 130.00 -1,571.98 4.46 2.17 370.87 P249 130.00 1.20 -302.55 1.93 602.79 8.00 P250 -164.33 1.05 0.42 130.00 8.00 656.30 P251 1.08 0.34 130.00 -169.31 501.81 8.00 P252 2.14 0.70 130.00 754.17 464.05 12.00 P253 795.42 2.26 0.42 12.00 130.00 250.56 P254 0.18 423.72 8.00 130.00 -131.97 0.84 P255 0.01 130.00 -39.59 0.25 8.00 235.04 P256

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427 - PIPE REPORT - GREENBRIAR

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm)       | Velocity<br>(ft/s) | Headlos<br>(ft) |
|------|----------------|------------------|-----------|---------------------|--------------------|-----------------|
| P257 | 344.48         | 8.00             | 130.00    | 121.97              | 0.78               | 0.13            |
| P258 | 656.00         | 8.00             | 130.00    | 96.84               | 0.62               | 0.16            |
| P259 | 497.14         | 8.00             | 130.00    | 174.71              | 1.12               | 0.36            |
| P260 | 494.52         | 8.00             | 130.00    | -189.73             | 1.21               | 0.42            |
| P261 | 466.36         | 8.00             | 130.00    | 170.14              | 1.09               | 0.32            |
| P262 | 616.00         | 8.00             | 130.00    | 95.60               | 0.61               | 0.15            |
| P263 | 651.25         | 8.00             | 130.00    | 150.49              | 0.96               | 0.36            |
| P264 | 246.49         | 8.00             | 130.00    | 135.81              | 0.87               | 0.11            |
| P265 | 375.42         | 12.00            | 130.00    | -343.91             | 0.98               | 0.13            |
| P266 | 665.79         | 8.00             | 130.00    | 319.78              | 2.04               | 1.47            |
| P267 | 285.98         | 8.00             | 130.00    | -211.72             | 1.35               | 0.29            |
| P268 | 272.69         | 8.00             | 130.00    | 97.00               | 0.62               | 0.07            |
| P269 | 744.21         | 8.00             | 130.00    | 20.53               | 0.13               | 0.01            |
| P270 | 105.50         | 8.00             | 130.00    | 4.26                | 0.03               | O.0000          |
| P271 | 892.22         | 8.00             | 130.00    | 57.32               | 0.37               | 0.08            |
| P272 | 193.00         | 8.00             | 130.00    | 19.52               | 0.12               | 0.00            |
| P273 | 105.50         | 8.00             | 130.00    | -0.83               | 0.01               | 0.00            |
| P274 | 698.75         | 8.00             | 130.00    | -4.17               | 0.03               | 0.000           |
| P275 | 181.50         | 12.00            | 130.00    | -573.86             | 1.63               | 0.16            |
| P276 | 112.20         | 8.00             | 130.00    | -66.66              | 0.43               | 0.01            |
| P277 | 698.70         | 8.00             | 130.00    | -37.95              | 0.24               | 0.03            |
| P278 | 713.00         | 8.00             | 130.00    | 20.96               | 0.13               | 0.01            |
| P279 | 422.00         | 8.00             | 130.00    | -125.18             | 0.80               | 0.16            |
| P280 | 117.50         | 8.00             | 130.00    | 22.33               | 0.14               | 0.00            |
| P281 | 589.97         | 8.00             | 130.00    | -271.4 <del>9</del> | 1.73               | 0.96            |
| P282 | 130.50         | 8.00             | 130.00    | -302.42             | 1.93               | 0.26            |
| P283 | 410.65         | 18.00            | 130.00    | -2,321.52           | 2.93               | 0.69            |
| P284 | 500.49         | 8.00             | 130.00    | -213.38             | 1.36               | 0.52            |
| P285 | 807.99         | 8.00             | 130.00    | 20.56               | 0.13               | 0.01            |
| P286 | 193.00         | 8.00             | 130.00    | 22.97               | 0.15               | 0.00            |
| P287 | 263.00         | 8.00             | 130.00    | 113.18              | 0.72               | 0.08            |
| P288 | 738.30         | 8.00             | 130.00    | 25.06               | 0.16               | 0.01            |
| P289 | 233.02         | 8.00             | 130.00    | -55.16              | 0.35               | 0.02            |
| P290 | 739.64         | 8.00             | 130.00    | -155.10             | 0.99               | 0.43            |
| P291 | 252.00         | 8.00             | 130.00    | -18.63              | 0.12               | 0.00            |
| P292 | 262.03         | 8.00             | 130.00    | -104.19             | 0.66               | 0.07            |
| P293 | 924.17         | 8.00             | 130.00    | -20.02              | 0.13               | 0.01            |
| P294 | 770.75         | 8.00             | 130.00    | -52.97              | 0.34               | 0.06            |
| P295 | 956.68         | 8.00             | 130.00    | 77.77               | 0.50               | 0.15            |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427 - PIPE REPORT - GREENBRIAR Headloss Flow Velocity Diameter Length Roughness ID (gpm) (ft/s) (ft) (in) (ft) 2.45 2.15 130.00 -384.04 8.00 693.81 P296 117.00 0.75 0.23 130.00 8.00 P297 678.13 0.06 130.00 48.96 0.31 837.42 8.00 P298 -335.82 2.14 1.35 8.00 130.00 557.94 P299 0.06 0.00 130.00 -8.73 696.14 8.00 P300 0.000 0.02 -2.70 8.00 130.00 468.04 P301 0.000 5.79 0.04 8.00 130.00 255.36 P302 0.0000130.00 -1.53 0.01 247.32 8.00 P303 -1,315.12 3.73 0.88 130.00 12.00 208.11 P304 0.02 0.52 8.00 130.00 80.99 88.53 P305 0.31 130.00 -268.33 1.71 8.00 P306 193.00 0.00 130.00 7.53 0.05 8.00 582.27 P307 0.49 -175.24 1.12 130.00 677.66 8.00 P308 130.00 -62.64 0.40 0.02 8.00 195.00 P309 0.05-347.09 0.98 130.00 12.00 P310 132.50 0.46 130.00 -229.48 1.46 8.00 380.98 P311 0.46 -203.54 1.30 8.00 130.00 475.68 P312 0.09 -69.44 0.44 130.00 8.00 P313 655.89 0.18 130.00 -103.08 0.66 653.93 8.00 P314 0.00 20.38 0.13 215.00 8.00 130.00 P315 92.49 0.59 0.04 8.00 130.00 195.01 P316 0.01 48.70 0.31 214.88 8.00 130.00 P317 0.06 0.000 -9.72 252.22 130.00 8.00 P318 0.00 8.00 130.00 22.49 0.14 245.38 P319 0.00 0.07 130.00 11.39 8.00 607.50 P320 0.00 130.00 13.10 80.0 8.00 574.53 P321 0.05 0.000 -8.32 130.00 105.50 8.00 P322 -2.01 0.01 O.0000 130.00 8.00 P323 212,18 0.0000 2.69 0.02 8.00 130.00 105.50 P324 0.28 0.01 -43.47 130.00 8.00 P325 211.00 0.34 0.02 130.00 -52.82 211.30 8.00 P326 0.000 -6.50 0.04 130.00 209.82 8.00 P327 0.22 108.13 0.69 130.00 728.60 8.00 P328 0.24 0.82 128.49 594.64 8.00 130.00 P329 0.93 0.13 -145.49 130.00 258.06 8.00 P330 0.18 0.76 130,00 118.84 8.00 499.01 P331 0.03 130.00 -41.99 0.27 545.88 8.00 P332 62.93 0.40 0.09 130.00 8.00 P333 783.02 0.10 1.01 12.00 130.00 355.76 260.55 P334

| ID   | Length<br>(ft) | Diameter<br>(in) | Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss (ft) |
|------|----------------|------------------|-----------|---------------|--------------------|---------------|
| P335 | 255.00         | 8.00             | 130.00    | -546.04       | 3.49               | 1.52          |
| P336 | 255.00         | 8.00             | 130.00    | -216.19       | 1.38               | 0.27          |
| P337 | 255.07         | 8.00             | 130.00    | -103.97       | 0.66               | 0.07          |
| P338 | 255.00         | 12.00            | 130.00    | 1,149.74      | 3.26               | 0.84          |
| P339 | 255.00         | 12.00            | 130.00    | -804.55       | 2.28               | 0.43          |
| P340 | 255.00         | 8.00             | 130.00    | -77.59        | 0.50               | 0.04          |
| P341 | 255.00         | 8.00             | 130.00    | -70.41        | 0.45               | 0.03          |
| P342 | 246.98         | 8.00             | 130.00    | 16.90         | 0.11               | 0.00          |
| P343 | 253.00         | 8.00             | 130.00    | -112.17       | 0.72               | 0.08          |
| P344 | 147.50         | 12.00            | 130.00    | 87.35         | 0.25               | 0.00          |
| P345 | 147.37         | 12.00            | 130.00    | 295.84        | 0.84               | 0.04          |
| P346 | 147.50         | 12.00            | 130.00    | 317.46        | 0.90               | 0.04          |
| P347 | 147.59         | 12.00            | 130.00    | -577.00       | 1.64               | 0.14          |
| P348 | 381.04         | 8.00             | 130.00    | -153.96       | 0.98               | 0.22          |
| P349 | 190.72         | 18.00            | 130.00    | -1,183.95     | 1.49               | 0.09          |
| P350 | 253.02         | 8.00             | 130.00    | 26.48         | 0.17               | 0.01          |
| P351 | 233.00         | 8.00             | 130.00    | 37.99         | 0.24               | 0.01          |
| P352 | 1,365.42       | 24.00            | 130.00    | 1,265.31      | 0.90               | 0.18          |
| P353 | 1,505.76       | 30.00            | 130.00    | -1,265.31     | 0.57               | 0.07          |
| P354 | 369.99         | 8.00             | 130.00    | -133.24       | 0.85               | 0.16          |
| P355 | 369.99         | 8.00             | 130.00    | -153.02       | 0.98               | 0.21          |
| P356 | 117.50         | 8.00             | 130.00    | -50.23        | 0.32               | 0.01          |
| P357 | 195.00         | 8.00             | 130.00    | -90.72        | 0.58               | 0.04          |
| P358 | 193.00         | 8.00             | 130.00    | -90.07        | 0.57               | 0.04          |
| P359 | 500.49         | 8.00             | 130.00    | -196.33       | 1.25               | 0.45          |
| P360 | 500.78         | 8.00             | 130.00    | -252.68       | 1.61               | 0.72          |
| P361 | 677.66         | 8.00             | 130.00    | -160.75       | 1.03               | 0.42          |
| P362 | 482.45         | 12.00            | 130.00    | 1,290.47      | 3.66               | 1.96          |
| P363 | 677.66         | 8.00             | 130.00    | -173.07       | 1.10               | 0.48          |
| P364 | 1,180.18       | 30.00            | 130.00    | -785.32       | 0.36               | 0.02          |
| P365 | 1,577.01       | 24.00            | 130.00    | -1,844.15     | 1.31               | 0.42          |
| P366 | 701.50         | 24.00            | 130.00    | -2,149.15     | 1.52               | 0.25          |
| P367 | 242.00         | 18.00            | 130.00    | 2,355.13      | 2,97               | 0.42          |
| P368 | 738.68         | 18.00            | 130.00    | 2,037.67      | 2.57               | 0.97          |
| P369 | 253.00         | 8.00             | 130.00    | -95.74        | 0.61               | 0.06          |
| P370 | 660.09         | 8.00             | 130.00    | -135.65       | 0.87               | 0.30          |
| P371 | 193.00         | 18.00            | 130.00    | 1,742.16      | 2.20               | 0.19          |
| P372 | 595.91         | 18.00            | 130.00    | 1,505.05      | 1.90               | 0.45          |
| P373 | 191.34         | 18.00            | 130.00    | 1,331.48      | 1.68               | 0.11          |

| ID   | Length<br>(ft) | Diameter<br>(in) | AT GB-427 - PIPE<br>Roughness | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>(ft) |
|------|----------------|------------------|-------------------------------|---------------|--------------------|------------------|
| P374 | 105.50         | 8.00             | 130.00                        | 49.41         | 0.32               | 0.01             |
| P375 | 607.50         | 8.00             | 130.00                        | -10.23        | 0.07               | 0.00             |
| P376 | 438.00         | 18.00            | 130.00                        | 1,299.56      | 1.64               | 0.25             |
| P377 | 650.57         | 18.00            | 130.00                        | 1,003.72      | 1.27               | 0.23             |
| P378 | 112.20         | 8.00             | 130.00                        | -187.90       | 1.20               | 0.09             |
| P379 | 117.50         | 8.00             | 130.00                        | -22.79        | 0.15               | 0.00             |
| P380 | 348.36         | 8.00             | 130.00                        | 16.54         | 0.11               | 0.00             |
| P381 | 178.10         | 12.00            | 130.00                        | -300.02       | 0.85               | 0.05             |
| P382 | 1,122.42       | 24.00            | 130.00                        | -4,470.67     | 3.17               | 1.56             |
| P383 | 93.09          | 8.00             | 130.00                        | -228.75       | 1.46               | 0.11             |
| P384 | 195.01         | 8.00             | 130.00                        | 128.90        | 0.82               | 0.08             |
| P385 | 4,416.05       | 30.00            | 130.00                        | 1,569.82      | 0.71               | 0.30             |
| P386 | 3,100.00       | 24.00            | 130.00                        | -4,498.78     | 3.19               | 4.35             |
| P388 | 1,581.75       | 18.00            | 130.00                        | 1,048.42      | 1.32               | 0.61             |
| P389 | 621.96         | 18.00            | 130.00                        | 1,059.29      | 1.34               | 0.24             |
| P990 | 235.86         | 99.00            | 130.00                        | 1,569.82      | 0.07               | 0.0000           |
| P991 | 377.34         | 99.00            | 130.00                        | 1,569.82      | 0.07               | 0.0000           |
| P992 | 233.99         | 99.00            | 130.00                        | 4,498.78      | 0.19               | 0.000            |
| P993 | 232.72         | 99.00            | 130.00                        | 4,498.78      | 0.19               | 0.000            |

MAXIMUM DAY DEMANDS WITH FIRE FLOW AT GB-427 - PUMP REPORT - GREENBRIAR

| ID      | Elevation<br>(ft) | Downstream Pressure<br>(psi) | Flow<br>(gpm) | Head Gain<br>(ft) |
|---------|-------------------|------------------------------|---------------|-------------------|
| PUMP105 | 22.00             | 24.89                        | 1,569.82      | 79.45             |
| PUMP107 | 26.00             | 26.00                        | 4,498.78      | 86.01             |



# APPENDIX E BOUNDARY CONDITIONS



DEPARTMENT OF UTILITIES

**ENGINEERING** SERVICES DIVISION

#### CITY OF SACRAMENTO CALIFORNIA

1395 35th AVENUE SACRAMENTO, CA 95822-2911

PH (916) 264-1400 FAX (916) 264-1497

July 14, 2005 BE:be

#### **MEMORANDUM**

TO:

Joshua Wolf, Project Engineer

FROM:

Brett Ewart, Assistant Engineer

SUBJECT:

DISTRIBUTION SYSTEM BOUNDARY CONDITIONS FOR GREENBRIAR

The GREENBRIAR project has been incorporated into the City's regional model to verify boundary conditions and fireflow capacity at three proposed connections to the existing distribution system. Please refer to the attached map and graphs for location of analysis points and associated results.

The following assumptions were incorporated into this review:

- 1. The developer appropriately allocated demands and required fireflow.
- 2. Max Day conditions were prevalent.
- 3. The conditioned T-main alignment of 24 & 30-inch main was added to the proposed project.

Based on these criteria, a Maximum Day Demand condition, steady state modeling analysis was performed. Three (3) hydraulic capacity curves were prepared for the proposed development to represent the general capacity of the existing system at the three connections. This assumes that the proposed development has been constructed with Max Day demands allocated by Wood Rodgers.

Wood Rogers is encouraged to review the conditions placed upon the proposed project. A new 24/30-inch transmission main traveling west from the existing 24-inch main at the corner of Natomas Bl and Elkhorn Bl will need to terminate at the 30-inch T-main currently being constructed to serve the Airport and Metro Air Park.

This analysis does not represent a verification of the proposed hydraulic model, rather it is the existing boundary conditions should such demands be placed upon the distribution system at proposed location.

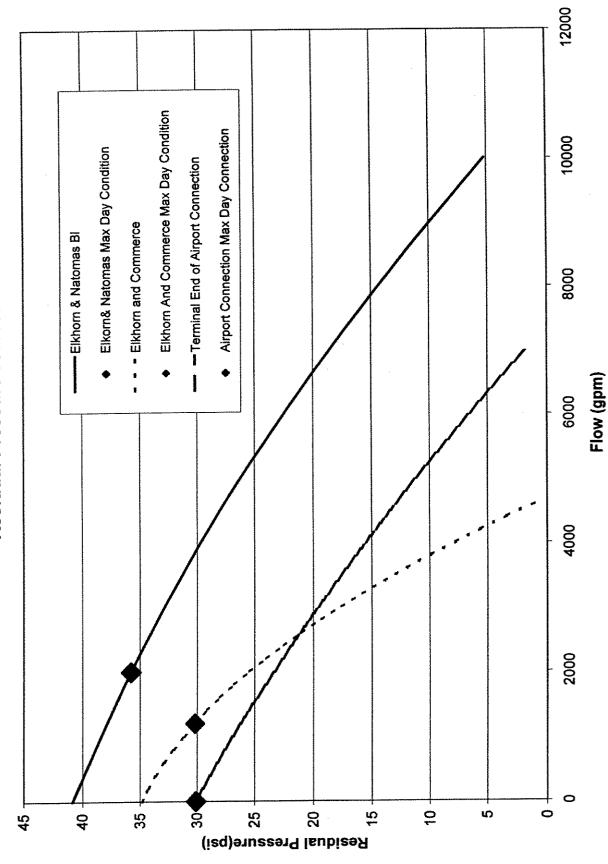
Should you have any further questions please do not hesitate to contact me at 808-1725.

The City does not certify or guarantee the accuracy or reliability of any information, data or modeling results set forth in this memorandum. Numerous factors, including unforeseen conditions and maintenance operations, may affect pressure conditions, and modeling results always should be verified by flow testing. By accepting a copy of this memorandum, any non-City user of this memorandum agrees to these conditions, and further agrees that the City of Sacramento will not be liable for any damages, costs, claims or other liability arising from any actions taken or omissions made in reliance on any information, data or results presented herein, nor will the City be liable for any other consequence arising from any such reliance.

12000 Elkhorn And Commerce Max Day Condition Airport Connection Max Day Connection 10000 Elkorn& Natomas Max Day Condition Terminal End of Airport Connection - - Elkhorn and Commerce - Elkhorn & Natomas Bl Greenbriar: Max Day Boundary Conditions 8000 Total Head vs. Flow Flow (gpm) 0009 4000 2000 0 0 20 9 100 00 80 120 -

(ff) bseH IstoT

Greenbriar: Max Day Boundary Conditions Residual Pressure vs. Flow



| merce (with<br>tomas BI) | 4" to Natom  | future 2   |            | rn & Natoma  |                   | 1  | n and Comr   |                                       |   | nal End of A<br>Connection | (   |
|--------------------------|--------------|--|------------|--------------|-------------------|--|--|---------------------------------------|---|----------------------------|---|
|                          | evertors (V) |  |            | avalisis (1) | <b>es</b> Node El |  | evalien (t)  | Note E                                | 4.00  | evāligi seid               | V(0)d(=:15)   |
| al L                     | Residual     | Available  |            | Residual     | Available         | x Day Boun   | Residual   | Available                             |   | A                          |   |
| Residual Head (ft)       | Pressure     | Flow   | Residual   | Pressure     | Flow              | Residual   | Pressure   | Flow                                  | Residual  | Residual Pressure          | \vailable<br>Flow   |
|                          | (psi)        | (gpm)  | Head (ft)  | (psi)        | (gpm)             | Head (ft)  | (psi)  | (gpm)                                 | Head (ft)   | (psi)                      | (gpm)   |
| 96                       | 30           | 3200   | 99         | 36           | 2000              | 93   | 30   | 1200                                  | 91  | 30                         | 0   |
| I PORSIGIIA              | Residual     | Available  | Residual   | Residual     | Available         | Residual   | Residual   | Available                             | المنابات المنابات   | Residual                   | vailable  |
| e Head (ft)              | Pressure     | Flow   | Head (ft)  | Pressure     | Flow              | Head (ft)  | Pressure   | Flow                                  | Residual<br>Head (ft)   | Pressure                   | Flow  |
| 115                      | (psi)        | (gpm)  | 440        | (psi)        | (gpm)             | ` '  | (psi)  | (gpm)                                 | rieau (it)  | (psi)                      | (gpm)   |
| 114                      | 38<br>38     | 0<br>200   | 110<br>109 | 41           | 0                 | 105  | 35   | 0                                     | 91  | 30                         | 0   |
| 113                      | 38           | 400  | 109        | 40<br>40     | 200<br>400        | 104<br>102   | 34   | 200                                   | 90  | 29                         | 200   |
| 112                      | 37           | 600  | 107        | 39           | 600               | 102  | 34<br>33   | 400<br>600                            | 89<br>87  | 29                         | 400   |
| 111                      | 37           | 800  | 106        | 39           | 800               | 98   | 32   | 800                                   | 86  | 28<br>28                   | 600<br>800  |
| 110                      | 36           | 1000   | 105        | 38           | 1000              | 96   | 31   | 1000                                  | 84  | 27                         | 1000  |
| 109                      | 36           | 1200   | 103        | 38           | 1200              | 93   | 30   | 1200                                  | 82  | 26                         | 1200  |
| 107                      | 35           | 1400   | 102        | 37           | 1400              | 91   | 29   | 1400                                  | 81  | 26                         | 1400  |
| 106<br>105               | 35<br>34     | 1600   | 101        | 37           | 1600              | 88   | 28   | 1600                                  | 79  | 25                         | 1600  |
| 105                      | 34<br>34     | 1800<br>2000   | 100<br>99  | 36<br>36     | 1800              | 85   | 27   | 1800                                  | 78  | 24                         | 1800  |
| 103                      | 33           | 2200   | 99         | 35           | 2000<br>2200      | 81<br>78   | 25   | 2000                                  | 76  | 23                         | 2000  |
| 101                      | 33           | 2400   | 96         | 35           | 2400              | 74   | 24<br>23   | 2200<br>2400                          | 74  | 23                         | 2200  |
| 100                      | 32           | 2600   | 95         | 34           | 2600              | 71   | 21   | 2600                                  | 72<br>71  | 22<br>21                   | 2400<br>2600  |
| 99                       | 32           | 2800   | 93         | 33           | 2800              | 67   | 19   | 2800                                  | 69  | 20                         | 2800  |
| 97                       | 31           | 3000   | 92         | 33           | 3000              | 62   | 18   | 3000                                  | 67  | 20                         | 3000  |
| 96                       | 30           | 3200   | 90         | 32           | 3200              | 58   | 16   | 3200                                  | 65  | 19                         | 3200  |
| 94<br>93                 | 30<br>29     | 3400   | 89         | 32           | 3400              | 54   | 14   | 3400                                  | 63  | 18                         | 3400  |
| 92                       | 28           | 3600<br>3800   | 88<br>86   | 31<br>30     | 3600              | 49   | 12   | 3600                                  | 62  | 17                         | 3600  |
| 90                       | 28           | 4000   | 85         | 30           | 3800<br>4000      | 44<br>39   | 10   | 3800                                  | 60  | 16                         | 3800  |
| 88                       | 27           | 4200   | 83         | 29           | 4200              | 34   | 8  | 4000<br>4200                          | 58<br>50  | 16                         | 4000  |
| 87                       | 26           | 4400   | 81         | 28           | 4400              | 28   | 3  | 4400                                  | 56<br>54  | 15<br>14                   | 4200  |
| 85                       | 26           | 4600   | 80         | 28           | 4600              | 26   | 1 1  | 4600                                  | 52  | 13                         | 4400<br>4600  |
| 84                       | 25           | 4800   | 78         | 27           | 4800              |  |  | _                                     | 50  | 12                         | 4800  |
| 82                       | 24           | 5000   | 77         | 26           | 5000              |  |  |                                       | 48  | 11                         | 5000  |
| 80<br>79                 | 24<br>23     | 5200   | 75<br>70   | 26           | 5200              |  |  |                                       | 46  | 10                         | 5200  |
| 77                       | 22           | 5400<br>5600   | 73<br>72   | 25           | 5400              |  |  |                                       | 44  | 9                          | 5400  |
| 75                       | 21           | 5800   | 70         | 24<br>23     | 5600<br>5800      |  |  |                                       | 41  | 8                          | 5600  |
| 73                       | 20           | 6000   | 68         | 23           | 6000              |  |  | and the second second                 | 39<br>37  | 8                          | 5800  |
| 71                       | 20           | 6200   | 66         | 22           | 6200              |  |  |                                       | 35  | 7 6                        | 6000<br>6200  |
| 69                       | 19           | 6400   | 64         | 21           | 6400              |  | ali mada masah badan di dalam di dalam<br>Managaran di dalam d | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 33  | 5                          | 6400  |
| 68                       | 18           | 6600   | 63         | 20           | 6600              |  |  |                                       | 30  | 4                          | 6600  |
| 66                       | 17           | 6800   | 61         | 19           | 6800              | e Transcours   |  | Service Annual Committee of           | 28  | 3                          | 6800  |
| 64<br>62                 | 16<br>15     | 7000<br>7200   | 59<br>57   | 19           | 7000              |  |  |                                       | 26  | 2                          | 7000  |
| 60                       | 15           | 7400   | 55         | 18<br>17     | 7200<br>7400      | Salah Sa<br>Salah Salah Sa |  |                                       |   |                            |   |
| 58                       | 14           | 7600   | 53         | 16           | 7400<br>7600      |  |  |                                       |   |                            |   |
| 56                       | 13           | 7800   | 51         | 15           | 7800              |  |  |                                       |   |                            |   |
| 53                       | 12           | 8000   | 49         | 14           | 8000              |  |  |                                       |   |                            |   |
| 51                       | 11           | 8200   | 47         | 13           | 8200              |  |  |                                       | dan San   |                            |   |
| 49<br>47                 | 10           | 8400   | 45         | 13           | 8400              |  |  |                                       |   |                            |   |
| 47                       | 8            | 8600<br>8800   | 43<br>41   | 12           | 8600              |  |  |                                       | y in the second   |                            |   |
| 43                       | 7            | 9000   | 39         | 11<br>10     | 9000<br>9000      |  |  |                                       |   |                            |   |
| 40                       | 6            | 9200   | 37         | 9            | 9200              |  |  |                                       |   |                            |   |
| 38                       | 5            | 9400   | 35         | 8            | 9400              | the second of the second of  |  |                                       |   |                            |   |
| 36                       | 4            | 9600   | 32         | 7            | 9600              |  |  |                                       |   |                            | ening of more than the  |
| 33                       | 3            | 9800   | 30         | 6            | 9800              |  | and the second   | No. of the second                     |   |                            | i digi kwaling digi Magazini (1885)<br>Promoning kwaling digi ya me |
| 31                       | 2            | 10000  | 28         | 5            | 10000             |  | As various months  |                                       |   |                            |   |
| 29                       | 1            | 10200  | 26         | 4            | 10200             | ng mga wani yani laba ili sagat ya<br>Sagat Sagat Ili sagat ili sagat ya sagat ili sagat ya sa   |  |                                       |   |                            |   |
|                          |              |  | 23         | 3            | 10400             | A Principal and Comments   | ed significant of feeting.   |                                       | a de la companya de<br>La companya de la co |                            |   |
|                          |              | and the state of the   | 21         | 2.           | 10600             |  |  |                                       |   |                            |   |
|                          |              | The second secon | 19         | 1 1          | 10800             | and and the second second second second  | . 40 GSE 14 7 - 179 11 E-111 CS  |                                       | 🔫 lasti ya Magazini a G   | All Shirt Street Commence  | 100000000000000000000000000000000000000                             |



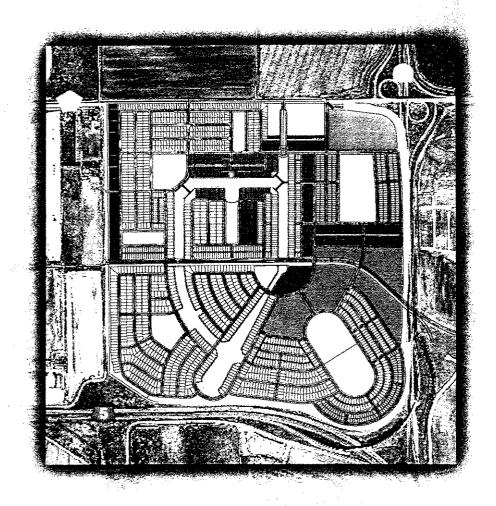
|   | (XNG5)   | on - PUMP-105  | Elkhorn and Commerce (with future 24" to Natomas<br>Blvd - PUMP-107 (XNG7) |  |                                   |  |  |
|---|--|--|--|--|-----------------------------------|--|--|
| atoto <b>a</b> G  |  |  | ু <mark>(তু</mark> তু গোলা)  | enceri.  |                                   |  |  |
|   | <u> </u>   | Max Day Bound  | lary Conditions  |  |                                   |  |  |
| Available Flow  | Residual   | Residual Head  | Available Flow   | Residual   | Residual Head                     |  |  |
| (gpm)   | Pressure (psi)   | (ft)   | (gpm)  | Pressure (psi)   | (ft)                              |  |  |
| 0   | 30.1   | 91.4   | 3069   | 30.6   | 96.7<br>Residual Head             |  |  |
| Available Flow  | Residual   | Residual Head  | Available Flow   | Residual   | 1                                 |  |  |
| (gpm)   | Pressure (psi)   | (ft)   | (gpm)  | Pressure (psi)   | (ft)<br>115                       |  |  |
| 0   | 30.1   | 91.42  | 0  | 38.5   | 114                               |  |  |
| 200   | 29.4   | 89.99  | 200  | 38.1<br>37.7   | 113                               |  |  |
| 400   | 28.8   | 88.53  | 400  | 37.7   | 112                               |  |  |
| 600   | 28.2   | 87.06  | 600  | 36.8   | 111                               |  |  |
| 800   | 27.5   | 85.53  | 800  | 36.4   | 110                               |  |  |
| 1000  | 26.8   | 83.99  | 1000   | 35.9   | 109                               |  |  |
| 1200  | 26.2   | 82.42  | 1200<br>1400   | 35.5<br>35.1   | 107                               |  |  |
| 1400  | 25.5   | 80.83  | 1600   | 34.6   | 106                               |  |  |
| 1600  | 24.8   | 79.21  | 1800   | 34.2   | 105                               |  |  |
| 1800  | 24.0   | 77.55<br>75.89   | 2000   | 33.8   | 104                               |  |  |
| 2000  | 23.3   | 75.89  | 2200   | 33.3   | 103                               |  |  |
| 2200  | 22.6   | 72.45  | 2400   | 32.5   | 101                               |  |  |
| 2400  | 21.8   | 70.72  | 2600   | 32.0   | 100                               |  |  |
| 2600  | 21.1   | 68.95  | 2800   | 31.6   | 99                                |  |  |
| 2800  | 20.3<br>19.5   | 67.15  | 3000   | 30.7   | 97                                |  |  |
| 3000  | 19.5   | 65.3   | 3200   | 30.3   | 96                                |  |  |
| 3200  | 17.9   | 63.46  | 3400   | 29.4   | 94                                |  |  |
| 3400  | 17.9   | 61.59  | 3600   | 29.0   | 93                                |  |  |
| 3600  | 16.3   | 59.67  | 3800   | 28.6   | 92                                |  |  |
| 3800  | 15.5   | 57.76  | 4000   | 27.7   | 90                                |  |  |
| 4000<br>4200  | 14.6   | 55.8   | 4200   | 26.8   | 88                                |  |  |
| 4400  | 13.8   | 53.84  | 4400   | 26.4   | 87                                |  |  |
| 4600  | 12.9   | 51.83  | 4600   | 25.5   | 85                                |  |  |
| 4800  | 12.0   | 49.8   | 4800   | 25.1   | 84                                |  |  |
| 5000  | 11.1   | 47.75  | 5000   | 24.2   | 82                                |  |  |
| 5200  | 10.3   | 45.69  | 5200   | 23.4   | 80                                |  |  |
| 5400  | 9.3  | 43.59  | 5400   | 22.9   | 79                                |  |  |
| 5600  | 8.4  | 41,47  | 5600   | 22.1   | 77                                |  |  |
| 5800  | 7.5  | 39.33  | 5800   | 21.2   | 75                                |  |  |
| 6000  | 6.5  | 37.13  | 6000   | 20.3   | 73                                |  |  |
| 6200  | 5.6  | 34.94  | 6200   | 19.5   | 71                                |  |  |
| 6400  | 4.6  | 32.73  | 6400   | 18.6   | 69                                |  |  |
| 6600  | 3.7  | 30.49  | 6600   | 18.2   | 68                                |  |  |
| 6800  | 2.7  | 28.23  | 6800   | 17.3   | 66                                |  |  |
| 7000  | 1.7  | 25.92  | 7000   | 16.5   | 64                                |  |  |
|   |  |  | 7200   | 15.6   | 60                                |  |  |
|   |  |  | 7400   | 14.7   | 58                                |  |  |
| Tanan populario de la comunidad.<br>Tanàna populario de la comunidad de la comunida |  |  | 7600   | 13.9   | 56                                |  |  |
|   | en de la companya de<br>La companya de la co   |  | 7800   | 13.0   | 53                                |  |  |
|   |  |  | 8000   | 10.8   | 51                                |  |  |
|   |  |  | 8200<br>8400   | 10.0   | 49                                |  |  |
|   |  |  | 8400<br>8600   | 9.1  | 47                                |  |  |
|   |  | in the second management of the  | 8800   | 8.2  | 45                                |  |  |
| Byrneyde, warr da'r bri   |  |  | 9000   | 7.4  | 43                                |  |  |
| <u> Zajenaj je podeje je je</u>   |  |  | 9200   | 6.1  | 40                                |  |  |
| en e  | and the second of the second o | - Commence of the commence of  | 9400   | 5.2  | 38                                |  |  |
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| and the second second second second   | The second of th |  | 9800   | 3.0  | 33                                |  |  |
|   |  |  | 10000  | 2.2  | 31                                |  |  |
| and Land Company of the   |  |  | 10200  | 1.3  | 29                                |  |  |
|   |  | Barrell Brown and Brown  |  | The second secon | and records develop the formation |  |  |
|   |  | and the second control of the second control |  |  |                                   |  |  |

| Terminal End o   | of Airport Connecti<br>(XNG5B)  | on - PUMP-105  | Elkhorn and Commerce (with future 24" to Natomas<br>Blvd - PUMP-107 (XNG7B) |                                     |  |  |  |
|--|---|----------------|---|-------------------------------------|--|--|--|
| Table 100  |   |                | astre case.   | ទៅលើមេ                              |  |  |  |
| 244 144 4 VOICE 10   | rainty(G)   | Peak Hour Bour |   | Andrew Michael St. Edward           | 1 - 1 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -  |  |  |
| Available Flow   | Residual  | Residual Head  | Available Flow  | Residual                            | Residual Head  |  |  |
| (gpm)  | Pressure (psi)  | (ft)           | (gpm)   | Pressure (psi)                      | (ft)   |  |  |
| 407  | 30.0  | 91.2           | 3582  | 30.2                                | 95.9   |  |  |
| Available Flow   | Residual  | Residual Head  | Available Flow  | Residual                            | Residual Head  |  |  |
| (gpm)  | Pressure (psi)  | (ft)           | (gpm)   | Pressure (psi)                      | (ft)   |  |  |
| 0  | 31.2  | 94.18          | 0   | 39.7                                | 117.8  |  |  |
| 200  | 30.6  | 92.8           | 200   | 39.3                                | 116.8  |  |  |
| 400  | 30.0  | 91.3           | 400   | 38.9                                | 115.8  |  |  |
| 600  | 29.4  | 89.8           | 600   | 38.4                                | 114.8  |  |  |
| 800  | 28.7  | 88.3           | 800   | 38.0                                | 113.8  |  |  |
| 1000   | 28.0  | 86.8           | 1000  | 37.6                                | 112.8<br>111.8   |  |  |
| 1200   | 27.4  | 85.2           | 1200  | 37.1<br>36.3                        | 109.8  |  |  |
| 1400   | 26.7  | 83.6           | 1400<br>1600  | 35.8                                | 108.8  |  |  |
| 1600   | 26.0  | 82.0           | 1800  | 35.4                                | 107.8  |  |  |
| 1800   | 25.2  | 80.3<br>78.7   | 2000  | 35.0                                | 106.8  |  |  |
| 2000   | 24,5<br>23.8  | 76.9           | 2200  | 34.5                                | 105.8  |  |  |
| 2200<br>2400   | 23.0  | 75.2           | 2400  | 33.7                                | 103.8  |  |  |
| 2600   | 22.3  | 73.5           | 2600  | 33.2                                | 102.8  |  |  |
| 2800   | 21.5  | 71.7           | 2800  | 32.8                                | 101.8  |  |  |
| 3000   | 20.7  | 69.9           | 3000  | 31.9                                | 99.8   |  |  |
| 3200   | 19.9  | 68.1           | 3200  | 31.5                                | 98.8   |  |  |
| 3400   | 19.1  | 66.2           | 3400  | 30.6                                | 96.8   |  |  |
| 3600   | 18.3  | 64.4           | 3600  | 30.2                                | 95.8   |  |  |
| 3800   | 17.5  | 62.4           | 3800  | 29.8                                | 94.8   |  |  |
| 4000   | 16.7  | 60.5           | 4000  | 28.9                                | 92.8   |  |  |
| 4200   | 15.8  | 58.6           | 4200  | 28.0                                | 90.8   |  |  |
| 4400   | 15.0  | 56.6           | 4400  | 27.6                                | 89.8   |  |  |
| 4600   | 14.1  | 54.6           | 4600  | 26.7                                | 87.8<br>86.8   |  |  |
| 4800   | 13.2  | 52.6           | 4800  | 26.3<br>25.4                        | 84.8   |  |  |
| 5000   | 12.3  | 50.5           | 5000<br>5200  | 24.6                                | 82.8   |  |  |
| 5200   | 11.5  | 48.5<br>46.4   | 5400  | 24.1                                | 81.8   |  |  |
| 5400   | 10.5<br>9.6   | 44.2           | 5600  | 23.3                                | 79.8   |  |  |
| 5600   | 8.7   | 42.1           | 5800  | 22.4                                | 77.8   |  |  |
| 5800<br>6000   | 7.7   | 39.9           | 6000  | 21.5                                | 75.8   |  |  |
| 6200   | 6.8   | 37.7           | 6200  | 20.7                                | 73.8   |  |  |
| 6400   | 5.8   | 35.5           | 6400  | 19.8                                | 71.8   |  |  |
| 6600   | 4.9   | 33.3           | 6600  | 19.4                                | 70.8   |  |  |
| 6800   | 3.9   | 31.0           | 6800  | 18.5                                | 68.8   |  |  |
| 7000   | 2.9   | 28.7           | 7000  | 17.6                                | 66.8   |  |  |
|  |   |                | 7200  | 16.8                                | 64.8   |  |  |
|  | Talanda da kabupatèn da kabupatèn Kulong.<br>Kabupatèn da kabupatèn da kabupatèn Kulong.  |                | 7400  | 15.9                                | 62.8   |  |  |
|  | ing and the state of the state |                | 7600  | 15.0                                | 60.8   |  |  |
|  |   |                | 7800  | 14.2                                | 58.8   |  |  |
|  |   |                | 8000  | 12.9                                | 55.8   |  |  |
| Les de la Companya de |   |                | 8200  | 12.0                                | 53.8<br>51.8   |  |  |
|  |   |                | 8400<br>8600  | 11,2<br>10,3                        | 49.8   |  |  |
|  |   |                | 8800  | 9.4                                 | 47.8   |  |  |
|  |   |                | 9000  | 8.6                                 | 45.8   |  |  |
|  |   |                | 9200  | 7.3                                 | 42.8   |  |  |
|  |   |                | 9400  | 6.4                                 | 40.8   |  |  |
|  |   |                | 9600  | 5.5                                 | 38.8   |  |  |
|  |   |                | 9800  | 4.2                                 | 35.8   |  |  |
|  |   |                | 10000   | 3.4                                 | 33.8   |  |  |
|  |   |                | 10200   | 2.5                                 | 31.8   |  |  |
| Marie Carlos Car |   |                | ere gestes Sineral  | a Linearen Saria Sana Sana Sana     | A STATE OF THE STA |  |  |
|  |   |                |   | a stranger to the stranger with the |  |  |  |
|  |   |                |   | a fileways a comment of the comment |  |  |  |

Note: Boundary conditions for peak hour demands were derived from the maximum day demand boundary conditions at the recommendation of the City of Sacramento's Department of Utilities staff. Rating curves were increased by a constant head of 2.8 ft to account for booster pumps and to give a minimum residual pressure of 30 psi at the boundary points during peak hour demands.



## Greenbriar Sewer Study





July 2005

Prepared by

### WOOD RODGERS

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## Sewer Study For

### Greenbriar

Sacramento County, California

**July 2005** 

Prepared By:





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#### **EXHIBITS**

- Exhibit A Greenbriar Vicinity Map
- Exhibit B Preliminary Greenbriar Tentative Map
- Exhibit C CSD-1 Sewerage Facilities Expansion Master Plan (portions of)
- Exhibit D Greenbriar Sewer System Exhibits
- Exhibit E Greenbriar Sewer Study Calculations
- Exhibit F Greenbriar Schematic Sewer Study



#### EXECUTIVE SUMMARY

#### **Purpose Statement**

This sewer study is a preliminary study for the purpose of the preparing the Environmental Impact Report (EIR) and to provide support documentation for the use in the Greenbriar improvement plans. This study will demonstrate the ability of the required facilities to service the site by a combination of gravity and force main and provide a general guideline of the domestic and commercial collection system for the Greenbriar development. This analysis will ensure that the proposed sewer system will be designed appropriately to meet or exceed the County Sanitation District 1 (CSD-1) system design criteria.

#### **Major Project and Study Characteristics**

The Greenbriar project will consist of mixed land use and densities. Mixed use includes low, medium and high-density residential, parks, open space, commercial and school land use. The project site is located west of the North Natomas area, bordered to the south by Interstate 5 and bordered to the north by Elkhorn Boulevard. The project site is currently located outside the City of Sacramento limits, but the application process for annexation has been initiated. This study depicts the ultimate service design; therefore interim facilities are not required. Offsite flows include two 16-inch force main sewer lines from Metro Air Park that will converge with on site sewerage at the most easterly on-site manhole.

The methodology used in this analysis was consistent with the County Sanitation District-1 design standards. The total acreage to be served is approximately 577 acres designed for approximately 4,650 equivalent dwelling units yielding an on-site peak wet weather design flow (PWWF) of 3.05 mgd. The ESD's differ from the 3,723 units depicted on the Tentative Subdivision Map dated May 2, 2005 due to the CSD-1 minimum design criteria of 6 ESD's per acre.

Upstream flows from Metro Air Park (MAP and Sacramento International Airport (SIA) will be conveyed by two 16-inch force mains that will be located in the open space buffer adjacent to Elkhorn Boulevard, following the buffer south adjacent to Highway 99. The force mains will convey design 8.73 mgd PWWF as presented in the Metro Air Park Sanitary Sewer Study prepared by Stantec Consulting, Inc.

The Greenbriar and Metro Air Park upstream sewerage converge with a combined design PWWF of 11.78 mgd, gravity across cross Highway 99 into the 33-inch diameter North Natomas Interceptor located in Greg Thatch Circle.

Development phasing will likely occur, however this study looked at build out conditions.

A lift station and 10-inch force main will be required to service approximately 75% of the site. This facility is anticipated to be permanent and no interim facilities will be needed.



The Greenbriar project has not been considered in the CSD-1 Sewerage Facilities Master Expansion Master Plan shed delineation due to being outside the current Urban Services Boundary.

#### Conclusion

The upstream flow of 11.78 mgd (including Greenbriar and Metro Air Park) does not appear to adversely affect the North Natomas Interceptor. Capacity was verified in the existing downstream 33, 36, and 42-inch diameter pipe lines extending south to Del Paso Boulevard. Our project team will be working with SCRSD to analyze the existing capacity in the SCRSD system south of Del Paso Boulevard. This will involve coordination with SCRSD and their regional sewer system model. It is anticipated that this report will be updated in the future based on the review, analysis and comments from SCRSD and CSD-1.

Details regarding the proposed on-site lift station, proposed on-site gravity service and connection to the existing system will also be provided pending comments from SCRSD and CSD-1.



#### INTRODUCTION

#### Level of Study

The Greenbriar sewer system analysis presented in this document is consistent with the Tentative Subdivision Map dated May 2, 2005 (Exhibit B) for the Greenbriar development project. This study is intended to provide a general guideline of the domestic and commercial collection system for the Greenbriar development. This analysis will ensure that the proposed sewer lines will be designed appropriately to meet or exceed the County Sanitation District-1 (CSD-1) system design criteria.

#### **Detail Description**

The Greenbriar site boundary contains Lone Tree Canal along the western border. This canal is of special interest and will be preserved due to the Giant Garder snake habitat. There is currently an unused RD-1000 canal at the east border adjacent to Highway 99/70. The site will require bore and jacking under Highway 99/70 in order to connect to the North Natomas Interceptor.

The adjacent Metro Air Park (MAP) and Sacramento International Airport (SIA) will be utilizing the same interceptor connection under Highway 99/70. Metro Air Park has proposed pumping sewerage to the crossing location.

#### Location

Interstate 5 binds Greenbriar to the south, Elkhorn Boulevard to the North, and Highway 99/70 to the east and Sacramento Metro Airport to the west. The project site is outside the City of Sacramento limits, however the annexation application process has been initiated. Refer to Figure 1 -Location Map for the project location. Exhibit A for a scaled vicinity map.

## 

Figure 1 - Location Map

#### Topography

The existing site's topography is characterized by its

previous agricultural use. The geometry of the several pond areas previously used for growing



rice are still evident and render the site's existing ground elevations as exceptionally irregular particularly in the change in elevation between adjacent pond areas where these may change from 3-5 feet in elevation. Despite the sites irregular topography, the drainage pattern is still clear and can be classified as draining in a north-east to south-west direction. The existing ground elevations range from elevation 21.3 feet to 10.5 feet (NGVD 29). There is a dirt oval track in the upper northwest section of the site with adjacent stables structures.

The adjacent lands are very similar in nature, with erratic elevation differences due to the levy / channelizing of drains and water for agricultural uses.

#### Land Use and Zoning

The projects site's current land use is classified as agricultural. The site is predominantly vacant with a few horse stables and other structures located at the northwest corner of the site. The annexation application includes an amendment to the General Plan land use.

The proposed development will consist of approximately 577 acres of mixed land uses and densities. Mixed use includes low, medium, and high density residential, commercial, parks, light rail and school consistent with the Tentative Subdivision Map dated May 2, 2005. These proposed land uses were the basis of the sewer flower flow calculations within this study.

The property to the north of Elkhorn Boulevard is outside the City of Sacramento limits and still used for agriculture consistent with the General Plan. Metro Air Park to the west is considered as heavy industrial use in the General Plan, but is proposed as mixed land use including industrial and commercial uses.

#### DESIGN

The Greenbriar sewer analysis consisted of calculating the sewer flows and of designing the sewer system that would service the site.

#### Assumptions

The following assumptions were used as part of this analysis:

- Offsite sewer flows will not be served by the onsite sewer system until converging at the manhole prior to crossing Highway 99/70.
- The downstream North Natomas Interceptor does have capacity to carry the study area flows based on the Schumacher Property North Natomas Sanitary Sewer Master Plan dated February 20,2003 prepared by Wood Rodgers, Inc and the CSD-1 Sewerage Facilities Final Report.
- The North Natomas Interceptor extension is built to within 550 feet east of Highway 99/70. This study assumes the gravity extension will be built by others to the west of Highway 99/70 prior to the construction of the Greenbriar project.
- Groundwater is relatively high in the project area, and will be confirmed through future geotechnical studies for the project.



- The school site was assumed to be an elementary school site.
- The North Natomas Interceptor has capacity downstream without surcharge conditions.

#### Approach

The following approach was used to calculate the project site's sewer flows:

- Gross areas based on the Greenbriar Tentative Subdivision Map dated May 2, 2005 were used to calculate sewer flows.
- The centerline of the street adjacent to the service area was used as the shed boundary.
- Sub-shed areas were defined by service line and land use.
- Land use densities were determined by calculating the ratio of dwelling units to shed area.
- 310 gpd per unit was assumed to be the average flow for all land use densities.
- Sewer lines and services were placed in alley ways as required to avoid parallel lines.
- Slope adjustments to the sewer lines were used in preference to drop connections to shallow sewer lines were needed.
- The proposed rough grading ground elevations were used to set sewer depth.
- Minimum sewer line slopes were used to set vertical alignment, except at the end of each of the runs were slopes were doubled.
- For large area sites (i.e. commercial) 8-inch lines with a minimum slope of 0.006 were used to serve the site. Lines were run from connecting node to furthest shed line boundary distance.
- Minimum sewer depth was set between 5-6 feet from proposed ground elevation at centerline.
- Flows were determined based on the County improvement standards and on the design criteria listed in this study

#### Design Criteria

Section 7 of the County of Sacramento Public Works Agency Improvement Standards dated June 1, 1999 and Chapter 7 of the County Sanitation District 1 Sanitary Trunk Sewer design manual dated April 2002 were used as the basis for this design. The flows were generated using the guidelines found in the design flow criteria table located in section 7-3 of the County of Sacramento Public improvement standards. That table was modified to include CSD-1 Peak flow criteria for the use of this report and is presented as Table 1.



Table 1 Design flow criteria

| Category                         | ······································ |  | Conditions            |   | Modifiers                                |  |  |  |
|----------------------------------|--|--|-----------------------|---|--|--|--|--|
| Development<br>Density           | Low<br>Density<br>Residential          |  | Commercial/Industrial | Transit<br>Oriented<br>Development  | Minimum Plan<br>density shall<br>be RD-6 |  |  |  |
| Flow generation<br>(310 gpd/ESD) | 6 ESD/Ac                               | ESD/Ac 15 ESD/Ac 6 ESD/Ac 11 ESD/Ac  |                       | Rainfall<br>dependent I/I:<br>Existing Areas<br>-1,600 gpd/Ac<br>*New areas -<br>1,200 gpd/Ac |  |  |  |  |
| Peaking Factor                   | PF=3                                   | PF=3.5-1.8Qa <sup>0.05</sup> (Qa=ADWF,mgd) -Collectors<br>PF=3.3-1.8Q <sup>0.04</sup> (Q=BWF, MGD) - Trunk |                       |   |  |  |  |  |
| Velocity Criteria                | Mii                                    | Minimum 2 fps at Peak Dry Weather Flow   |                       |   |  |  |  |  |
| Hydraulic<br>Grade Line          | Maximur                                | Maximum HGL at crown of pipe at Peak Wet Weather Flow  |                       |   |  |  |  |  |
| Friction Factor                  |  | n=0.013  |                       |   |  |  |  |  |
| Minimum Depth                    |  | 5' at periphery of service area  |                       |   |  |  |  |  |

For the onsite elementary school site, the greater of the specified average daily flow was used as stated in section 7-2A.4 of the Sacramento County Improvement standards.

Sewer flows were calculated by land use in accordance with the Tentative Subdivision Map. Collector peaking factors were used until the flows exceeded 1 mgd. After the flows exceeded 1 mgd, the trunk peaking factor was utilized. Greenbriar sewer study calculations are included in spreadsheet form in **Exhibit E**.

#### SEWER FLOW INFORMATION

Flow data from this project were calculated within this study. Upstream flow data was obtained from the Metro Air Park CSD-1 Sanitary Sewer Study prepared by Stantec Consulting Inc.

#### Onsite Flows (Total Project Acreages, ESD's & PWWF)

The combined sewer system for the Greenbriar project site will serve approximately 577 acres (4650 ESD's). The proposed development will produce approximately 3.05 mgd PWWF of which an onsite lift station will service approximately 2.07 mgd. Development phasing was not considered at this time.

The lift station design is not included in this study and will be a separate design report. The lift station is expected to be located generally in the middle of the site as shown on the schematic sewer study, **Exhibit F**. The depth of the lift station will be roughly 25 feet. A 10-inch force



main will convey flows from the wet well approximately 200 feet to a transition manhole. Flows of 2 mgd will produce velocities of roughly 6 fps.

#### Offsite Flows

The upstream flows from Metro Air Park and the Sacramento International Airport are considered at full development to be 8.73 mgd based on the Metro Air CSD-1 Sewer Study prepared by Stantec Consulting, Inc. Upstream flows were considered at build out conditions and phasing was not considered. The upstream flows converge with onsite flows for combined flow of 11.78 mgd at Node 1 (located in Exhibit F) before connecting with the North Natomas Interceptor. Upstream flows will be conveyed to Node 1 by two 16-inch force mains proposed to be located within the Greenbriar green space buffer adjacent to Elkhorn Boulevard and Highway 99/70. Upstream flows will not be conveyed through the onsite system until Node 1 shown on Exhibit F) where flows cross the Highway to the existing interceptor.

The downstream connection to the North Natomas Interceptor is at the end of Greg Thatch Circle on the east side of Highway 99/70. Our connection is to a 33-inch interceptor with a slope of 0.0020 with an available capacity of 15.28 mgd PWWF. The 33-inch continues at this slope connecting to a 36-inch section of interceptor (at minimum slope S=0.0010) with a capacity of 11.78 mgd in Greg Thatch Circle.

Estimated flows from the west of Highway 99/70 were higher than those reflected in the Schumacher Property North Natomas Sanitary Sewer Master Plan dated February 20, 2003 prepared by Wood Rodgers, Inc. Estimated flows from the west of Highway 99/70 in the Schumacher study were 7.70 mgd PWWF (not including the Greenbriar project). The flows reflected in the CSD-1 Sewerage Facilities Expansion Master Plan for the area west of Highway 99 (not including the Greenbriar project) are 9.79 mgd (Exhibit C). Though the actual flows from the combined west area (MAP, SIA, and the Greenbriar project) are higher than those originally assumed, it appears that the North Natomas Interceptor has capacity for the additional flows down to Del Paso Boulevard.

The impact to the existing downstream interceptor (south of Del Paso Road) is not known at this time. CSD-1 / SRCSD are in the process of initiating modeling of this interceptor conditions downstream and searching for the interceptor studies and design reports. We expect to update this study when the information is available.

#### SEWER ALIGNMENT AND FACILITIES

#### **Ultimate Sewer Alignment**

The Greenbriar site will be served by a combination of gravity flow and force main sewer system. Approximately ¼ of the project area will be able to gravity flow to the existing North Natomas interceptor. The remaining project site area will gravity flow to a centrally located lift station lift station (Exhibit D). Flows from the lift station will be conveyed to the gravity line via an 18-inch sewer force main or combination 16 and 12-inch force mains. A preliminary location for the lift station has been selected. A detailed design report for the lift station will be prepared for submittal as the project progresses.



For the purpose of presenting this analysis, the Greenbriar sewer system was divided into two major sewer systems: System A and System B. System A is a gravity system that will convey the onsite flows to the existing 33-inch sewer line bypassing the lift station. System B is also a gravity system; however, this system will convey the onsite flows to the lift station which will subsequently connect to System A via a sewer force main. Exhibit D shows the System A and System B service areas.

#### System A

Sewer system A will serve approximately 123.5 Acres. Approximately 0.98 mgd will bypass the lift station and gravity flow directly into the existing 33-inch sewer trunk line. Minimum sewer line depth from existing ground to the top of pipe for this system is of 6.0 feet.

#### System B

Two separate pipe systems will convey flows to the lift station. The first system approaches the lift station from the west and services approximately 45% of the lift station flows. This system will convey approximately 0.86 mgd via a 15-inch sewer line. The second system B sub shed approaches the lift station from the south and services the remaining 55% of the lift station service area. This system will convey approximately 0.62 mgd by means of a 10-inch sewer line. The sewer invert entering the lift station is approximately 22.2 feet and 22.9 feet respectively. Flows from the lift station will be conveyed via an 10-inch sewer force main line to the nearest manhole, Node 4 on **Exhibit F**, and will gravity flow under Highway 99-70 to the existing North Natomas Interceptor. The hydraulic head between the lift station's sump elevation and the manhole's sump elevation is 13.6 feet. The length of the 10-inch sewer force main is approximately 200 feet, producing velocities of approximately 6 fps.

The flows from Metro Air Park, Sacramento International Airport and the Greenbriar development converge at Node 1, **Exhibit F**, prior to crossing Highway 99/70. The depth of the sewer line crossing Highway 99/70 is 17.0 feet to top of pipe. The slope of the 33-inch interceptor crossing is designed to convey the flows at a velocity of 3 ft/s.

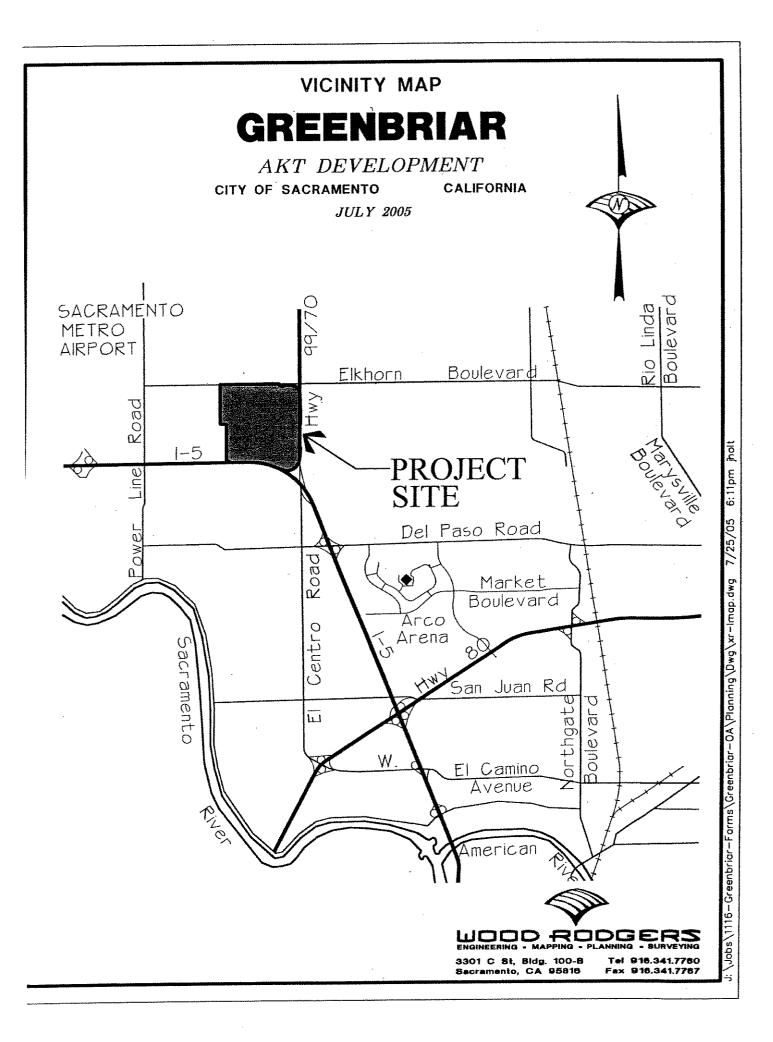
#### CONCLUSIONS

This sewer study is a preliminary study for the purpose of the preparing the Environmental Impact Report (EIR) and to provide support documentation for the use in the Greenbriar improvement plans. As configured, the on site project flows and off site shed flows converge and ultimately gravity sewer to the North Natomas interceptor.

The overall Greenbriar project of 577 acres account for 4,650 ESD's producing a peak wet weather flow of 3.05 mgd. Off site flows from the MAP and SIA include 1,911 acres accounting for 8.726 mgd PWWF. The combined flow of 11.78 mgd does not appear to adversely affect the North Natomas Interceptor. Conditions downstream of the North Natomas Interceptor are unclear and under investigation and further analysis by CSD-1 and not considered in this analysis.

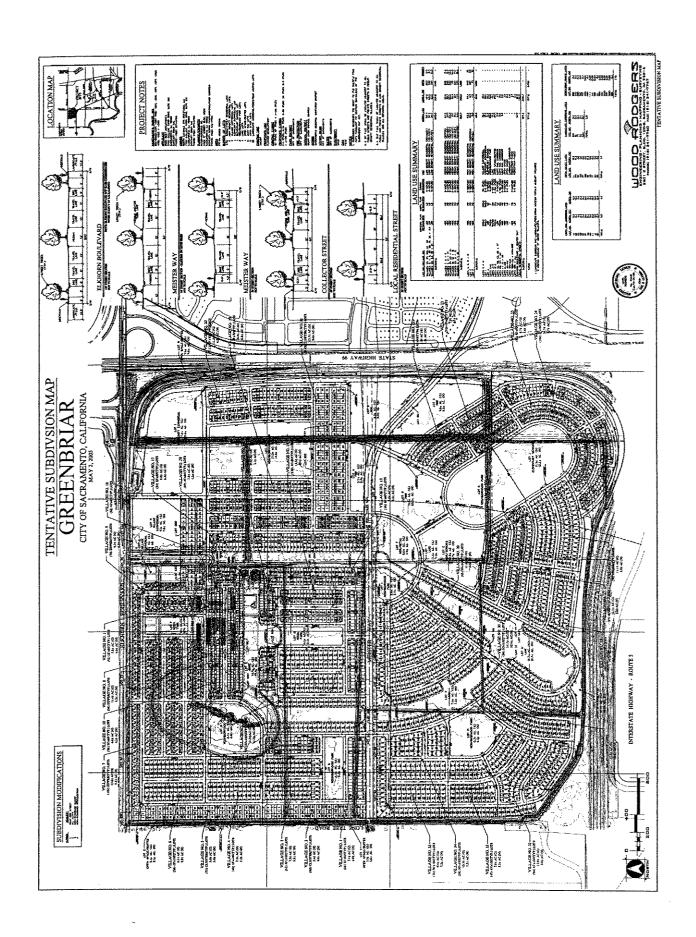


## EXHIBIT A GREENBRIAR VICINITY MAP





## EXHIBIT B PRELIMINARY GREENBRIAR TENTATIVE MAP





# EXHIBIT C CSD-1 SEWERAGE FACILITIES EXPANSION MASTER PLAN (PORTIONS OF)

#### CSD-1 SEWERAGE FACILITIES EXPANSION MASTER PLAN

#### NN NATOMAS NORTH TRUNK SHED

#### Area Description

The NN Natomas North Trunk Shed is located east of Highway 99, north of Del Paso Road, and south of Elkhorn Boulevard. The Trunk Shed includes the Schumacher, Northborough, and a portion of the Northpointe Park developments, which are located, respectively, in the western, central, and eastern portions of the trunk shed. The Schumacher and Northborough developments are anticipated to develop within the 2000 to 2005 year time frame. The portion of the Northpointe Park development contained in the NN Natomas North Trunk Shed is anticipated to start developing within the 2005 to 2010 year time frame.

#### **Trunk System Facilities**

A major trunk sewer (Trunk NNI) extending north along the western side of the East Drainage Canal and a permanent pump station would serve most of the Northborough development. This trunk would connect into the recently constructed trunk sewer that discharges to the existing North Natomas Interceptor. Minor trunk sewers that cross the East Drainage Canal and connect to Trunk NNI would serve the portion of the Northpointe Park development that is part of this trunk shed. The Schumacher development would be served by minor trunks and local collectors that would connect to the future extension of the North Natomas Interceptor.

Since the downstream trunk and interceptor sewers that would serve the Northborough and Northpoint Park developments are already constructed, interim facilities would not be required for these areas. Similarly, because the extension of the North Natomas Interceptor is expected to be on line prior to the time trunk sewer connections are required to serve the Schumacher Development, there would be no need for interim facilities for this area.

#### **Trunk Projects**

Four trunk projects are identified for this trunk shed, as shown in the table below.

| Project<br>ID | Diam.<br>(in.) | Length<br>(ft.) | Phase | Estimated Construction Cost (\$) | Estimated<br>Capital Cost<br>(\$) |
|---------------|----------------|-----------------|-------|----------------------------------|-----------------------------------|
| NNH           | 12-15          | 1,650           | 1     | 489,000                          | 611,000                           |
| NNI           | 15-27          | 7,300           | 1     | 3,801,000                        | 4,751,000                         |
| NNJ-3         | 18             | 2,450           | 1     | 665,000                          | 831,000                           |
| NNJ-4         | 15             | 3,050           | 1     | 1,003,000                        | 1,254,000                         |

#### NN Natomas North Trunk Shed

#### Attachments

- Trunk shed map showing proposed trunk sewers, sizes, model manhole ID numbers, and sewersheds.
- Project map showing trunk projects and interim facilities (if needed).
- Trunk shed ESD projections by sewershed.
- Sewershed load manholes.
- Cross-reference sewershed manholes to recently constructed manholes (as of February 2002).
- Trunk sewer data and model results.
- Profile(s) of major trunk sewers.
- Trunk project cost estimates.

NN Natomas N
Trunk Shed Buildout Projections

|           |       | ES    | Ds     |          | Area (acres) |      |       |          |  |
|-----------|-------|-------|--------|----------|--------------|------|-------|----------|--|
| Sewershed | 2005  | 2010  | 2020   | Buildout | 2005         | 2010 | 2020  | Buildout |  |
| NNH-01    | 0     | 0     | 281    | 490      | 0            | 0    | 45    | 78       |  |
| NNH-02    | 0     | 0     | 335    | 585      | 0            | 0    | 34    | 59       |  |
| NNH-03    | 0     | 0     | 177    | 309      | 0            | 0    | 24    | 42       |  |
| NNH-04    | 0     | 0     | 687    | 1,199    | 0            | 0    | 89    | 156      |  |
| NNH-05    | 351   | 351   | 351    | 1,459    | 36           | 36   | 36    | 150      |  |
| NNH-06    | 87    | 246   | 307    | 377      | 9            | 26   | 32    | 40       |  |
| NNH-07    | 184   | 184   | 184    | 764      | 21           | 21   | 21    | 87       |  |
| NNH-08    | 97    | 97    | 97     | 403      | 16           | 16   | 16    | 67       |  |
| NNH-09    | 71    | 71    | 71     | 297      | 12           | 12   | 12    | 49       |  |
| NNH-10    | 169   | 475   | 592    | 728      | 19           | 54   | 68    | 83       |  |
| NNI-01    | 50    | 57    | 64     | 86       | 8            | 10   | 11    | 14       |  |
| NNI-02    | 568   | 647   | 729    | 974      | 74           | 84   | 95    | 126      |  |
| NNI-03    | 256   | 719   | 896    | 1,102    | 31           | 87   | 109   | 134      |  |
| NNI-04    | 435   | 495   | 558    | 746      | 70           | 80   | 90    | 121      |  |
| NNI-05    | 257   | 293   | 330    | 441      | 37           | 42   | 47    | 63       |  |
| NNI-06    | 85    | 240   | 299    | 368      | 9            | 24   | 30    | 37       |  |
| NNI-07    | 63    | 177   | 221    | 272      | . 8          | 21   | 27    | 33       |  |
| NNI-08    | 159   | 448   | 558    | 687      | 26           | 73   | 91    | 112      |  |
| NNI-09    | 312   | 878   | 1,095  | 1,346    | 49           | 137  | 171   | 211      |  |
| NNI-10    | 94    | 264   | 330    | 405      | 16           | 44   | 55    | 68       |  |
| NNJ-04    | 1     | 588   | 1,521  | 1,836    | 0            | 74   | 191   | 230      |  |
| NNJ-05    | 1     | 1     | 11     | 531      | 0            | 0    | 2     | 85       |  |
| NNJ-06    | 0     | 144   | 373    | 451      | , 0          | 24   | 62    | 75       |  |
| NNJ-07    | 0     | 371   | 959    | 1,158    | 0            | 55   | 141   | 170      |  |
| NNJ-08    | 1     | 1     | 11     | 577      | 0            | 0    | 2     | 96       |  |
| Total     | 3,243 | 6,748 | 11,038 | 17,591   | 441          | 921  | 1,501 | 2,387    |  |

#### Trunk Shed NN Natomas North Sewershed Load Manholes

| Sewershed | Load Manhole |
|-----------|--------------|
|           |              |
| NNH-01    | NNH120       |
| NNH-02    | NNH120       |
| NNH-03    | NNH910       |
| NNH-04    | NNH210       |
| NNH-05    | NNH320       |
| NNH-06    | NNH310       |
| NNH-07    | NNH430       |
| NNH-08    | NNH440       |
| NNH-09    | NNH430       |
| NNH-10    | NNH420       |
| NNI-01    | NNI9030      |
| NNI-02    | NNI9090      |
| NNI-03    | NNI910       |
| NNI-04    | NNI9230      |
| NNI-05    | NNI010       |
| NNI-06    | NNI020       |
| NNI-07    | NNI030       |
| NNI-08    | NNI040       |
| NNI-09    | NN1070       |
| NNI-10    | NNI060       |
| NNJ-04    | NNJ120       |
| NNJ-05    | NNJ140       |
| NNJ-06    | NNJ910       |
| NNJ-07    | NNJ220       |
| NNJ-08    | NNJ240       |

## Trunk Shed NN Natomas North Cross-reference Sewershed Manholes to Recently Constructed Manholes (as of February 2002)

| Trunk Shed  | MH No. in Future  Trunk Model <sup>1</sup> | GIS MH No. 2 |  |  |  |  |
|---|--|--------------|--|--|--|--|
|   |  |              |  |  |  |  |
| NN Natomas North  | NN1040                                     | 22500406     |  |  |  |  |
| NN Natomas North  | NNI9010                                    | 22500405     |  |  |  |  |
| NN Natomas North  | NNI9020                                    | 22500404     |  |  |  |  |
| NN Natomas North  | NNI9030                                    | 22500403     |  |  |  |  |
| NN Natomas North  | NNI9040                                    | 22500402     |  |  |  |  |
| NN Natomas North  | NNI9210                                    | 22500401     |  |  |  |  |
| NN Natomas North  | NNI9220                                    | 20103515     |  |  |  |  |
| NN Natomas North  | NNI9230                                    | 20103514     |  |  |  |  |
| NN Natomas North  | NNI9240                                    | 20103513     |  |  |  |  |
| NN Natomas North  | NNI9250                                    | 20103511     |  |  |  |  |
| NN Natomas North  | NNI9260                                    | 20103516     |  |  |  |  |
| NN Natomas North  | NN19050                                    | 20103617     |  |  |  |  |
| NN Natomas North  | NNI9060                                    | 20103614     |  |  |  |  |
| NN Natomas North  | NNI9070                                    | 20103616     |  |  |  |  |
| NN Natomas North  | NNI9080                                    | 22511403     |  |  |  |  |
| NN Natomas North  | NN19090                                    | 22511402     |  |  |  |  |
| NN Natomas North  | NNI9110                                    | 22511401     |  |  |  |  |
| NN Natomas North  | NNJ9210                                    | 3            |  |  |  |  |
| NN Natomas North  | NNJ9220                                    | 3            |  |  |  |  |
| NN Natomas North  | NNJ9230                                    | 3            |  |  |  |  |
| NN Natomas North  | NNJ9240                                    | 3            |  |  |  |  |
| The Trunk Shed Maps do not show all manholes below     Closest manhole to future model node |  |              |  |  |  |  |
| 3) Not available  |  |              |  |  |  |  |

#### Trunk Shed NN Natomas North Buildout 10-Year Design Storm

| us                 | DS                 |              | Length      | US Rim     | DS Rim       | US Invert      | De Invent          |              | E C         | Peak         | A/ E-11  |              |
|--------------------|--------------------|--------------|-------------|------------|--------------|----------------|--------------------|--------------|-------------|--------------|----------|--------------|
| Manhole            |                    | Dia. (in.)   | (ft.)       | Elev.      | Elev.        | Elev.          | DS Invert<br>Elev. | Slope        | Full Cap.   | Flow         | % Full   | DS           |
| Mannore            | indiator:          | Dia. (111.)  | 7,27        | Elea.      | LIBY.        | Elev.          | EI6A"              | Siope        | (mgd)       | (mgd)        | Cap.     | d/D          |
| NNH110             | NN1010             | 12           | 151         | 20         | 22           | -2.46          | -2.80              | 0.0022       | 1.1         | 0.78         | 71       | 0.4          |
| NNH120             | NNH110             | 12           | 591         | 20         | 20           | -1.04          | -2.46              | 0.0024       | 1.1         | 0.78         | 68       | 0.6          |
| NNH910             | NN1050             | 10           | 299         | 20         | 10           | -1.12          | -2.17              | 0.0035       | 8.0         | 0.23         | 27       | 0.3          |
| NNH210             | NN1060             | 12           | 591         | 20         | 10           | 0.07           | -1.35              | 0.0024       | 1.1         | 0.87         | 76       | 0.4          |
| NNH410             | NN1080             | 42           | 541         | 20         | 10           | -3.29          | -3.62              | 0.0006       | 16.0        | 10.34        | 65       | 0.3          |
| NNH420             | NNH410             | 42           | 1040        | 20         | 20           | -2.67          | -3,29              | 0.0006       | 15.9        | 10.38        | 65       | 0.5          |
| NNH430             | NNH420             | 42           | 1460        | 20         | 20           | -1.80          | -2.67              | 0.0006       | 15.9        | 10.11        | 63       | 0.5          |
| NNH440             | NNH430             | 42           | 2139        | 20         | 20           | -0.51          | -1.80              | , 0.0006     | 16.0        | 9.65         | 60       | 0.58         |
| NNH310             | NN1080             | 15           | 659         | 20         | 10           | 1.16           | -0.09              | 0.0019       | 1.8         | 1,23         | 68       | 0.44         |
| NNH320             | NNH310             | 12           | 991         | 20         | 20           | 3.78           | 1.41               | 0.0024       | 1.1         | 0.98         | 88       | 0.52         |
| NNI9010            | NN1040             | 36           | 440         | 15         | 15           | -5.29          | -5.53              | 0.0006       | 10.1        | 8.01         | 79       | 0.37         |
| NNI9020<br>NNI9030 | NNI9010            | 36           | 479         | 17         | 15           | -5.05          | -5.29              | 0.0005       | 9.6         | 8.01         | 83       | 0.5          |
| NNI9040            | NNI9020<br>NNI9030 | 36<br>36     | 479<br>469  | 18<br>17   | 17           | -4.80          | -5.05              | 0.0005       | 9.8         | 8.01         | 81       | 0.61         |
| NNI9050            | NNI9040            | 36           | 961         | 12         | 18           | -4.56          | -4.80              | 0.0005       | 9,7         | 7.94         | 81       | 0.64         |
| NNI9060            | NNI9050            | 36           | 230         | 12         | 17<br>12     | -4.09<br>-3.97 | ~4.56              | 0.0005       | 9.5         | 6.64         | 70       | 0.66         |
| NNI9070            | NN19060            | 36           | 509         | 11         | 12           | -3.72          | -4.09<br>-3.97     | 0.0005       | 9.9<br>9.5  | 6.64         | 67       | 0.64         |
| NNI9080            | NNI9070            | 36           | 449         | 12         | 11           | -3.72          | -3.72              | 0.0005       | 9.7         | 6.64         | 70       | 0.63         |
| NNI9090            | NNI9080            | 36           | 341         | 12         | 12           | -3.32          | -3.49              | 0.0005       | 9.6         | 6.64<br>6.64 | 68<br>69 | 0.63<br>0.62 |
| NNI9110            | NNI9090            | 36           | 469         | 12         | 12           | -3.09          | -3.32              | 0.0005       | 9.5         | 5.98         | 63       | 0.62         |
| NNIFM1             | NNI9110            | 27           | 194         | 30         | 12           | -2.11          | -2.34              | 0.0003       | 6.9         | 6.00         | 87       | 0.62         |
| NNIFM2             | NNIFM1             | 24           | 30          | 12         | 30           | -21.96         | -2.11              | -0.6616      | -120.2      | 6.00         | -5       | 0.68         |
| NNI9210            | NNI9040            | 15           | 279         | 16         | 17           | -2.88          | -3.30              | 0.0015       | 1.6         | 1.37         | 85       | 0.57         |
| NNI9220            | NNI9210            | 15           | 459         | 16         | 16           | -2.20          | -2.88              | 0.0015       | 1.6         | 1.37         | 86       | 0.68         |
| NNI9230            | NNI9220            | 15           | 381         | 16         | 16           | -1.63          | -2.20              | 0.0015       | 1.6         | 1.37         | 85       | 0.71         |
| NNI9240            | NNI9230            | 15           | 381         | 16         | 16           | -1.06          | -1.63              | 0.0015       | 1.6         | 0.78         | 48       | 0.71         |
| NNI9250            | NNI9240            | 15           | 180         | 19         | 16           | -0.69          | -0.96              | 0.0015       | 1.6         | 0.78         | 48       | 0.44         |
| NNI9260            | NNI9250            | 15           | 331         | 20         | 19           | -0.20          | -0.69              | 0.0015       | 1.6         | 0.78         | 49       | 0.49         |
| NNI910             | NNI9260            | 12           | 591         | 20         | 20           | 1.22           | -0.20              | 0.0024       | 1.1         | 0.78         | 68       | 0.62         |
| NNIO10             | NNIPS1             | 27           | 1129        | 10         | 12           | -9.61          | -10.96             | 0.0012       | 6.9         | 6.05         | 87       | 0.70         |
| NNI020             | NNI010             | 27           | 699         | 10         | 10           | -8.77          | -9.61              | 0.0012       | 7.0         | 5.73         | 82       | 0.72         |
| NNJ9210            | NNI020             | 18           | 200         | 19         | 10           | -0.60          | -0.92              | 0.0016       | 2.7         | 1.73         | 64       | 0.42         |
| NNJ9220            | NNJ9210            | 18           | 69          | 19         | 19           | -0.49          | -0.60              | 0.0016       | 2.7         | 1.73         | 63       | 0.56         |
| NNJ9230            | NNJ9220            | 18           | 390         | 14         | 19           | 0.13           | -0.49              | 0.0016       | 2.7         | 1.73         | 64       | 0.57         |
| NNJ9240            | NNJ9230            | 18           | 341         | 15         | 14           | 0.67           | 0.13               | 0.0016       | 2.7         | 1.73         | 64       | 0.58         |
| NNJ110             | NNJ9240            | 18           | 1260        | 11         | 15           | 2.69           | 0.67               | 0.0016       | 2.7         | 1.73         | 64       | 0.58         |
| NNJ120             | NNJ110             | 18           | 1201        | 13         | 11           | 4.61           | 2.69               | 0.0016       | 2.7         | 1.73         | 64       | 0.58         |
| NNJ130             | NNJ120             | 10           | 1381        | 11         | 13           | 10.10          | 5.27               | 0,0035       | 0.8         | 0.41         | 49       | 0.43         |
| NNJ140             | NNJ130             | 10           | 679         | 15         | 11           | 12.48          | 10.10              | 0.0035       | 0.8         | 0.41         | 49       | 0.50         |
| NNI030             | NNI020             | 24           | 1030        | 10         | 10           | -7.28          | -8.52              | 0.0012       | 5.1         | 3.77         | 74       | 0.67         |
| NNI040             | NNI030             | 24           | 951         | 10         | 10           | -6,14          | -7,28              | 0.0012       | 5.1         | 3.58         | 71       | 0.64         |
| NNJ910<br>NNI050   | NNI040<br>NNI040   | 10<br>21     | 322<br>1801 | 11<br>10   | 10<br>10     | -2.35<br>-3.55 | -3,48<br>-5.89     | 0.0035       | 0.8<br>3.7  | 0.37         | 43       | 0.40         |
| NNJ210             | NNI040             | 15           | 2090        | 11         | 10           | 0.92           | -3.05              | 0.0013       | 1.8         | 2.69         | 73<br>74 | 0.58         |
| NNJ220             | NNJ210             | 15           | 971         | 11         | 11           | 2.76           | 0.92               | 0.0019       | 1.8         | 1.35         | 74       | 0.50         |
| NNJ230             | NNJ220             | 10           | 761         | 11         | 11           | 5.84           | 3.18               | 0.0019       | 0.8         | 1.35<br>0.46 | 54       | 0.64<br>0.46 |
| NNJ240             | NNJ230             | 10           | 699         | 25         | 11           | 8.29           | 5.84               | 0.0035       | 0.8         | 0.46         | 54       | 0.46         |
| NNI060             | NNI050             | 15           | 322         | 10         | 10           | -2.43          | -3.05              | 0.0033       | 1.8         | 1.37         | 75       | 0.50         |
| NNI070             | NNI060             | 15           | 1181        | 10         | 10           | -0.18          | -2.43              | 0.0019       | 1.8         | 1.05         | 57       | 0.64         |
|                    |                    |              |             |            | - ' '        |                | *******            | 3.00.13      |             | 1,00         |          | - 0.04       |
| Note: Pipes        | with peak fl       | ow less than | 1 1 mod are | considered | local collec | ctors and a    | re labeled "       | LC" on the f | runk shed r | naps.        |          |              |
|                    | <u></u>            |              |             |            |              |                |                    |              |             |              |          |              |

Trunk NNI

Trunk NNJ

| TRUNK SEWER SYSTEM PROJECT DESCRIPTION             |   |  |  |  |  |  |  |
|--|---|--|--|--|--|--|--|
| PROJECT ID:  | NNH TRUNK SHED NN Natomas North   |  |  |  |  |  |  |
| LOCATION:  | South of Elkhorn Boulevard and east of interstate 5. Connects to North Watomas Interceptor at MH NN1080.      |  |  |  |  |  |  |
| BRIEF PROJECT DESCRIPTION:                         | . 1,650 feet of 12" and 15" pipe  |  |  |  |  |  |  |
| MODEL REFERENCE:                                   | NNH320 to NN1080  |  |  |  |  |  |  |
| LOCATION OF CAPACITY DEFICIENCY:                   | .,N/A   |  |  |  |  |  |  |
| REASON FOR PROJECT:                                | Expansion for future development (Schumacher)   |  |  |  |  |  |  |
| DESIGN FLOW:                                       | 1.0 mgd (upstream) to 1.26 mgd (downstream)   |  |  |  |  |  |  |
| PERCENT FOR EXISTING FLOW:PERCENT FOR FUTURE FLOW: |   |  |  |  |  |  |  |
| SPECIAL CONSIDERATIONS:                            | Project requires the North Natomas Interceptor.   |  |  |  |  |  |  |
| ASSUMPTIONS:                                       | Assumes easements granted by developer and interceptor/trunk junction structure constructed with interceptor. |  |  |  |  |  |  |
| ALTERNATIVES:                                      | . Pipeline location could be modified to accommodate development patterns.                                    |  |  |  |  |  |  |

| MAJOR ITEMS   | DIA. (in.) | DEPTH<br>(feet) | LENGTH<br>(feet) | UNIT COST        | COST      |
|---|------------|-----------------|------------------|------------------|-----------|
| Baseline Pipe Construction Cost                         |            |                 |                  |                  |           |
| NNH320 to NNH310  | 12         | 16-20           | 990'             | 120 \$/ft        | \$118,800 |
| NNH310 to NN1080  | 15         | 16-20           | 660'             | 130 \$/ft        | \$85,800  |
| Geotechnical Factors                                    |            |                 |                  |                  |           |
| Increased Dewatering                                    |            |                 | 1,650'           | 53 \$/ft         | \$87,450  |
| Increased Sheeting/Shoring Partially Laid Back Trench   |            |                 | 1,650'           | 40 <b>\$</b> /ft | \$66,000  |
| Traffic and Productivity Factors                        |            |                 |                  |                  |           |
| Surface Restoration                                     |            |                 |                  |                  |           |
| Structures, Pits, and Pump Stations                     |            |                 |                  |                  |           |
| Subtotal  |            |                 |                  | -                | \$358,050 |
| Mobilization and Demobilization                         |            |                 |                  | 5%               | \$17,903  |
| Construction Cost Subtotal                              |            |                 |                  |                  | \$375,953 |
| Contingencies for Unknown Subsurface Conditions         | s          |                 |                  | 30%              | \$112,786 |
| Construction Cost Total                                 |            |                 |                  |                  | \$488,738 |
| Engineering, Administration, and Legal Costs            |            |                 |                  | 25%              | \$122,185 |
| Capital Improvement Cost Total                          |            |                 |                  |                  | \$610,923 |
| ENR =6474 (Average of S.F. and 20 Cities, January 2000) |            |                 |                  | rounded          | \$611,000 |

| TRUNK SEWER SYSTEM PROJECT DESCRIPTION             |   |  |  |  |  |  |  |
|--|---|--|--|--|--|--|--|
| PROJECT ID:  | NNI TRUNK SHED NN Natomas North   |  |  |  |  |  |  |
| LOCATION:  | South of Elkhorn Boulevard and west of the East Drainage Canal. Connects to existing trunk at MH NNI9110.   |  |  |  |  |  |  |
| BRIEF PROJECT DESCRIPTION:                         | 7,300 feet of 15" to 27" pipe and 6.5 mgd pump station  |  |  |  |  |  |  |
| MODEL REFERENCE:                                   | NNI070 to NNI9110   |  |  |  |  |  |  |
| LOCATION OF CAPACITY DEFICIENCY:                   | N/A   |  |  |  |  |  |  |
| REASON FOR PROJECT:                                | Expansion for future development (Northborough)   |  |  |  |  |  |  |
| DESIGN FLOW:                                       | .1.05 mgd (upstream) to 6.0 mgd (downstream)  |  |  |  |  |  |  |
| PERCENT FOR EXISTING FLOW:PERCENT FOR FUTURE FLOW: | 0%<br>100%  |  |  |  |  |  |  |
| SPECIAL CONSIDERATIONS:                            | The flow from the east side of the canal provides the initial start-up flow for the North Natomas Interceptor and maintains cleaning velocities. The NNI trunk should be designed at a depth that enables trunks from east side of the Main Drainage Canal to connect and maintain clearance under the canal and the Upper Northwest Interceptor. |  |  |  |  |  |  |
| ASSUMPTIONS:                                       | Assumes easements granted by developer and trunk junction structure constructed with existing trunk.  |  |  |  |  |  |  |
| ALTERNATIVES:                                      | Pipeline location could be modified to accommodate development patterns.  |  |  |  |  |  |  |

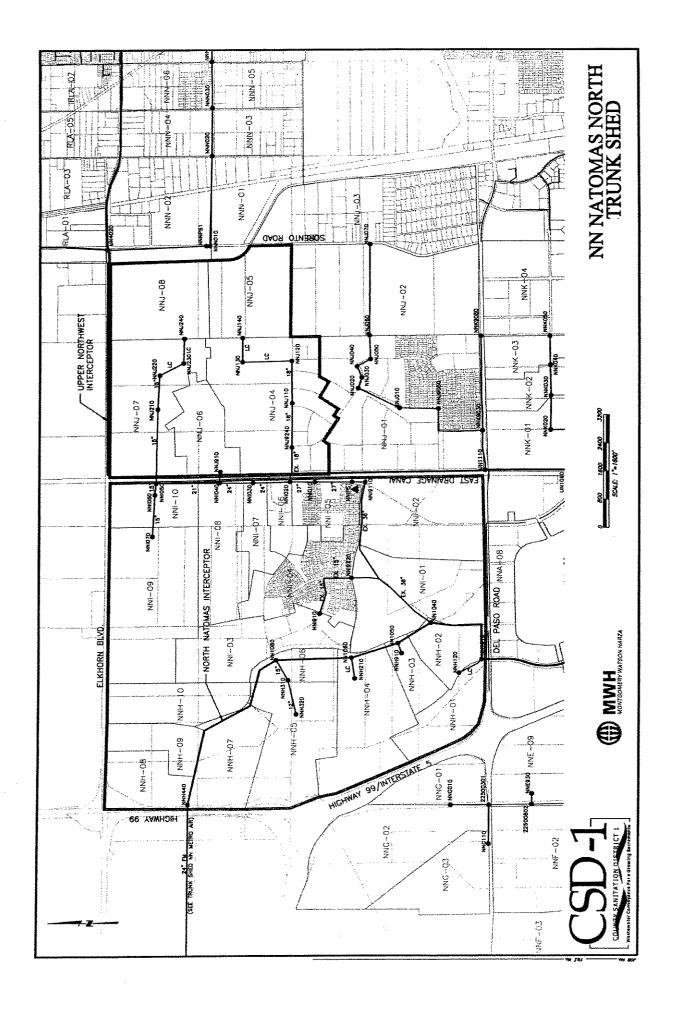
| MAJOR ITEMS   | DIA. (in.) | DEPTH<br>(feet) | LENGTH<br>(feet) | UNIT COST | cost                  |
|---|------------|-----------------|------------------|-----------|-----------------------|
| Baseline Pipe Construction Cost   |            |                 |                  |           |                       |
| NNI070 to NNI060  | 15         | 8-16            | 1,180'           | 110 \$/ft | \$129,800             |
| NN1060 to NN1050  | 15         | 8-16            | 320'             | 110 \$/ft | \$35,200              |
| NNI050 to NNI040  | 21         | 8-16            | 1,800'           | 140 \$/ft | \$252,000             |
| NNI040 to NNI030  | 24         | 8-16            | 950'             | 160 \$/ft | \$152,000             |
| NN1030 to NN1020  | 24         | 16-20           | 1,030'           | 185 \$/ft | \$190,550             |
| NNI020 to NNI010  | 27         | 16-20           | 700'             | 210 \$/ft | \$147,000             |
| NNI010 to NNIPS1  | 27         | 20-24           | 1,130'           | 240 \$/ft | \$271,200             |
| NNIPS1 to NNI9110   | 27         | 20-24           | 194'             | 240 \$/ft | \$46,560              |
| Geotechnical Factors Increased Dewatering   | •          |                 | 7,304            | 53 \$/ft  | \$387,112             |
| Increased Sheeting/Shoring Partially Laid Back Trench   |            |                 | 7,304'           | 40 \$/ft  | \$292,160             |
| Traffic and Productivity Factors  |            |                 |                  |           |                       |
| Surface Restoration   |            |                 |                  |           |                       |
| Structures, Pits, and Pump Stations 2-Trunk Junction Structure (24- to 36-inch dia out Pump Station - 6.5 mgd | tlet pipe) |                 |                  |           | \$16,000<br>\$865,000 |
| Subtotal  |            |                 |                  | •         | \$2,784,582           |
| Mobilization and Demobilization   |            |                 |                  | 5%        | \$139,229             |
| Construction Cost Subtotal  |            |                 |                  |           | \$2,923,811           |
| Contingencies for Unknown Subsurface Condition  | าร         |                 |                  | 30%       | \$877,143             |
| Construction Cost Total   |            |                 |                  |           | \$3,800,954           |
| Engineering, Administration, and Legal Costs  |            |                 |                  | 25%       | \$950,239             |
| Capital Improvement Cost Total  |            |                 |                  |           | <b>\$</b> 4,751,193   |
| ENR = 6474 (Average of S.F. and 20 Cities, January 2000)  |            |                 |                  | rounded   | \$4,751,000           |

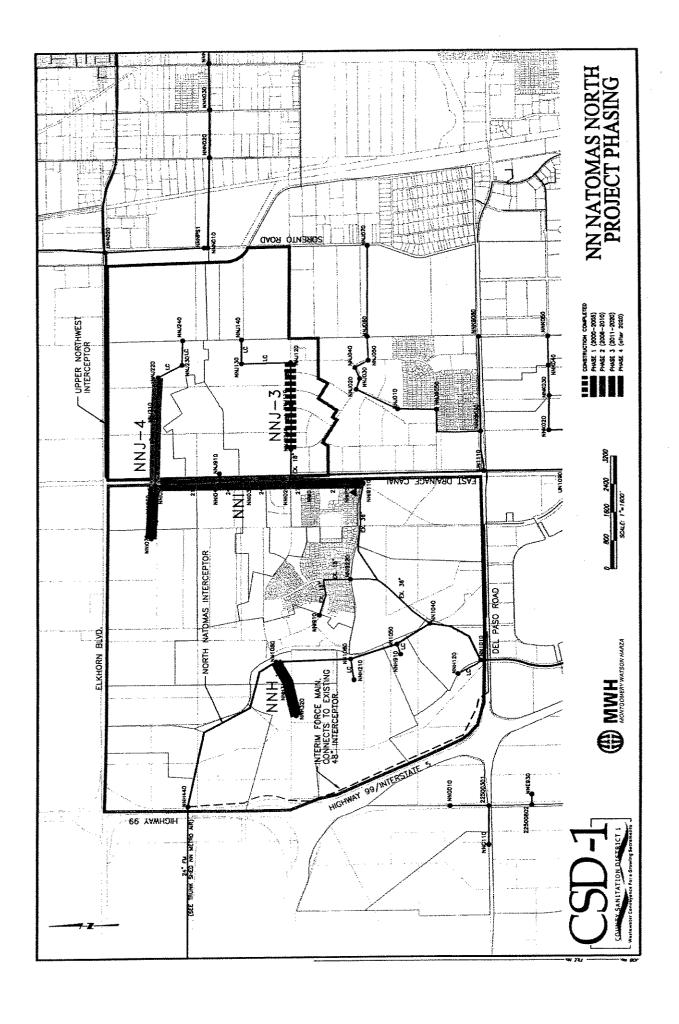
| TRUNK SEWER SYSTEM PROJECT DESCRIPTION                             |   |  |                                    |     |  |  |  |
|--|---|--|------------------------------------|-----|--|--|--|
| PROJECT ID:  | NNJ-3 TR                                | UNK SHED N   | IN Natomas North                   |     |  |  |  |
| LOCATION:  | South of Elkhorn E to existing trunk at | Boulevard and east on the Boulevard and East of the East | of the East Drainage Canal. Connec | ts  |  |  |  |
| BRIEF PROJECT DESCRIPTION:   | 2,450 feet of 18" p                     | ipe  |                                    |     |  |  |  |
| MODEL REFERENCE:   | NNJ120 to NNJ92                         | 40   |                                    |     |  |  |  |
| LOCATION OF CAPACITY DEFICIENCY:                                   | N/A                                     | •  |                                    |     |  |  |  |
| REASON FOR PROJECT:  | Expansion for futu                      | re development (No   | rthpoint)                          |     |  |  |  |
| DESIGN FLOW:  PERCENT FOR EXISTING FLOW:  PERCENT FOR FUTURE FLOW: | 1.73 mgd<br>0%<br>100%                  |  |                                    |     |  |  |  |
| SPECIAL CONSIDERATIONS:  | Project requires Tr                     | runk Project NNI.  |                                    |     |  |  |  |
| ASSUMPTIONS:   | Assumes easemer constructed with ex     | nts granted by devel<br>xisting trunk.   | loper and trunk junction structure |     |  |  |  |
| ALTERNATIVES:  | Pipeline location co                    | ould be modified to  | accommodate development patterns   | i - |  |  |  |

| MAJOR ITEMS  | DIA. (in.) | DEPTH<br>(feet) | LENGTH<br>(feet) | UNIT COST        | COST      |
|--|------------|-----------------|------------------|------------------|-----------|
| Baseline Pipe Construction Cost                          |            |                 |                  |                  |           |
| NNJ120 to NNJ110   | 18         | 8-16            | 1,200'           | 125 \$/ft        | \$150,000 |
| NNJ110 to NNJ9240  | 18         | 8-16            | 1,260'           | 125 \$/ft        | \$157,500 |
| Geotechnical Factors                                     |            |                 |                  |                  |           |
| Increased Dewatering                                     |            |                 | 2,460'           | 53 <b>\$</b> /ft | \$130,380 |
| Increased Sheeting/Shoring                               |            |                 |                  | 00.00            | ***       |
| Partially Laid Back Trench                               |            |                 | 2,460'           | 20 \$/ft         | \$49,200  |
| Traffic and Productivity Factors                         |            |                 |                  |                  |           |
| Surface Restoration                                      |            |                 |                  |                  |           |
| Structures, Pits, and Pump Stations                      |            |                 |                  |                  |           |
| Subtotal   |            |                 |                  | -                | \$487,080 |
| Mobilization and Demobilization                          |            |                 |                  | 5%               | \$24,354  |
| Construction Cost Subtotal                               |            |                 |                  |                  | \$511,434 |
| Contingencies for Unknown Subsurface Conditions          | S          |                 |                  | 30%              | \$153,430 |
| Construction Cost Total                                  |            |                 |                  |                  | \$664,864 |
| Engineering, Administration, and Legal Costs             |            |                 |                  | 25%              | \$166,216 |
| Capital Improvement Cost Total                           |            |                 |                  |                  | \$831,080 |
| ENR = 6474 (Average of S.F. and 20 Cities, January 2000) |            |                 |                  | rounded          | \$831,000 |

| . TRUNK SEWER SYSTEM PROJECT DESCRIPTION               |  |  |  |  |  |  |
|--|--|--|--|--|--|--|
| PROJECT ID:  | NNJ-4 TRUNK SHED NN Natomas North  |  |  |  |  |  |
| LOCATION:  | South of Elkhom Boulevard and east of the East Drainage Canal. Connects to Project NNI at MH NNI050. |  |  |  |  |  |
| BRIEF PROJECT DESCRIPTION:                             | 3,050 feet of 15" pipe   |  |  |  |  |  |
| MODEL REFERENCE:                                       | NNJ220 to NNI050   |  |  |  |  |  |
| LOCATION OF CAPACITY DEFICIENCY:                       | .N/A   |  |  |  |  |  |
| REASON FOR PROJECT:                                    | Expansion for future development (Northpoint)  |  |  |  |  |  |
| DESIGN FLOW:   | 1.35 mgd   |  |  |  |  |  |
| PERCENT FOR EXISTING FLOW:<br>PERCENT FOR FUTURE FLOW: | 0%<br>100%   |  |  |  |  |  |
| SPECIAL CONSIDERATIONS:                                | Project requires Trunk Project NNI-1.  |  |  |  |  |  |
| ASSUMPTIONS:   | Assumes easements granted by developer.  |  |  |  |  |  |
| ALTERNATIVES:  | Pipeline location could be modified to accommodate development patterns.                             |  |  |  |  |  |

| MAJOR ITEMS  | DIA. (in.) | DEPTH<br>(feet) | LENGTH<br>(feet) | UNIT COST        | COST                 |
|--|------------|-----------------|------------------|------------------|----------------------|
| Baseline Pipe Construction Cost                          |            |                 |                  |                  |                      |
| NNJ220 to NNJ210   | 15         | 8-16            | 970'             | 110 \$/ft        | \$106,700            |
| NNJ210 to NNI050   | 15         | 8-16            | 2,090'           | 110 \$/ft        | \$229,900            |
| Channel Crossing (36" casing) Jacking Pit                | 15         | Microtunnel     | 100'             | 800 \$/ft        | \$80,000<br>\$60,000 |
| Receiving Pit  |            |                 |                  |                  | \$35,000             |
| Geotechnical Factors                                     |            |                 |                  | •                |                      |
| Increased Dewatering<br>Increased Sheeting/Shoring       |            |                 | 3,060'           | 53 <b>\$</b> /ft | \$162,180            |
| Partially Laid Back Trench                               |            |                 | 3,060'           | 20,\$/ft         | \$61,200             |
| Traffic and Productivity Factors                         |            |                 |                  |                  |                      |
| Surface Restoration                                      |            |                 |                  |                  |                      |
| Structures, Pits, and Pump Stations                      |            |                 |                  | -                | •                    |
| Subtotal   |            |                 |                  | •                | \$734,980            |
| Mobilization and Demobilization                          |            |                 |                  | 5%               | \$36,749             |
| Construction Cost Subtotal                               |            |                 |                  | •                | \$771,729            |
| Contingencies for Unknown Subsurface Conditions          | 3          |                 |                  | 30%              | \$231,519            |
| Construction Cost Total                                  |            |                 |                  |                  | \$1,003,248          |
| Engineering, Administration, and Legal Costs             | •          |                 |                  | 25%              | \$250,812            |
| Capital Improvement Cost Total                           |            |                 |                  |                  | .\$1,254,060         |
| ENR = 6474 (Average of S.F. and 20 Cities, January 2000) |            |                 |                  | rounded          | \$1,254,000          |





#### CSD-1 SEWERAGE FACILITIES EXPANSION MASTER PLAN

#### NN METRO AIR TRUNK SHED

#### **Area Description**

The NN Metro Air Trunk Shed is located north of Interstate 5 and west of Lone Tree Road. The Trunk Shed includes the Metro Air Park development and the Sacramento International Airport. Metro Air Park is anticipated to start developing within the 2000 to 2005 year time frame. It is anticipated that Sacramento International Airport will cease treating their wastewater on-site and convey wastewater to the CSD-1 system when the Metro Air Park trunk facilities come on line.

#### **Trunk System Facilities**

The trunk shed would be served by a major trunk sewer (Trunk NNM) and a permanent pump station located in the Metro Air Park development. This gravity trunk sewer would discharge to the pump station located in the south portion of the development, and a force main would connect to the future extension of the North Natomas Interceptor at El Centro Road.

If the North Natomas Interceptor extension to El Centro Road is not on line by the time the trunk facilities are constructed to serve this trunk shed, an interim connection could be made extending the force main to the existing upstream end of the North Natomas Interceptor north of Del Paso Road .

#### **Trunk Project**

Three trunk projects are identified for this trunk shed, as shown in the table below.

| Project<br>ID | Diam.<br>(in.)     | Length<br>(ft.) | Phase | Estimated Construction Cost (\$) | Estimated<br>Capital Cost<br>(\$) |
|---------------|--------------------|-----------------|-------|----------------------------------|-----------------------------------|
| NNM-1         | 27-33 &<br>24 (FM) | 2,900           | 1     | 6,665,000                        | 8,973,000                         |
| NNM-2         | 12-24              | 10,500          | 1     | 4,903,000                        | 6,128,000                         |
| NNM-3         | 15-18              | 5,500           | 1     | 2,396,000                        | 2,995,000                         |

#### Attachments

- Trunk shed map showing proposed trunk sewers, sizes, model manhole ID numbers, and sewersheds.
- Project map showing trunk projects and interim facilities (if needed).
- Trunk shed ESD projections by sewershed.
- Sewershed load manholes.
- Trunk sewer data and model results.
- Profile(s) of major trunk sewers.
- Trunk project cost estimates.

NN Metro Air Trunk Shed Buildout Projections

|               |              | ESI         | Ds       |          | Area (acres) |      |      |          |  |
|---------------|--------------|-------------|----------|----------|--------------|------|------|----------|--|
| Sewershed     | 2005         | 2010        | 2020     | Buildout | 2005         | 2010 | 2020 | Buildout |  |
| NNM-01        | 0            | 0           | 0        | 594      | 0            | 0    | 0    | 99       |  |
| NNM-02        | 0            | 0           | 0        | 289      | 0            | 0    | 0    | 48       |  |
| NNM-03        | 0            | 0           | 0        | 171      | 0            | 0    | 0    | 28       |  |
| NNM-04        | 0            | 0           | 0        | 229      | 0            | 0    | 0    | 38       |  |
| NNM-05        | 0            | 0           | 0        | 778      | 0            | 0    | 0    | 130      |  |
| NNM-06        | 0            | 0           | 0        | 584      | 0            | 0    | 0    | 97       |  |
| NNM-07        | 1            | 1           | 1        | 907      | 0            | 0    | 0    | 151      |  |
| NNM-08        | 0            | 0           | 0        | 470      | 0            | 0    | 0    | 78       |  |
| NNM-09        | 0            | 0           | 0        | 796      | 0            | 0    | 0    | 133      |  |
| NNM-10        | 1            | 1           | 1        | 906      | 0            | 0    | 0    | 151      |  |
| NNM-11        | 1            | 1           | 1        | 574      | 0            | 0    | 0    | 96       |  |
| NNM-12        | 2            | 2           | 2        | 1,025    | 0            | 0    | 0    | 171      |  |
| NNM-13        | 1            | 1           | 1        | 1,071    | 0            | 0    | 0    | 179      |  |
| NNM-14        | 2            | 2           | 2        | 728      | 0            | 0    | 0    | 121      |  |
| NNM-15        | 0            | 0           | 0        | 0        | 0            | 0    | 0    | 0        |  |
| Total         | 9            | 9           | 9        | 9,122    | 1            | 1    | 1    | 1,520    |  |
| Note: ESDs re | flect reside | ential deve | elopment | only.    |              |      |      |          |  |

#### Trunk Shed NN Metro Air Sewershed Load Manholes

| Sewershed | Load Manhole |
|-----------|--------------|
|           |              |
| NNM-01    | NNM090       |
| NNM-02    | NNM090       |
| NNM-03    | NNM080       |
| NNM-04    | NNM080       |
| NNM-05    | NNM070       |
| NNM-06    | NNM070       |
| NNM-07    | NNM060       |
| NNM-08    | NNM060       |
| NNM-09    | NNM040       |
| NNM-10    | NNM040       |
| NNM-11    | NNM120       |
| NNM-12    | NNM010       |
| NNM-13    | NNMPS1       |
| NNM-14    | NNM010       |
| NNM-15    | NNM130       |

#### Trunk Shed NN Metro Air Buildout 10-Year Design Storm

| US<br>Manhole | DS<br>Manhole | Dia. (in.) | Length<br>(ft.) | US Rim<br>Elev. | DS Rim<br>Elev. | US Invert<br>Elev. | DS invert<br>Elev. | Slope   | Full Cap.<br>(mgd) | Peak<br>Flow<br>(mgd) | % Full<br>Cap. | DS<br>d/D |
|---------------|---------------|------------|-----------------|-----------------|-----------------|--------------------|--------------------|---------|--------------------|-----------------------|----------------|-----------|
|               |               |            |                 |                 |                 |                    |                    |         |                    |                       |                |           |
| NNMFM1        | NNH440        | 24         | 6414            | 20              | 20              | -27.35             | -2.51              | -0.0039 | -9.1               | 9.79                  | -107           | 1.00      |
| NNM010        | NNMPS1        | 33         | 1601            | 20              | 20              | -15.08             | -17.00             | 0.0012  | 11.8               | 8.35                  | 71             | 0.54      |
| NNM020        | NNM010        | 27         | 1299            | 20              | 20              | -13.02             | -14.58             | 0.0012  | 7.0                | 6.34                  | 91             | 0.49      |
| NNM030        | NNM020        | 24         | 2001            | 20              | 20              | -10.37             | -12.77             | 0.0012  | 5.1                | 4.50                  | 89             | 0.71      |
| NNM040        | NNM030        | 24         | 2402            | 20              | 20              | -7.99              | -10.37             | 0,0010  | 4.6                | 4.50                  | 98             | 0.73      |
| NNM050        | NNM040        | 21         | 1860            | 20              | 20              | -4.82              | -7.24              | 0.0013  | 3.7                | 3.17                  | 86             | 0.50      |
| NNM060        | NNM050        | 21         | 951             | 20              | 20              | -3.58              | -4.82              | 0.0013  | 3.7                | 3,17                  | 86             | 0.72      |
| NNM070        | NNM060        | 18         | 1001            | 20              | 20              | -1.73              | -3.33              | 0.0016  | 2.7                | 2.10                  | 77             | 0.67      |
| NNM080        | NNM070        | 12         | 2349            | 20              | 20              | 4.40               | -1.23              | 0.0024  | 1.1                | 1.03                  | 90             | 0.53      |
| NNM090        | NNM080        | 12         | 1499            | 20              | 20              | 8.00               | 4.40               | 0.0024  | 1.1                | 0.71                  | 62             | 0.76      |
| NNM110        | NNM020        | 18         | 2369            | 20              | 20              | -7.35              | -11.14             | 0.0016  | 2.7                | 1.85                  | 68             | 0.43      |
| NNM120        | NNM110        | 18         | 699             | 20              | 20              | -6.23              | -7.35              | 0.0016  | 2.7                | 1.85                  | 68             | 0.61      |
| NNM130        | NNM120        | 15         | 2500            | 20              | 20              | -1.23              | -5.98              | 0.0019  | 1.8                | 1.39                  | 76             | 0.54      |

Trunk NNM

| TRUNK SEWER SYSTEM PROJECT DESCRIPTION                 |  |  |  |  |  |  |
|--|--|--|--|--|--|--|
| PROJECT ID:  | NNM-1 TRUNK SHED NN Metro Air  |  |  |  |  |  |
| LOCATION:  | North of Interstate 5 and east of Powerline Road. Connects to North Natomas Interceptor at MH NNH440.  |  |  |  |  |  |
| BRIEF PROJECT DESCRIPTION:                             | . 2,900 feet of 27" to 33" pipe and 9.6 mgd pump station   |  |  |  |  |  |
| MODEL REFERENCE:                                       | . NNM020 to NNH440   |  |  |  |  |  |
| LOCATION OF CAPACITY DEFICIENCY:                       | . N/A  |  |  |  |  |  |
| REASON FOR PROJECT:                                    | Expansion for future development (Metro Air Park)  |  |  |  |  |  |
| DESIGN FLOW:   | 6.34 mgd (upstream) to 9.79 mgd (downstream)   |  |  |  |  |  |
| PERCENT FOR EXISTING FLOW:<br>PERCENT FOR FUTURE FLOW: | . 14%<br>86%<br>Project requires the future North Natomas Interceptor. Sewer studies   |  |  |  |  |  |
| SPECIAL CONSIDERATIONS:                                | showed oversized trunks to minimize slope. The CSD-1 Master Plan designed trunks and the slopes consistent with the master plan design criteria.   |  |  |  |  |  |
| ASSUMPTIONS:   | Assumes easements granted by developer with the exception of the area east of the Metro Air Park development (force main alignment). The interceptor/junction structure will be constructed with interceptor. Pipes designed to accommodate existing flow from the Sacramento International Airport. |  |  |  |  |  |
| ALTERNATIVES:  | Pipeline location could be modified to accommodate development patterns.   |  |  |  |  |  |

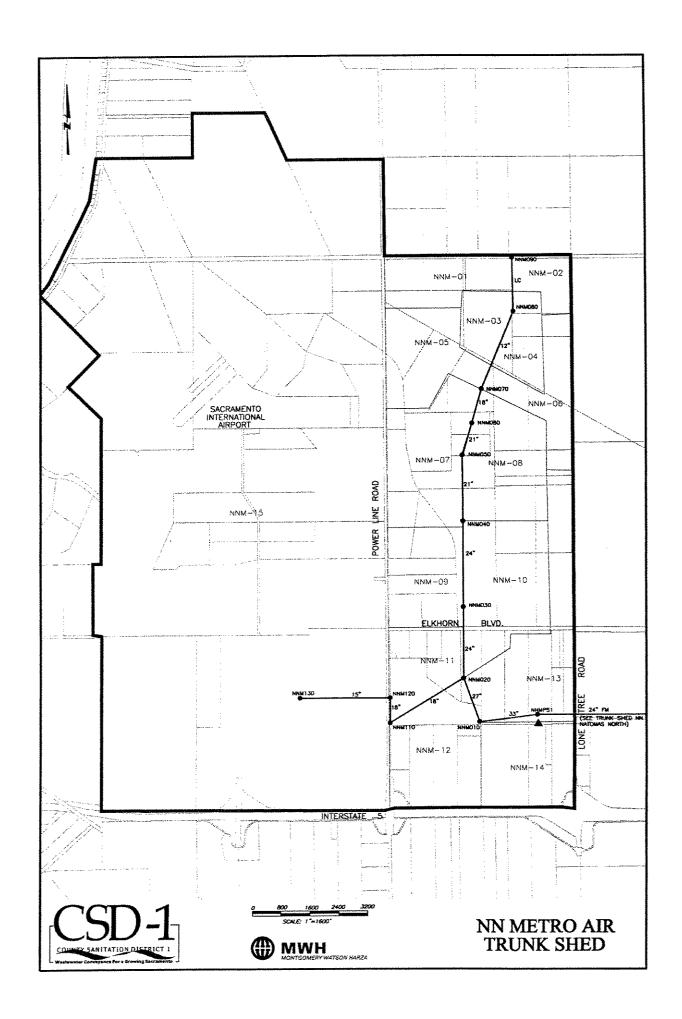
| DIA. (in.) | DEPTH<br>(feet)      | LENGTH<br>(feet)                               | UNIT COST                    | cost                                   |
|------------|----------------------|--|------------------------------|--|
|            |                      |  |                              |  |
|            |                      | • " " "  |                              | \$448,500                              |
|            |                      | •  |                              | \$576,000                              |
|            |                      | *  |                              | \$898,100                              |
| 24         | Microtunnel          | 375'   | 1,040 \$/ft                  | \$390,000                              |
|            |                      |  |                              | \$60,000                               |
|            |                      |  |                              | \$35,000                               |
|            |                      |  |                              |  |
|            |                      | 9,315'   | 53 \$/ft                     | \$493,695                              |
|            |                      | 9,315'   | 80 \$/ft                     | \$745,200                              |
|            |                      |  |                              |  |
|            | 001                  | C 4451   | ስ ጋድ ድር <sub>ተ</sub> ና       | \$128,300                              |
|            | an wide              | 0,410  | 0.25 \$/\$1                  | \$120,300                              |
|            |                      |  |                              | \$1,108,000                            |
|            |                      |  |                              | \$4,882,795                            |
|            |                      |  | 5%                           | \$244,140                              |
|            |                      |  |                              | \$5,126,935                            |
| ns         |                      |  | 30%                          | \$1,538,080                            |
|            |                      |  |                              | \$6,665,015                            |
|            | 80' wide             | 6,415'   | 0.50 \$/sf                   | \$256,600                              |
|            | 30' wide             | 6,415'   | 2 \$/sf                      | \$384,900                              |
|            |                      |  | 25%                          | \$1,666,254                            |
|            |                      |  |                              | \$8,972,769                            |
|            |                      |  | rounded                      | \$8,973,000                            |
|            | 27<br>33<br>24<br>24 | 27 >28 33 >28 24 8-16 24 Microtunnel  80' wide | DIA. (in.) (feet) (feet)  27 | DIA. (in.) (feet) (feet) UNIT COST  27 |

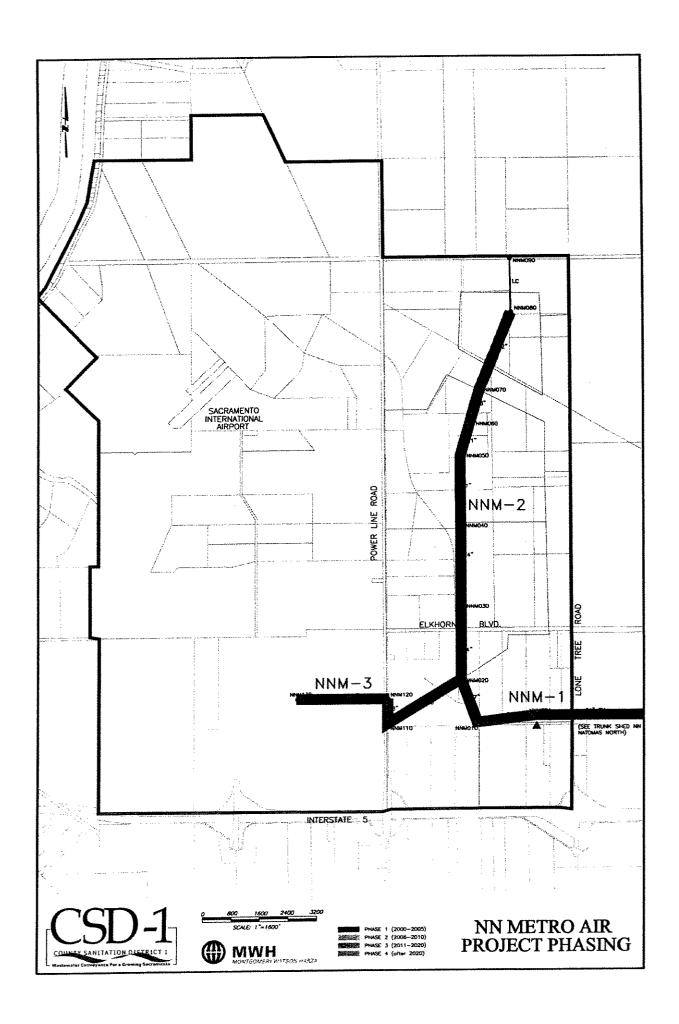
| TRUNK SEWER SYSTEM PROJECT DESCRIPTION                         |  |  |  |  |  |  |  |
|--|--|--|--|--|--|--|--|
| PROJECT ID:  | NNM-2 TRUNK SHED NN Metro Air  |  |  |  |  |  |  |
|  | Next of Internation 5 and cost of Powerline Pond Connects to Project NNM   |  |  |  |  |  |  |
| BRIEF PROJECT DESCRIPTION:                                     | . 10,500 ft of 12 to 24-inch pipe  |  |  |  |  |  |  |
| MODEL REFERENCE:   | NNM080 to NNM020   |  |  |  |  |  |  |
| LOCATION OF CAPACITY DEFICIENCY:                               | N/A  |  |  |  |  |  |  |
| REASON FOR PROJECT:  | Expansion for future development   |  |  |  |  |  |  |
| DESIGN FLOW:PERCENT FOR EXISTING FLOW:PERCENT FOR FUTURE FLOW: |  |  |  |  |  |  |  |
| SPECIAL CONSIDERATIONS:  | Project requires NNM-1 and future North Natomas Interceptor. Sewer         |  |  |  |  |  |  |
| ASSUMPTIONS:   | Assumes easements granted by developer and high groundwater.               |  |  |  |  |  |  |
| ALTERNATIVES:  | . Pipeline location could be modified to accommodate development patterns. |  |  |  |  |  |  |

| MAJOR ITEMS   | DIA. (in.)     | DEPTH<br>(feet) | LENGTH<br>(feet) | UNIT COST | cost        |
|---|----------------|-----------------|------------------|-----------|-------------|
| Baseline Pipe Construction Cost   |                |                 |                  |           |             |
| NNM080 to NNM070  | 12             | 16-20           | 2,350'           | 120 \$/ft | \$282,000   |
| NNM070 to NNM060  | 18             | 20-24           | 1,000'           | 165 \$/ft | \$165,000   |
| NNM060 to NNM050  | 21             | 24-28           | 950'             | 215 \$/ft | \$204,250   |
| NNM050 to NNM040  | 21             | 24-28           | 1,860'           | 215 \$/ft | \$399,900   |
| NNM040 to NNM030  | 24             | 24-28           | 2,400'           | 245 \$/ft | \$588,000   |
| NNM030 to NNM020  | 24             | >28             | 2,000'           | 270 \$/ft | \$540,000   |
| Geotechnical Factors  |                |                 |                  |           |             |
| Increased Dewatering Increased Sheeting/Shoring                                       |                |                 | 10,560'          | 53 \$/ft  | \$559,680   |
| Partially Laid Back Trench  |                |                 | 10,560'          | 80 \$/ft  | \$844,800   |
| Traffic and Productivity Factors  |                |                 |                  |           |             |
| Surface Restoration   |                |                 |                  |           |             |
| Structures, Pits, and Pump Stations Trunk Sewer Junction Structures (24- to 36-inch d | ia. outlet pip | e)              |                  |           | \$8,000     |
| Subtotal  |                |                 |                  | •         | \$3,591,630 |
| Mobilization and Demobilization   |                |                 |                  | 5%        | \$179,582   |
| Construction Cost Subtotal  |                |                 |                  |           | \$3,771,212 |
| Contingencies for Unknown Subsurface Condition  | s              |                 |                  | 30%       | \$1,131,363 |
| Construction Cost Total   |                |                 |                  |           | \$4,902,575 |
| Engineering, Administration, and Legal Costs  |                |                 |                  | 25%       | \$1,225,644 |
| Capital Improvement Cost Total  |                |                 |                  |           | \$6,128,219 |
| ENR = 6474 (Average of S.F. and 20 Cities, January 2000)                              |                |                 |                  | rounded   | \$6,128,000 |

| TRUNK SEWER SYSTEM PROJECT DESCRIPTION  |  |   |  |  |  |  |  |  |  |
|---|--|---|--|--|--|--|--|--|--|
| PROJECT ID:   | NNM-3 T  | RUNK SHED NN Metro Air  |  |  |  |  |  |  |  |
| LOCATION:   | North of Interstat<br>1 at MH NNM020                 | e 5 and east of Powerline Road. Connects to Project NNM-<br>).  |  |  |  |  |  |  |  |
| BRIEF PROJECT DESCRIPTION:  | 5,500 feet of 15*                                    | and 18" pipe  |  |  |  |  |  |  |  |
| MODEL REFERENCE:  | NNM130 to NNM  | 020   |  |  |  |  |  |  |  |
| LOCATION OF CAPACITY DEFICIENCY:  | N/A  |   |  |  |  |  |  |  |  |
| REASON FOR PROJECT:   | Convey Sacrame                                       | ento International Airport flow to CSD-1 system.  |  |  |  |  |  |  |  |
| DESIGN FLOW:  PERCENT FOR EXISTING FLOW:  PERCENT FOR FUTURE FLOW:  SPECIAL CONSIDERATIONS: | 80%<br>20%<br>Project requires I<br>Sewer studies sh | North Natomas Interceptor and Trunk Project NNM-1. Nowed oversized trunks to minimize slope. The CSD-1 gned trunks and the slopes consistent with the master plan |  |  |  |  |  |  |  |
| ASSUMPTIONS:  | Costs assume ea                                      | asements granted by developer.  |  |  |  |  |  |  |  |
| ALTERNATIVES:   | Pipeline location                                    | could be modified to accommodate development patterns.  |  |  |  |  |  |  |  |

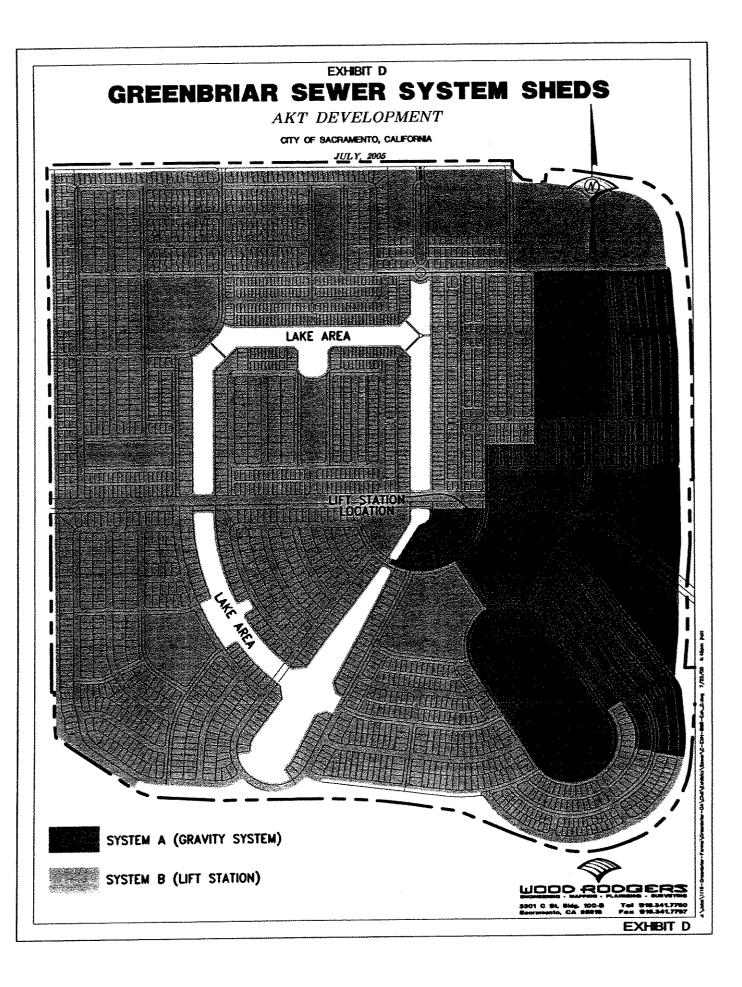
| MAJOR ITEMS  | DIA. (in.) | DEPTH<br>(feet) | LENGTH<br>(feet) | UNIT COST        | COST        |
|--|------------|-----------------|------------------|------------------|-------------|
| Baseline Pipe Construction Cost                          |            |                 |                  |                  |             |
| NNM130 to NNM120   | 15         | 20-24           | 2,500'           | 150 \$/ft        | \$375,000   |
| NNM120 to NNM110   | 18         | 24-28           | 700'             | 185 \$/ft        | \$129,500   |
| NNM110 to NNM020   | 18         | 24-28           | 2,370'           | 185 \$/ft        | \$438,450   |
| Geotechnical Factors                                     |            |                 |                  |                  |             |
| Increased Dewatering                                     |            |                 | 5,573'           | 53 \$/ft         | \$295,369   |
| Increased Sheeting/Shoring                               |            |                 |                  |                  |             |
| Partially Laid Back Trench                               |            |                 | 5,573'           | 80 <b>\$</b> /ft | \$445,840   |
| Traffic and Productivity Factors                         |            |                 |                  |                  |             |
| Surface Restoration                                      |            |                 |                  |                  |             |
| Pavement Restoration                                     |            | 15' wide        | 700'             | 2.00 \$/sf       | \$21,000    |
| Revegetation   |            | 80' wide        | 2,500'           | 0.25 \$/sf       | \$50,000    |
| Structures, Pits, and Pump Stations                      |            |                 |                  |                  |             |
| Subtotal   |            |                 |                  |                  | \$1,755,159 |
| Mobilization and Demobilization                          |            |                 |                  | 5%               | \$87,758    |
| Construction Cost Subtotal                               |            |                 |                  | •                | \$1,842,917 |
| Contingencies for Unknown Subsurface Condition           | s          |                 |                  | 30%              | \$552,875   |
| Construction Cost Total                                  |            |                 |                  |                  | \$2,395,792 |
| Engineering, Administration, and Legal Costs             |            |                 |                  | 25%              | \$598,948   |
| Capital Improvement Cost Total                           |            |                 |                  | ,                | \$2,994,740 |
| ENR = 6474 (Average of S.F. and 20 Cities, January 2000) |            |                 |                  | rounded          | \$2,995,000 |

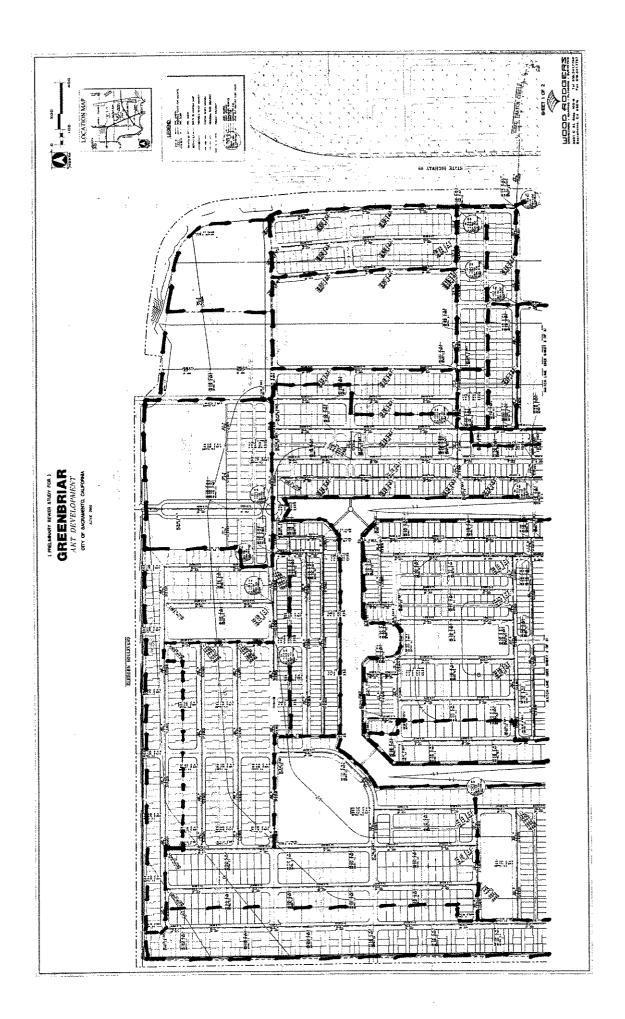


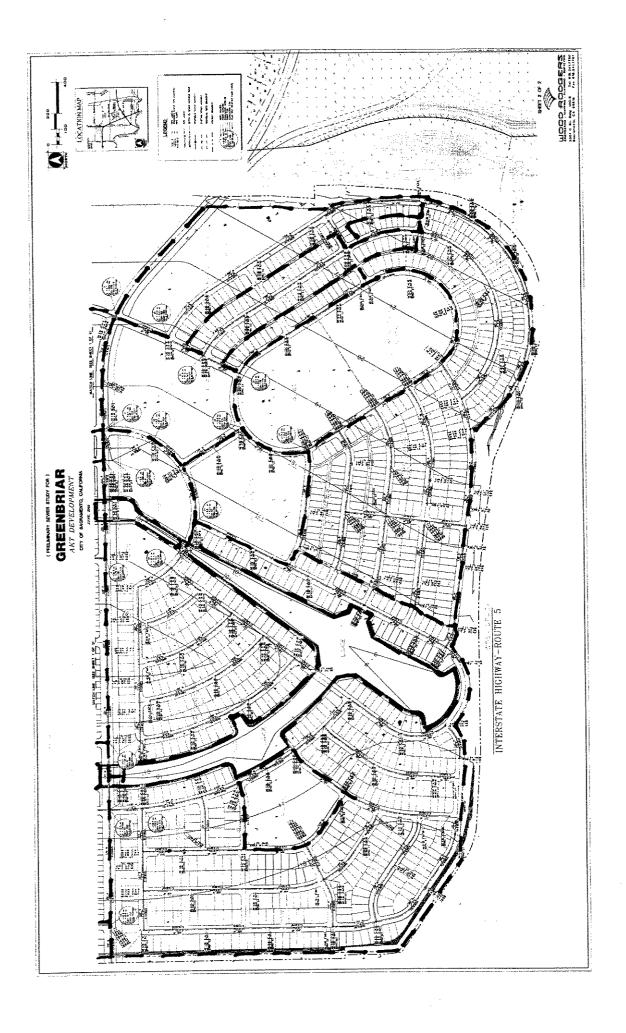




## EXHIBIT D GREENBRIAR SEWER SYSTEM EXHIBITS









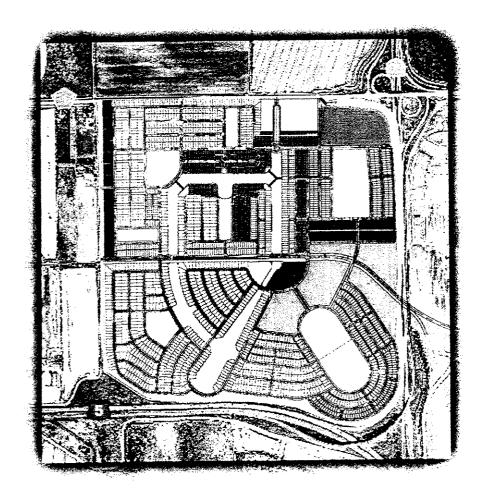
# EXHIBIT E GREENBRIAR SEWER STUDY CALCULATIONS

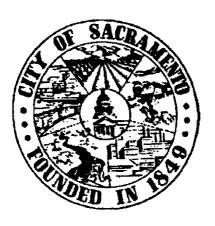
| П                                       | À                     | J   | _        |          | П                                       |         |         |         | П      | J      | _         |         |   |        |   | _                                       |          |   | _                                       |  | _     |         |          | _  |         |         | 1                                       | _             |   |
|---|-----------------------|---|----------|----------|---|---------|---------|---------|--------|--------|-----------|---------|---|--------|---|---|----------|---|---|--|-------|---------|----------|--|---------|---------|---|---------------|---|
| 8                                       | Velocit               |   | 3.5      | 60<br>60 |   | 5 2.2   | 1       | 2.2     | 1,     | 1.9    | _         | 1       | 5 2.2                                   | 2.1    | 2                                       | 5 1.8                                   | 5, 2.0   |   | 5.9                                     |  | 1     | 2       | - 1      |  |         | 2 2.3   | 1 2.4                                   | _             | 1 2.5                                   |
| Pipe Size                               | Slape                 | (FME)   | 0,0035   | 0.0035   | 0.0035                                  | 0.0035  | 0.0025  | 0.002   | 0.0035 | 0.0035 | 0.0035    | 0.0035  | 0.0025                                  | 0.0035 | 0.0025                                  | 0.0035                                  | 0.0035   | 0.0020                                  | 0.0035                                  | 0.0035                                       | 0.003 | 0.0020  | 0.002    | 0.0015   | 0.0012  | 0.0012  | 0.0011                                  | 0.001         | 0.00                                    |
|   | Diameter Slope        | (uj)  | œ        | w        | ĸ                                       | 8       | 10      | 12      | ထ      | æ      | 100       | es)     | 10                                      | 80     | 10                                      | œ                                       | æ        | 15                                      | <b>&amp;</b>                            | 8  | æ     | 12      | 12       | 15   | 5       | KO<br>F | 21                                      | 53            | 51                                      |
| -                                       | J.W.M.d.              | (MGD)   | 0.136    | 0.130    | 0.248                                   | 0.330   | 0.438   | 0.687   | 0.121  | 0.194  | 0.133     | 0.355   | 0.532                                   | 0.240  | 0.429                                   | 0.156                                   | 0.202    | 0.617                                   | 0.185                                   | 0.117  | 0.323 | 0.835   | 0.662    | 0.861  | 2.075   | 2 163   | 2.749                                   | 2.831         | 3.015                                   |
|   | DWF                   |   | 0.106    |          |   |         | 0.352   | Н       |        |        | -         |         | -                                       |        | 0.363                                   | -                                       | -        | -                                       |   | 0.095  | -     | -       | 0.489    | -  | 1812    | -       |   |               | 2.403                                   |
| Flows                                   | Peaking PDWF          |   | -        |          | 893 (                                   | 998.    | 843     | _       |        | 913    | -         |         | -                                       | _      | 1.840                                   | Н                                       | 315      | _                                       | _                                       | .953   |       | ***     | 1.812    | -  | 705     | -       | Т                                       | _             | 667                                     |
|   | P. P.                 |   |          | 0.025    | 0.050                                   | 0.063   | 0.085   | _       | 0.027  |        |           | 0.057   | Ш                                       |        | 0.066                                   | Ш                                       | 0.051    | Ľ                                       | Ľ                                       | 0.022  |       |         |          | 0.207  | 0.483   | 0.470   |   | Ц             | 0.812                                   |
|   | Oave                  |   | 0.055 0  | 0.054 0  | 0.104 0                                 | 0.144.0 | 0.191 0 | 0.303 0 | 0.048  |        | 0.053   0 | 0.180 0 | 0.250 0                                 |        | 0.197 0                                 |   | 0.078 0  | 0.276 0                                 | 0.065 0                                 | 0.049 0                                      | _     |         | 0.275 0  | 0.366 0  | 0.945 0 |         |   | .352 0        | 2.                                      |
| -                                       |                       |   | 1762   0 |          | 1                                       | Н       | 615,4 0 | H       | -      | 261 0  |           |         |   |        | 636.1                                   |   | <b>-</b> | H                                       | Т                                       | 156.8  | -     | 850.4 ( |          | 1179.4   | 3049.2  | -       | 4217.5                                  | _             | 4649.9                                  |
|   | S Cum                 | E   | -3       |          | 33                                      | Ť       | 9       | 63      | 7      | 5      | 11        | 51      | 8                                       | 31     | 63                                      | 19                                      | 25       | 88                                      | 20                                      | 15   | .4    | 85      | 88       | =  | 30      | 32      | 42                                      | 43            | 48                                      |
| Areas                                   | Cumulative Cumulative | Area  | 24.5     | 21       | 43.4                                    | 52.1    | 7.07    | 116.6   | 22.4   | 32.8   | 25.7      | 47.8    | 64.4                                    | 44.3   | 9                                       | 32.4                                    | 42.2     | 97.1                                    | 32.8                                    | 82   | 68.9  | 8       | 136.2    | 172.5  | 3862    | 391.6   | 465.1                                   | 474.4         | 510                                     |
|   | Total 10              |   | 176.2    | 174      | 160.6                                   | 128.4   | 152.4   | 187.3   | 156    | 105    | 170.1     | 247.1   | 288.9                                   | 318.3  | 318                                     | 194.4                                   | 60.4     | 0                                       | 209.8                                   | 156.8  | 4:3.4 | 70.4    | 37.2     | 291.8  | 0       | 162     | 2002                                    | 344.4         | 27                                      |
|   | Logar                 | Area  | 24.5     | 21       | ŧ                                       | 10.7    | ـــ     |         | 22.4   | 10.5   | 125.7     | L_      | 16.8                                    | £      | 10.6                                    | 32.4                                    | 8.8      | 0                                       | 32.8                                    | <u>.                                    </u> |       | 10.3    | L        | 36.3   | 0       | 5.4     | ٠                                       | 8.3           | 2.7                                     |
|   | -                     | te ESD  | -        | _        | L                                       | -       | -       | L       | _      | -      | _         | _       |   | _      | _                                       | L                                       | -        |   | -                                       | -  | L     | L       | _        | L  | L       |         | -                                       |               |   |
|   | -                     | ESD's Offsite ESD                             | -        | L        | 24.6                                    |         | -       | -       | 102    | L      | 40        | -       | L                                       | -      |   | L                                       | -        | l                                       | 49.2                                    |  | 41.4  | 8.      | 9        | 26.4   | L       | -       | L                                       | -             | _                                       |
|   | L                     |   | -        | _        | 4.1 24                                  |         | -       |         | 12     | -      | 11.3 67.  | _       |   |        |   | 3.5 21                                  | -        | -                                       | 8.2 45                                  | ₽  | 8.8   | 4.1 24  | 0.8      | 4.4 26   | -       | -       | -                                       | -             | -                                       |
|   | -                     | ESD's Park                                    | -        | -        | Ť                                       | r       | l       | -       |        | -      | -         | -       | -                                       |        |   |   | r        | İ                                       |   | T  | Ī     | _       | <u> </u> |  | l       | -       | -                                       |               | -                                       |
|   |                       | WOP   |          |          |   |         |         |         |        |        |           |         |   |        |   |   |          |   |   |  |       |         |          |  |         |         |   |               |   |
|   |                       | ESD's   | 103.2    |          | L                                       | L       | 70.8    |         |        |        | L         | L       |   | L      |   |   |          | _                                       | L                                       |  |       | L       | L        |  |         |         |   | L             | L                                       |
|   | -                     | School ESD's Commercial ESD's WCP             | 17.2     | -        | *************************************** |         | 118     |         |        |        |           |         | *************************************** |        | *************************************** |   |          | *************************************** | *************************************** | ***************************************      |       |         |          | ***************************************  |         |         |   |               | *************************************** |
|   |                       | ESD's   |          | I        |   |         |         |         |        |        | 80.6      |         |   |        |   |   |          | I                                       |   |  |       |         |          | I  |         |         |   |               |   |
|   | 1                     | School  |          | L        |   |         |         |         |        |        | 11.3      |         |   |        |   |   |          |   |   | L  |       |         | L        | L  |         | -       |   |               | L                                       |
|   |                       | ESD's   |          | ļ        | L                                       | ļ       | L       | L       |        |        |           | ļ.      | L                                       |        | 318                                     | ļ.                                      | L        | -                                       |   | -  | -     |         | L        | ļ  | ļ       | 182     | ╀                                       |               | -                                       |
| Re Area (AC)                            |                       | ESD's RD-30                                   | L        | -        | ļ                                       | ŀ       | -       |         | -      | -      | L         | 77      |   |        | 10.8                                    | l                                       | L        | -                                       |   | -  | ļ     | -       | -        | -  | ŀ       | 54      | 1                                       | 1 60          |   |
| 1-                                      | , [-                  |   |          | -        | -                                       | ŀ       | 1       | -       | -      | L      | -         | 7 979 4 | +                                       | ļ-     | l                                       | -                                       | ŀ        | ļ                                       | +                                       | -  | ļ     | -       | ļ        | -  | -       | -       | t                                       | 88            | †-                                      |
| l and                                   | 1                     | ESD's RD-22                                   | -        | a.       | 16.9                                    | 128 4   | 81.8    | -       | -      |        | -         | 13      | -                                       | -      | +                                       |   | +        | -                                       | 4.5                                     | -  | -     |         |          | 5K 4   | +       | +       | ٥                                       | 4.4           | 1                                       |
|   | -                     | 2-12 ES                                       |          | 1        | +                                       | +       | R R     | ╀       | H      |        | -         | l       | 1                                       | l      | +                                       | -                                       | ŀ        | -                                       | -                                       | -  | -     | ╁       | +        | 47   | ╁       | ╁       | +                                       | H             | -                                       |
|   | -                     | ESD's RD-8 ESD's RD-9 ESD's RD-10 ESD's RD-12 | 7.2      | ╀        | t                                       | ľ       |         | 4.8     | 54     | 90     | -         | :       | 23                                      | 85     | +                                       | +                                       | l        | +                                       | +                                       | 425  | +     | t       | -        | t  | +       | +       | $\dagger$                               | *             | 22                                      |
|   | ŀ                     | D-10 E  | 7.3      |          | t                                       | t       | T       | 4.8     | 4      | 10.5   |           | -       | ,                                       | 8.5    | l                                       | -                                       | t        | Ť                                       | -                                       | 133  | +     | t       | +        | t  | -       | T       | t                                       | 16.           | -                                       |
|   | ľ                     | ESO'S   | T        | T        | Ť                                       | T       | T       | 58.5    | t      |        | l         |         | T                                       | T      | T                                       |   | T        |   | -                                       |  | İ     |         | Ī        | 45   |         | T       | T                                       | 128           | -                                       |
| *************************************** |                       | 80.9  |          |          |   |         | 1       | 8.5     | +      |        | L         | 1       | 1                                       |        | ļ                                       | 1                                       |          |   | 1                                       | 1  | ]     | L       | 1        | 4  | ,       |         | Ţ                                       | 7             | -                                       |
| *************************************** |                       | 8 ESD's                                       |          | 125      | 1.                                      |         |         | 1 80 8  | L      | L      |           | -       | L                                       | -      | -                                       | *************************************** | ļ        |   | 30                                      | 1  | -     | 34.4    | 4        | 4 499 9  |         | -       | 1                                       | 1             |   |
| *************************************** | 1                     | D's RD.                                       | -        | 105      | 14.9                                    |         | 1       | 101     |        | -      | _         | 1       | 95.9                                    | 8.1    | -                                       | 1                                       | 11.9     | -                                       | 2.5                                     | 1  | ł     | 4       | -        | 15.4   | -       | +       | +                                       | $\frac{1}{1}$ | +                                       |
|   | -                     | D-7 ES  |          |          | -                                       | ł       | +       | 1       | +      | -      | 3 1 21    | ╌       | 3.7                                     | +-     | 1_                                      | -                                       | 4 8      | ٠                                       | -                                       | +  | 1     | ŀ       | -        | -  | +       | -       |   | ł             | ł                                       |
| *************************************** | -                     | ESD's RD-7                                    |          | -        | +                                       | ľ       | t       | T       | t      | T      | t         | †       | T                                       | 105    | ╁┈                                      | 173 A                                   | t        | -f                                      | 120 A                                   | 2.6 A  | 1     | -       | 21 2     | 1 1 1  |         | t       | t                                       | T             | T                                       |
| *************************************** | f                     | RD-6  |          |          | +                                       |         | T       | T       | T      |        | T         | Ī       | T                                       | 17.5   |   | ·-                                      | 2        | ,                                       | 30.4                                    | 8 5  | 3     | 6       | 5,5      | 2 4  | ;       |         |   | Ī             | T                                       |
| 200000                                  | Dougharten            | Node  | 50       | 23       | 63                                      | 1.5     | 55      | 5       | 40     |        | 34        | 30      |   | 23     | 30                                      | 24                                      | 30       | 2                                       |   |  | , 00  | 7       |          | 5  | Y       | -       | 6                                       | -             | Tomk                                    |
| Alode                                   | Ī                     | Dostream Node                                 | RO       |          | 5 4                                     | 62      | K1      | 105     | 4.5    | 40     | 32        | 16      | 30                                      | 24     | 23                                      |   | 16       | 20                                      | -                                       | 10   | -     | R       | -        | A Company of the Comp |         |         | *************************************** | +             | +                                       |

GREENBRIAR 1116.003



# Greenbriar Master Drainage Study





July2005

Prepared by

DEVELOPING INNOVATIVE DESIGN SOLUTIONS

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### **EXECUTIVE SUMMARY**

Greenbriar is a proposed residential development of approximately 577 acres located in the County of Sacramento, California. The project has initiated the application process into the City of Sacramento.

The purpose of this report is to present the design of required on-site and offsite drainage facilities.

The proposed development will require an on-site detention basin, outfall structure and gravity storm drain systems which will mitigate the outfall runoff to the existing RD1000 system at a peak discharge value set by RD1000 at 0.1 cfs/acre.



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#### 1. INTRODUCTION

#### 1.1 OVERVIEW

Greenbriar is a proposed mix-use development of approximately 577 acres located in the County of Sacramento, California. There are approximately an additional 50 acres of offsite freeway drainage area draining into the site under existing conditions. The site is bordered by Elkhorn Blvd. along the north boundary, the future Metro Air Park on the west boundary, Interstate-5 along the south, and Highway 99 to the east. See **FIGURES 1**, 2, and 3 for the vicinity map, site plan, and the proposed land use plan.

#### 1.2 PURPOSE

This Drainage Study analyzes drainage systems in pre-development conditions and documents the design of the post-development onsite storm drainage system, detention basin, and outfall structure to mitigate storm runoff in post-development conditions.

#### 1.3 PREVIOUS STUDIES

The 2002 Final Metro Air Park Master Drainage Study, prepared by Watermark Engineering, was developed to address drainage associated with the future Metro Airport Park project west of Greenbriar.

The Metro Air Park Off-Site Drainage Improvements Plans by Stantec (formerly known as The Spink Corporation) were developed to improve the drainage facilities from the proposed Metro Air Park pump station outfall to the West Drainage Canal. The data from the improved channel and Interstate 5 crossing was used to analyze the developed Greenbriar downstream condition.

#### 1.4 EXISTING CONDITIONS

The existing site is flat and used for agriculture. The drainage on the site consists of several drainage/irrigations ditches which ultimately convey flows south. The site slopes from westward and southward. Elevations range from approximately 5 to 25 feet mean sea level (MSL).

The existing project site consists of two major watersheds. A narrow eastern shed drains into the existing Natomas Mutual channel, under Highway 99, then southward towards the West Drainage Canal. The western part of the site drains into the Lone Tree Canal, joins runoff from the southern part of the site, and flows under Interstate-5 through three existing 5-ft by 8-ft box culverts towards the West Drainage Canal. The West Drainage Canal drains south and terminates in the Natomas Main Drainage Channel, which is pumped into the Sacramento River.

#### 1.5 FEMA INFORMATION

The most recent Federal Emergency Management Agency's (FEMA) Flood Insurance Study (FIS) Flood Insurance Rate Maps (FIRMs), revised July 06, 1998, shows the site in Zone X, which is designated as outside of a special flood hazard zone. The Flood Insurance Rate Map is displayed in **FIGURE** 

#### 1.6 SOILS INFORMATION

Based on the Soil Survey of Sacramento County, the Greenbriar watershed consists primarily of soil classified by the Natural Resources Conservation Service (NRCS) as Hydrologic Soil Group "D". Type "D" soil generally has a high runoff rate and low infiltration rate. (See FIGURE 5)

#### 1.7 PROPOSED CONDITIONS ONSITE GRADING

It is intended that the proposed development will not be required to import fill. Earthwork cut and fill volumes were balanced onsite using an Autocad Digital Terrain Model. The model included a soil shrinkage factor of 0.85 to depict the potential shrinkage when the excavated soil is spread and compacted over the site.

#### 1.8 CRITERIA AND METHODOLOGY

#### 1.8.a Existing Conditions

Under Existing Conditions, the 100-year and 10-year storms with 10-day and 24-hour durations were examined. These storms utilized the historic West Drain Canal 100-year 10-day stage hydrograph provided by RD1000 as the downstream boundary condition in the southerly RD1000 Canal. With the Greenbriar site's peak flow discharging into the channel much earlier than the channel's peak flow, the assumption of using the first 24 hours of the 10-day stage hydrograph as the 24-hour storm's boundary condition is conservative. Hydrographs were developed using SACCALC software as documented in the City of Sacramento Drainage Manual, Volume 2 Hydrology Standards (City of Sacramento Standards).

Hydrographs at outlets and places of interest were developed to depict the existing condition. However, no hydraulic model was developed under this condition as there are no significant drainage facilities present at the site.

#### 1.8.b Ultimate Conditions

100-year and 10-year storm hydrographs with 10-day and 24-hour durations were developed for this study reflecting Ultimate Conditions. Hydrology was computed using SACCALC as documented in the City of Sacramento Hydrology Standards.

The 10-year storm was used to analyze the onsite pipe drainage system while the 100-year storm was used to size the detention pond and outfall structure.

To determine detention storage and system outflow, the system was analyzed using an unsteady HEC-RAS model per City of Sacramento Standards. SACCALC output hydrographs were used as input hydrographs in the HEC-RAS model. The outfall structure was modeled such that the peak outflow from the site would be lower than 0.1 cfs per acre or total of 62cfs (set forth by RD1000). The maximum pond water surface was designed to have one foot of freeboard to the top of the pond.

A preliminary on-site storm drain trunk system was designed according to City of Sacramento standards using the Sacramento method for quantifying 10-year peak runoff and hydraulic grade lines. Only major trunk systems



were analyzed and those pipes were designed based on the proposed grading pad and minimum pipe velocity. For the downstream end boundary condition, the 10-year peak stage in the pond from the HEC-RAS model was used.

#### 2. ANALYSIS AND RESULTS

#### 2.1 ANALYSIS OF EXISTING CONDITIONS

The drainage pattern of Greenbriar and its adjacent properties are illustrated in FIGURE 6. Part of the existing drainage area as reported in the "Metro Air Park Master Drainage Study," 2002, prepared by Watermark Engineering, are included. Aerial photographs and topographic maps were utilized to determine the drainage trends of the project site and its surroundings. A site visit determined the approximate size of drainage features.

FIGURE 7 shows the results of the Existing Conditions analysis of the project site. The Existing Conditions SACCALC peak flow is summarized in Table 1.

| TABLE 1. Existing Conditions 100-Year Po | eak Flow |
|--|----------|
|--|----------|

| Subbasin                                    | Area<br>(ac) | *100yr-10day<br>Peak Flow<br>(cfs) | *100yr-24hr<br>Peak Flow<br>(cfs) |
|---|--------------|------------------------------------|-----------------------------------|
| East Basin – E1                             | 448          | 199                                | 307                               |
| West Basin – E2 (Different drainage system) | 173          | 82                                 | 134                               |
| Metro Offsite - E4                          | 735          | 253                                | 327                               |
| North Offsite – E5                          | 538          | 252                                | 407                               |
| Outflow @ HWY 5 Crossing<br>(Excludes E2)   | 1721         | 660                                | 904                               |

<sup>\*</sup>Note that these flows do not reflect onsite and offsite storage that would likely considerably reduce peak flows.

See APPENDIX A for watershed flows, land use summaries, watercourse lengths, and rainfall hyetographs in the SACCALC output file.

#### 2.1a Interstate-5 Crossing Drainage Conditions

There are three existing 5-ft by 8-ft box culverts at the I-5 crossing with inverts at approximately 5.5 ft (REFERENCE NO. 5). With 904 csf passing through the three existing box culverts, the headwater stage is 13.0 ft (see APPENDIX C) which is about a foot lower than the edge of the I-5 pavement. The adjacent low-lying area would likely provide enough storage attenuation to the high water surface and most likely lower headwater elevation.

#### 2.1b Offsite Drainage Conditions

Runoff from the 540 ac offsite watershed north of the project site discharges into the Lone Tree Canal during storms. The drainage ditch parallels the west



property boundary and drains from north to south. The ditch will remain in place under post-development conditions to convey runoff from the offsite watershed. The ditch measures approximately 12 ft wide at bottom and 6 ft deep with 1.5 horizontal to 1 vertical side slopes and 0.0007 ft/ft bottom slope (REFERENCE NO. 5). With a 100-year peak flow of 355 cfs in the channel, it is at capacity but not overflowing.

#### 2.2 ANALYSIS OF ULTIMATE CONDITIONS

#### 2.2a Ultimate Detention Basins

Under ultimate conditions, the Greenbriar watershed consists of approximately 620 acres of low, medium, and high-density residential land use, parks, commercial land use and offsite highway drainage.

FIGURE 8 shows the proposed ultimate condition drainage in the context of surrounding drainage features. FIGURE 9 shows drainage within the project site as developed.

A hydrologic model was developed in SACCALC and its output hydrographs were entered in HEC-RAS around the detention pond.

As shown in **FIGURE 10**, the stormwater detention storage ranges from a water surface of 11.0 ft to 16.0 ft while the permanent pool ranges from a water surface of 3.0 ft to 11.0 ft. The outflow from the detention pond is constrained to 62 cfs with two eight-foot wide Rubicon gates, a 48" reinforced concrete pipe and a flap gate. During the peak stage in the pond, water will overtop the fully closed Rubicon gates. (see **APPENDIX D**)

#### 2.2b Proposed Ultimate Peak Flows, Stages, and Volumes

Required stormwater detention storage volumes and peak stages were developed in the HEC-RAS model. Ultimate conditions runoff and storage results are summarized in **Table 2**.

 
 Peak Parameter Values
 100-yr 10-day
 100-yr 24-hr
 10-yr 24-hr

 1. Total Inflow to pond (cfs)
 408
 912
 609

 2. Stage (ft)
 14.9
 14.9
 13.5

**TABLE 2.** Pond Ultimate Condition Results

See APPENDIX B for ultimate condition SACCALC and HEC-RAS input and output files.

330

62

330

62

279

61

#### 2.2c Water Quality

Storage (ac-ft)
 Outflow (cfs)

Water quality treatment will be provided in the detention pond per the requirements set out in the "North Natomas Design and Procedures Manual" (REFERENCE NO.6). The water quality storage was sized using the Sato Design Curve for Sizing of Water Quality Wet Pond per section 11.6222b of the Sacramento County Hydrology Standards (REFERENCE NO. 6). Based



on the 620 ac drainage area and 50% percent imperviousness, Sato volume was determined to be 25 ac-ft. The volume was then multiplied by 1.25 and rounded up for a 35 ac-ft permanent pool requirement. The proposed permanent pool depth of 8.0 ft in the detention pond yields a total wet pool volume of 198 ac-ft, which exceeds the required 35 ac-ft.

#### 2.2d Interstate-5 Crossing Drainage Conditions

The future Metro Air Park plans to improve the Interstate 5 undercrossing by adding two- 78" reinforced concrete pipes. Upstream to downstream flowlines will be 5.6 ft to 5.5 ft, respectively. All of the HEC-RAS models presented in this report were simulated with the proposed pipes.

For the worst-case scenario, a 100-year 24-hr model was simulated without the proposed pipes to reflect that the construction of the two undercrossing pipes did not occur. Differences were only found at the immediate upstream of the crossing where the water surface was about a foot higher and flow was about ten percent more than the existing condition. These changes did not project far enough to influence the hydraulic conditions at the Greenbriar site and in the Lone Tree Channel.

Existing Proposed Crossing Crossing 3-8'x5' Box 2-78" RCP & **I-5 Crossing Parameters** 3-8'x5' Box 391 Peak Flow (cfs) 376 8.9 9.7 Upstream Stage (ft) 13 13 Top of Bank (ft)

TABLE 3. I-5 Crossing Analysis – Ultimate Conditions

#### 2.2e Offsite Drainage Conditions

Under the Ultimate Conditions, Lone Tree Channel was modeled utilizing HEC-RAS, yielding an average freeboard to top of bank of 0.5 ft during the 100-year storm. With the proposed house pad elevations at approximately 18.0 ft along the western site boundary, the freeboard below the house pads is 2.5 ft.

The proposed Metro Air Park 100-year peak pump outflow of 270 cfs was introduced into Lone Tree Channel in the HEC-RAS model during the whole storm duration. This conservative approach generates higher water surfaces than will likely occur.

## 3. PROPOSED ON-SITE STORM DRAINAGE PIPE SYSTEM

A preliminary design of the on-site storm drainage trunk system was developed consistent with the City of Sacramento requirements. Trunks were sized using the prorated SACCALC watershed flows and the 10-year



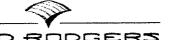
detention pond water surface from HEC-RAS output results. The pipes were sized with approximately two feet of freeboard below the proposed grading.

See FIGURE 9 and APPENDIX E for results and calculations.

#### 4. CONCLUSION

Greenbriar can be developed under ultimate conditions with the proposed facilities outlined in this report. The proposed detention basins with permanent water quality features, outlet described and the on-site storm system will adequately convey runoff from the design storm.

The analyses of the adjacent offsite Lone Tree Channel and Interstate 5 crossing proved adequate for severe storms.



#### 5. REFERENCES

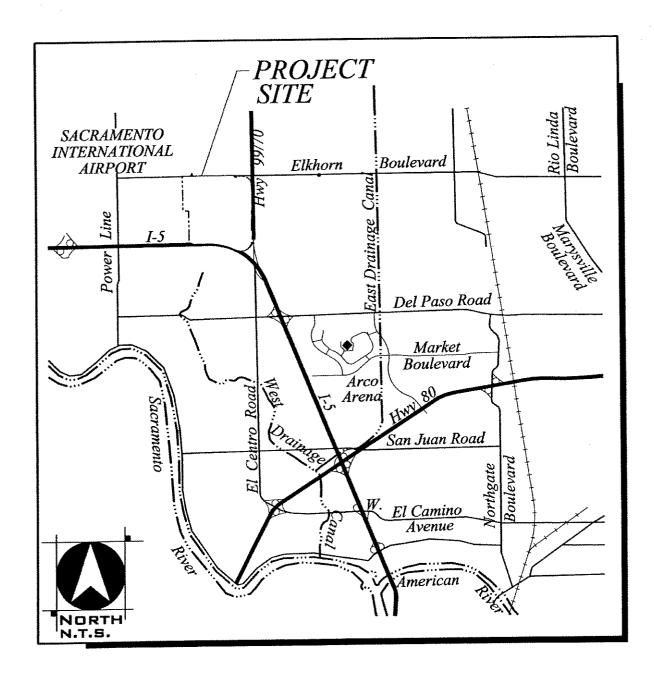
- Federal Emergency Management Agency, Flood Insurance Study, revised July 06, 1998 and Rate Map for West Sacramento, California, Community Panel Numbers 0602660020F, 060262004E, 0602620045E, Revised July 01, 1998.
- 2. Watermark Engineering, "Metro Air Park Master Drainage Study," Final 2002.
- 3. Aerials Express, Digital Aerial Viewer, 2003.
- 4. USGS Quadrangle Map.
- 5. Metro Air Park, Offsite Drainage Improvements, The Spin Corporation.
- 6. North Natomas Drainage Design & Procedures Manual, West Yost & Associates, July 1998.
- 7. Hydrology Standards, Vol.2 of the Sacramento City/County Drainage Manual, Dec. 1996.

#### VICINITY MAP

## GREENBRIAR

CITY OF SACRAMENTO, CALIFORNIA

JULY, 2005





#### SITE PLAN

## GREENBRIAR

CITY OF SACRAMENTO, CALIFORNIA

JULY, 2005



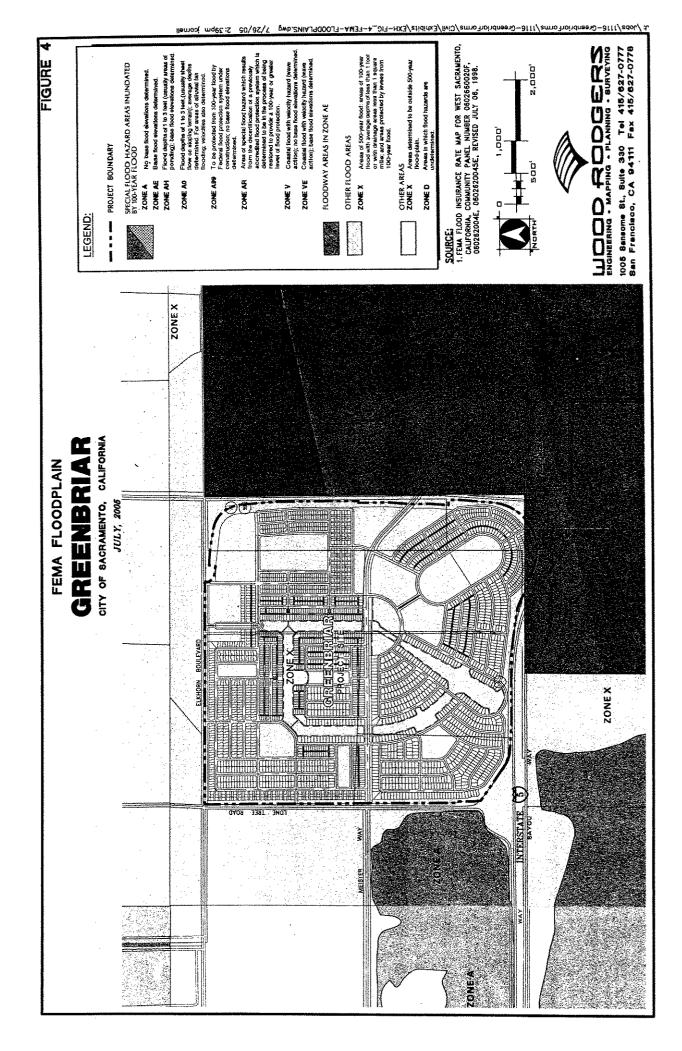
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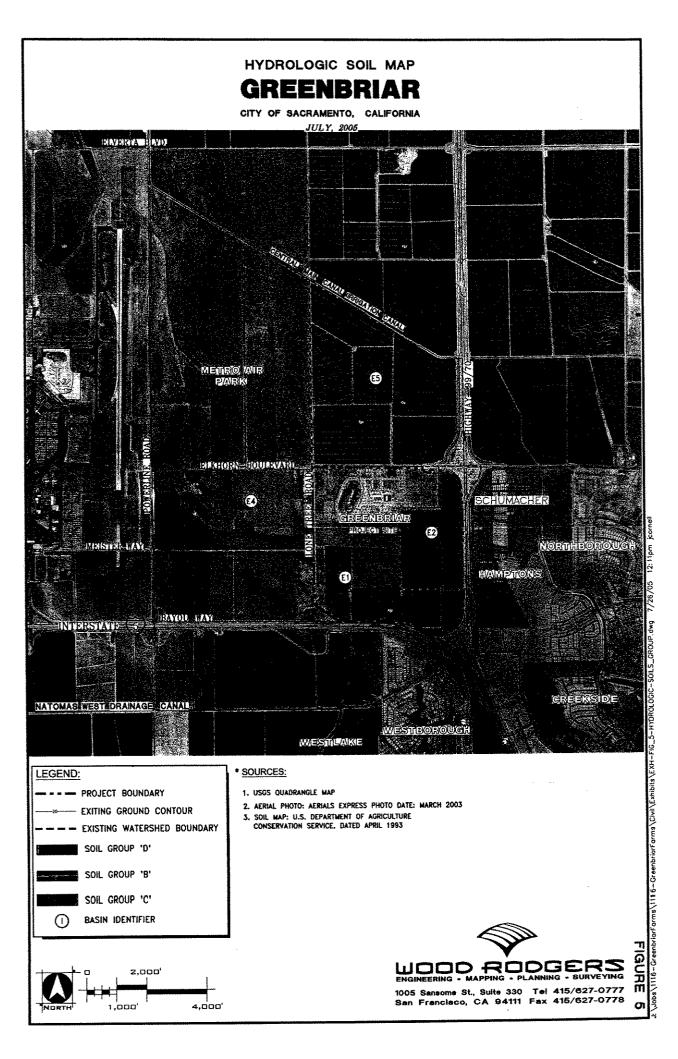
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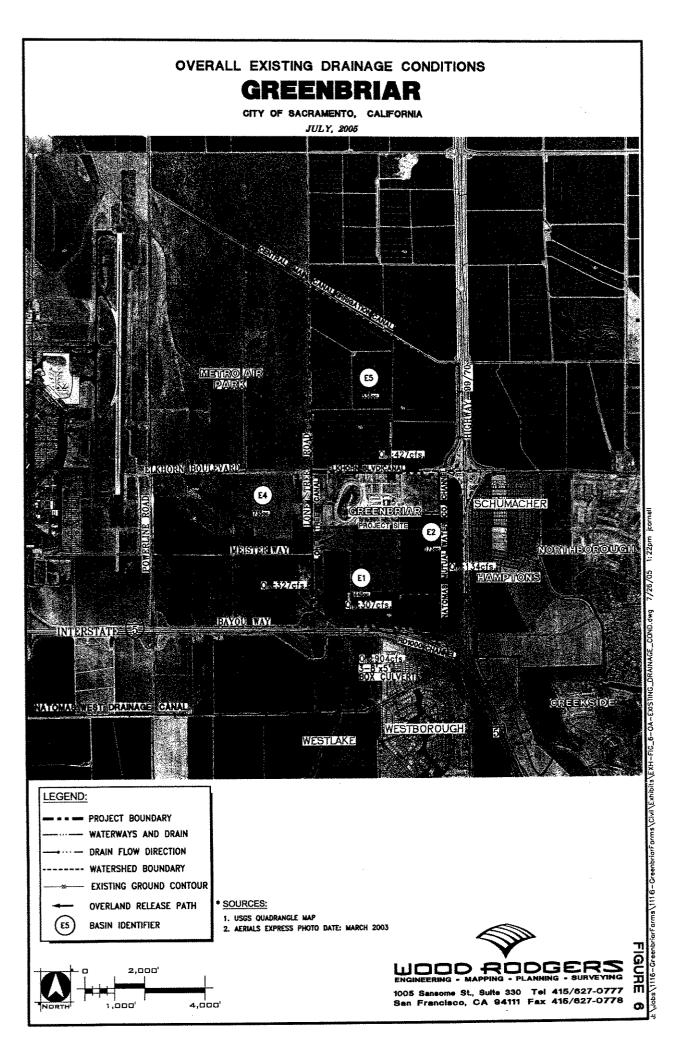
2,000

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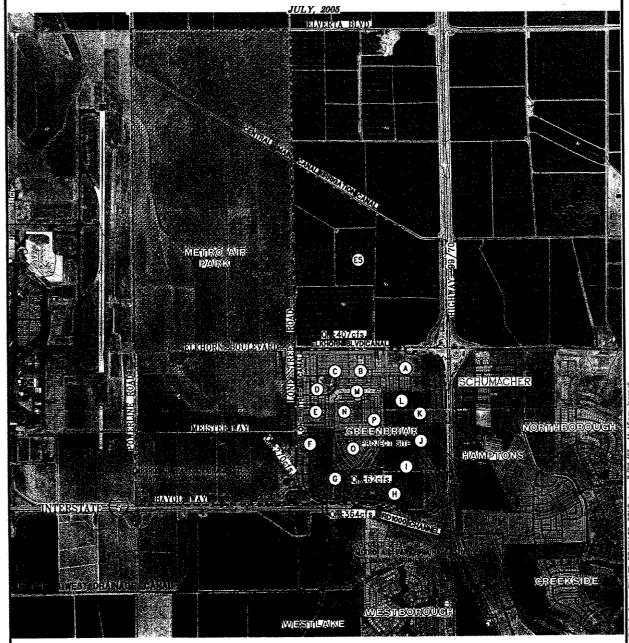


## **EXISTING ONSITE DRAINAGE CONDITIONS GREENBRIAR** CITY OF SACRAMENTO, CALIFORNIA JULY, 2005 ELKHORN BOULEVARD GREENBRIAR PROJECT SITE E1 0<sub>166</sub><u>3</u>07cfs. INTERSTATE 45 Q<sub>100</sub>:904cfs. TO NATOMAS WEST DRAINAGE CANAL EXISTING 3-8'x5' BOX CULVERT TBOROUGH! LEGEND: - PROJECT BOUNDARY EXISTING GROUND CONTOUR WATERWAYS AND DRAIN DRAIN FLOW DIRECTION - WATERSHED BOUNDARY £2 BASIN IDENTIFIER GURE 600 1005 Sansome St., Suite 330 Tel 415/527-0777 San Francisco, CA 94111 Fax 415/627-0778 ado'

#### OVERALL ULTIMATE DRAINAGE CONDITIONS

### **GREENBRIAR**

CITY OF SACRAMENTO, CALIFORNIA

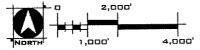


#### LEGEND:

- -- PROJECT BOUNDARY
  - WATERWAYS AND DRAIN
  - ..... DRAIN FLOW DIRECTION
- PROPOSED IMPROVEMENTS
- ---- EXISTING GROUND CONTOUR
- OVERLAND RELEASE PATH
- PROPOSED DETENTION BASIN
- DEVELOPED PROPERTY
- (1) BASIN IDENTIFIER
- PUMP STATION

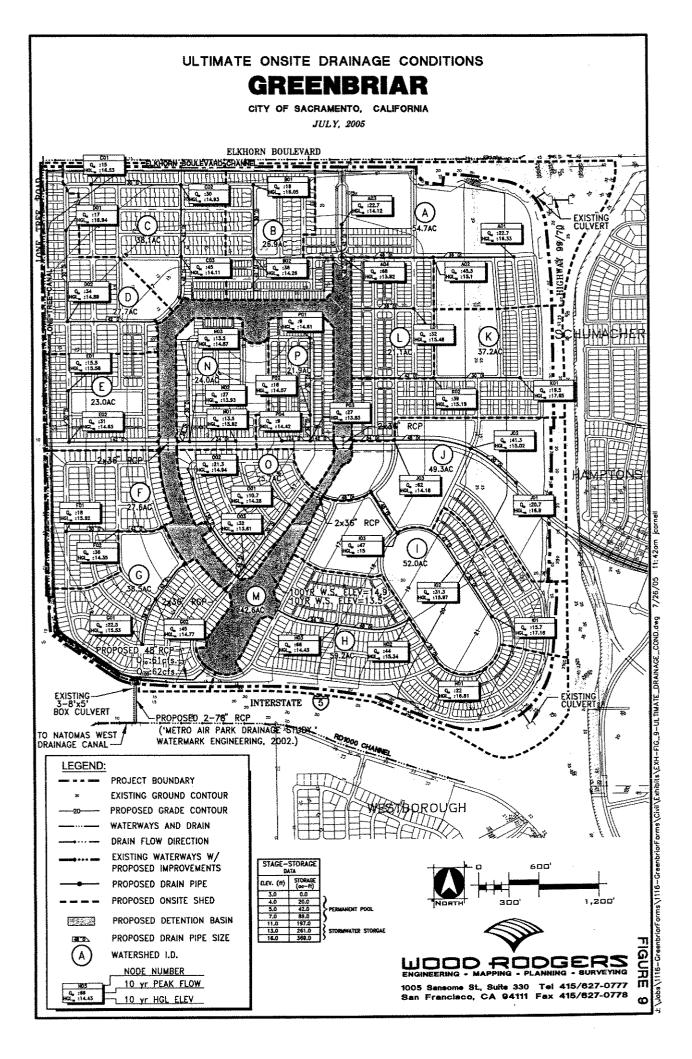
#### • SOURCES

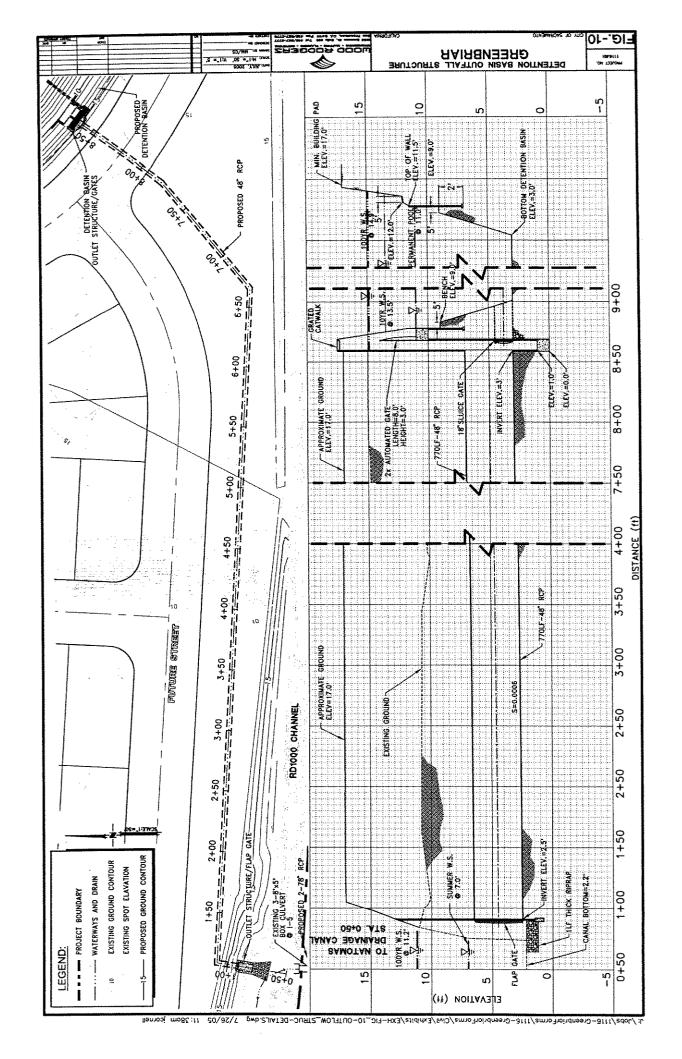
- 1. USGS QUADRANGLE MAP
- 2. AERIALS EXPRESS PHOTO DATE: MARCH 2003





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## 6. APPENDIX A -

**Existing Conditions SacCalc Model** 

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FLOOD HYDROGRAPH PACKAGE (HEC-1L) JULY 1998 VERSION 4.1(L) \* RUN DATE 13JUL05 TIME 10:17:29  U.S. ARMY CORPS OF ENGINEERS U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

x xxxxxxx x x XXXXX XXXXX XXXXX XXXXXXXX x XXX XXXX X XXXXXXX XXXXX

Special version of HEC-1 with Extra-large array Modified by David Ford Consulting Engineers (2000) Program dimensions: Number of hydrograph ordinates: 20000 Unit hydrograph ordinates: 3000

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIME- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF VARIABLES STITUTE AND STITUTE HAVE CHANGED FROM INDEPENDENT OF STRUCTURE OF THE DEFINITION OF AMSKE ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRANTY VERSION NEW OFFICES: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INVERVAL. LOSS RATE: GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

REC-1L INPUT PAGE 1 LINE ID.....1.....2.....3.....4......5,.....6......7.....8......9.....10 \* SacCalc, developed by David Ford Consulting Engineers \* File generated 07/13/2005 10:17:28 1 ID 10010 & 1010 &10024&1024 Lag computation for station El Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl Basin "n" composition (based on Table 7-1)

Developed Undeveloped Developed n adj n fract d Undevelo fract 0.030 0.0300 0.0000 0.031 0.0310 0.0000 0.067 0.0670 0.0000 0.070 0.0700 0.0000 0.032 0.0320 0.0000 0.071 0.0710 0.0000 0.033 0.0330 0.0000 0.072 0.0720 0.0000 0.073 0.0730 0.0000 0.034 0.0340 0.0000 0.035 0.0350 0.0370 0.0000 0.074 0.0740 0.0000 0.0000 0.040 0.0000 0.080 0.0800 0.0000

0.0400 0.042 0.0000 0.084 0.046 0.0460 0.0000 0.088 0.0880 0.0000 0.0500 0.0000 0.090 0.0900 0.050 0.0000 0.0000 0.053 0.056 0.0560 0.0000 0.096 0.0960 0.0000 0.0600 0.1000 0.060 0.0000 0.065 0.0650 0.0000 0.110 0.1100 0,0000 0.070 0.0700 0.5000 0.115 0.5000 0.075 0.0750 0.0000 0.120 0.1200 0.0000 0.080 0.0800 0.0000 0.150 0.1500 0.0000

Equation (7-1) with b=1.1364, Lc=0.5682, S=6.864, n=0.0925 Resulting lag: 90.9 minutes

\* Lag computation for station E2
\* Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl

Lag frequency factor of 1.0 (Table 7-6) for frequency
Basin "n" composition (based on Table 7-1)

Developed Undeveloped

n adj n fract n adj n fract

0.030 0.0300 0.0000 0.067 0.0670 0.0000

0.031 0.0310 0.0000 0.070 0.0700 0.0000

0.032 0.0320 0.0000 0.071 0.0710 0.0000 0.033 0.0330 0.0000 0.034 0.0340 0.0000 0.072 0.0720 0.0000 0.073 0.0730 0.0000

```
0.0760
                                                                            0.0000
                                  0.0370
                                           0.0000
                                                          0.076
                          0.037
                          0.040
                                  0.0400
                                           0.0000
                                                          0.080
                                            0.0000
                                                          0.084
                                                                  0.0840
                                                                            0.0000
                                           0.0000
                                                          0.088
                                                                  0.0880
                                                                            0.0000
                          0.046
                                  D.0460
                                           0.0000
                          0.050
                                  0.0500
                                                          0.090
                                                                  0.0900
                                                                            0.0000
                                                                  0.0930
                                                          0.093
                                                                            0.0000
                                  0.0530
                          0.053
                          0.056
                                  0.0560
                                           0.0006
                                                          0.096
                                                                  0.0960
                                                                            0.0000
                                                           0.100
                                                                   0.1000
                                                                            0.0000
                                  0.0600
                                           0.0006
                          0.060
                          0.065
                                  0.0650
                                           0.0006
                                                          0.110
                                                                  0.1100
                                                                            0.0000
                                                          0.115
                          0.070
                                  0.0700
                                           0.5006
                                                                  0.1150
                                                                            0.5000
                                                                  0.1200
                                                                            0.0000
                          0.075
                                  0.0750
                                           0.0000
                                 0.0800 0.0000
                                                          0.150 0.1500
                                                                           0.0000
                  * Equation (7-1) with L= 0.7576, Lc= 0.3822, S= 4.224, n=0.0925

* Resulting lag: 75.6 minutes

* Lag computation for station E4

* Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl

* Basin *n* composition (based on Table 7-1)

* Developed

* Developed

* Ondeveloped

* Ondeveloped

* Ondeveloped

* Ondeveloped

* Ondeveloped

* Ondeveloped
                      n adj n fract
                                                            n adj n fract
                         0.030 0.0300 0.0006
0.031 0.0310 0.0000
                                                          0.067 0.0670
                                                                            0.0000
                                                          0.070 0.0700
                                                                            0.0000
                                          0.0000
                          0.032 0.0320
                                                          0.071
                                                                  0.0710
                                                                            0.0000
                                                          0.072
                                                                  0.0720
                                                                            0.0000
                          0.033
                                  0.0330
                                 0.0340 0.0006
0.0350 0.0000
                                                          0.073
0.074
                          0.034
                                                                  0.0730
                                                                            0.0000
                          0.035
                          0.037
                                  0.0370 0.0006
                                                          0.076
                                                                  0.0760
                                                                            0.0000
                                                                            0.0000
                                  0.0400
                                           0.0000
                                                           0.080
                                                                   0.0800
                          0.040
                                                                  0.0840
                          0.042
                                  0.0420
                                           0.0000
                                                          0.084
                          0.046
                                  0.0460
                                           0.0000
                                                           0.088
                                                                  0.0880
                                                                            0.0000
                                 0.0500
                                           0.0000
                                                          0.090
                                                                  0.0900
                                                                            0.0000
                          0.050
                          0.053
                                  0.0530
                                           0.0000
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                                                                  0.0930
                                                                            0.0000
                          0.056
                                  0.0560
                                           0.0000
                                                                            0.0000
                                                           0.096
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                          0.075
                                0.0750 0.0000
0.0800 0.0000
                                                          0.120
                                                                  0.1200
                                                                            0.0000
                                                                            0.0000
                                                          0.150
                                                                 0.1500
                          0.080
                       .....
                      Equation (7-1) with L= 2.3674, Lc= 1.1364, S= 2.640, n=0.0925
                  * Resulting lag: 170.4 minutes
* Lag computation for station E5
                      Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl
                      Basin "n" composition (based on Table 7-1)

Developed Undeveloped
n adj n fract n adj n fr
                                                                        n fract
                                                      0.067 0.0670
                        0.030 0.0300 0.0000
0.031 0.0310 0.0000
                                                                            0.0000
                                                                 0.0700
                                                                            0.0000
                                                          0.070
                                                                           0.0000
                                 0.0320 0.0000
                                                          0.071
                          0.032
                          0.033
                                 0.0330
                                           0.0000
                                                          0.072
                                                                  0.0720 0.0000
                                                          0.073
                                                                  0.0730
                                                                            0.0000
                          0.034
                                 0.0340
                                           0.0006
                          0 035
                                 0.0350
                                           0.0000
                                                          0 074
                                                                  0 0740
                                                                            0.0000
                          0.037
                                 0.0370
                                           0.0000
                                                          0.076
                                                                  0.0760
                                                                              .0000
                                           0.0000
                                                          0.080
                                                                           0.0000
                         0.040
                                 0.0400
                         0.042
                                 0.0420
                                           0.0000
                                                          0.084
                                                                  0.0840
                                                                           0.0000
                                                          0.088
                                                                  0.0880
                                                                            0.0000
                         0.050
                                 0.0500
                                           0.0000
                                                          0.090
                                                                  0.0900
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                          0.053
                                           0.0000
                                                          0.093
                                                                  0.0930
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                                                                  0.0960
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                                           0.0000
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                                                                              .0000
                                 0.0650
                                                                           0.0000
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                                           0.0000
                         0.070
                                 0.0700
                                          0.5000
                                                          0.115
                                                                  0.1150
                                                                              .5000
                         0.075
                                 0.0750
                                          0.0000
                                                          0.120
                                                                  0.1200
                                                                           0.0000
                         0.080 0.0800
                                          0.0000
                                                          0.150 0.1500 0.0000
                     Equation (7-1) with L= 0.9470, Lc= 0.3788, S= 5.280, n=0.0925
                 * Resulting lag: 78.2
* End of lag computations
                                         78.2 minutes
                     NMIN JXDATE JXTIME
                                                    NQ
HEC-1L INPUT
                                                                                                                      PAGE 2
               ID.....1....2....3....4....5....6....7...8....9....10
LINE
                     1 31DEC99
IPRT IPLT
3 0
                                       2400 15592
   2
                 m
                 IO
   3
   4
                 KK
                    JEMEN Time interval for input data
                 IN
   5
                 * Design storm construction details
                 * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 2.959
                   multiplier from table 4-4: 0.9808
                * Adjusted depths for each duration from table 4-1: frequency: 10 * Duration----Regional------Elev-----Areal (adjustments)
```

0.074 0.0740 0.0000

0.035 0.0350 0.0000

```
0.2452
                * 5 min
                                  0.2500
                                             0.2500
                                  0.3600
                                             0.3600
                * 10 min
                                                         0.3531
                  15 min
                  30 min
                                   0.5700
                                             0.5700
                                                         0.5591
                  1 hour
                 * 2 hours
                                   1.0400
                                             1.0400
                                                         1.0196
                                  1,2300
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                   5 days
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                * Storm duration: 10, length: 240 ordinates
* Distrubution using table 4-8 of total rainfall: 7.4646
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                * Precipitation losses computation (Chapter 5)
                    Computing RTIMP (percent impervious) from land use and table 5-2
Computing CNSTL (infiltration rate) from soil type and table 5-2
                   TAREA subbasin area (sq mi)
0.2703
 32
                BA
                     0.2703
PRTL CNSTL RTIMP
0.20 0.070 2.000
                   STRTL
 33
                LU
                * Runoff hydrograph computation (Chapter 6)
                    Using basin lag:
                                        75.6 minutes
                    Using unit duration (Step 2): 1. min
Lag Time + Unit Duration / 2 (Step 3): 76.07659
                    Volume of runoff (Step 4) V=
0.96 1.93 2.89 3.9
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                                        Time interval for input data
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                             * Design storm construction details
                             * Regional multiplier (zone 2) applied: 1.000
                              Areal adjustment using area: 2.959
multiplier from table 4-4: 0.9808
                              Adjusted depths for each duration from table 4-1: frequency: 10
                             * Duration----Regional------Elev-----Areal (adjustments)
                                                        0.2500
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                                                                   0.2452
                              5 min
                              to min
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                               15 min
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                                                                    7.4646
                              Storm duration: 10. length: 240 ordinates
                            * Distrubution using table 4-8 of total rainfall: 7.4646
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                            * Precipitation losses computation (Chapter 5)
                                Computing RTIMP (percent impervious) from land use and table 5-2 computing CNSTL (infiltration rate) from soil type and table 5-2
                               TAREA
                                      subbasin area (sq mi)
                                0,7000
             109
                            ₿A
                              STRTL CNSTL RTIMP
0.20 0.070 2.000
                            LU
             110
                            * Runoff hydrograph computation (Chapter 6)
                                Using basin lag: 90.9 minutes
Using unit duration (Step 2): 1. min
Lag Time + Unit Duration / 2 (Step 3): 91.39346
                                Volume of runoff (Step 4) V= 18.822222
1.73 3.46 5.19 6.92 8.98 1
                                                                    8,98 11.47
34.80 37.64
                                                                                               16.44
43.32
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                                1.73 3.46 5.19
24.11 26.70 29.30
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                                                                    97.53 101.39
                                                                                   105.33
            114
                                 82.81
                                                                                             109.36
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UI

3.06

3.03

3.00

2.97

2.94

2.86

2.91

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UI 121.45 125.86 130.32 134.78 139.24 143.72 148.24 UI 166.93 172.32 177.70 183.08 188.53 194.31 200.10 UI 222.43 227.70 232.97 238.15 239.42 240.69 241.96
                                                                                                      205.89 211.67
243.23 244.24
                                                                                                                          217,15
              116
                               UI
                                    222.43
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                                             246.35
                                                                246.51
                                                                          245.81 245.11
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                                    245,65
              118
                                                                          226.61 222.42
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                                   239.71
200.89
                                             238.44 234.99
196.54 192.15
158.10 155.69
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              120
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                                   160.50
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107.70 105.83
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                                              133.21 130.40
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67.21
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              127
                               UI
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                                               62.97
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              128
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              129
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              131
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HEC-1L INPUT
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              159
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              165
                                     CoFLOW Fo010YR-10DY A-GREENERI
                               2W
                              KK E4

* JXMIN Time interval for input data
IN 60
              167
              162
                               KM Part of future Metro Air Park
              169
                               * Design storm construction details
                              * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 2.959
* multiplier from table 4-4: 0.9808
                               * Adjusted depths for each duration from table 4-1: frequency: 10
                               * 10 min
                                                  0.3600
                                                              0.3600
                                                                          0.3531
                                                             0.4300
                                                  0.4300
                                 15 min
                                 30 min
                                                  0 5700
                                                                          0.5591
                                                  0.7700
                                                                          0.7552
                                 1 hour
                                                                          1.0196
                               * 2 hours
                                                  1.0400
                                                             1.0400
                               * 3 hours
                                                  1.2300
                                                              1.2300
                                                                          1.2177
                                                  1.6500
                                                              1.6500
                                                                          1.6335
                               * 6 hours
                               * 12 hours
                                                  2.2500
                                                             2.2500
                                                                          2.2284
                                                  2.9800
                                                              2.9800
                                 24 hours
                               * 36 hours
                                                  3 5400
                                                             3 5400
                                                                          3.5046
                                2 days
                                                  3.9500
                                                              3.9500
                               * 3 days
                                                  4.6500
                                                              4.6500
                                                                          4.6500
                                                              5.7600
                              * 10 days 7.5400 7.5400 7.4646

* Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646
                                                  7.5400
                                                                                                                                        PAGE 7
                                                                  REC-11, INDIE
            LINE
                             ID.....1....2....3.....4.....5,.....6......7.....9.....10
             170
                              PB
                              PI 0.0224 0.0821 0.2015 0.1120 0.0373 0.0224 0.0075 0.0000 0.0000 0.0000 PI 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
              171
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172

152.75 157.27

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 176
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 180
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 185
                 PI
                      0.0970
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PI
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                               0.0373
                 PI 0.0149
                 * Precipitation losses computation (Chapter 5)

* Computing RTMP (percent impervious) from land use and table 5-2

* Computing CNSTL (infiltration rate) from soil type and table 5-2

* TAREA subbasin area (sq mi)

BA 1.1484

* STRTL CNSTL RTMP

LU 0.20 0.070 2.000
 195
 196
                 * Runoff hydrograph computation (Chapter 6)
                      Using basin lag: 170.4 minutes
Using unit duration (Step 2): 1. min
                      Lag Time + Unit Duration / 2 (Step 3):170.92508
Volume of runoff (Step 4) V= 30.880209
                                                    3.25
                                                                                                               8 63
                      0.81
9.80
21.67
                               1.62
10.97
22.89
                                                              4.06
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13.30
25.32
 197
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                                          12.13
                                                                                          18.02
                 UI
                                                             14.47
                                                                       15.64
 198
                                                                                          30.46
42.52
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43.52
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                                                                       27.80
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                                          24.10
 199
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103.37
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 203
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130.25
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 212
                                                     HEC-1L INPUT
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                ID.,....1.......2......3.......4.......5,......6......7......8.......9......10
LINE
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                 * Design storm construction details
                 * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 2.959
* multiplier from table 4-4: 0.9808
                   Adjusted depths for each duration from table 4-1: frequency: 10
                   Duration----Regional------Elev-----Areal (adjustments)
                                                          0.2452
                   5 min
                                    0.2500
                                               0.2500
                                   0.3600
                                               0.3600
                 * 10 min
                                   0.4300
                                               0.4300
0.5700
                                                           0.4217
                                                           0.5591
                   30 min
                 * 1 hour
                                   0.7700
                                               0.7700
                                                           0.7552
                                    1.0400
                                               1.0400
                                                           1.0196
                   2 hours
                 * 3 hours
                                   1.2300
                                               1.2300
                                                           1.2177
                                                           1.6335
                                    1.6500
                                               1.6500
                   6 hours
                                    2.2500
                                               2.2500
                 * 12 hours
                                   2.9800
                                               2.9800
3.5400
                   24 hours
                                                           2.9800
                                                           3,5046
                   36 hours
                   2 days
                                   3.9500
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                                               4.6500
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                   3 days
                                                           5.7024
7.4646
                   5 days
                                    5 7600
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                                               7.5400
                   10 days
                                    7.5400
                 * Storm duration: 10, length: 240 ordinates
                 * Distrubution using table 4-8 of total rainfall: 7.4646
                                                                                                                       PAGE 10
                                                   HEC-1L INPUT
                ID.....1......2......3......4......5,......6......7......8.......9.....10
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                                Precipitation losses computation (Chapter 5)

Computing RTIMP (percent impervious) from land use and table 5-2

Computing CNSTL (infiltration rate) from soil type and table 5-2
                                   TAREA subbasin area (sq mi)
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                                BA
                                     0.8406
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                                * Runoff hydrograph computation (Chapter 6)
                                    unoff hydrograph Computer Using basin lag: 78.2 winutes Using unit duration (Step 2): 1. win Lag Time + Unit Duration / 2 (Step 3): 78.67958 Volume of runoff (Step 4) V= 22.603472 2.80 5.61 8.41 11.30 15.33 19.36 40.06 44.35 48.95 53.55 58.15 62.45 10.06 44.35 48.95 53.55 58.15 62.45
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U.S. ARMY CORPS OF ENGINEERS
   FLOOD HYDROGRAPH PACKAGE (HEC-1L) *
                                                                                                             HYDROLOGIC ENGINEERING CENTER
                JULY 1998
                                                                                                                 609 SECOND STREET
DAVIS, CALIFORNIA 95616
              VERSION 4.1(L)
                                                                                                                     (916) 756-1104
   RUN DATE 13JULOS TIME 10:17:29
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                              10010 & 1010 &10024&1024
                   OUTPUT CONTROL VARIABLES
   3 TO
                                      3 PRINT CONTROL
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                                          0. HYDROGRAPH PLOT SCALE
                          OSCAL
                   HYDROGRAPH TIME DATA
     IT
                                    1 MINUTES IN COMPUTATION INTERVAL
31DEC99 STARTING DATE
0000 STARTING TIME
15592 NUMBER OF HYDROGRAPH ORDINATES
11JAN 0 ENDING DATE
                                           1 MINUTES IN COMPUTATION INTERVAL
                           NMTN
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NDDATE
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19 CENTURY MARK
                         NDTIME
                          ICENT
                     COMPUTATION INTERVAL 0.02 HOURS
TOTAL TIME BASE 259.85 HOURS
           ENGLISH UNITS
                DRAINAGE AREA
PRECIPITATION DEPTH
                                          SOURCE MILES
                                          INCHES
                                          FEET
                 LENGTH, ELEVATION
                                          CUBIC FRET PER SECOND
                                          ACRE-FEET
                 STORAGE VOLUME
                 SURFACE AREA
                                          ACRES
                 TEMPERATURE
                                          DEGREES FAHRENHEIT
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   4 KK
                  TIME DATA FOR INPUT TIME SERIES
   5 IN
                                    60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE
2400 STARTING TIME
                         JYMYN
                        JXTIME
                SUBBASIN RUNOFF DATA
                  SUBBASIN CHARACTERISTICS
TAREA, 0.27 SUBBASIN AREA
 32 BA
                  PRECIPITATION DATA
                         STORM
                                        7.46 BASIN TOTAL PRECIPITATION
  7 PB
                  UNIFORM LOSS RATE
 33 LU
                                       0.20 INITIAL LOSS
                         STRTL
                         CNSTL
                                        0.07 UNIFORM LOSS RATE
                                        2.00 PERCENT IMPERVIOUS AREA
                         RTIMP
                  INPUT UNITGRAPH, 456 ORDINATES, VOLUME = 1.00
 32 UI
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HYDROGRAPH AT STATION E2

TOTAL RAINFALL = 7.46, TOTAL LOSS = 4.55, TOTAL EXCESS = 2.92 MAXIMUM AVERAGE FLOW 259.85-HR (CFS) (HR) (CFS) 2. 2.916 52. 153.58 (INCHES) 1,969 0.949 1.484 14. 42. (AC-FT)

> CUMULATIVE AREA = 0.27 SQ MI

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81 KK E1

TIME DATA FOR INPUT TIME SERIES 82 IN

JXMIN JXDATE 60 TIME INTERVAL IN MINUTES 31DEC99 STARTING DATE JXTIME 2400 STARTING TIME

SUBBRASTN SUBSORP DATA

SUBBASIN CHARACTERISTICS 109 BA

TAREA. 0.70 SUBBASIN AREA

PRECIPITATION DATA

7.46 BASIN TOTAL PRECIPITATION 84 PB STORM

UNIFORM LOSS RATE 110 LU

STRTL 0.20 INITIAL LOSS 0.07 UNIFORM LOSS RATE RTIMP 2.00 PERCENT IMPERVIOUS AREA

INPUT UNITGRAPH, 548 ORDINATES, VOLUME = 1.00 109 UI 3.5 26.7 5.2 29.3 6.9 32.0 9.0 34.8 1.7

11.5 37.6 40.5 43.3 45.7 47.8 79.7 52.1 85.9 54.5 89.8 58.4 93.7 62.3 97.5 66.2 101.4 109.4 152.8 113.4 157.3 117.4 161.8 105.3 82.8 121.4 166.9 222.4 143.7 125.9 172.3 130.3 177.7 134.8 139.2 148.2 188.5 194.3 240.7 200.1 242.0 183.1 205.9 211.7 217.1 243.2 244.2 238.1 244.9 227.7 233.0 247.1 235.0 246.5 230.8 245.8 226.6 245.1 222.4 244.4 218.2 243.5 242.3 241.0 245.6 213.9 238.4 239.7 187.8 153.3 183.4 150.9 171.4 143.7 200.9 196.5 192.1 179.0 175.2 167.5 163.7 148.5 160.5 158.1 155.7 125.6 107.7 120.4 118.7 136.0 133.2 130.4 127.6 123.9 122.1 116.8 105.8 109.6 113.2 111.4 115.0 97.9 84.3 90.8 77.8 89.3 76.8 86.8 75.0 95.5 95.1 93.7 92.2 88.1 85.5 83.0 81.7 80.4 79.1 75.9 66.4 73.2 63.8 68.1 67.2 65.5 64.7 72.1 71.1 70.0 69.0 63.0 62.1 56.6 50.5 56.0 55.3 54.7 54.0 53.5 52.9 52.3 51.8 51.1 44.8 49.8 41.9 41.5 41.1 40.8 44.3 43.8 43.3 42.9 42.4

13.9

16.4

18.9

|      |      |      |      |      |      |       | 200  | 36.6 | 36.3 |
|------|------|------|------|------|------|-------|------|------|------|
| 40.1 | 39.5 | 39.0 | 38.5 | 37.9 | 37.5 | 37.2  | 36.9 |      | 32.7 |
| 35.8 | 35.3 | 34.8 | 34.4 | 33.9 | 33.7 | 33.5  | 33.3 | 33.1 |      |
| 32.4 | 32.0 | 31.5 | 31.3 | 31.1 | 30.9 | 30.8  | 30.6 | 30.4 | 30.1 |
| 29.8 | 29.6 | 29.3 | 29.1 | 26.9 | 28.7 | 28.5  | 28.3 | 28.1 | 27.8 |
| 27.6 | 27.4 | 27.1 | 26.9 | 26.6 | 26.4 | 26.1  | 25.9 | 25.7 | 25.5 |
| 25.3 | 25.1 | 24.9 | 24.8 | 24.6 | 24.5 | 24.2  | 24.0 | 23.8 | 23.6 |
| 23.4 | 23.2 | 23.0 | 22.8 | 22.5 | 22.5 | 22.4  | 22.2 | 22.1 | 21.9 |
| 21.7 | 21.5 | 21.4 | 21.2 | 21.0 | 20.8 | 20.6  | 20.4 | 20.2 | 20.1 |
| 20.0 | 19.9 | 19.8 | 19.6 | 19.5 | 19.3 | 19.1  | 18.9 | 18.8 | 18.7 |
| 18.6 | 18.5 | 18.3 | 18.1 | 17.9 | 17,7 | 17.5  | 17.5 | 17.4 | 17.3 |
| 17.2 | 17.1 | 16.9 | 16.7 | 16.5 | 16.3 | 16.2  | 16.1 | 16.0 | 15.9 |
| 15.8 | 15.6 | 15.5 | 15.4 | 15.2 | 15.2 | 15.1  | 15.1 | 15.0 | 14.9 |
| 14.0 | 14.6 | 14.4 | 14.3 | 14.1 | 14.0 | 13.9  | 13.8 | 13.7 | 13.6 |
| 13.5 | 13.4 | 13.3 | 13.2 | 13.1 | 13.0 | 12.9  | 12.7 | 12.7 | 12.6 |
| 12.5 | 12.4 | 12.3 | 12.3 | 12.2 | 12.1 | 12.0  | 11.9 | 11.8 | 11.7 |
| 11.6 | 11.5 | 11.4 | 11.3 | 11.2 | 11.2 | 11.1  | 11.0 | 10.9 | 10.8 |
| 10.8 | 10.7 | 10.6 | 10.5 | 10.4 | 10.4 | 10.3  | 10.2 | 10.1 | 10.0 |
|      | 9.9  | 9.8  | 9.7  | 9.6  | 9.5  | 9.4   | 9.4  | 9.3  | 9.2  |
| 9.9  | 9.1  | 9.1  | 9.0  | 8.9  | 8.8  | 8.7   | 8.6  | 8.5  | 8.4  |
| 9.2  | 8.3  | 8.3  | 8.2  | 8.1  | 8.0  | 7.9   | 7,9  | 7.8  | 7.8  |
| 8.4  | 7.7  | 7.6  | 7.6  | 7.5  | 7.4  | 7.4   | 7.3  | 7.3  | 7.2  |
| 7.7  | 7.1  | 7.1  | 7.0  | 7.0  | 6.9  | 6.9   | 6.8  | 6.8  | 6.7  |
| 7.2  |      | 6.5  | 6.5  | 6.4  | 6.4  | 6.3   | 6.3  | 6.2  | 6.2  |
| 6.6  | 6.6  | 6.1  | 6.1  | 6.0  | 5.0  | 6.0   | 5.9  | 5.9  | 5.9  |
| 6.1  | 6.1  | 5.7  | 5.7  | 5.6  | 5.6  | 5.6   | 5.6  | 5.5  | 5.4  |
| 5.8  | 5.8  | 5.1  | 5.2  | 5.2  | 5.1  | 5.1   | 5.0  | 5.0  | 5.0  |
| 5.4  | 5.3  | 4.9  | 4.9  | 4.8  | 4.8  | 4 . B | 4.7  | 4.7  | 4.6  |
| 5.0  | 4.9  |      | 4.5  | 4.5  | 4.4  | 4.3   | 4.3  | 4.3  | 4.2  |
| 4.6  | 4.5  | 4.5  | 4.1  | 4.1  | 4.0  | 4.0   | 4.0  | 4.0  | 3.9  |
| 4.2  | 4.1  | 4.1  | 3.8  | 3.8  | 3.8  | 3.7   | 3.7  | 3.7  | 3.7  |
| 3.9  | 3.9  | 3.8  | 3.5  | 3.5  | 3.5  | 3.5   | 3.4  | 3.4  | 3.4  |
| 3.6  | 3.6  | 3.6  | 3.5  | 3.3  | 3.2  | 3.2   | 3.2  | 3.1  | 3.1  |
| 3.4  | 3.3  | 3,3  | 3.3  | 3.0  | 3.0  | 3.0   | 3.0  | 3.0  | 3.0  |
| 3.1  | 3.1  | 3.0  |      | 2.8  | 2.8  | 2.8   | 2.8  | 2.7  | 2.7  |
| 2.9  | 2.9  | 2.9  | 2.9  | 2.5  | 2.6  | 2.6   | 2.6  |      |      |
| 2.7  | 2.6  | 2.6  | 2.6  | 2.0  | 2.0  | 2.0   | 2.0  |      |      |
|      |      |      |      |      |      |       |      |      |      |

女女者 女女者 哲女者 有力者

HYDROGRAPH AT STATION E1

TOTAL RAINFALL = 7.46, TOTAL LOSS = 4.55, TOTAL EXCESS = 2.92

| PEAK FLOW |       | TIME   |                     | lage flow           |                     |                     |                     |
|-----------|-------|--------|---------------------|---------------------|---------------------|---------------------|---------------------|
|           |       | tern l |                     | 6-HR                | 24-HR               | 72-HR               | 259.85-HR           |
| +         | (CFS) | (HR)   | (CFS)               |                     |                     |                     |                     |
| +         | 127.  | 153.78 | (INCHES)<br>(AC-FT) | 70.<br>0.929<br>35. | 28.<br>1.483<br>55. | 12.<br>1.969<br>74. | 5.<br>2.916<br>109. |
|           |       |        | (MC E. 7.)          | 32.                 | ~~.                 |                     |                     |

CUMULATIVE AREA - 0.70 SQ MI

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167 KK E4 Part of future Metro Air Park TIME DATA FOR INPUT TIME SERIES

JXMIN 50 TIME INTERVAL IN MINUTES

JXDATE 31DEC99 STARTING DATE

JXTIME 2400 STARTING TIME SUBBASIN RUNOFF DATA SUBBASIN CHARACTERISTICS
TAREA, 1.15 SUBBASIN AREA 195 BA PRECIPITATION DATA 7.46 BASIN TOTAL PRECIPITATION STORM 170 PB UNIFORM LOSS RATE 196 LU 0.20 INITIAL LOSS 0.07 UNIFORM LOSS RATE 2.00 PERCENT IMPERVIOUS AREA STRTL CNSTL RTIMP INPUT UNITGRAPH, 1025 ORDINATES, VOLUME = 1.00 195 UI 6.5 18.0 30.5 42.5 56.9 72.7 4.9 15.6 27.8 40.5 53.2 69.8 7.5 19.2 31.8 43.5 8.6 20.5 33.1 44.5 4.1 14.5 26.5 39.5 51.4 0.8 9.8 21.7 34.5 45.5 62.4 1.6 2.4 3.3 13.3 16.8 29.1 41.5 55.1 71.2 88.3 22.9 35.8 46.5 63.9 79.3 24.1 37.1 47.8 65.4 81.1 25.3 28.5 49.6 66.8 82.9 58.7 74.1 60.5 75.7 93.9 92.0

| 95.8       | 97.7  | 99.6  | 101.5      | 103.4 | 105.3        | 107.2 | 109.3  | 1.11.3 | 113.4 |
|------------|-------|-------|------------|-------|--------------|-------|--------|--------|-------|
| 115.5      | 117.6 | 119.7 | 121.8      | 123.9 | 126.0        | 128.1 | 130.3  | 132.4  | 134.5 |
|            | 138.7 | 140.8 | 143.0      | 145.5 | 148.0        | 150.5 | 153.1  | 155.6  | 158.1 |
| 136.6      |       | 165.8 | 168.5      | 171.2 | 173.9        | 176.6 | 179.3  | 182.0  | 184.8 |
| 160.5      | 163.1 |       | 194.9      | 197.4 | 199.9        | 202.3 | 204.8  | 207.3  | 209.1 |
| 187.5      | 190.0 | 192.4 |            | 212.1 | 212.7        | 213.3 | 213.9  | 214.3  | 214.6 |
| 209.7      | 210.3 | 210.9 | 211.5      |       | 215.6        | 216.7 | 216.4  | 216.1  | 215.7 |
| 214.9      | 215.2 | 215.6 | 215.9      | 216.2 |              | 213.0 | 212.4  | 211.8  | 211.2 |
| 215.4      | 215.1 | 214.7 | 214.4      | 214.1 | 213.5        |       | 200.7  | 198.7  | 196.8 |
| 210.6      | 216.0 | 209.4 | 208.6      | 206.6 | 204.6        | 202.7 |        | 178.6  | 176.6 |
| 194.8      | 192.8 | 190.8 | 188.8      | 186.8 | 184.7        | 182.7 | 180.7  |        |       |
| 174.6      | 172.5 | 170.5 | 158.4      | 166.4 | 164.3        | 162.3 | 150.2  | 158.1  | 156.2 |
| 154.4      | 152.6 | 150.8 | 149.0      | 147.2 | 145.4        | 143.6 | 141.8  | 140.7  | 139.6 |
| 138.4      | 137.3 | 136.2 | 135.0      | 133.9 | 132.8        | 131.6 | 130.5  | 129.4  | 120.3 |
|            | 126.1 | 124.9 | 123.8      | 122.7 | 121.4        | 120.1 | 118.8  | 117.5  | 116.2 |
| 127.2      |       | 112.2 | 111.1      | 110.2 | 109.4        | 108.6 | 107.8  | 107.0  | 106.2 |
| 114.8      | 113.5 | 103.7 | 102.9      | 102.0 | 101.2        | 100.3 | 99.5   | 98.6   | 97.8  |
| 105.4      | 104.6 |       | 94.3       | 93.4  | 92.5         | 91.7  | 90.8   | B9.9   | 89.2  |
| 96.9       | 96.0  | 95.2  |            |       | 85.2         | 84.6  | 83.9   | 83.2   | 82.6  |
| 88.5       | 87.9  | 87.2  | 86.5       | 85.9  |              | 77.9  | 77.3   | 76.7   | 76.1  |
| 81.9       | 81.2  | 80.5  | 79.9       | 79.2  | 78.5         | 71.9  | 71.3   | 70.7   | 70.1  |
| 75.5       | 74.9  | 74.3  | 73.7       | 73.1  | 72.5         |       | 66.1   | 65.7   | 65.2  |
| 69.5       | 68.9  | 68.3  | 67.8       | 67.3  | 66.9         | 66.5  |        | 60.9   | 60.4  |
| 64.8       | 64.4  | 63.9  | 63.4       | 62.9  | 62.4         | 61.9  | 61.4   |        |       |
| 60.0       | 59.6  | 59.2  | 58.8       | 58.4  | 58.0         | 57.6  | 57.2   | 56.8   | 56.4  |
| 56.0       | 55.6  | 55.2  | 54.8       | 54.4  | 54.0         | 53.6  | 53.2   | 52.8   | 52.5  |
| 52.1       | 51.7  | 51.4  | 51.0       | 50.6  | 50.3         | 50.0  | 49.6   | 49.3   | 49.0  |
| 48.7       | 48.4  | 48.1  | 47.8       | 47.5  | 47.3         | 47.0  | 46.7   | 46.5   | 46.2  |
| 45.9       | 45.7  | 45.4  | 45.1       | 44.8  | 44.5         | 44.1  | 43.8   | 43.5   | 43.2  |
| 42.9       | 42.6  | 42.3  | 42.1       | 41.8  | 41.5         | 41.3  | 41.0   | 40.8   | 40.5  |
|            | 40.1  | 39.8  | 39.6       | 39.4  | 39.2         | 38.9  | 38.7   | 38.5   | 38.2  |
| 40.3       |       | 37.6  | 37.3       | 37.1  | 36.9         | 36.6  | 36.5   | 36.3   | 36.1  |
| 38.0       | 37.6  | 35.6  | 35.5       | 35.3  | 35.1         | 34.9  | 34.6   | 34.4   | 34.1  |
| 36.0       | 35.8  |       |            |       | 32.8         | 32.6  | 32.5   | 32.3   | 32.2  |
| 33.9       | 33.6  | 33.3  | 33.1       | 32.9  |              | 30.9  | 30.6   | 30.4   | 30.2  |
| 32.1       | 31.9  | 31.8  | 31.6       | 31.3  | 31.1         | 29.3  | 29.2   | 29.1   | 29.0  |
| 30.0       | 29.8  | 29.7  | 29.6       | 29.5  | 29,4         |       | 27.6   | 27.4   | 27.3  |
| 28.8       | 28.6  | 28.5  | 28.3       | 28.1  | 27.9         | 27.7  |        |        |       |
| 27.3       | 27.2  | 27.1  | 27.0       | 27.0  | 26.9         | 26.8  | 26.7   | 26.6   | 26.4  |
| 26.3       | 26.2  | 26.0  | 25,9       | 25.8  | 25.7         | 25.6  | 25.5   | 25.4   | 25.3  |
| 25.2       | 25.1  | 25.1  | 25.0       | 24.9  | 24.6         | 24.6  | 24.5   | 24.4   | 24.3  |
| 24.2       | 24.1  | 24.0  | 23.8       | 23.7  | 23.6         | 23.5  | 23.4   | 23.3   | 23.1  |
| 23.0       | 22.9  | 22.8  | 22.7       | 22.6  | 22.5         | 22.4  | 22.3   | 22.2   | 22.1  |
| 22.0       | 22.0  | 21.9  | 21.8       | 21.7  | 21.7         | 21.6  | 21.5   | 21.4   | 21.3  |
|            | 21.1  | 21.0  | 20.9       | 20.8  | 20.7         | 20.6  | 20.5   | 20.4   | 20.3  |
| 21.2       |       | 20.1  | 20.0       | 19.9  | 19.8         | 19.8  | 19.7   | 19.6   | 19.6  |
| 20.3       | 20.2  |       | 19.3       | 19.2  | 19.1         | 19.0  | 19.0   | 18.9   | 18.8  |
| 19.5       | 19.4  | 19.4  |            |       | 18.3         | 18.2  | 18.1   | 18.0   | 17.9  |
| 18.7       | 18.6  | 18.5  | 18.4       | 18.3  |              | 17.5  | 17.4   | 17.4   | 17.3  |
| 17.8       | 17.7  | 17.7  | 17.6       | 17.6  | 17.5         |       | 16.6   | 16.5   | 16.5  |
| 17.2       | 17.1  | 17.1  | 17.0       | 16.9  | 16.8         | 16.7  |        | 16.0   | 15.9  |
| 16.5       | 16.4  | 16.4  | 16.3       | 16.3  | 16.2         | 16.1  | 16.1   |        |       |
| 15.8       | 15.7  | 15.6  | 15.5       | 15.4  | 15.4         | 15.3  | 15.3   | 15.3   | 15.2  |
| 15.2       | 15.1  | 15.1  | 15.1       | 15.0  | 14.9         | 14.8  | 14.7   | 14.6   | 14.5  |
| 14.4       | 14.4  | 14.3  | 14.2       | 14.2  | 14.1         | 14.1  | 14.0   | 14.0   | 13.9  |
| 13.9       | 13.8  | 13.8  | 13.7       | 13.6  | 13.6         | 13.5  | 13.4   | 13.4   | 13.3  |
| 13.3       | 13.3  | 13.3  | 13.2       | 13.2  | 13.2         | 13.I  | 13.1   | 13.1   | 13.0  |
|            | 12.8  | 12.8  | 12.7       | 12.6  | 12.5         | 12.4  | 12.4   | 12.4   | 12.3  |
| 12.9       |       | 12.1  | 12.1       | 12.1  | 12,0         | 11.9  | 11.9   | 11.9   | 11.8  |
| 12.3       | 12.2  |       |            | 11.5  | 11.5         | 11.4  | 11.4   | 11.3   | 11.3  |
| 11.7       | 11.7  | 11.6  | 11.6       |       | 11.0         | 11.0  | 10.9   | 10.9   | 10.9  |
| 11.2       | 11.2  | 11.1  | 11.1       | 11.1  |              | 10.6  | 10.6   | 10.5   | 10.5  |
| 10.8       | 10.8  | 10.8  | 10.7       | 10.7  | 10.6<br>10.2 | 10.1  | . 10.1 | 10.1   | 10.0  |
| 10.4       | 10.4  | 10.3  | 10.3       | 10.2  |              | 9.7   | 9.7    | 9.7    | 9.6   |
| 10.0       | 9.9   | 9.9   | 9.9        | 9.8   | 9.8          |       | 9.3    | 9.3    | 9.3   |
| 9.6        | 9.6   | 9.5   | 9.5        | 9.4   | 9.4          | 9.4   | 8.9    | 8.9    | 8.9   |
| 9.2        | 9.2   | 9.1   | 9.1        | 9.1   | 9.0          | 9.0   |        |        |       |
| 8.8        | 8.8   | 8.8   | 8.7        | 8.7   | 8.6          | 8.6   | 8.6    | 8.5    | 8.5   |
| 8.4        | 8.4   | B.4   | 8.3        | 8.3   | 8.3          | 8.2   | 8.2    | 8.1    | 8.1   |
| 8.1        | 8.1   | 8.0   | 8.6        | 8.0   | 8.0          | 7.9   | 7.9    | 7.9    | 7.8   |
| 7.8        | 7.7   | 7.7   | 7.6        | 7.6   | 7.5          | 7.5   | 7,4    | 7.4    | 7.4   |
| 7.4        | 7.3   | 7.3   | 7.3        | 7.3   | 7.2          | 7.2   | 7.2    | 7.1    | 7.1   |
| 7.0        | 7.0   | 7.0   | 6.9        | 6.9   | 6.9          | 6.8   | 6.8    | 6.8    | 6.8   |
| 6.8        | 6.7   | 6.7   | 6.7        | 6.7   | 6.6          | 6.6   | 6,6    | 6.5    | 6.5   |
| 6.5        | 6.5   | 6.4   | 6.4        | 6-4   | 6.4          | 6.3   | 6.3    | 6.3    | 6.3   |
| 6.2        | 6.2   | 5.2   | 6.2        | 6.1   | 6.1          | 6.1   | 6.1    | 6.0    | 6.8   |
| 6.0        | 6.0   | 5.9   | 5.9        | 5.9   | 5.9          | 5.8   | 5.8    | 5.8    | 5.8   |
| 5.7        | 5.7   | 5.7   | 5.7        | 5.6   | 5.6          | 5.6   | 5.6    | 5.5    | 5.5   |
|            | 5.4   | 5.4   | 5.4        | 5.4   | 5.4          | 5.4   | 5.4    | 5.3    | 5.3   |
| 5.5<br>5.3 | 5.3   | 5.3   | 5.3        | 5.3   | 5.3          | 5.3   | 5.2    | 5.2    | 5.2   |
|            |       |       |            | 5.1   | 5.1          | 5.0   | 5.0    | 5.0    | 5.0   |
| 5.2        | 5.2   | 5.1   | 5.1<br>4.9 | 4.9   | 4.9          | 4.9   | 4.9    | 4.8    | 4.8   |
| 5.0        | 4.9   | 4.9   |            | 4.7   | 4.7          | 4.6   | 4.6    | 4.6    | 4.6   |
| 4.8        | 4.8   | 4.7   | 4.7        |       |              |       |        | 4.4    | 4.4   |
| 4.5        | 4.5   | 4.5   | 4.5        | 4.4   | 4.4          | 4.4   | 4.4    | 4.3    | 4.3   |
| 4.4        | 4.3   | 4.3   | 4.3        |       | 4.3          | 4.3   | 4.3    |        |       |
| 4.2        | 4.2   | 4.2   | 4.2        |       | 4,1          | 4.1   | 4.1    | 4.0    | 4.0   |
| 4.0        | 4.0   | 4.0   | 4.0        |       | 3.9          | 3.9   | 3.9    | 3.9    | 3.9   |
| 3.8        | 3.8   | 3.8   | 3.8        | 3.8   | 3.7          | 3.7   | 3.7    | 3.7    | 3.7   |
| 3.6        | 3.6   | 3.5   | 3.6        | 3.6   | 3.6          | 3.6   | 3.5    | 3.5    | 3.5   |
| 3.5        | 3.5   | 3.5   | 3.5        | 3.5   | 3.5          | 3.4   | 3.4    | 3.4    | 3.4   |
| 3.4        | 3.4   | 3.4   | 3.3        | 3.3   | 3.3          | 3.3   | 3.3    | 3.3    | 3.3   |
| 3.3        | 3,3   | 3.2   | 3.2        | 3.2   | 3.2          | 3.2   | 3.2    | 3.2    | 3.1   |
| 3.1        | 3.1   | 3.1   | 3.1        | 3.1   | 3.1          | 3.1   | 3.0    | 3.0    | 3.0   |
|            | 3.0   | 3.0   | 3.0        | 3.0   | 2.9          | 2.9   | 2.9    | 2.9    | 2.9   |
| 3.0        |       | 2.8   | 2.8        | 2.8   | 2.8          | 2.8   | 2.8    | 2.8    | 2.8   |
| 2.9        | 2.9   |       |            |       | 2.8          | 2.7   | 2.7    | 2.7    | 2.6   |
| 2.8        | 2.7   | 2.7   | 2.7        | 2.7   | 2.7          | 2.5   | 2.6    | 2.6    | 2.6   |
| 2.5        | 2.6   | 2.6   | 2.6        | 2.6   |              |       | 2.5    | 2,5    | 2.5   |
| 2.6        | 2.6   | 2.6   | 2.6        | 2.6   | 2.5          | 2.5   |        |        |       |
| 2.5        | 2.5   | 2.5   | 2.4        | 2.4   | 2.4          | 2.4   | 2.4    | 2.4    | 2.4   |
| 2.3        | 2.3   | 2.3   | 2.3        | 2.3   | 2.3          | 2.3   | 2.3    | 2.3    | 2.3   |
|            |       |       |            |       |              |       |        |        |       |

```
2.3
2.3
          2.3
                    2.3
                               2.3
```

HYDROGRAPH AT STATION

4.55, TOTAL EXCESS = 2.92 7.46, TOTAL LOSS = TOTAL RAINFALL -

MAXIMUM AVERAGE FLOW TIME PEAR FLOW 72-HR 6-KR 24-HR

(HR) (CFS) (CFS)

103. 45. 20. 154.75 158. 1.456 1.968 2.916 (INCHES) 0.837 (AC-FT) 51. 89. 121. 179.

> CUMULATIVE AREA = 1.15 SO MI

301 KK

302 IN

TIME DATA FOR INPUT TIME SERIES

JXMIN 50 TIME INTERVAL IN MINUTES

JXDATE 31DEC99 STARTING DATE JXDATE JXTIME

STARTING TIME 2400

SUBBASIN CHARACTERISTICS 329 BA

0.84 SUBBASIN AREA TAREA.

PRECIPITATION DATA

SUBBASIN RUNOFF DATA

STORM 7.46 BASIN TOTAL PRECIPITATION 304 PB

UNIFORM LOSS RATE 330 LU

STRTL 0.20 INITIAL LOSS UNIFORM LOSS RATE CNSTL

PERCENT IMPERVIOUS AREA RTIMP 2.00

INPUT UNITGRAPH, 472 ORDINATES, VOLUME = 1.00 329 ffT 2.8 40.1 83.6 5.6 44.3 8.4 49.0 11.3 53.5 27.5 31.6 35.9 15.3 19.4 23.4 65.9 117.1 181.7 58.2 107.0 62.5 112.1 69.4 122.7 72.8 129.0 77.2 135.2 89.9 96.2 102.0 141.5 210.7 160.9 167.5 242.4 174.4 251.1 154.4 188.9 196.1 203.4 259.9 269.1 218.0 225.4 305.9 314.4 331.5 342.4 323.0 334.1 336.1 338.2 340.2 341.4 333.8 342.5 343.5 330.9 324.1 254.3 317.3 247.5 275.6 268.5 310 5 303.7 296.6 289.6 282.6 228.9 187.7 223.7 219.8 178.6 215.9 212.0 241.3 175.2 183.2 172.4 208.1 204.3 200.4 196.6 192.3 158.0 131.5 155.1 129.1 152.1 126.8 163.9 160.9 149.1 146.0 143.0 124.5 140.6 138.3 136.1 133.8 118.3 116.3 114.2 97.0 112.1 109.9 107.9 106.5 105.0 103.6 102.1 89.9 94.0 91.3 95.3 85.7 74.3 75.2 84.3 83.1 81.8 80.5 79.3 78.3 76.2 71.4 62.2 68.1 67.2 66.3 65.4 64.6 57.0 61.4 60.6 59.0 58.2 57.6 63.7 63.0 59.8 54.2 47.4 52.4 46.7 55.9 55.1 53.3 51.9 51.5 51.0 47.0 46.3 45.9 45.3 49.7 48.9 48.1 50.5 44.7 42.8 39.1 42.4 38.7 41.6 37.9 44.1 43.5 43.3 43.0 42.0 41.1 40.4 40.1 39.8 39.5 37.1 33.9 36 7 36 3 36.0 35.6 35.3 35.0 34.7 34.5 34.2 33.5 32.8 32.5 32.2 31.6 33.2 30.4 27.7 29.2 28.6 30.9 30.7 30.1 29.8 28.3 27.2 26.9 26.6 26.3 26.2 28.1 24.4 24.0 23.9 25.8 25.6 25.3 25.0 24.7 24.3 24.2 23.5 23.2 22.3 20.7 21.7 19.9 21.5 19.7 22.9 22.7 22.5 22.1 22.0 20.4 21.1 21.0 20.9 20.2 19.4 17.6 19.2 19.0 17.4 18.1 16.7 19.5 18.8 18.6 18.5 18.3 18 0 17.2 17.1 17.0 16.9 17.8 16.4 16.2 16.0 15.9 15.8 15.6 15.5 15.4 15.2 15.1 14.2 12.9 14.1 12.8 13.6 13.4 13.3 13.1 13.0 13.5 12.7 12.6 11.0 10.9 10.7 10.6 10.5 11.2 11.1 10.8 10.4 10.4 9.9 9.8 8.9 10.3 10.2 10.1 10.0 9.7 9.6 9.5 9.4 9.3 8.5 7.9 8.9 8.8 8.7 9,2 9.1 8.6 8.5 8.4 7.8 8.4 7.7 8.3 7.6 8.2 7.5 8.0 7.8 7.4 7.4 7.3 5.7 7.2 7.0 7.0 6.9 6.9 6.9

6.3

6.3

6.3

€.2

6.0 5.5 5.1 4.6 4.2 3.9 3.6 5.9 5.5 5.0 4.6 4.2 3.9 3.6

\*\*\* \*\*\*

HYDROGRAPH AT STATION ES

7.46, TOTAL LOSS = 4.55, TOTAL EXCESS = 2.92 TOTAL RAINFALL =

MAXIMUM AVERAGE FLOW PEAK FLOW 259.85-HR (HR) (CFS) 6. 2.916 131. 34. 1.484 67. 15. 1.969 88. 85. 0.945 42. 161. 153.62

CUMULATIVE AREA -

(AC-FT)

15CROS 380 KK

HYDROGRAPH COMBINATION 382 HC

3 NUMBER OF HYDROGRAPHS TO COMBINE ICOMP

HYDROGRAPH AT STATION ISCROS

MAXIMUM AVERAGE FLOW TIME FEAK FLOW 259.85-HR 6-HR 24-HR 72-HR (CFS) (BR) (CFS) 106. 1.466 47. 1.968 19. 2.916 153.85 255. 415. (INCHES) 0.883 210.

> CUMULATIVE AREA = 2.69 SQ MI

> > RUNOFF SUMMARY
> > FLOW IN CUBIC PEET PER SECOND
> > TIME IN HOURS, AREA IN SQUARE MILES

|          |               |         | PEAK  | TIME OF<br>PEAK | average fl | OW FOR MAXIME | M PERIOD | hasin<br>Area | Maximum<br>Stage | TIME OF<br>MAX STAGE |
|----------|---------------|---------|-------|-----------------|------------|---------------|----------|---------------|------------------|----------------------|
| +        | OPERATION     | STATION | FL/OW | PEAL            | 6-HOUR     | 24-HOUR       | 72-HOUR  | Aren          | SIMOL            | AMALO AMA            |
| 4        | HYDROGRAPH AT | E2      | 52.   | 153.58          | 28.        | 11.           | 5.       | 0.27          |                  |                      |
| +        | HYDROGRAPH AT | El      | 127.  | 153.78          | 70.        | 28.           | 12.      | 0.70          |                  |                      |
| •        | HYDROGRAPH AT | E4      | 158.  | 154.75          | 103.       | 45.           | 20.      | 1.15          |                  |                      |
| +        | HYDROGRAPH AT | E5      | 161.  | 153.62          | 85.        | 34.           | 15.      | 0.84          |                  |                      |
| <b>,</b> | 3 COMBINED AT | ISCROS  | 415.  | 153.85          | 255.       | 106.          | 47.      | 2.69          |                  |                      |

\*\*\* NORMAL END OF HEC-1L \*\*\*

## 7. APPENDIX B -

**Ultimate Conditions SacCalc Model** 

INPUT FILENAME ====>J:\Jobs\1116-GreenbriarFarms\1116-GreenbriarFarms\Civil\Docs\Report\SACCALC\Developed\sc.dat
OUTPUT FILENAME ===>J:\Jobs\1116-GreenbriarFarms\1116-GreenbriarFarms\Civil\Docs\Report\SACCALC\Developed\sc.hecout
DSS FILENAME ===>hcalc.dss

| * |
|---|
| * |
| • |
| * |
|   |
| * |
| * |
|   |

\* U.S. ARMY CORPS OF ENGINEERS

\* HYDROLOGIC ENGINEERING CENTER

\* 609 SECOND STREET

\* DAVIS, CALIFORNIA 95616

\* (916) 756-1104

| х        | х | XXXXXXXXX | XXXXX |   |       | x   |      |
|----------|---|-----------|-------|---|-------|-----|------|
| x        | X | x         | х     | X |       | XX  | X    |
| x        | x | x         | х     |   |       | x   | x    |
| XXXXXXXX |   | XXXX      | x     |   | XXXXX | x   | x    |
| X        | х | x         | х     |   |       | X   | х    |
| X        | x | x         | x     | x |       | x   | x    |
| X        | x | XXXXXX    | XXXXX |   |       | XXX | XXXX |

Special version of HEC-1 with Extra-large array Modified by David Ford Consulting Engineers (2000) Program dimensions: Number of hydrograph ordinates: 20000 Unit hydrograph ordinates: 3000

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HECIGS, HECIDB, AND HECIKM.

THE DEFINITIONS OF VARIABLES -RTIME- AND -PTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKX- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTHAM77 VERSION NEW OPTIONS: DAMREAX OUTFLOW SUBMERGENCE . SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEWATIC WAVE. NEW FINITE DIFFERENCE ALGORITHM

PAGE 1 HEC-3L INPUT ID.....1.....2......3.....4......5,.....6......7.....8......9......10 LINE \* SacCalc, developed by David Ford Consulting Engineers File generated 07/12/2005 19:20:26 ID 10010 & 1010 &10024&1024 \* Lag computation for station A \* Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl Lag frequency factor of 1.0 (Table 7-6) for frequency massin \*n\* composition (based on Table 7-1)

Developed

n adj n fract

0.030 0.0300 0.0000 0.067 0.0670 0.0000

0.031 0.0310 0.3757 0.070 0.0700 0.0000 0.030 0.0300 0.0000 0.031 0.0310 0.3757 0.070 0.0700 0.0000 0.071 0.0710 0.0000 0.032 0.0320 0.0000 0.033 0.0330 0.0000 0.0000 0.072 0.0720 0.0000 0.073 0.0730 0.034 0.0340 0.0350 0.1751 0.0370 0.0000 0.074 0.076 0.035 0.0740 0.0000 0.0000 0.037 0.040 0.0400 0.1337 0.0420 0.0000 0.0800 0.080 0.1350 0.0840 0.0000 0.084 0.046 0.0450 0.0000 0.088 0.090 0.050 0.0500 0.0000 0.0900 0.0000 0.0930 0.0000 0.053 0.0530 0.0000 0.0560 0.0000 0.056 0.096 0.0960 0.0000 0.100 0.1000 0.060 0.065 0.0650 0.0414 0.070 0.0700 0.0856 0.0414 0.110 0.0535 0.115 0.1150 0.0000 0.075 0.0750 0.0000 0.120 0.1200 0.0000 0.080 0.0800 0.0000 0.150 0.1500 0.0000 Equation (7-1) with L= 0.6705, Lc= 0.2765, S= 13.200, n=0.0485

Resulting lag: 28.3 minutes

Lag computation for station B

Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl

Basin \*n\* composition (based on Table 7-1)

Developed

Undeveloped

Developed

> 0.070 0.0700 0.0000 0.071 0.0710 0.0000 0.072 0.0720 0.0000 0.073 0.0730 0.0000

 n
 adj n
 fract
 n
 adj n
 fract

 0.030
 0.0300
 0.0000
 0.067
 0.0670
 0.0000

 0.031
 0.0310
 0.0000
 0.070
 0.0700
 0.0000

0.031 0.0310 0.0000 0.032 0.0320 0.0000 0.033 0.0330 0.0000 0.034 0.0340 0.0000

```
0.074 0.0740 0.0000
      0.035 0.0350 0.7942
       0.037
              0.0370
                       0.0000
                                      0.076 0.0760
                                                       0.0000
                                       0.080 0.0800
                                                       0.0000
       0.040
                                              0.0840
                                      0.084
       0.042
               0.0420
                       0.0000
                                       0.088
                                              0.0880
                                                       0.0000
               0.0460
       0.046
                                              0.0900
                                       0.090
       0.050
               0.0500
                        0.0000
                          0000
                                       0.093
                                              0.0930
                                                       0.0000
       0.053
                                       0.096
       0.056
              0.0560
                       0.0000
               0.0600
                        0.0000
                                       0.100
                                             0.1000
                                                       0.0000
                                       0.110
                                             0.1100
0.1150
                                                        0.0000
                        0.1480
       0.065
               0.0650
                                                       0.0144
       0.070
              0.0700
                       0.0144
                                       0.115
                                       0.120 D.1200
                                                        0.0000
              0.0750
                        0.0000
       0.075
                                       0.150 0.1500 0.0000
       0.080 0.0800 0.0000
     _____
   Equation (7-1) with L= 0.3504, Lc= 0.1186, S= 13.200, n=0.0412
* Resulting lag: 14.7 minutes
* Lag computation for station C
   ag computation for station (
Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl
Basin "n" composition (based on Table 7-1)
Developed
Dindeveloped
Dind in fract
Developed
Dind in fract
   Developed
n adj n fract
                                           n adjn
                                                         fract
       0.030 0.0300 0.0000
0.031 0.0310 0.0000
                                       0.067 0.0670
                                                        0.0000
                                       0.070
                                              0.0700
0.0710
                                                        0.0000
                                                        0.0000
       0.032
              0.0320
                        0.000
                                       0.072
                                               0.0720
                                                        0.000
               0.0330
                        0.0000
       0.033
                                              0.0730
                                                        0.0000
                                       0.073
       0.034
               0.0340
                        0.0000
                        0.6675
       0.035
               0.0350
                                       0.074
                                              0.0740
                                                        0.0000
                                       0.076
                                               0.0760
                                                        0.0000
       0.037
               0.0370
       0.040
               0.0400
                        0.0914
                                       0.080
                                              0.0800
                                                        0.1015
                                       0.084 0.0840
0.088 0.0880
                        0.0000
                                                        0.0000
       0.042
               0.0420
                                                        0.0000
       0.046
               0.0460
                        0.0000
                                       0.090 0.0900
0.093 0.0930
               0.0500
                                                        0.0000
       0.050
                        0.0000
                                                        0.0000
       0.053
               0.0530
                        0.0000
       0.056
                        0.0000
                                       0.096
                                               0.0960
                                                        0.0000
                                                        0.0000
                                       0.100
       0.060
               0.0600
                        0.0000
       0.065
               0.0650
                        0.1041
                                       0.110 0.1100
                                                        0.0000
                        0.0178
                                       0.115
                                                        0.0178
               0.0700
       0.070
                                                        0.0000
       0.075 0.0750
0.080 0.0800
                                       0.120 0.1200
                        0.000
                                       0.150 0.1500
                                                       0.0000
                        0.0000
   Equation (7-1) with L= 0.4465, Lc= 0.1420, S= 13.200, n=0.0452 Resulting lag: 18.6 minutes
 Lag computation for station D
Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl
    Basin "n" composition (based on Table 7-1)

Developed Undeve
    Developed Undeveloped n adj n fract n adj n frac
                                             Undeveloped
      0.030 0.0300 0.0000
0.031 0.0310 0.0000
                                                        0.0000
                                       0.067 0.0670
                                       0.070 0.0700
                                                       0.0000
                        0.0000
                                       0.071
                                               0,0710
                                                        0.0000
              0.0320
       0.032
       0.033
               0.0330
                                                        0.0000
                        0.000
                                       0.072
                                               0.0720
                        0.0000
                                       0.073
                                               0.0730
                                                        0.0000
                                               0.0740
                                                        0.0000
                                       0.074
       0.035
               0.0350
                        0.3054
       0.037
               0.0370
                        0.0000
                                       0.076
                                               0.0760
                                                          0000
                                       0,080
                                               0.0800
                                                          .0000
       0.040
               0.0400
                        0.4966
       0.042
               0.0420
                        0.0000
                                       0.084
                                               0.0840
                                                        0.0000
       0.046
               0.0460
                        0.0000
                                       880.0
                                               0.0880
                                                          0000
                                                          .0000
                                       0.090
                                               0.0900
       0.050
               0.0500
                        0.0000
       0.053
               0.0530
                        0.0000
                                       0.093
                                               0.0930
                                                        0.0000
                                       0.096
                                               0.0960
                        0.0000
       0.056
               0.0560
       0.060
               0.0600
                        0.0000
                                       0.100
                                               0.1000
                                                        0.0000
                                                          . 0000
                        0.1443
       0.065
              0.0650
       0.070
              0.0700
                        0.0201
                                       0.115
                                              0.1150
                                                        0.0336
                                       0.120
       0.075
                                              0.1200
                                                        0.0000
                                       0.150 0.1500
                                                       0.0000
       0.080 0.0800
                       0.0000
 Equation (7-1) with L= 0.4555, Lc= 0.1290, S= 13.200, n=0.0452
Resulting lag: 18.1 minutes
Lag computation for station E
Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl
   Basin *n* composition (based on Table 7-1)
Developed Undeveloped
                Developed
                         .u
fract
           n adjo
                                           n adj n
                                                         fract
    ______
       0.030 0.0300
                        0.2282
                                       0.067 0.0670
                                                       0.0000
                                       0.070
       0.031 0.0310
                        0.0000
       0.032
               0.0320
                        0.0000
                                       0.071
                                               0.0710
                                                        0.0000
                        0.0000
                                       0.072
                                               0.0720
                                                          .0000
       0.033
               0.0330
                                                        0.0000
       0.034
               0.0340
                        0.0000
                                       0.073
                                               0.0730
                        0.3983
                                       0.074
                                               0.0740
                                                          . 0000
       0.035
               0.0350
                                               0.0760
                                                          .0000
       0.037
               0.0370
                        0.0000
                                       0.076
       0.040
               0.0400
                        0.2075
                                       0.080 0.0800
                                                          aooa
                                               0.0840
                                                        0.0000
       0.042
               0.0420
                        0.0000
                                       0.084
       0.046
               0.0450
                        0.0000
                                       0.088
                                              0.0880
                                                        0.0000
                                       0.090
                                               0.0900
               0.0500
                        0.0000
       0.050
       0.053
               0.0530
                        0.000
                                       0.093
                                              0.0930
                                                        0.0000
                        0.0000
                                       0.096
                                               0.0960
                                                          0000
               0.0560
       0.056
       0.60
               0.0600
                        0.0000
                                       0.100
                                               0.1000
                                                        0.0000
               0.0650
                        0.1660
                                               0.1100
                                                          0000
       0.065
       0.070
              0.0700
                       0.0000
                                       0.115 0.1150
                                                        0.0000
                                       0.120 0.1200
0.150 0.1500
                                                        0.000
                                                       0.0000
       0.080 0.0800
                       0.0000
```

```
Equation (7-1) with L= 3.3797, Lc= 0.1150, S= 10.560, n=0.0399
 Resulting lag: 15.0 minutes
Lag computation for station F
     Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl
    Lag frequency factor of 1.0 (Table 7-7)
Basin "n" composition (based on Table 7-1)
Developed Undeveloped
                Developed
    Developed Undevelope
n adj n fract n adj n
                                                      fract
                                 0.067 0.0670 0.0000
                      0.0000
       0.030 0.0300
                                      0.070 0.0700
                                                      0.0000
       0.031 0.0310 0.0000
                                      0.071 0.0710
       0.032 0.0320 0.0000
                                                      0.0000
                        0.0000
                                      0.072
                                             0.0720
                                                      0.0000
       0.033
               0.0330
                                                      0.0000
       0.034
               0.0340
                        0.0000
                                      0.073
                                             0.0730
               0.0350
                                      0.074 0.0740
                                                      0.0000
       0.035
                        0.0000
                                      0.076 0.0760
                                                      0.0000
       0.037
               0.0370
                       0.0000
                                             0.0800
0.0840
                                      0.080
                                                      0.0000
       0.040
               0.0400
                                                      0.0000
       0.042
               0.0420
                        0.0000
                                      0.084
               0.0460
       0.046
                        0.0000
                                      0.088 0.0880
                                                      0.0000
                                      0.090 0.0900
       0.050
               0.0500
                        0.0000
       0.053
               0.0530
                        0.0000
                                      0.093 0.0930
                                                      0.0000
                                      0.096
                                             0.0960
                        0.0000
       0.056
               0.0560
        0,060
               0.0600
                       0.0000
                                      0.100 0.1000
                                                      0.0000
                                      0.110
                                             0.1100
                                                      0.0000
               0.0650 0.0000
       0.065
       0.070
               0.0700 0.0051
0.0750 0.0000
                                      0.115 0.1150
                                                      0.0051
                                      0.120 0.1200
0.150 0.1500
               0.0750
                                                      0.0000
                                                      0.0000
       0.080 0.0800
                       0.0000
    Equation (7-1) with L= 0.3589, Lc= 0.1383, S= 10.560, n=0.0405
  Resulting lag: 15.9 minutes
Lag computation for station G
Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl
    Basin "n" composition (based on Table 7-1)
                         ed Undeveloped fract n adj n fr
        Developed
n adj n fract
                                                  jn fract
                                 0.067 0.0670
      0.030 0.0300
0.031 0.0310
                      0.0000
                                      0.070 0.0700
0.071 0.0710
                        0.0000
                                                     0.0000
       0.032 0.0320
                      0.0000
        0.033
               0.0330
                        0.0000
                                      0.072 0.0720
                                                      0.0000
                        0.0000
                                      0.073
                                             0.0730
                                                       0.0000
       0.034
               0.0340
                                                      0.0000
       0.035
               0.0350
                        0.0000
                                      0.074
                                             0.0740
        0.037
                        0.0000
                                      0.076 0.0760 0.0000
0.080 0.0800 0.0000
                       0.7583
       0.040
               0.0400
               0.0420
                       0.0000
       0.042
                                      0.084 0.0840
                                                      0.0000
                                      0.088
                                             0.0880
                                                       0.0000
       0.046
       0.050
               0.0500
                       0.0000
                                      0.090 0.0900
                                                      0.0000
               0.0530
                       0.0000
                                      0.093 0.0930
                                                       0.0000
       0.053
                                      0.096 0.0960
                                                      0.0000
       0.056
               0.0560 0.0000
               0.0600
                        0.0000
                                      0.100 0.1000
0.110 0.1100
                                                      0.000
       0.060
                                                      0.0000
                       0.1730
       0.065
               0.0650
                                      0.115 0.1150
0.120 0.1200
        0.070
               0.0700
                       0.0433
                                                      0.0254
                                                       0.0000
       0.075
               0.0750
                       0.0000
                                      0.150 0.1500 0.0000
      0.080 0.0800 0.0000 0.150
Developed Undeveloped n adj n fract n adj n frac
                                                       fract
                      0.0000 0.067 0.0670 0.0000
0.0000 0.070 0.0700 0.0000
       0.031 0.0310
       0.032
               0.0320
                       0.0000
                                      0.071 0.0710
                                                      0.0000
                       0.0000
                                      0.072 0.0720
       0.033
               0.0330
       0.034
               0.0340
                       0.0000
                                      0.073 0.0730
                                                      0.0000
                                      0.074
                                             0.0740
       0.035
               0.0350
                                                      0.0000
       0.037
               0.0370
                       0.0000
                                      0.076 0.0760
                       0.6798
                                      0.080 0.0800
                                                      0.0845
                                      0.084 0.0840
                       0.0000
       0.042
               0.0420
       0.046
              0.0460
                       0.0000
                                      0.088 0.0880
                                                      0.0000
                                      0.090
                                             0.0900
                       0.0000
                                                      0.0000
       0.053
               0.0530
                       0.0000
                                      0.093 0.0930
                                                      0.0000
               0.0560
                       0.0000
                                      0.096
                                             0.0960
       0.056
       0.060 0.0600 0.0000
                                      0.100 0.1000
                                                      0.0000
       0.065
               0.0650
                       0.0000
                                      0.110 0.1100
0.115 0.1150
                                                      0.0000
                       0.0578
                                                      0.0564
       0.070
              0.0700
                                      0.120 0.1200 0.0000
0.150 0.1500 0.0000
       0.075
               0.0750
                       0.0000
       0.080 0.0800 0.0000
 Equation (7-1) with L= 0.5178, Lc= 0.2131, S= 10.560, n=0.0487 Resulting lag: 25.4 minutes Lag computation for station I
   ag computation for station 1
Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl Basin "n" composition (tased on Table 7-1)

Developed Undeveloped
          Develope
n adj n fract
                                          n adjn
                                                       fract
      0.030 0.0300 0.0000 0.067 0.0670 0.0000 0.031 0.0310 0.0000 0.070 0.0700 0.0000
      0.032 0.0320 0.0000
0.033 0.0330 0.1959
                                      0.071 0.0710
                                                      0.0000
                                      0.072 0.0720 0.0000
                                      0.073 0.0730 0.0000
      0.034 0.0340 0.0000
       0.035 0.0350 0.0591
                                     0.074 0.0740 0.0000
```

```
0.037 0.0370 0.0000
                                         0.076 0.0760 0.0000
                                                           0.0000
                                         0.080 0.0800
       0.040
               0.0400
                         0.5083
        0.042
                0.6426
                         0.0000
                                         0.084 0.0840
                                                           0.0000
                                         0.088
                                                 0.0880
                                                           0.0000
                         0.0000
       0.046
                0.0460
        0.050
                0.0500
                         0.0000
                                         0.00
                                                 0.0900
                                                           0.0000
                                         0.093
                                                 0.0930
                                                           0.0000
                          0.0000
                0.0530
        0.053
                                                           0.0000
        0.056
                0.0560
                         0.0000
                                         0.095
                                                 0.0960
                                         0.100
                                                0.1000
                                                           0.0000
        0.060
                0,0600
                                                0.1100
        0.065
                0.0650
                         0.2089
                          0.0092
                                         0.115
                                                0.1150
                                                           0.0185
        0.070
                                         0.120
                                                0.1200
                         0.0000
        0.075
                0.0750
        0.080
               0.0800
                         0.0000
                                         0.150 0.1500 0.0000
   Equation (7-1) with L= 0.6780, Lc= 0.3822, S= 10.560, n=0.0452 Resulting lag: 30.6 minutes
Lag computation for station J
   ag computation for station J
Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl
Basin "n" composition (based on Table 7-1)
Developed
Undeveloped
n adj n fract
n adj n fract
                                   0.067 0.0670 0.0000
       0.030 0.0300
                                         0.070 0.0700
       0.031 0.0310 0.0000
        0.032
                0.0320
                          0.0000
                                         0.071 0.0710
                                                           0.0000
                                         0.072
                0.0330
                          0.6964
        0.033
        0.034
                0.0340
                         0.0000
                                         0.073 0.0730
                                                           0.0000
                          0.0000
                                         0.074 0.0749
0.076 0.0760
                                                           0.0000
                0.0350
        0.035
                                                           0.0000
        0.037
                0.0370
                          0.0000
                                         0.080
                0.0400
                          0.1164
                                                0.0800
                                                           0.0545
        0.040
                                                  0.0840
        0.042
                0.0420
                          0.0000
                0.0460
        0.046
                          0.0000
                                         0.088 0.0880
                                                           0.0000
                                         0.090
                          0.0000
        0.050
        0.053
                0.0530
                                                           0.0000
                          0.000
                                         0.093 0.0930
                                                  0.0960
                          0.0000
                                          0.096
                                                           0.0000
                                                            0.0000
               0.0600
                                         0,100
        0.060
                          0.0000
                                         0.110 0.1100
0.115 0.1150
                          0.0000
                                                           0.0000
        0.065
        0.070 0.0700
                         0.0091
                0.0750 0.0000
                                         0.120 0.1200
                                                           0.0000
                                         0.150 0.1500
        0.080 0.0800 0.0000
    Equation (7-1) with L= 0.5758, Lc= 0.2036, S= 10.560, n=0.0371 Resulting lag: 19.3 minutes
 Rquation (7-1) with December 19: 19:3 minutes
Lag computation for station X
Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl
Basin "n" composition (based on Table 7-1)
Developed Undeveloped
n adj n fract n adj n fract
       0.030 0.0300 0.0000
0.031 0.0310 0.0000
                                         0.070 0.0700
                                                          0.0000
                                         0.071 0.0710
                                                           0.0000
        0.032 0.0320
                         0.0000
                         0.0000
        0.033
                                         0.072 0.0720
                                                           0.0000
                                         0.073
        0.034
                0.0340
        0.035
                0.0350
                         0.6104
                                         0.074
                                                  0.0740
                                                           0.0000
                                         0.076
                                                            0.000
                0.0370
                          0.0000
        0.037
        0.040
                0.0400
                          D.0248
                                         0.080 0.0800
                                                           0.0521
                                         0.084
        0.042
                          0.0000
                                                  0.0840
                                                           0.0000
                                                  0.0880
                                                            0.0000
        0.046
                0.0460
                          0.0000
        0.050
                0.0500
                          0.0000
                                         0.090
                                                 0.0900
                                                           0.0000
                                         0.093
                0.0530
                          0.0000
        0.053
        0.056
                0.0560
                          0.0000
                                         0.096
                                                  0.0960
                                                           0.0000
        0.060
                0.0600
                          0.0000
                                          0.100
                                                  0.1000
                                                            0.0000
                                         0.110
                                                  0.1100
                                                            0.0000
        0.065
                0.0650
                         0.2481
                                         0.115 0.1150
0.120 0.1200
                                                           0.0248
        0.075 0.0750
                         0.0000
                         0.0000 0.150
        0.080 0.0800
                                         0.150 0.1500
                                                           0.0000
       .....
    Equation (7-1) with L= 0.4909, Lc= 0.2286, S= 10.560, n=0.0483
* Equation (7-1) with L= 0.4909, Lc= 0.2286, S= 10.560, n=0.0483

* Resulting lag: 24.8 minutes

* Lag computation for station L

* Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl

* Basin *n* composition (based on Table 7-1)

Developed Undeveloped

* n adj n fract n adj n fract
      0.030 0.0300 0.0000 0.067 0.0670
0.031 0.0310 0.0000 0.070 0.0700
                                                          0.000
       0.031 0.0310
0.032 0.0320
                                                           0.0000
                                         0.071
                         0.0000
                                                  0.0710
                                                           0.0000
                                                0.0720
                                                           0.0000
       0.033
                0.0330
                         0.0000
                0.0340
                         0.000C
1.000C
        0.034
                                         0.073 0.0730
                                                           0.0000
                                         0.074
       0.035
        0.037
                0.0370
                          0.0000
                                         0.076 0.0760
                                                           0.0000
                          0.0000
                                         0.080
        0.040
                0.0400
       0.042
                0.0420
                          0.0000
                                         0.084 0.0840
                                                           0.0000
                          0.0000
                                         880.0
                                                 0.0880
                                                            0.0000
       0.046
                0.0460
       0.050
                0.0500
                          0.0000
                                         0.090
                                                 0.0900
                                                           0.0000
        0.053
                0.0530
                          0.0000
                                         0.093
                                                 0.0930
                                                           0.0000
                                         0.096
                                                           0.0000
       0.056
                0.0560
                          0.0000
                                                 0.0960
                                                 0.1000
                0.0600
                          0.0000
                                         0.100
                                                           0.0000
                                                           0.0000
                                         0.110
       0.065
                0.0650
                          0.0000
        0.070
                0.0700
                          0.0000
                                         0.115
                                                0.1150
                                                           0.0000
       0.075
               0.0750
                         0.0000
                                         0,120 0.1200
                                                           0.0000
       0.080 0.0800
                        0.0000
                                         0,150 0.1500 0.0000
   Equation (7-1) with L= 0.2784, Lc= 0.0848, S= 10.560, n=0.0350
```

```
Resulting lag:
* Lag computation for station M

* Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl

* Basin *n* composition (based on Table 7-1)
                                                 Undeveloped
                  Developed
     n adj n fract
                                                              fract
                                     0.067 0.0670 0.0090
0.070 0.070
        0.030 0.0300
                          1.0000
        0.031 0.0310 0.0000
        0.032
                0.0320
                          0.0000
                                          0.071
                                                   0.0710
                                                             0.0000
                                           0.072
                                                                0000
        0.033
                0.0340
                          0.0000
                                          0.073
                                                   0.0730
                                                             0.0000
                                           0.074
                                                                .0000
                0.0350
                          0.0000
        0.035
                                                             0.0000
        0.037
                 0.0370 0.0000
                                           0.076
                                                   0.0760
                           0.0000
                                           0.080
                                                   0.0800
                                                                .0000
                 0.0400
        0.040
                                                             0.0000
        0.042
                 0.0420 0.0000
                                          0.084
                                                   0.0840
                 0.0460
                                           0.088
                                                   0.0880
                                                             0.0000
        0.046
                                                   0.0900
                                                             0.0000
                                           0.090
        0.050
                0.0500
                          0.0000
                                                   0.0930
                 0.0530
                           0.0000
                                           0.093
                                                             0.000
        0.053
                                                              0.0000
                                           0.096
        0.056
                 0.0560
                           0.0000
                 0.0600
                           0.0000
                                           0.100
                                                   0.1000
                                                             0.0000
                                           0.110
                0.0650 0.0000
        0.065
        0.070
                0.0700 0.0000
                                           0.115
                                                   0.1150
                                                             0.0000
                 0.0750
                           0.0000
                                                   0.1200
                                                             0.0000
        0.075
                                                             0.0000
                                          0.150 0.1500
        0.080 0.0800 0.0000
 Equation (7-1) with L= 0.8854, Lc= 0.4290, S= 4.752, n=0.0300
Resulting lag: 26.3 minutes
Lag computation for station N
    Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl Basin "n" composition (based on Table 7-1)

Developed Undeveloped
     Developed Undevelon adj n fract n adj n
                                                              fract
                                      0.067 0.0670
       0.030 0.0300 0.0000
0.031 0.0310 0.0000
                                                             0.0000
                                           0.070 0.0700 0.0000
0.071 0.0710 0.0000
        0.032 0.0320 0.0000
        0.033
                 0.0330
                           0.0000
                                           0.072
                                                   0.0720
                                                             0.0000
                                           0.073
                                                    0.0730
                           0.0000
        0.034
                 0.0340
        0.035
                 0.0350
                           0.2500
                                           0.074
                                                   0.0740
                                                             0.0000
                           0.0000
                                           0.076
                                                                .0000
                 0.0370
        0.037
        0.040
                0.0400
                           0.4917
                                           0.080
                                                   0.0800
                                                             0.0000
                 0.0420
                           0.0000
                                           0.084
                                                   0.0840
                                                              0.000
        0.042
                                                              0.0000
        0.046
                 0.0460
                           0.0000
                                           0.088
                                                   0.0880
                 0.0500
                           0.0000
                                           0,090
                                                   0.0900
                                                             0.0000
                          0.0000
                                           0.093
                                                   0.0930
                0.0530
        0.053
                0.0560
        0.056
                           0.0000
                                           0.096
                                                   0.0960
                                                             0.0000
                           0.0000
                                           0.100
                                                    0.1000
                                                              0.0000
        0,060
                                                   0.1100
        0.065
                0.0650
                          0.1708
                                           0.110
                                                              0.0000
                                                              0.0000
                                           0.115
        0.070
                                                             0.0000
        0.075
                0.0750 0.0000
                                           0.129
                                                   0.1200
    0.080 0.0800 0.0000 0.150 0.1500 0.0000

Equation (7-1) with L= 0.4350, Lc= 0.1388, S= 10.560, n=0.0456
 Equation (7-1) with L= 0.4350, Lc= 0.1388, S= 10.560, n=0.0458

Resulting lag: 19.1 minutes

Lag computation for station 0

Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl

Basin "n* composition (based on Table 7-1)

Developed

Undeveloped

adj n fract

n adj n fract

10.560, n=0.0458

Undeveloped

The composition (based on Table 7-1)
        0.030 0.0300 0.0000 0.067 0.0670 0.0000 0.031 0.0310 0.0000 0.070 0.0700 0.0000
                          0,0000
                0.0320
                                           0.071
                                                   0.0710
                                                             0.0000
                                           0.072
                                                   0.0720
                                                             0.0000
        0.033
                0.0330
        0.034
                0.0340
                          0.0000
                                          0.073
                                                   0.0730
                                                             0.0000
                           0.0000
                                           0.074
                                                   0.0740
                0.0350
        0.037
                 0.0370
                          0.0000
                                          0.076
                                                   0.0760
                                                             0.0000
                0.0400
                                                   0.0800
                                                             0.0000
                           1.0000
        0.042
                0.0420
                           0.0000
                                           0.084
                                                   0.0840
                                                             0.0000
                                          0.088
                                                   0.0880
                 0.0460
                           0.0000
                                                                0000
                                                             0.0000
                0.0500
                           0.0000
        0.050
        0.053
                0.0530
                          0.000
                                          0.093
                                                   0.0930
                                                             0.0000
                0.0560
                          0.0000
                                           0.096
                                                   0.0960
        0.056
        0.060
                0.0600
                          0.0000
                                          0.100
                                                   0.1000
                                                             0.0000
                                          0.110
                 0.0650
                          0.0000
        0.065
                                                   0.1150
                                                             0.0000
        0.070
                0.0700
                          0.0000
                0.0750
                          6.0000
                                           0.120 0.1200
                                                             0.000
                                          0.150 0.1500
        0.080 0.0800 0.0000
                                                             0.0000
    Equation (7-1) with L= 0.2949, Lc= 0.1515, S= 10.560, n=0.0400
 Resulting lag: 15.2 minutes

Lag computation for station P

Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl

Basin 'n' composition (based on Table 7-1)
    Developed Undeveloped n adj n fract n adj n fr
                                                              fract
       0.030 0.0300 0.0000 0.067 0.0670 0.0000 0.031 0.0310 0.0000 0.070 0.0700 0.0000
        0.032
                0.0320
                          0.0000
                                          0.071 0.0710
                                                             0.0000
                                          0.072
                          0.0000
        0.033
                0.0330
        0.034
                0.0340 0.0000
                                         0.073 0.0730 0.0000
                                         0.074 0.0740 0.0000
0.076 0.0760 0.0000
        0.037 0.0370 0.0000
```

```
0.096
                                                 0.0960
         0.056
                          0.0000
                                                           0.0000
                 0.0560
                          0.0000
         0.060
                 0.0600
                          0.1187
         0.065
                 0.0650
                                         0.110
                                                 0.1100
                                                           0.0000
                                                           0.0000
         0.070
                 0.0780
         0.075
                 0.0750
                          0.0000
                                         0.120 0.1200
                                                           0.0000
                 0.0800
                                          0.150 0.1500 0.0000
     Equation (7-1) with L= 0.3576, Lc= 0.1437, S= 10.560, n=0.0416
Resulting lag: 16.5 minutes
         0.080
  Equation (7-1) with L= 0.32...

Resulting lag: 16.5 minutes

Lag computation for station OFF-N

Lag frequency factor of 1.0 (Table 7-6) for frequency 10 years will be appl

Basin *n* composition (based on Table 7-1)

Developed Undeveloped

n adj n fract n adj n fract

0.030 0.0300 0.0000 0.067 0.0670 0.0000

0.031 0.0300 0.0000 0.070 0.0700 0.0000
                                         0.071 0.0710
                          0.0000
         0.032
                 0.0320
         0.033
                 0.0330
                          0.0000
                                         0.072 0.0720
                                                           0.0000
                          0.0000
                                          0.073
                                                 0.0730
                                                           0.0000
         0.034
         0.035
                 0.0350
                                                 0.0740
                                                           0.0000
                          0.0000
                                         0.074
                                         0.076 0.0760
0.080 0.0800
                                                           0.0000
         0.040
                 0.0400
                          0.0000
                          0.0000
                                         0.084 0.0840
0.088 0.0880
0.090 0.0900
         0.042
                 0.0420
                                                           0.0000
                                                             0000
         0.046
                 0.0460
                                                           0.0000
         0.050
                 0.0500
                          0.0000
         0.053
                 0.0530
                                          0.093
                                                 0.0930
                                                           0.0000
                                          0.096
                                                 0.0960
         0.056
                 0.0560
                          0.0000
                          0.0000
                                          0.100 0.1000
0.110 0.1100
         0.060
                 0.0600
                                                           0.0000
                                                             0000
                0.0650
0.0700
0.0750
         0.065
                                                           0.5000
         0.070
                          0.5000
                                          0.115
                                                 0,1150
                                         0.120 0.1200
0.150 0.1500
                                                           0.0000
         0.075
                                                          0.0000
         0.080 0.0800 0.0000
     Equation (7-1) with L= 0.9470, Lc= 0.3788, S= 5.280, n=0.0925
 * Resulting lag: 78.2 minutes
* End of lag computations
 * NMIN JXDATE JXTIME
                                   NQ
HEC-1L INPUT
                                                                                                      PAGE 2
1 31DEC99
IPRT IPLT
3 0
                       2400 14947
 10
 KK
*
    JXMIN Time interval for input data
 IN
 * Design storm construction details
 * Regional multiplier (zone 2) applied: 1.000
 * Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
   Adjusted depths for each duration from table 4-1: frequency: 10
 0.4300
0.5700
0.7700
   15 min
30 min
                               0.4300
0.5700
                                           0.4300
 * 1 hour
* 2 hours
                               0.7700
                                           0.7700
                              1.0400
                                          1.0315
                   1.0400
                   1.2300
 * 3 hours
                   1.6500
2.2500
                              1.6500
2.2500
                                          1.6366
   12 hours
 * 24 hours
* 36 hours
                   2.9800
3.5400
                               2.9800
                                          2.9800
                               3.5400
 * 2 days
* 3 days
                   3.9500
                               3.9500
                                           3,9500
                   4.6500
                                           4.6500
                               5.7600
                                           5.7024
   5 days
                   5.7600
 * 10 days 7.5400 7.5400 7.4646 * Storm duration: 10, length: 240 ordinates
 * Distrubution using table 4-8 of total rainfall: 7.4646
PI 0.0224 0.0821 0.2015 0.1120 0.0373 0.0224 0.0075
PI 0.0000 0.0000 0.0000 0.0000 0.0000
                                                                      0.0000 0.0000 0.0000
                                                                      0.0000 0.0000 0.0000
     0.0000
              0.0000
                        0.0000
                                0.0000
                                          0.0000
                                                    0.0000
                                                             0.0000
                                                                       0.0000
                                                                               0.0000
                                                                                         0.0000
     0.0000
                        0.0000
                                 0.0000
                                          0.0000
                                                    0.0000
                                                              0.0000
                                                                                0.0149
              0.0000
                                                                                0.0448
PT
     0.0373
              0.0523
                        0.0672
                                 0.0970
                                          0.2239
                                                    0.1418
                                                             0.0746
                                                                       0.0597
                                                                                         0.0373
                                                    0.0000
                                                             0.0000
                                                                                0.0000
     0.0299
              0.0224
                        0.0149
                                 0.0075
                                          0.0000
                                                                       0.0000
                                                                                         0.0000
                                          0.0000
                                                                       0.0000
                                                                                         0.0000
PΙ
     0.0000
              0.0000
                        0.0000
                                 0.0000
     0.0000
              0.0000
                        0.0000
                                0.0000
                                          0.0000
                                                    0.0000
                                                             0.0000
                                                                       0.000
                                                                                0.0000
                                                                                         0.0000
                       0.0000 0.0000
                                          0.0000
                                                   0.0000
                                                             0.0000
                                                                      0.0000 0.0000
                                                                                         0.0000
PI
     0.0000
              0.0000
                                                   0.0224
                                                             0.0299
     0.0000
              0.0000
                       0.0000 0.0075
                                          0.0149
                                                                       0.0373
                                                                                0.0448
                                                                                         0.0523
                       0.3956 0.1642
                                         0.0746
              0.1120
```

0.000.0 0.000.0 0.0000 0.0840 0.0000 0.0880 0.0000

6.0900

0.0930

6.0000

0.084

0.088

0.090

0.093

0.040 0.0400 0.0000

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0.0420

0.0460

0.0500

0.0530

0.042

0.046

0.050

0.053

LINE

3

5

10 11 12

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0.0075 0.0075 0.0000
0.0000 0.0000 0.0000
                  PT 0.0224 0.0149 0.0149
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                                                                                                         0.0075
0.0746
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                                            0.0149
                                                      3.0224
                                                                0.0373
                                                                          0.0448
                                                                                    0.0523
                                                                                               0.0672
                                  0.0149
  21
22
                        0.0149
                   PI
                                                                          0.1418
                                                                                     0.1568
                                                                                                         0.0896
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                                                                0.1344
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                        0.0970
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                                            0.1194
                                                      3.1269
                                                                0.0373
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                                                       3.2463
                                                                          0.0224
                                                                                     0.0149
                                                                                               0.0075
                                  0.2911
                                            0.5001
  23
24
                   PΙ
                        0.2314
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PI
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  25
                                                                           0.0523
                                                                                     0.0672
                                                                                               0.0970
                                                                                                         0.2911
                                                                                                                   0.1493
                      0.0075 0.0149
                                            0.0224
                                                                                                                                 PAGE 3
                                                         HEC-1L INPUT
                 ID.....1.....2.....3.....4......5,......6......7,.....8......9.....10
LINE
                                                                                               0.0149
                                                                                                         0.0075
                       0.0746 0.0597 0.0523 0.0448 0.0373
                                                                          0.0299
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                   PI
  28
                                                                                     0.0000
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                   PI
PI
                        0,0000 0,0000
   29
                                  0,0000
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                                                                0.0000
   30
                                                     0.0746
                                                                 0.2165
                                                                          0.1194
                                                                                     0.0597
                                                                                               0.0446
                                                                                                         0.0299
                                                                                                                   0.0149
                                           0.0523
                       0.0149 0.0373
   31
                  * Precipitation losses computation (Chapter 5)

* Computing RTIMP (percent impervious) from land use and table 5-2

* Computing CNSTL (infiltration rate) from soil type and table 5-2

* TAREA subbasin area (sq mi)

BA 0.1169
   32
                      0.1169
STRTL CNSTL RTIMP
0.20 0.061 60.151
   33
                   LU
                   * Runoff hydrograph computation (Chapter 6)

* Using basin lag: 28.3 minutes

* Using unit duration (Step 2): 1. min
                        Using unit duration (Step 2): 1. min
Lag Time + Unit Duration / 2 (Step 3): 28.83720
Yolume of runoff (Step 4) V= 3.142639
2.90 6.51 10.71 15.06 19.69 24.18
51.33 57.94 64.71 72.19 79.73 87.50
127.74 129.51 130.69 129.66 128.03 125.67
90.17 84.40 80.36 76.37 72.09 67.37
52.59 50.23 47.82 45.62 43.48 41.30
                                                                                      96.53 106.03 115.51
118.64 111.48 104.21
64.39 51.41 58.37
                                                                                                                   124.36
  35
36
                   UI
                                                                                                                     96.86
55.24
   37
38
39
40
41
42
43
                                                                                                38.10
25.40
                                                                                                           36,33
                                                                                                                     34.92
                   UI
UI
                                             30.73
21.45
15.74
                         33.49
                                    32.05
22.04
                                                       29.57
                                                                  28.51
                                                                            27.55
                                                                                       26.46
                                                                                      18.61
14.21
11.03
8.56
6.69
                                                                            19.32
14.62
                                                                                                17.90
13.81
                                                        20.68
                                                                  19,82
                                                                                                           17.53
                                                                                                                     16.96
                         22.85
16.45
                   UI
UI
UI
UI
                                                                  15.03
                                    16.18
                                                        15.35
                                                                            11.34
8.82
                                                                                                                     10.27
                                    12.49
                                                                  11.65
                                                                                                 10.72
                                                                                                           10.53
                         12.85
                                                                                                            8.15
6.42
                                                                                                                      8.00
                                               9.51
7.41
5.81
                          9.97
7.89
                                     9.79
7.62
                                                         9.25
                                                                   9.11
                                                                              6.86
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   44
45
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                                                         5.68
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                   ni
ni
                           6.09
                                     5.95
                                                                                                  3.95
                                                                                                            3.86
                          4.78
                                     4.61
                                               4.47
3.50
                                                         4.38
                                                                    4.24
                                                                              4.13
   46
47
48
49
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                                                                              3.25
                                                                                        3.20
                                                                                                   3.16
                                                                                                            3.09
                                                                                                                      3.00
                                                                                        2.55
                                                                                                                       2.35
                                                                              2.60
                   UI
                          2.96
                                                         2.70
                                                                    2.64
                                     2 88
                                               2.79
                                                                   2.06
                                               2.15
                                                         2.11
                                                                              2.01
                                                                                        1.97
                                                                                                  1.92
                                                                                                             1.88
                                                                                                                       1.83
                   UI
                                     1.74
                                               1.70
                                                         1.65
                          1.79
                                      . 37
                                               1.37
   51
                         C=FLON P=010YR-10DY A=GREENBRI
   52
                   KK
*
   53
                      JXMIN Time interval for input data 60
                   TN
   54
55
                   * Design storm construction details
                   * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                    * Adjusted depths for each duration from table 4-1: frequency: 10
                   0.2500
                                                    0.3600
                      10 min
                                       0.3600
                                                                 0.4300
                                                    0.4300
                      15 min
                    * 30 min
                                       0.5700
                                                    0.5700
                      1 hour
                                       0.7700
                                                    0.7708
                                                                 0.7700
                                                    1.0400
                                                                 1.0315
                                       1.0400
                     2 hours
                   • 3 hours
                                       1.2300
                                                    1.2300
                                                                 1.2200
                                        1.6500
                                                    1.6500
                                                                 1.6366
                     6 hours
                   * 12 hours
* 24 hours
                                       2.2500
                                                    2.2500
                                                                 2.2500
                                                    2.9800
                                                                 2.9800
                                                                 3.5046
                                       3,5400
                                                    3.5400
                    * 36 hours
                     2 days
                                        3.9500
                                                    3.9500
                                                                 3.9500
                                                    4.6500
                     3 days
                                       4.6500
                   * 5 days
                                       5,7600
                                                    5.7600
                                                                 5,7024
                                       7.5400
                                                    7.5400
                     10 days
                   * Storm duration: 10, length: 240 ordinates
                   * Distrubution using table 4-8 of total rainfall: 7.4646
**HEC-1L INPUT
                                                                                                                                  PAGE 4
                 ID.....1.....2.....3.....4......5,.....6......7.....8......9.....10
LINE
  56
                   PB
                       0.0224
                                                                                      0.0075
                                                                                               0,0000 0,0000 0,0000
  57
                   PI
PI
                                  0.0821 0.2015 0.3120
                                                                0.0373 0.0224
                                                      0.0000
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                                  0.0000
  58
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  59
60
                                                                 0.0000
                   PI
                        0.0000
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                                            0.0000
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                                                                 0.0000
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                                                                                                                    0.0224
                   PI
  61
62
                   ΡI
                        0.0373
                                  0.0523
                                            0.0672
                                                      0.0970
                                                                 0.2239
                                                                           0.1418
                                                                                      0.0746
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                                                      0.0075
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                        0.0299
                                  0.0224
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  63
                   ÞΙ
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0.0448
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                                         0.0000
                                                   0.0075
                                                             0.0149
                 PI
                      0.0000
                               0.0000
                                                                                                   0.0299
                                                                                                             0.0224
                      0.0672
                               0.1120
                                         0.3956
                                                   J.1642
                                                             0.0746
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                                         0.0149
                                                             0.0075
                                                                      0.0000
                                                                                0.0000
                                                                                          0.0000
                                                                                                   0.0000
                      0.0224
  68
                 PI
                               0.0149
                                                                                                   0.0075
                                                                                0.0000
                                                                                                             0.0075
                                                                      0.0000
  69
                      0.0000
                               0.0000
                                         0.0000
                                                   3.0000
                                                             0.0000
                                                                                                             0.0821
                               0.0149
                                         0.0149
                                                   3.0224
                                                             0.0373
                                                                      0.0448
                                                                                0.0523
                                                                                          0.0672
  70
71
72
                      0.0149
                 PI
                                                                      0.1418
                                                                                          0.1120
                                                                                                   0.0896
                                                                                                             0.0672
                                                             0.1344
                 PI
PI
                      0.0970
                               0.1045
                                         0.1194
                                                   0.1269
                                                                                                   0.0075
                                                                                          0.0075
                                         0.5001
                                                   0.2463
                                                             0.0373
                                                                      0.0224
                                                                                0.0149
                      0.2314
                                                                      0.0000
                                                                                0.0000
                                                                                          0.000
                                                                                                   0.0000
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                                                   0.0000
                                                             0.0000
  73
                 PI
PI
                      0.0000
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                                         0.0000
                                                   0.0000
                                                             0.0000
                                                                      0.0000
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  74
                                                                      0.0523
                                                   0.0299
                                                             0.0373
                                                                                0.0672
                                                                                          0.0970
                                                                                                   0.2911
                                                                                                             0.1493
  75
76
                 PT
                      0.0075
                               0.0149
                                                                                                             0.0000
                                                                                          0.0149
                                                                                                   0.0075
                                                                                0.0224
                      0.0746
                               0.0597
                                         0.0523
                                                   0.0448
                                                             0.0373
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                                         0.0000
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 77
78
                               0.0000
                 PI
                      0.0000
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                               0.0000
                      0.0000
  79
                 PI
                                                                                                  0.0299
                                                                      0.1194
                                                                                0.0597
                 PI 0.0149
                               0.0373
                                        0.0523 0.0746
                                                            0.2165
                 * Precipitation losses computation (Chapter 5)
                      Computing RTIMP (percent impervious) from land use and table 5-2
Computing CNSTL (infiltration rate) from soil type and table 5-2
                 * TAREA subbasin area (sq mi)
BA 0.0433
  81
                    A 0.0433
STRTL CNSTL RTIMP
J 0.20 0.062 57.838
                  LU
  62
                 * Runoff hydrograph computation (Chapter 6)

* Using basin lag: 14.7 minutes

* Using unit duration (Step 2): 1. min

* Lag Time + Unit Duration / 2 (Step 3): 15.21310

* Volume of runoff (Step 4) V= 1.163785

UI 4.266 9.933 16.116 21.721 29.648 37.728 45.837 56.841 68.140

UI 99.443 91.531 90.410 85.565 76.047 66.329 58.610 53.270 47.241

UI 39.201 35.757 32.628 29.766 27.467 25.216 23.323 21.504 20.029

UI 17.346 16.237 15.239 14.230 13.438 12.502 11.842 11.349 10.791

UI 9.772 9.304 8.893 8.449 8.119 7.696 7.383 7.004 6.705
  83
                                                                                                             43.300
  84
                                                                                                              18.681
  85
86
                                                                                                             10.315
                                                                                                               6.417
                                 9.304
5.792
  87
88
                                                    8,449
                                                                                                               4.010
                                                                                            4.406
                                                                                                     4.191
                                           5.583
                                                              5.039
                                                                        4.797
                                                                                  4.599
                                                                                  2.838
                                                                                           2.718
1.740
                                                    3.325
                                                                        2.970
                                                                                                     2.597
                                                                                                               2.476
  89
                  UI
                       3.829
                                 3.648
                                          3.467
  90
                 UI
                       2.355
                                 2.265
                                          2,205
                                                    2.098
                                                              2,010
                                                                        1,890
                                           1.372
                                                     1.311
                                                                        1.191
                                                                                  1.130
                                                                                           1.102
                                                                                                     1.055
                                                                                                               0.995
                       1.492
                                 1.432
  91
                       0 964
                       C=FLOW F=010YR-10DY A=GREENBRI
  93
                                                                                                                           PAGE 5
                                                     HEC-1L INPUT
                ID......2.....3.....4......5,......5......7......8......9......10
LINE
                  KK C
  94
                   JXMIN Time interval for input data
                  IN
                           60
  95
  96
                  KМ
                  * Design storm construction details
                   Regional multiplier (zone 2) applied: 1.000
                  * Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                  * Adjusted depths for each duration from table 4-1: frequency: 10
                   Duration---Regional------Elev-----Areal (adjustments)
5 min 0.2500 0.2500 0.2500
                   10 min
                                     0.3600
                                                 0.3600
                                                             0.3600
                                                             0.4300
                                                 0.4300
                   15 min
                                     0.4300
                                     0.5700
                                                 0.5700
                                                             0.5700
                                     0.7700
                                                 0.7700
                                                             0.7700
                   1 hour
                  * 2 hours
                                     1.0400
                                                 1.0400
                                                             1.0315
                                     1.2300
                                                 1.2300
                                                             1.2200
                   3 hours
                                                             1.6366
                  * 6 hours
                                     1.6500
                                                 1.6500
                                                 2.2500
                                                             2.2500
                  * 12 hours
                                                             2.9800
                                     2.9800
                  * 24 hours
                                    3.5400
3.9500
                                                 3.5400
3.9500
                   36 hours
                                                             3.5046
                                                             3.9500
                   2 days
                  * 3 days
                                     4.6500
                                                 4.6500
                                                             4.6500
                                     5.7600
                   5 days
                   10 days 7.5400 7.540
Storm duration: 10, length:
                                                 7.5400
                                                             7.4646
                                                       240 ordinates
                  * Distrubution using table 4-8 of total rainfall: 7.4646
                                                                                                    0.0000
                                                                                           0.0000
                                                                                                             0.000
                 PI 0.0224 0.0821 0.2015 0.1120
                                                             0.0373
                                                                                0.0075
  98
99
                      0.0000
                               0.0000 0.0000 0.0000
0.0000 0.0000 0.0000
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                 PI
PI
                                                             0.0000
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 100
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                                                                                           0.0075
 101
                      0.0000
                               0.0000 0.0000
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                                                                      0.1418
                      0.0373
                                                             0.2239
                                                                                 0.0746
                                                                                           0.0597
                                                                                                    0.0448
                                                                                                              0.0373
                                0.0523
 102
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                               0.0224 0.0149
                                                   0.0075
 103
                 PI
                      0.0299
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 104
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105
                 PΙ
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                 PI
                      0.0000
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107
                                                                                0.0448
                                                                                           0.0373
                                                                                                    0.0299
                                                                                                              0.0224
 108
                 PI
                      0.0672
                               0.1120
                                         0 3956
                                                   0.1642
                                                             0.0746
                                                                      0.0597
                                                                      0.0000
                      0.0224
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                 PI
109
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                                                                                           0.0000
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                                                             0.0373
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                                                                                 0.0523
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                                                                                                    0.0746
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                      0.0149
                 PI
111
                                                                                0.1568
                                                                                           0.1120
                                                                                                    0.0896
                                                                                                              0.0672
                                                                      0.1418
112
                 PΙ
                      0.0970
                               0.1045
                                         0.1194
                                                   0.1269
                                                             0.1344
                                         0.5001
                                                   0.2463
                                                             0.0373
                                                                      0.0224
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114
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PI 0.0000 0.0000 0.0000
PI 0.0075 0.0149 0.0224
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0.0373
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 115
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 118
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 120
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                                                   HEC-1L INPUT
               LINE
                PI 0.0149 0.0373 0.0523 3.0746 0.2165 0.1194 0.0597 0.0448 0.0299 0.0149
 121

    Precipitation losses computation (Chapter 5)
    Computing RTIMP (percent impervious) from land use and table 5-2
    Computing CNSTL (infiltration rate) from soil type and table 5-2

                            subbasin area (sq mi)
                    TAREA
                   0.0616
STRTL CNSTL RTIMP
J 0.20 0.063 56,962
 122
                 LU
                 * Runoff hydrograph computation (Chapter 6)
* Using basin lag: 18.6 minutes
* Using unit duration (Step 2): 1. min
                     Lag Time + Unit Duration / 2 (Step 3): 19.06322

Volume of runoff (Step 4) V= 1.655347

3.57 8.62 13.94 19.41 24.56 31.99

74.33 85.66 96.73 102.08 103.85 103.14
                                                                                       45.71
                                                                                                         64.30
 124
                                                                                                          75.69
                                                                                       93.26
                                                                                                84.54
                                85.66
63.14
                                        96.73 102.08 103.85 103.14
58.22 52.91 49.38 45.68
                                                                            100.80
 125
                                                           49.38
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21.98
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                                                                                                         33.98
 126
                      68.00
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                                29,78
16.81
                                        27.91
15.77
                                                                     23.16
 127
                       31.77
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9.64
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                                                                     13.72
                                                                              13.08
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                                                                                                          11.77
7.99
 128
                 UI
                      17.55
                                                                      9.34
                 UI
UI
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7.39
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                                         10.44
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 130
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 134
                        1.23
 135
                 UI
                      C=FLOW F=010YR-10DY A=GREENBRI
 137
                 KK D
                          Time interval for input data
                    JXMIN
                 IN
 139
                 KM
                 * Design storm construction details
                 * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
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                   3 days
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                   5 days
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7.5400
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                                                           5.7024
                                               7.5400
                   10 days
                 * Storm duration: 10, length: 240 ordinates
* Distrubution using table 4-8 of total rainfall: 7.4646
HEC-1L INPUT
                                                                                                                      PAGE 7
                ID.....1.....2.....3......4......5,......6,......7......8.......9.....10
LINE
 140
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                                             * Precipitation losses computation (Chapter 5)
                                                    Computing RTIMP (percent impervious) from land use and table 5-2
Computing CNSTL (infiltration rate) from soil type and table 5-2
                                                                subbasin area (sq mi)
                                                  TAREA
                                                   0.0466
                                                  0.0466
STRTL CNSTL RTIMP
0.20 0.067 47.037
                     165
                                             LU
                     166
                                             * Runoff hydrograph computation (Chapter 6)

* Using basin lag: 18.1 minutes

* Using unit duration (Step 2): 1. min

* Lag Time + Unit Duration / 2 (Step 3): 18.57796

* Volume of runoff (Step 4) V= 1.252014

UI 2.873 6.902 11.165 15.414 19.858 25.588 31.201 37.574 44.506 51.751

GI 60.110 69.329 77.880 79.895 80.715 79.393 76.031 69.207 62.206 55.583

UI 23.431 21.878 20.508 19.188 18.063 17.110 16.061 15.156 14.365 13.594

UI 23.431 21.878 20.508 19.188 18.063 17.110 16.061 15.156 14.365 13.594
                     167
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                      259
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9.746
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5.857
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7.667 7.373 7.138 6.833
                                                     12.989
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8.011
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                                                                                                                                             6.573
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5.661
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                                              UI
                                                       3.852
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                                                                     1.180
                                                                                   1.137
                      178
                                                       C=FLOW F=010YR-10DY A=GREENBRI
                      179
                                                                                                                                                                                                           PAGE 8
                                                                                                    HEC-1L INPUT
1
                                            ID.....1.....2......3......4......5,......6.......7.....8........9.....10
                    LINE
                      180
                                                 JXMIN Time interval for input data 60
                                               IN
                      181
                      182
                                               * Design storm construction details
                                                 Regional multiplier (zone 2) applied: 1.000
                                               * Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                                               0.3600
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Storm duration: 10, length:
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                                                                                                      240 ordinates
                                               * Distrubution using table 4-8 of total rainfall: 7.4646
                      183
                                               PB
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                      206
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                                                                                                    HEC-1L INPUT
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                    T.TNE
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PI 0.0149 0.0373 0.0523 0.0746 0.2165 0.1194 0.0597 0.0448 0.0299 0.0149
207
                * Precipitation losses computation (Chapter 5)

* Computing RTIMP (percent impervious) from land use and table 5-2

* Computing CNSTL (infiltration rate) from soil type and table 5-2

* TAREA subbasin area (sq mi)
                * TAREA Subbasin area (sq mi)
BA 0.0377
208
                  STRTL CNSTL RTIMP
U 0.20 0.059 60.768
                LU
209
                • Runoff hydrograph computation (Chapter 6)
• Using basin lag: 15.0 minutes
                     Using basin lag: 15.0 minutes

Using unit duration (Step 2): 1. min

Lag Time + Unit Duration / 2 (Step 3): 15.50161

Volume of runoff (Step 4) V= 1.012535

3.555 8.297 13.458 17.994 24.763 31.391

75.874 77.854 77.595 75.140 67.234 59.093
                                                                              38.884 47.252 56.463
51.633 47.003 42.232
                                                                                                            67.056
                    3.555 8.297 13.458
75.874 77.854 77.595
210
                ш
                                                                     59.093
22.447
211
                                                                                        19.140
                                                                                                  17.755
                                                                                                            16.624
                     34.861 31.628 28.972
15.406 14.416 13.506
                                                  26.519 24.243
212
                UI
                                                                                          9.909
6.282
                                                                                                   9.556
                                                 12.766 11.847
                                                                      11.168
                                                                               10.546
                ui
ui
213
                                                                                 6.526
                                                                                                   5.962
                                                                                                             5.700
                                                             7.160
                                                                       6.880
                                8.250
5.159
                                         7 883
                                                   7.519
214
                                                                                          3.939
                                                                                                              3.596
                                          4.942
                                                   4.768
                                                             4.516
                                                                       4.311
                                                                                 4.109
                       5.471
                tII
                                                                                                             2.249
                                                                                2.574
                                                                                          2.451
                                                                                                   2.350
                       3.445
                                3.293
216
                                                                                 1.658
                                                                                                    1.531
                                                                                                             1.442
                                2.046
                                                    1 902
                                                              1.821
                                                                       1.759
217
                UI
                                                                                                    0.947
                                                              1,150
                                                                       1.099
                                                                                 1.048
                                                                                          0.998
                                                   1.200
218
                 υī
                       1.371
                                1.301
                                          1.251
                                0.835
                                          0.823
                 UI
219
                       C=FLOW F=010YR-10DY A=GREENBRI
                 2₩
                 ĸĸ
                     DEMMY1
                 Ю
222
                 HC
                       C=FLOW
224
225
                 ĸĸ
                   JXMIN Time interval for input data
                 IN
226
                 КМ
                 * Design storm construction details
                 * Regional multiplier (zone 2) applied: 1.000

Areal adjustment using area: 1.813
multiplier from table 4-4: 1.0000

                 * Adjusted depths for each duration from table 4-1: frequency: 10
                 * Duration---Regional-----Elev----Areal (adjustments)
* S min 0.2500 0.2500 0.2500
                 * 5 min
                                                0.3600
0.4300
                                    0.3600
                                                             0.3600
                   10 min
                 + 15 min
                                    0.4300
                                    0.5700
                                                 0.5700
                                                             0.5700
                 * 30 min
                                                             0.7700
                                                 0.7700
                 * 1 hour
                 * 2 hours
                                    1.0400
                                                 1.0400
                                                 1.2300
                                                             1,2200
                                    1.2300
                  * 3 hours
                                                             1,6366
                 * 6 hours
                                    1 6500
                                                 1.6500
                                                 2.2500
                                                             2,2500
                   12 hours
                                                             2.9800
                                    2,9800
                 * 24 hours
                    36 hours
                                    3.5400
3.9500
                                                 3.5400
                                                             3.5046
                                                             3.9500
                                                 3.9500
                  * 2 days
                                                             4.6500
                                                 4.6500
                 * 3 days
                                     4.6500
                                     5.7600
                                                 5.7600
                                                             5.7024
                   5 days
                                                 7.5400
                 * 10 days 7.5400 7.5400 7.4646

* Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646
                                                                                                                          PAGE 10
                                                     HEC-1L INPUT
                ID......1.....2......3......4......5,......6......7......8......9......10
LINE
 228
                    0.0224 0.0821 0.2015 0.1120 0.0373 0.0224 0.0075 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
                                                                                                   0.0000 0.0000
 229
                                                                                                   0.0000 0.0000
                                                  0.0000 0.0000
 230
                 PÍ
                                                                                0.0000
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                     0.0000
                               0.0000
                                         0.0000
 231
                                                                                                    0.0149
                                                   0.0000
                                                                                0.0000
                                                                                          0.0075
                                0.0000
                                         0.0000
                                                             0.0000
                                                                       0.0000
 232
                 PI
                                                                                0.0746
                                                             0.2239
                                                                                          0.0597
                                                                                                    0.0448 0.0373
                 PI
                      0.0373
                               0.0523
                                         0.0672
                                                                                          0.0000
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                                                                                                             0.0000
                 ΡI
                      0.0299
                                0.0224
                                         0.0149
                                                   0.0075
                                                             0.0000
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 234
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 235
                 PΙ
                      0.0000
                               0.0000
                                         0.0000
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                                                                                                      0000
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                                                                                0.0000
                      0.8000
                               0,0000
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                                                             0.0000
                                                                       0.0000
 236
                                         0.0000
                                                   0.0080
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                                                                                                            0.0000
 237
                 PI
                      0.0000
                                                                                0.0299
                                                                                                      .0448
                                                                                                             0.0523
                                                                       0.0224
                      0.0000
                               0.0000
                                         0.0000
                                                   0.0075
                                                             0.0149
 238
                                                             0.0746
                                                                                                    0.0299
                                                                                                             0.0224
                                         0.3956
                                                   0.1642
                                                                       0.0597
                                                                                0.0448
                                                                                          0.0373
 239
                 PI
                     0.0672
                                                                       0.0000
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                                                                                          0.0000
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                 PI
                                                   0.0075
                      0.0224
                               0.0149
                                         0.0149
 240
                                                                                                    0.0075
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                                                             0.0000
                                                                       0.0000
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                                                                                          0.0000
                      0.0000
 241
                                                                       0.0448
                                                                                0.0523
                                                                                          0.0672
                                                                                                    0 0746
                                                                                                             0.0821
                                                             0.0373
                 PT
                      0.0149
                               0.0149
                                         0.0149
 242
                                                                                                    0.0896
                                                                                          0.1120
                      0.0970
                                         0.1194
                                                   0.1269
                                                             0.1344
                                                                       0.1418
                                                                                0.1568
                 ΡI
 243
                                                   0.2463
                                                             0.0373
                                                                       0.0224
                                                                                0.0149
                                                                                          0.0075
                                                                                                    0.0075 0.0075
                                         0.5001
                 PI
                     0.2314
                               0.2911
                                                                                          0.0000
                                                                                                    0.0000
                                                                                                             0.0000
                      0,0000
                               0.0000
                                         0.0000
                                                   0.0000
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 245
                                                                       0.0000
                                                   0.0000
                                                             0.0000
                                                                                0.0000
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                                                                                                             0.0000
 246
                 PI
                      0.0000
                                                                                                             0.1493
                                                                                0.0672
                                                                                          0.0970
                      0.0075
                               0.0149
                                         0.0224
                                                   0.0299
                                                             0.0373
 247
                                                   0.0448
                                                             0.0373
                                                                       0.0299
                                                                                0.0224
                                                                                          0.0149
                                                                                                    0.0075
                               0.0597
                                         0.0523
                     0.0746
 248
                 PI
                                                                                0.0000
                                                                                                    0.0000
                                                                                                             0.0000
                                                                                          0.0000
                 PT
                     0.0000
                               0.0000
                                         0.0000
                                                   0.0000
                                                             0.0000
                                                                      0.0000
 249
                               0.0000
                                         0.0000
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                                                                      0.0000
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                                                                                          0.0000
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                     0.0000
 250
                 PI
                                                                       0.0000
                                                                                0.0000
                                                                                          0.0000
                                                                                                    0.0000
                                                                                                            0.0075
                 PI
                      0.0000 0.0000
                                         0.0000
                 PI 0.0149 0.0373 0.0523
                                                  0.0746 0.2165
                                                                      0.1194 0.0597
                                                                                         0.0448
                                                                                                    0.0299
                                                                                                             0.0149
 252
                 * Precipitation losses computation (Chapter 5)
```

```
Computing RTIMP (percent impervious) from land use and table 5-2 Computing CNSTL (infiltration rate) from soil type and table 5-2 TAREA subbasin area (sq mi)
                * TAREA subbasin area (sq mi)
BA 0.0458
253
                    STRTL CNSTL
0.20 0.07
                                NSTL RTIMP
0.070 49.509
                 T.CT
254
                * Runoff hydrograph computation (Chapter 6)

* Using basin lag: 15.9 minutes

* Using unit duration (Step 2): 1. min

* Lag Time + Unit Duration / 2 (Step 3): 16.40914

* Volume of runoff (Step 4) V= 1.231007

UI 3.787 8.913 14.446 19.182 26.594 33.298 41.287 50.002 59.141

UI 81.534 88.062 89.842 88.719 84.767 76.150 67.308 59.265 54.244

UI 81.534 20.890 37.147 34.283 31.502 28.893 26.873 24.804 23.088
255
                                                                                       59.265 54.244
24.804 23.088
                                                                                                           49.145
256
                                                                                                           21.408
                     44.512 40.890
                                        37.147
                                                 34.283 31.502
                                                                     28,893
                                                                              26.873
 257
                 υI
                     19.994 18.812 17.490 16.433 15.445
11.125 10.608 10.187 9.693 9.237
                                                                              13.636
                                                                                       12.933
                                                                                                 12,186
                                                                                                           11.543
 258
                                                                                                            7.400
                                                   9.693
6.281
                                                                                8.462
                                                                      8.888
 259
                 UI
                                                                      5.704
                                                                                5.494
3.557
                                                                                                            4.793
                                                             5.935
                                                                                         5.259
                                                                                                  5.012
                 UI
                      7.151
                                6.819
                                         6.518
                                                                                                            3.077
                                                                                         3.392
                                                                                                   3.268
                       4.589
                                          4.225
                                                   4,050
                                                             3,886
                 UI
 261
                                                   2.593
                                                                                                   2.135
                                                             2.484
                                                                      2.374
                                                                                2.264
                                                                                         2.202
 262
                 TŤŤ
                       2 943
                                2.813
                                          2,703
                                                                                         1.429
                                                                                                   1.374
                                                                                                            1,319
                                1.850
                                         1.793
                                                   1.721
1.100
                                                             1.638
                                                                      1.547
                 UI
 263
                                                             1,080
                                                                      1.035
                                                                                0.980
                                                                                         0.945
                       1.264
                 UI
                       C=FLOW F=010YR-10DY A=GREENBRI
 265
                                                                                                                         PAGE 11
                                                    HEC-1L INPUT
                LINE
                 KK G * JXMIN Time interval for input data
266
 267
 268
                 * Design storm construction details
                 * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                 * Adjusted depths for each duration from table 4-1: frequency: 10
                 0.3600
                 * 10 min
                                    0.3500
                                    0.4300
0.5700
                                                0.4300
                                                            0.4300
                                                0.5700
                                                            0.5700
                   30 min
                   1 hour
2 hours
                                    0.7700
                                                 1.0400
                                                            1.0315
                                                            1.2200
                                                1.2300
                 * 3 hours
                                    1,2300
                   6 hours
                                    1.6500
                                                1.6500
2.2500
                                                            1.6366
                                                            2.2500
                 * 12 hours
                                    2.2500
                                    2.9800
3.5400
                                                2.9800
                                                            2.9800
                                                            3.5046
                 * 36 hours
                 * 2 đays
                                    3.9500
                                                3.9500
                                                4.6500
                                                            4.6500
                   3 days
                                    5.7600
                                                5.7600
                 * 5 days
                 * Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646
                 PI 0.0224 0.0821 0.2015 0.1120
PI 0.0000 0.0000 0.0000
                                                                               0.0075
                                                                                         0.0000
                                                                                                  0.0000 0.0000
                                                                                         0.0000
                                                                                                  0.0000
                                                                                                            0,0000
                     0.0000 0.0000 0.0000 0.0000 0.0000
0.0000 0.0000 0.0000 0.0000
                                                                     0.0000
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 271
                                                                               0.0000
                                                                      0.0000
                                                                                         0.0000
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                                                                                                            0.0000
 272
273
                                                                                         0.0075
                               0.0000
                                         0.0000
                                                  0.0000
                                                            0.0000
                                                                      0.0000
                                                   0.0970
                                                            0.2239
                                                                      0.1418
                                                                               0.0746
                                                                                         0.0597
                                                                                                  0.0448
                                                                                                            0.0373
                                         0.0672
 274
275
                 PI
                     0.0373
                               0.0523
                                                                      0.0000
                                                                               0.0000
                                                                                                   0.0000
                                                                                                            0.0000
                      0.0299
                               0.0224
                                         0.0149
                                                  0.0075
                                                            0.0000
                                                                                                            0.0000
                                         0.0000
                                                   0.0000
                                                            0.0000
                                                                      0.0000
                                                                               0.0000
                                                                                         0.0000
                                                                                                  0.0000
                               0.0000
                 PI
 276
                     0.0000
                                                                                         0.0000
                                                                                                   0.0000
                                                                                                            0.0000
                                                                      0.0000
 277
                 PI
PI
                      0.0000
                               0.0000
                                         0.0000
                                                  0.0000
                                                            0.0000
                                                                                                            0.0000
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                               0.0000
                                         0.0000
                                                            0.0000
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                                                                               0.0000
                                                                                         0.0000
                      0.0000
 278
                                                                               0.0299
                                                            0.0149
                                                                      0.0224
                                                                                         0.0373
                                                                                                  0.0448
                                                                                                            0.0523
                 PI
                     0.0000
                               0.0000
                                         0.0000
                                                                                                            0.0224
                                                                                         0.0373
                               0.1120
                                         0.3956
                                                   0.1642
                                                            0.0745
                                                                      0.0597
 280
                                                                     0.0000
                                         0.0149
                                                   0.0075
                                                            0.0075
                                                                               0.0000
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                                                                                                            0.0000
 281
                 PΙ
                     0.0224
                                                                               0.0000
                                                                                                   0.0075
                                                                                                            0.0075
                     0.0000
                                                            0.0000
                 PΙ
                               0.000
                                         0.0000
                                                  0.0000
 282
                                         0.0149
                                                  0.0274
                                                            0.0373
                                                                                                            0.0821
                               0.0149
                                                                      0.0448
                                                                               0.0523
                                                                                         0.0672
                                                                                                  0.0746
 283
                 PI
                                                                                         0.1120
                                                                               0.1568
                                                                                                   0 0896
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                 PΤ
                     0.0970
                               0.1045
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                                                                                                            0.0075
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                      0.2314
                               0.2911
                                         0.5001
                                                   0.2463
                                                            0.0373
                                                                      0.0224
                 ΡI
 285
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                                         0.0000
 286
                 PΙ
                     0.0000
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                                0.0000
                                         0.0000
                                                   0.0000
                                                            0.0000
                                                                      0.0000
 287
                                         0.0224
                                                   0.0299
                                                            0.0373
                                                                      0.0523
                                                                               0.9672
                                                                                         0.0970
                                                                                                   0.2911
                                                                                                            0.1493
 288
                 PΙ
                      0.0075
                               0.0149
                                                                               0.0224
                                                                                         0.0149
                                                                                                   0.0075
                                                                                                            0.0000
                               0.0597
                                                                      0.0299
                     0.0746
                                         0.0523
                                                  0.0448
                                                            0.0373
 289
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 290
                 PI
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                 PI 0.0000 0.0000
PI 0.0000 0.0000
                                         0.0000
                                                  0.0000 0.0000
                                                                      0.0000
                                                                              0.0000
                                                                                         0.0000
                                                                                                  0.0000 0.0075
 292
                                                     HEC-1L INPUT
                                                                                                                          PAGE 12
                LINE
                 PT 0.0149 0.0373 0.0523 0.0746 0.2165 0.1194 0.0597 0.0448 0.0299 0.0149
293
                 * Precipitation losses computation (Chapter 5)
                     Computing RTIMP (percent impervious) from land use and table 5-2
Computing CNSTL (infiltration rate) from soil type and table 5-2
                  * TAREA subbasin area (sq mi)
                     0.0614
 294
                            CNSTL RTIMP
```

1

STRTL

```
* Runoff hydrograph computation (Chapter 6)
                     Using basin lag: 17.8 minutes
Using unit duration (Step 2): 1. min
                      Using time + Unit Duration / 2 (Step 3): 18.33008
Volume of runoff (Step 4) V= 1.651146
3.91 9.38 15.17 20.85 27.11 34.74
                                                                                        51.16
                                                                               42.49
                        3.91
                                                                   105.53
                                9.38 15.17 20.85 27.11
94.59 104.62 107.08 107.58
                                                                               99.55
40.57
                                                                                        90.24
                                                                                                  80.72
                                                                                                           72.06
 297
                 UI
                       82.07
                                                                                         37.62
                                                                                                  34.82
18.65
                                                                                                           32.58
17.76
                                                                      43.66
                       66,30
30.37
                                61.10
28.46
                                         55.18
26.58
                                                  51.37
                                                           47.39
23.51
                 UI
UI
                                                                                         19.71
                                                   24.90
                                                                      22.21
                                                                               28.84
 299
                                                                                         12.25
                                                                                                            11.22
                                                            13.64
                 UI
UI
                       16.72
                                15.94
                                         14.94
                                                   14.42
                                          9,95
6.72
                                                    9.64
6.56
                                                             9.24
6.24
                                10.38
                                                                       8.84
                                                                                8.57
                                                                                          8.21
 301
                                                                                5.76
3.94
                                                                       6.00
                                                                                          5.54
                                                                                                   5.36
                                                                                                             5.16
 302
                        7.30
                                 6.99
                                                                                          3.72
                                           4.60
 303
                        4.95
                                 4.77
                                                    4.42
                                                              4.24
                                                                       4.07
                                                                       2.72
                                                                                2.65
                                                                                          2.59
                                                                                                   2.48
                                                                                                             2.41
                                                    2.96
 304
                 UI
                        3.31
                                 3.19
                                                              1.96
                        2.29
                                 2.20
                                           2.14
                                                    2.05
                                                                       1.87
                        1.56
                                 1.50
                                                                                1.26
                                                                                                   1.14
                 UI
 306
                       C=FLOW F=010YR-10DY A=GREENBRI
 307
 308
                 KK
                            Time interval for input data
                   JXMIN
                 IN
                           60
 310
                 ΚM
                 * Design storm construction details
                 * Regional multiplier (zone 2) applied: 1,000
                 * Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                  * Adjusted depths for each duration from table 4-1: frequency: 10
                 * Duration----Regional------Elev-----Areal (adjustments)
                                    0.2500
                                                          0.2500
                   5 min
                 * 10 min
                                    0.3600
                                                0.3600
                                                           0.3600
                                                0.4300
                                                           0.4300
0.5700
                    15 min
                                                0.5700
                 * 30 min
                                    0.5700
                                    0.7700
                                               0.7700
                   1 hour
                                                           0.7700
                                                           1.0315
                 * 2 hours
                                    1.2300
1.6500
                                                1.2300
                                                           1.2200
                 * 6 hours
                                                           1.6366
                 * 12 hours
                                    2.2500
                                               2,2500
                                                           2.2500
                                    2.9800
                                                           2,9800
                   24 hours
                                                           3,5046
                 * 36 hours
                                    3.5400
                                               3.5400
                                               3.9500
4.6500
                                                           3.9500
                   2 days
                                    3.9500
                                                           4.6500
                   3 days
                                    4.6500
                                    5.7600
                                               5.7600
                                                           5.7024
                                                7.5400
                                    7.5400
                   10 days
                 * Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646
                                                                                                                        PAGE 13
                                                    HEC-1L INPUT
               ID.....1.....2.....3.....4......5,.....6......7.....8.......9.....10
LINE
 311
                 PI 0.0224 0.0821 0.2015 0.1120 0.0373 0.0224 0.0075
PI 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
                                                                                      0.0000 0.0000
 312
                                                           0.0000 0.0000 0.0008
0000.0 0000.0 0000.0
                                                                                      0.0000
                                                                                                 0.0000
                                                                                                          0.0000
 313
                                                                                        0.0000
                                                  0.0000
 374
                 PI
                     0.0000
                               0.0000
                                        0.0000
                 PI
                      0.0000
                                        0.0000
                                                  0.0000
 315
                               0.0000
                                                           0.0000
                                                                   0 0000
                                                                              0.0000
                                                                                        0.0075
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                                                          0.2165
                                                                    0.1194
 335
                 * Precipitation losses computation (Chapter 5)
                     Computing RTIMP (percent impervious) from land use and table 5-2
Computing CNSTL (infiltration rate) from soil type and table 5-2
                    TAREA subbasin area (sq mi)
                     0.1108
                   STRIL CNSTL RIMP
0.20 0.069 46.942
337
                * Runoff hydrograph computation (Chapter 6)
                     Using basin lag:
                                         26.4 minutes
                     Using unit duration (Step 2): 1. min
Lag Time + Unit Duration / 2 (Step 3): 26.89606
Volume of runoff (Step 4) V= 2.978785
3.16 7.23 11.84 16.58 21.76 26.15 30.94 38.05 43.83 50.33
338
```

LU 0.20 0.070 38.916

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99.52 109.99 120.08 128.45 130.77
                                                                                                     89.69 99.52
121.97 114.20
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                                                                  1.73
                                                                                                                                                                                              PAGE 14
                                                                                             HEC-1L INPUT
                                         ID......2.....3.....4.....5,.....6......7.....8.....9.....10
                 LINE
                                                    1 40
                                                   C=FLOW F=010YR-10DY A=GREENBRI
                   355
                   356
                                           KK I
                                              JXMIN Time interval for input data
60
                                           IN
                   357
                                           * Design storm construction details
                                            * Regional multiplier (zone 2) applied: 1.800
                                           * Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                                                 multiplier from table 4-4: 1.0000
                                            0.2500
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                                            * 10 min
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                                            * 3 hours
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                                              12 hours
                                            * 24 hours
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                                            * 36 hours
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                                                                                                        5.7024
                                            * 5 days
                                           * 10 days 7.5400 7.5400 7.4646

* Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646

* Distrubution using table 4-8 of total rainfall: 7.4646
                                            PI 0.0224 0.0821 0.2015 0.1120 0.0373 0.0224 0.0075 0.0000 0.0000 0.0000
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                                                                                              HEC-1L INPUT
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                                          ID.....1.....2.....3.....4......5,.....6......7.....8......9.....10
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                    381
                    382
                    383
                                            * Precipitation losses computation (Chapter 5)
                                                  Computing RTIMP (percent impervious) from land use and table 5-2
Computing CNSTL (infiltration rate) from soil type and table 5-2
                                                TAREA subbasin area (sq mi)
                                               0.0845
STRTL CNSTL RTIMP
0.20 0.066 46.331
                                            BA
                    384
                    125
                                            LU
                                            * Runoff hydrograph computation (Chapter 6)
                                                 Using basin lag: 30.5 minutes
Using unit duration (Step 2): 1. min
Lag Time + Unit Duration / 2 (Step 3): 31.11960
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Volume of runoff (Step 4) V= 2.272951
1.803 3.955 6.546 9.238 12.026 14.983 17.372 20.000 24.055 27.569
30.893 34.920 39.041 43.238 47.883 52.555 57.259 62.759 68.502 74.530
                 सङ
                                                                                            62.759 68.502 74.530
84.458 80.116 75.689
                  UI
387
                                                                       86.838
52.894
                                          86.058
                                                    a6.991
                                                              87.571
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388
                  IJΙ
                       80.144
                                 84.734
                                                                                                      44.826
28.547
                                                                                             47.642
                                                                                                                43.023
                                                                                   50.415
                                 66.627
                                          62.247
37.345
                                                    58.247
                                                              55.395
                       71.182
389
                                                              34.144
                                                                       32.655
                                                                                   31,216
                                                                                             29.892
390
                  IIT
                       41.175
                                 39.288
                                         24.238
16.794
12.118
                                                                       21.575
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14.735
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                       26.354
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                                 25.334
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391
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                                                    16.242
11.856
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392
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1.986
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                        2.014
 401
                  UI
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                                                                                              1.360
                                                                          1.416
                                                                                                        1.332
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                                  1.568
                                            1.511
                                                      1.472
                        1.601
 402
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                                                                1.163
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                                                                                    1.106
                  UI
                        1,275
 403
                                                                0.925
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                        C=FLOW P=010YR-10DY A=GREENBRI
 405
 406
                  KK J
                     JXMIN Time interval for input data
60
                  IN
 407
 408
                  KM
                  * Design storm construction details
                  * Regional multiplier (zone 2) applied: 1.000
                  * Areal adjustment using area: 1.813
                       multiplier from table 4-4: 1.0000
                  * Adjusted depths for each duration from table 4-1: frequency: 10
* Duration---Regional-----Elev----Areal (adjustments)
* 5 min 0.2500 0.2500 0.2500
                                      0.3600
                                                  0.3600
                                                               0.3600
                                                   0.4300
                                                               0.4300
                                      0.4300
                    15 min
                    30 min
                                      0.5700
                                                  0.5700
                                                               0.5700
                                                   0.7700
                                                               0.7700
                    1 hour
                                                  1.0400
                                                               1.0315
                  * 2 hours
                                      1.0400
                    3 hours
                                       1.2300
                                                  1.2300
                                                               1,2200
                                                               1.6366
                  * 6 hours
                                      1.6500
                                      2.2500
2.9800
                                                  2.2500
                                                               2.2500
                                                   2.9800
                                                               2.9800
                  * 24 hours
                    36 hours
                                      3.5400
                                                  3.5400
                                                               3.5046
                                      3.9500
                                                  3.9500
                                                               3.9500
                    2 days
                                                               4.6500
                  * 3 days
                                      4.6500
                                                  4.6500
                                                  5.7600
7.5400
                                                               5.7024
                    5 days
                  * 10 days 7.5400 7.5400 7.4646

* Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646
                                                                                                                                PAGE 16
                                                       HRC-IL INPUT
                 ID...,.1.....2.....3.....4......5,.....6......7......8.....9.....10
LINE
 409
                  PR

        0.0821
        0.2015
        0.1128
        0.0373
        0.0224
        0.0075
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 413
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 419
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                                           0.3956
                                                     0.1642
                                                                                   0.0448
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                                 0.1120
 420
                  PI
                       0.0672
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 422
                                                                0.0373
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                                                                                    0.0523
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                                                                                                                  0.0821
 423
                  PI
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                                 0.1045
                                          0.1194
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                  PI
                       0.0970
                                                     0.1269
                                                               D.1344
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 424
                                                                         0.0224
                                                     0.2463
                                                                0.0373
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 425
                  PI
                       0.2314
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 427
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                  PI
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                  PI
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                                           0.0523
                                                     0.0448
                                                               0.0373
                                                                          0.0299
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 429
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 431
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 432
                  PI 0.0000
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                                                                                   0.0597
                                                                                                       0.0299
                                                                                                                  0.0149
                  PI 0.0149 0.0373 0.0523 0.0746
                                                              0.2165 0.1194
                  * Precipitation losses computation (Chapter 5)
                       Computing RTIMP (percent impervious) from land use and table 5-2
Computing CNSTL (infiltration rate) from soil type and table 5-2
                  * TAREA Subbasin area (sq mi)
BA 0.0859
* STRTL CNSTL RIMP
LU 0.20 0.056 75.173
 434
 435
                  * Runoff hydrograph computation (Chapter 6)
                       Using basin lag: 19.3 minutes
Using unit duration (Step 2): 1. min
Lag Time + Unit Duration / 2 (Step 3): 19.84462
```

```
Volume of runoff (Step 4) V=
                                                                           49.10
                       4.52
                            11.00
107.46
                                       17.78
                                               25.11
                                                        30.86
                                                                  40.90
 436
                UI
                                                                139.50
                                                                         137.48
61.58
                                                                                  133.10 122.14
                                                                                                    110.85
                                      122.39
                                              134.99
 437
                IIT
                     93.35
                                                                                            53.31
                                                                                                     49.67
                                       84.05
40.80
                                                                  66.33
                UI
                               90.31
                                                77.65
                                                         70.88
 438
                                                                  33.80
                                                                                            28.67
                                                          36.00
                                                                           33 86
                                                                                    30.23
                                                38.20
 439
                III
                      46.35
                              43.23
                                                                                    18,29
                                                                                             17.52
                                                                                                      16.98
                              24.39
15.81
                     25.66
15.36
                                       23.24
                                                22.16
                                                         20.97
 440
                                                                                                      11.72
                                                                                    12.63
                                                          14.07
                                                                  13.59
                                                                           13.06
 443
                uı
                                                                            9.08
                                                                                     8.76
                                                                                              8.52
                                                                                                       8.22
                OI
OI
                     11.32
                                                           9.81
                              10.94
                                       10.55
                                                10.16
                                                                                                       5.74
3.95
                                         7.32
                                                 7.07
                                                           6.86
                                                                   6.61
 443
                                                 4.92
                                                                   4.54
                                                                            4.38
3.16
                                                                                     4.24
                                                                                              4.09
                UI
                       5.53
                                5.31
                                        5.15
                                                                                                       2.81
                                        3.53
                                                           3.37
                                                 3.44
 44.5
                                                                                     2.11
                                                                                              2.04
                                                                                                       1.97
                                                           2.32
                                                                    2 25
                                                                            2.18
 446
                UI
                       2.74
                               2.61
                                                                   1.61
                                                                            1.54
                       1 90
                               1.83
                                         1.75
                                                 1.68
                                                           1.68
 447
                      C-FLOW F-010YR-10DY A-
 448
                21
                                                                                                                 PAGE 17
                                                 HEC-1L INPUT
               ID.....1.....2.....3......4......5,......6......7.....8.....9.....10
LINE
                KK OFF-N
 449
                            Time interval for input data
                   JXMIN
                        60
                IN
 450
                     R5
 451
                KM
                 * Design storm construction details
                 * Regional multiplier (zone 2) applied: 1.000
                * Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                5 min
                                   6.2500
                                             0.2500
                                                         0.2500
                                                         0.3600
                  10 min
                                  0.3600
                 * 15 min
                                  0.4300
                                             0.4300
                                                         0.4300
                                             0.5700
                                                         0.5700
                                  0.5700
                   30 min
                                                         0.7700
                 * 1 hour
                                  0.7700
                                             1.0400
                   2 hours
                                  1.0400
                                                         1.0315
                                                         1.2200
                 * 3 hours
                                  1.2300
                                  1.6500
2.2500
                                             1.6500
                                                         1.6366
                                                         2.2500
                                              2.2500
                   12 hours
                 * 24 hours
                                  2,9800
                                             2.9800
                                             3.5400
3.9500
                                                         3.5046
                   36 hours
                * 2 days
* 3 days
                                  3.9500
                                  4.6500
5.7600
                                              4.6500
                                                         4.6500
                                              5.7600
                   5 days
                * 10 days 7.5400 7.5400 7.4546

* Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646
 452
                 PT 0.0224 0.0821 0.2015 0.1120
                                                                          0.0075 0.0000 0.0000 0.0000
 453
454
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457
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 458
                 PI
                     0.0299
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 459
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 450
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 461
462
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 464
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 466
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                                                0.0224
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                                                                  0.1418
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                                                         0.1344
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                     0.0970
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 467
                 ΡI
                                                                  0.0224
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 469
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 472
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 474
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                    0.0000 0.0000 0.0000
                                               0.0000 0.0000
                                                                                                                  PAGE 18
                                                  HEC-1L INPUT
               ID.....1,.....2.....3......4......5,.....6......7......8,......9.....10
LINE
                PI 0.0149 0.0373 0.0523 0.0746 0.2165 0.1194 0.0597 0.0448 0.0299 0.0149
 476

    Precipitation losses computation (Chapter 5)

                   Computing RTIMP (percent impervious) from land use and table 5-2 Computing CNSTL (infiltration rate) from soil type and table 5-2 TARRA subbasin area (sq mi)
                HA 0.8438
* STRTL CNSTL RTIMP
LU 0.20 0.070 2.000
 477
 478
                 * Runoff hydrograph computation (Chapter 6)
                    Using basin lag: 78.2 minutes
Using unit duration (Step 2): 1. min
                    Using Time + Unit Duration / 2 (Step 3): 78.67958
Volume of runoff (Step 4) V= 22.687500
2.81 5.63 8.44 11.34 15.39 19.43
40.21 44.51 49.13 53.75 58.37 62.68
                                                                          23.48
                                                                                   27.55
                 ui
                                                                                              73.11
                                                                            66.16 69.63
 480
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2.310764

1

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102.35 107.41 112.47 117.52
161.55 168.10 175.07 182.33
                      83.86
                               90.19
                                         96.52
                UI
481
                                                                   175.07
252.06
                                                                                     189.59
                                                                                              196.84
                                                                                                        204,16
                              148.44 155.00
218.85 226.19
                 ŦŦŦ
                     142.02
211.50
 482
                                                                                      270.09
                                                                            260.81
                                                234.56
324.17
                                       226.19
                                                          243.31
                 ΨI
 483
                                                          332.74
                                                                    335.30
                                                                            337.37
                                                                                      339.44
                                                                                              341.51
                                                                                                        342.66
                                        315.59
                 UI
                     298.32
                              307.02
                                                                                      339.21
                                                                                                        335.07
                                                                            341.27
                                       345.96
318.48
                                                344.82
311.66
                                                          343.67
                                                                    342.53
 485
                                                                   297.75
229.72
                                                                            290.71
                                                                                      283.68
                                                                                              276.61
                                                                                                        269.49
 486
487
                 trr
                     332.11
                              325.29
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                              255.24
205.02
                                                          235.96
                     262.36
                                        248.45
                                                242.21
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                                                                                                        173.04
                                        201.15
                                                 197.28
                                                          193.00
                                                                    188.43
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                     208.89
 488
                                                                    155.66
                                                                            152.64
                                                                                      149.61
                                                                                               146.57
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ni
                     170.22
                              167.41
                                        164.50
                                                161.55
 489
                                                                                               122.89
                                                                                                        120.82
                                                          131.95
110.35
                                                                                      124.96
                                        136.57
                                                 134.28
                                                                    129.62
                                                                            127,29
                              138.85
                     141.14
 490
                                                                    108.31
                                                                             106.85
                                                                                      105.41
                                                                                               103.96
                                                                                                        102,46
                OI.
                     118.75 116.68
100.75 99.03
                                        114.57
                                                112.16
                                                                                       90.22
                                         97.32
                                                  95.69
82.09
                                                            94.32
                                                                     92.96
                                                                              91.60
                                                                                                88.81
 492
                                                                              78.58
68.39
                                                                                       77.53
57.43
                                                                                                76.47
                                                                                                          75.48
                                                            80.82
                 UI
                      86.00
                                84.64
                                         83.37
                                                                                                          65.67
                                                  71.69
62.39
                       74.56
                                73.64
                                         72.71
                                                            70.59
                                                                     69.49
 494
                                                                     60.81
                                                                              60.02
                                                                                       59,22
                                                                                                58.43
                                                                                                          57,83
                 UI
UI
                                         63.18
 495
                      64.79
                                63.97
                                                                              52.62
                                                                                                          51.16
                      57.25
                                56.68
49.87
                                         56.11
                                                  55.26
48.29
                                                            54.38
                                                                     53.50
 496
                                                            47.54
43.18
                                                                                       46.49
                                                                                                46.09
                                                                                                          45.47
                                         49.08
                                                                     47.39
                                                                              46.84
                 IJΙ
                      50.66
 497
                                                                                       42.16
                                                                                                41.72
38.04
                                                                     42.92
                                                                              42.60
                                                                                                          41 28
                 UI
                                44.24
40.58
                      44.86
                                         43.71
                                                  43.45
 498
                                                  39.97
36.13
                                                            39.62
                                                                     39.23
                                                                              38.83
                      40.89
 499
                                                                              35.13
32.02
                                                                                       34.86
31.71
                                                            35.78
                                                                                                 34.60
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                 UI
UI
                                36.85
                                         36.48
                                                                                                          31.26
28.37
                      34.01
                                         33.31
30.52
                                                  32.96
30.21
                                                                     32.33
                                33.66
                                                            32.64
 501
                                                            29.90
27.35
                                                                     29.60
27.04
                                                                                       28.98
                                                                              29.29
                                                                                                28.67
                                30.82
 502
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24.27
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                 OI
OI
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 503
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22.76
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                                25.71
 504
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IU
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                                         23.02
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                                         21.14
19.25
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                                                            20.97
                                                                     20.77
 506
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17.18
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 507
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                                         13.44
                                                            13.18
                                                                     13.04
 511
                                                                              11.71
                                                            11.88
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                 UI
UI
 512
                      12.53
                                12.36
                                         12.18
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                       11.24
                                         11.01
                                                   16.92
                                                            10.93
                                                                     10.74
 513
                                                                      9.86
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8.90
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 514
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                      10.30
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UI
                                 9.34
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8.51
                        9,42
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 515
                                                    8.47
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7.81
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                        8.60
 516
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                                                                      5.98
                                                                               6.94
                                                                                         6.89
                        7.30
 518
                                                                                                                      PAGE 19
                                                    HEC-1L INPUT
                                                                      ...6......7......8.....9.....10
               ID.....3......4...
LINE
                                                    6.51
                                                             6.42
                                                                      6.37
                                                                                6.32
                                                                                         6.28
                 UI
 519
                                                             5.80
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5.31
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5.27
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5.23
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5.18
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5.14
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 520
                 UI
                       6.06
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                                 5.98
                                          5.89
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                 UI
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 521
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                        4.21
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 526
                      C=FLOW F=010YR-10DY A=GREENBRI
 527
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 528
 529
                 KM
                 H.
                      C-PLOW
 531
 532
                 KK
                   JXMIN Time interval for input data
                 IN
 533
                 * Design storm construction details
                * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                 * Adjusted depths for each duration from table 4-1: frequency: 10
                 * Duration----Regional------Elev-----Areal (adjustments)
                                   0.2500
                                             0.2500
                                                          0.2500
                                               0.3600
                                                           0.3600
                                   0.3600
                   10 min
                   15 min
                                   0.4300
                                               0.4300
                                                           0.4300
                   30 min
                                               0.5700
                                                           0.5700
                                   0.5700
                * 1 hour
                                   0.7700
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                                                           0.7700
                     hours
                                   1.0400
                                              1.0400
                                                           1.0315
                                                           1,2200
                 * 3 hours
                                   1.6500
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                                                           1 6366
                                                           2.2500
                  12 hours
                * 24 hours
                                   2.9800
                                               2.9800
                                                           2.9800
                                               3.5400
                                                           3.5046
                                   3.5400
                  36 hours
                * 2 days
                                   3.9500
                                               3.9500
                                                          3.9500
                * 3 days
                                   4.6500
                                                           4.6500
                * 5 days
                                   5.7600
                                               5.7600
                                                          5,7024
                                   7.5400
                                              7.5400
                                                           7 4545
                 * Storm duration: 10, length: 240 ordinates
                * Distrubution using table 4-8 of total rainfall: 7.4646
535
                PB
                PI 0.0224 0.0621 0.2015
536
537
                                                0.1120
                                                          0.0373
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540
                PI 0.0373 0.0523 0.0672 0.0970
                                                         0.2239
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123.15 129.44

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PI 0.0299 0.0224 0.0149 0.0075 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 PI 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
                      542
                                                                                                                                                                                                                        PAGE 20
                                                                                                           HEC-1L INPUT
1
                                               ID......1.....2......3.....4......5,.....6......7.....8......9......10
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                                                 PI 0.0149 0.0373 0.0523 0.0746 0.2165
                                                                                                                                     0.1194
                       559
                                                 * Precipitation losses computation (Chapter 5)
                                                         Computing RTIMP (percent impervious) from land use and table 5-2
Computing CNSTL (infiltration rate) from soil type and table 5-2
                                                       TAREA subbasin area (sq mi)
                                                  * TAREA
                      560
                                                                     CNSTL RTIMP
                                                  * STRTL
                       561
                                                 133
                                                           0.20 0.064 47.945
                                                 * Runoff hydrograph computation (Chapter 6)
                                                        Using basin lag: 24.8 minutes
Using unit duration (Step 2): 1. min
                                                        Lag Time + Unit Duration / 2 (Step 3): 25.30745
Volume of runoff (Step 4) V= 1.693160

        volume
        or runoff
        (Step 4)
        V=
        1.693160

        2.030
        4.713
        7.691
        10.795
        14.126
        16.683
        20.577
        24.770
        28.545
        33.081

        37.785
        42.822
        48.078
        53.458
        59.771
        66.472
        72.929
        77.779
        79.257
        80.081

        79.662
        78.512
        76.256
        71.339
        66.270
        61.150
        56.282
        52.049
        49.226
        46.431

        43.313
        40.484
        38.444
        36.318
        34.140
        32.258
        30.599
        28.925
        27.434
        25.918

        24.637
        23.544
        22.307
        21.318
        20.312
        19.339
        18.448
        17.686
        17.012
        16.264

                      563
                                                 u
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6.625
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6.106
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                      568
                                                 UI
                                                        10.602
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                                                          7.913
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4.005
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3.910
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                      575
                                                 UI
                                                          1.464
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                                                          0.843
                      577
                                                 UI
                      578
                                                          C=FLOW F=010YR-10DY A=GREENBRI
                                                                                                                                                                                                                          PAGE 21
                                                                                                           HEC-1L INPUT
1
                                               ID.....1.,.....2......3......4.......5,......6......7.....8......9......10
                    LINE
                      579
                                                 KK L
                                                     JXMIN
                                                                     Time interval for input data
                                                                60
                                                 IN
                      580
                                                 * Design storm construction details
                                                 * Regional multiplier (zone 2) applied: 1.000
                                                 * Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000

    Adjusted depths for each duration from table 4-1: frequency: 10
    Duration----Regional------Elev-----Areal (adjustments)

                                                                                0.2500
                                                                                                   0.2500
                                                                                                                      0.2500
                                                                                0.3600
                                                                                                   0.3600
                                                                                                                      0.3600
                                                   10 min
                                                                                                   0.4300
                                                 * 15 min
                                                                                0.4300
                                                                                                                      0.4300
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                                                    30 min
                                                                                0.5700
                                                   1 hour
                                                                                0.7700
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                                                    2 hours
                                                                               1.0400
                                                                               1.2300
1.6500
                                                 * 3 hours
                                                                                                   1.2300
                                                                                                                      1,2200
                                                                                                                       1.6366
                                                    6 hours
                                                   12 hours
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                                                    24 hours
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                                                    5 days
                                                                               5.7600
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                                                                                                                      5.7024
                                                                                7.5400
                                                                                                   7.5400
                                                    10 days
                                                   Storm duration: 10, length: 240 ordinates
                                                    Distrubution using table 4-8 of total rainfall: 7.4646
                      582
                                                                a
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                                                PI 0.0224
                                                                     0.0821 0.2015 0.1120 0.0373
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                      586
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0.0523 0.0672 0.0970 0.2239 0.1418 0.0746 0.0597 0.0448 0.0373 0.0224 0.0149 0.0075 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
                   PI 0.0373
 587
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 588
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                                                                                               0.1120 0.0896
                                                                                                                   0.0672
                        0.0970
  597
                   PI
                                                                                                        0.0075
                                  0.2911 0.5001
0.0000 0.0000
                                                                 0.0373 0.0224
                                                                                               0.0075
                                                                                                                   0.0075
                        0.2314
                                                      0 2463
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                   PI
PI
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                                            0.0224
                                                       0.0299
                                                                 0.0373 0.0523
                                                                                    0.0672
                                                                                               0.0970 0.2911
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                                  0.0149
                        0.0075
  601
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                                                                                     0.0224
  602
                   PI
                        0.0746
                                  0.0597
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                                                      0.0448
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  605
                                                                                                                                 PAGE 22
                                                        HEC-1L INPUT
                 ID......1.....2.....3.....4.....5,.....6......7....8......9......10
LINE
                   PI 0.0149 0.0373 0.0523 0.0746 0.2165 0.1194 0.0597 0.0448 0.0299 0.0149
 606
                   * Precipitation losses computation (Chapter 5)

* Computing RTIMP (percent impervious) from land use and table 5-2

* Computing CNSTL (infiltration rate) from soil type and table 5-2

* TAREA subbasin area (sq mi)
                   BA 0.0330
* STRTL CNSTL RTIMP
LU 0.20 0.060 70.000
  607
  608

    Runoff hydrograph computation (Chapter 6)

                        Using basin lag: 10.8 minutes
Using unit duration (Step 2): 1. min
Lag Time + Unit Duration / 2 (Step 3): 11.25192
                       Lag Time + Unit Duration / 2 (Step 3): 11.25192

Volume of runoff (Step 4) V= 0.886493
6.407 14.667 22.873 33.597 45.864 59.705 76.233 91.581
79.589 66.331 57.178 49.115 43.425 38.013 33.648 29.652
21.516 19.636 17.744 16.220 14.903 13.668 12.625 11.742
9.615 9.027 8.495 7.940 7.493 7.046 6.604 6.137
5.081 4.776 4.504 4.225 3.973 3.721 3.494 3.232
2.680 2.512 2.354 2.270 2.139 1.982 1.876 1.745
                                                                                              91.581 94.540
29.652 26.656
                                                                                                                   91 593
 609
                                                                                                                   23.939
                                                                                                        11.022
                                                                                                                   10.309
  611
  612
                   TI
                                                                                                           3.016
                                                                                                                     2.848
  613
                                                                           1.982
  614
                   UI
                                 2.512
1.361
                                           2.354
                                                       1.193
                                                                  1.135
                                                                                      0.993
                         C-FLOW F-010YR-10DY A-GREENBRI
  616
                  KK M * JXMIN Time interval for input data IN \phantom{+} 50 \phantom{+}
 617
 618
                   * Design storm construction details
                   * Regional multiplier (zone 2) applied: 1.000
                   * Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                    Adjusted depths for each duration from table 4-1: frequency: 10
                   * Duration---Regional-----Elev-----Areal (adjustments)
* 5 min 0.2500 0.2500 0.2500
                                                    0.3600
                                                                 0.3600

10 min

                                       0.3600
                                                   0.4300
                                                                0.4300
                                       0.4300
                     30 min
                                       0.5700
                   * 1 hour
* 2 hours
                                       0.7700
                                                    0.7700
                                                                 0.7700
                                       1.0400
                                                    1.0400
                                                                 1.0315
                   * 3 hours
                                       1 2300
                                                   1.2300
                                                                 1.2200
                                      1.6500
2.2500
                                                                 1.6366
                   * 6 hours
                                                   2,2500
                    12 hours
                                                                 2,2500
                                       2.9800
3.5400
                                                   2.9800
3.5400
                    24 hours
36 hours
                                                                2,9800
                                                                 3.5046
                   * 2 days
                                       3.9500
                                                   3.9500
                                                                 3.9500
                     3 days
                  * 5 days 5.7600 5.....

* 10 days 7.5400 7.5400 7.4646

* Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646

HEC-1L INPUT
                                                                                                                                  PAGE 23
                 ID......3......4.......5,......6......7.....8......9......10
LINE
 620
                      0.0224 0.0821 0.2015 0.1120 0.0373 0.0224 0.0075 0.0000 0.0000 0.0000
                  PI
PI
 621
                                                                0.000.0 0.000.0
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                                                                                               0.0597
                                                                                                         0.0448
                                                                                                                   0.0373
                  PI
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                                           0.0672
                                                      0.0970
 625
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 626
                  PI
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                                 0.0224
                                           0.0149
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 630
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                                                                0.0149 0.0224
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                                                                                               0.0373 0.0448
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                                                               0.0746 0.0597
0.0075 0.0000
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632

0.0224 0.0149

0.0149 0.0075

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0.0373 0.0448 0.0523
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633
                 PI 0.0000
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0.0896
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                                0.0149 0.0149
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 634
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                                0.1045
 635
                  PI
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                  PΙ
                      0.0075
 639
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                 PI
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                                                  0.0746
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                                                                      0.1194 0.0597
                                                                                          0.0448
                               0.0373
                                         0.0523
                  PI 0.0149
                 * Precipitation losses computation (Chapter 5)

* Computing RTIMP (percent impervious) from land use and table 5-2

* Computing CNSTL (infiltration rate) from soil type and table 5-2

* TARKA subbasin area (sq mi)

BA 0.0666
 645
                    STRTL CNSTL RTIMP
J 0.20 0.040 95.000
                  LU
 646
                  * Runoff hydrograph computation (Chapter 6)
                      Using basin lag: 26.3 minutes
Using unit duration (Step 2): 1. min
Lag Time + Unit Duration / 2 (Step 3): 26.79198
                      Lag Time + (Unit Diraction / 2 (seep 3): 28.7333

Volume of runoff (Step 4) V= 1.789792

1.915   4.383   7.174   10.047   13.183   15.826

34.851   39.310   44.219   49.193   54.442   60.397

79.827   79.723   78.803   77.397   73.123   68.404
                                                                               18.777 23.086
66.766 72.836
                                                                                                  26.559
77.583
                                                                                                             30.522
                  TIT
                                                                                                             78.990
51.019
 648
                  ΨI
                                                                      68.404
36.253
                                                                                63,604
                                                                                          58.757
                                                                                                    54.429
 649
650
                  u
                                                                                                             29.237
18.246
                                                                                          32.383
                                                                                                    30.823
                                                                                34.198
                  UI
                      48.362
                               45.729 42.689
26.377 25.000
                                                   40.188
24.013
                                                             38.257
                                                   24.013 22.883 21.825
15.503 14.909 14.371
                                                                                20.894
                                                                                                    19.048
                                                                                          19.936
 651
                                                                                13,832
                                                                                          13.353
                                                                                                    12.952
                                                                                                             12.354
                  UI
                      17,536
                                16.908 16.189
                                                   8.119
                                                             10.409 10.076
7.939 7.701
                                                                                  9.894
7.481
5.707
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                      11.949
                                11.540
                                         11.013
                                                                                           9.595
 653
                                                                                           7.290
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                                 8.588
 654
                  UI
                       8.858
                                           8.339
                                                                                                               5.261
4.050
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                                 6.539
                                           6.420
4.896
                                                     6.215
4.809
                        6.723
                                                              6.060
                                                                        5.917
 655
                                                               4.629
                                                                        4.503
                                                                                  4.383
                                                                                            4.264
                                                                                                     4.144
 656
                  UI
                       5.142
                                                                                                               3.113
2.358
                                                                                  3.382
                                                                        3,472
                  ui
                        3.961
                                 3.865
                                           3.745
                                                     3.651
                                                              3.561
 657
                                                     2,758
                                                              2.698
                       3.023
                                           2.869
                                                                        2.614
                                                                                  2.538
                                                                                           2.478
                                                                                                     2.418
 658
                                                                                           1.942
                                                                                                               1.842
                                                                        2.002
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                  UI
                       2 299
                                 2.239
                                           2.179
                                                     1,642
                                                              1.612
                                                                                            1.482
                                                                                                     1.452
                                           1.701
                                                                        1.582
                                                                                  1.542
                       1.812
 660
                                                                                  1.173
                                                                                           1.143
0.884
                                                                                                     1 113
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                  UI
UI
                       1.353
                                 1.323
                                           1.293
                                                                                                               0.842
                                 1.023
                                           0.993
                                                     0.964
                                                              0.962
                                                                        0.944
 662
                                                                                                                           PAGE 24
                                                      HEC-1L INPUT
                LINE
                      C=FLOW F=010YR-10DY A=GREENBRI
 663
 564
                  KK N
                     JXMIN Time interval for input data
                  IN
                           60
 665
                  * Design storm construction details
                  * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 1.813
* multiplier from table 4-4: 1.0000
                  * Adjusted depths for each curation from table 4-1: frequency: 10
                  * Duration----Regional-----Elev-----Areal (adjustments)
                  * 5 min
                                     0 2500
                                                0.2500
                                                             0.2500
                                                              0.3600
                    10 min
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                    15 min
                                     0.4300
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                                                              0.4300
                                                              0.5700
0.7700
                                     0.5700
                    30 min
                                                 0.7700
                  * 7 hour
                                     0.7760
                                      1.0400
                                                 1.0400
                                                              1.0315
                    2 hours
                                                              1.2200
                                                 1.2300
                  * 3 hours
                                     1.2300
                  * 6 hours
                                     1.6500
                                                 1.6500
                                                              1.6366
                                     2.2500
                                                 2.2500
                                                              2,2500
                   12 hours
                  * 24 hours
                                     2,9800
                                                 2.9800
                                                              2.9800
                    36 hours
                                                              3.5046
                                                              3.9500
                  * 2 days
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                                     4.6500
5.7600
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5,7600
                   3 days
                                                              4 6500
                                                              5.7024
                   5 days
                  * 10 days 7.5400 7.5400 7.4646

* Storm duration: 10, length: 240 ordinates

* Distrubution using table 4-8 of total rainfall: 7.4646
 667
                                                                                 0.0075
                                                                                                              0.0000
                  PT 0.0224 0.0821 0.2015 0.1120
                                                             0.0373
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 668
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                                                              0.2239
                                                                       0.1418
                                                                                 0.0746
                                                                                                       0448
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                                                   0.0970
 672
                  PI
                      0.0373
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 681
                  PI
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                       688
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                                                                                                         HEC-1L INPUT
1
                                               LINE
                                                 PI 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 PI 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0
                       689
                       690
                                                 PI 0.0149 0.0373
                                                                                     0.0523 0.0746 0.2165 0.1194 0.0597 0.0448 0.0299 0.0149
                       691
                                                 * Precipitation losses computation (Chapter 5)

* Computing RTIMP (percent impervious) from land use and table 5-2

* Computing CNSTL (infiltration rate) from soil type and table 5-2
                                                        Computing Casts (Intititation
TAREA subbasin area (sq mi)
0.0375
STRTL CNSTL RTIMP
                                                      TAREA
                       692
                                                      0.0375
STRTL
                       693
                                                 111
                                                         0.20 0.068 43.112
                                                      tunoff hydrograph computation (Chapter 6)

Using basin lag: 19.1 winutes

Using unit duration (Step 2): 1. min

Lag Time + Unit Duration / 2 (Step 3): 19.61394

Volume of rusoff (Step 4) V= 1.008333

2.030     4.928     7.964     11.204     13.886     18.309     22.045     26.572     31.346     36.548

42.014     48.382     54.963     9.839     61.126     61.438     60.404     57.745     52.812     47.756

42.915     39.157     36.372     33.371     30.707     28.647     26.506     24.625     22.972     21.414

43.915     39.157     36.372     33.371     30.707     28.647     26.506     24.625     27.7315
                                                 * Runoff hydrograph computation (Chapter 6)
                       594
                                                 ETT
                       695
                                                 UI
                       696
                                                 UI
                                                                      18.699 17.541
10.491 10.056
                                                                                                     16.479
9.460
                                                        11.057
                                                                                                                      9.076
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4.544
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2.728
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                                                          C=FLOW F=010YR-10DY A=GREENBRI
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                      707
                                                      JXMIN Time interval for input data
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                                                               60
                                                 KIM
                       709
                                                 * Design storm construction details
                                                 * Regional multiplier (zone 2) applied: 1.000
* Areal adjustment using area: 1.813
                                                        multiplier from table 4-4: 1.0000
                                                    Adjusted depths for each duration from table 4-1; frequency: 10 Duration---Regional-----Elev-----Areal (adjustments) 5 min 0.2500 0.2500 0.2500
                                                    10 mis
                                                                              0.3600
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                                                    2 hours
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7.5400
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7.4646
                                                   10 days
                                                * Storm duration: 10, length: 240 ordinates
* Distrubution using table 4-8 of total rainfall: 7.4646
1
                                                                                                       HEC-1L INPUT
                                                                                                                                                                                                                   PAGE 26
                    LINE
                                              710
                                                      0.0224 0.0821
0.0000 0.0000
                                                                                    0.2015 0.1120 0.0373 0.0224 0.0075
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0.2911 0.5001 0.2463 0.0373 0.0224 0.0149 0.0075 0.0075 0.0075

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PI 0.2314

PI

684

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0.0672 0.0970
0.0224 0.0149
                    0.0075 0.0149 0.0224 0.0299 0.0373
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                                                                   0.0523
729
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                                        0.0523
                                                 0.0746
                                                          0.2165
                                                                    0.1194
                              0.0373
734
                    0.0149
                Precipitation losses computation (Chapter 5)

* Computing RTIMP (percent impervious) from land use and table 5-2

* Computing CNSTL (infiltration rate) from soil type and table 5-2
                    TAREA subbasin area (sq mi)
0.0402
STRTL CNSTL RTIMP
                   TAREA
735
                      0.20 0.070 50.000
                T.T.
736
                 * Runoff hydrograph computation (Chapter 6)

* Using basin lag: 15.2 winutes

* Using unit duration (Step 2): 1. min
                     Using unit duration (Step 2): 1. min

Lag Time + Unit Duration / 2 (Step 3): 15.66410

Volume of runoff (Step 4) V= 1.079757

3.700 8.650 14.029 18.671 25.815 32.663 40.437 49.127 58.596

79.786 81.989 82.075 79.942 72.282 63.797 55.826 50.481 45.662

37.576 34.011 31.250 28.611 26.091 24.250 22.347 20.679 19.122
                                                                                                         69.581
                                                                                                          41.057
 738
                                                                                                          17.893
                                                                    12.134
                                                                              7,070
                                                                                       10.743
6.735
                                                                                                           9.781
                              15.545 14.582
8.907 8.469
                                                 13.717
8.130
                                                           12,831
 740
                                                                                                  5.454
                                                            7.726
                                                                      7.41?
 741
                 UI
                      9.383
                                                                               4.462
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                                                            4.949
                                                                      4.673
                                                                                                  4.095
                                                                                                           3.911
                      5.858
                               5.635
3.578
                                         5.348
                                                  5.098
 742
                                                  3,261
                                                            3.103
1.995
                                         3.420
                                                                      2.975
                 UI
UI
 743
                                                                      1.901
                                                                                                  1.660
                                         2.134
1.366
0.879
                                                                               1 835
                                                                                        1.730
                                                                                                           1.601
                       2.345
                                2.239
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                                                   1.313
                                                            1.260
 745
 746
747
                 III
                       0.985
                                0.932
                       C=FLOW F=010YR-10DY A=GREENERI
                                                                                                                       PAGE 27
                                                    HEC-1L INPUT
               ID.....1.....2.....3.....4......5,.....6.....7.....8......9.....10
LINE
                          N Time interval for input data
                * JXMIN
 748
                 TN
 750
                 * Design storm construction details
                 * Regional multiplier (zone 2) applied: 1.000
                   Areal adjustment using area: 1.813
multiplier from table 4-4: 1.0000
                 * Adjusted depths for each duration from table 4-1: frequency: 10
                   Duration----Regional------Elev-----Areal (adjustments)
                                                            0.2500
                                    0.2500
                   5 min
                                                            0.3600
                   10 min
                                    0.3600
                                                0.3600
                                                            0.4300
0.5700
                   15 min
                 * 30 min
                                    0.5700
                                                0.5700
                                                0.7780
1.0400
                                    0.7700
                                                            0.7700
                   1 hour
                                                            1.0315
                 = 2 hours
                                    1.0400
                      hours
                                    1.2300
1.6500
                                                1.2300
                                                            1,2200
                                                            1.6366
                 * 6 hours
                 * 12 hours
* 24 hours
                                                            2.2500
                                    2.2500
                                                2,2500
                                                2.9800
3.5400
                                                            2.9800
                                                            3.5046
                 * 36 hours
                                    3.5400
                                    3.9500
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                 * 2 days
                                    4.6500
                 * 3 days
                 * 5 days
                                    5.7600
                                                5.7600
                                                            5.7024
                                    7.5400
                                                7.5400
                                                            7.4646
                   10 days
                   Storm duration: 10, length: 240 ordinates
                 * Distrubution using table 4-8 of total rainfall: 7.4646
 751
752
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                 PI 0.0224
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 755
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                                                     HEC-1L INPUT
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PI 0.0149 0.0373 0.0523 0.0746 0.2165 0.1194 0.0597 0.0448 0.0299 0.0149
               775
                                  * Precipitation losses computation (Chapter 5)
                                        Computing RTIMP (percent impervious) from land use and table 5-2 Computing CNSTL (infiltration rate) from soil type and table 5-2
                                     computing CMSTL (infiltration
TAREA subbasin area (sq mi)
A 0.0342
STRTL CMSTL RTIMP
U 0.20 0.062 56.384
               776
               777
                                   1.11
                                  * Runoff hydrograph computation (Chapter 6)

* Using basin lag: 16.5 minutes

* Using unit duration (Step 2): 1. min

* Lag Time + Unit Duration / 2 (Step 3): 17.01644

* Volume of runoff (Step 4) V= 0.920104

UI 2.600 6.153 9.967 13.380 18.241 22.789 28.286 34.177 40.506

UI 55.696 62.676 64.278 66.502 63.082 58.466 52.398 46.323 41.479

UI 34.392 31.539 28.996 26.479 24.484 22.572 20.756 19.368 17.921

UI 15.552 14.546 13.707 12.781 12.021 11.335 10.728 10.081 9.564

UI 8.577 8.137 7.838 7.527 7.202 6.861 6.571 6.316 6.030

UI 5.561 5.305 5.124 4.903 4.688 4.527 4.284 4.125 3.968
                                                                                                                                            47.656
38.101
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                                   UI
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                                                                                                             1.249
                                                                                                                        1.186
                                                                                                                                               1.078
               786
                                                                                       0.887
                                                                                                             0.811
                                   ш
                                          1 040
                                                    1.001
                                   UI
                                                     0.681
               788
                                          C-FLOW F-010YR-10DY A-GREENBRI
               789
                                   ZW
                                   ЖK
                                       DUMMY3
                                   KM
               791
               792
                                   HC
               793
                                   22
                                                                                                                                 _____
                                                                                                                                       U.S. ARMY CORPS OF ENGINEERS HYDROLOGIC ENGINEERING CENTER
     FLOOD HYDROGRAPH PACKAGE (HEC-1L)
                 JULY 1998
VERSION 4.1(L)
                                                                                                                                           609 SECOND STREET
DAVIS, CALIFORNIA 95616
                                                                                                                                                 (916) 756-1104
  RUN DATE 12JUL05 TIME 19:20:27
                                     10010 # 1010 #10024#1024
    3 IO
                       OUTPUT CONTROL VARIABLES
                                               3 PRINT CONTROL
0 PLOT CONTROL
                                IPRNT
                                TPLOT
                                                    D. HYDROGRAPH PLOT SCALE
                                QSCAL
                       HYDROGRAPH TIME DATA
                                                      1 MINUTES IN COMPUTATION INTERVAL
                                 NMIN
                                              31DEC99 STARTING DATE
                                IDATE
                                               0000 STARTING TIME
14947 NUMBER OF EYDROGRAPH ORDINATES
                                ITIME
                                   NO
                               NDDATE
                                              STAND O ENDING DATE
                                                  0906
                                                          ENDING TIME
                               NOTIME
                               ICENT
                                                   19 CENTURY MARK
                                                           0.02 HOURS
                          COMPUTATION INTERVAL
                                TOTAL TIME BASE 249.10 HOURS
              ENGLISH UNITS
                     DRAINAGE AREA
                                                   SQUARE MILES
                     PRECIPITATION DEPTH
                                                   TNCHES
                     LENGTH, ELEVATION
                                                   CUBIC FEET PER SECOND
                     PLOW
                     STORAGE VOLUME
                                                    acre-feet
                                                   ACRES
                     SURFACE AREA
                                                   DEGREES FAHRENHEIT
                     TEMPERATURE
TIME DATA FOR INPUT TIME SERIES
   5 IN
                                             60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE
2400 STARTING TIME
                               JXMIN
                              JXDATE
                              JXTIME
```

SUBBASIN RUNOFF DATA

```
SUBBASIN CHARACTERISTICS
TAREA, 0.12 SUBBASIN AREA
 32 BA
                   PRECIPITATION DATA
                                          7.46 BASIN TOTAL PRECIPITATION
                           STORM
  7 PB
                   INTFORM LOSS RATE
 33 LU
                                         0.20 INITIAL LOSS
                           STRTL
                                         0.06 UNIFORM LOSS RATE
60.15 PERCENT IMPERVIOUS AREA
                           CNSTL
                   INPUT UNITGRAPH, 173 ORDINATES, VOLUME = 1.00
2.9 6.5 10.7 15.1 15
51.3 57.9 64.7 72.2 75
 32 UI
                                                                                      24.2
87.5
125.7
                                                                                                               33.7
                                                                                                                           39.7
                                                                                                                                        45.0
                                                             15.1
72.2
129.7
                                                                         19.7
79.7
128.0
                                                                                                                           115.5
104.2
                                                                                                                                       124.4
96.9
                                                                                                              106.D
                                                                                                   96.5
                         51.3
127.7
                                                                                                  118.6
                                                                                                              111.5
61.4
                                                 130.7
80.4
                                     129.5
                                                                                                                                        55.2
                                                                                       67.4
41.3
27.5
                                                                           72.1
43.5
                                                               76.4
                                      84.4
                          90.2
                                                                                                   39.7
26.5
                                                                                                                            36.3
                                                                                                                                        34.9
                                                                                                               38.1
                          52.6
                                      50.2
32.0
                                                  47.8
30.7
                                                               45.6
                                                                                                                            24.5
17.5
                                                                                                                                        23.7
17.0
                                                              29.6
20.7
                                                                           28.5
19.8
                          33.5
                                                                                       19.3
14.6
                                                                                                   18.6
14.2
                                                                                                                17.9
                                                  21.5
15.7
12.2
                          22.9
                                      22.0
                                                                                                                13.8
                                                                                                                            13.4
                                                                                                                                         13.1
                                      16.2
12.5
                                                              15.4
11.9
                                                                           15.0
                                                                                                                            10.5
                                                                           11.6
9.1
7.0
                                                                                        11.3
                                                                                                   11.0
                          12.9
                                                                                                     8.6
                                                                                                                 8.4
                                                                                                                             8.1
6.4
                                                                                                                                          8.0
                                                                9.3
7.2
5.7
4.4
3.4
2.7
                                       9.8
7.6
                                                   9.5
7.4
                                                                                                                                          6.3
                                                                                         6.9
                           7.9
                                                                                                                 5.1
4.0
                                                                                                                              5.0
                                                                            5.5
                                                                                                     5.3
                                       5.9
4.6
3.6
                           6.1
                                                   5.8
                                                                                                                             3.9
                                                                                                                                          3.8
                                                                                                     4.0
                                                                            4.2
3.3
2.6
                                                                                        4.1
3.3
2.6
                                                   4.5
                           4.8
                                                                                                                 3.2
2.5
1.9
                                                                                                     3.2
                           3.7
                                                                                                                             2.4
1.9
                                                                                                                                          2.3
                                       2.9
2.2
1.7
                                                   2.8
                                                                2.1
                                                                            2.1
1.6
                                                                                         2.0
                                                                                                     2.0
                           2.3
1.8
                                                                                                                 1.5
                                                                                                                              1.5
                                                   1.7
                           1.4
                          ***
                                             ***
                             HYDROGRAPH AT STATION A
                                                      1.72. TOTAL EXCESS *
                                                                                     5.74
    TOTAL RAINFALL *
                           7.46, TOTAL LOSS =
                                                      MAXIMUM AVERAGE FLOW
PEAK FLOW
                 TIME
                                                                                    249.10-HR
                                                                         72-HR
                                            5-HR
                                                         24 - HR
                 (HR)
   (CFS)
                               (CFS)
               153.07
                                             16.
      33.
                                                                         3.390
                                                                                         5.736
                                           1.245
                           (INCHES)
                                                                           21.
                             (AC-FT)
                                                            15.
                            CUMULATIVE AREA =
                                                      0.12 SQ MI
*
 53 KK
                   TIME DATA FOR INPUT TIME SERIES

JOHN 60 TIME INTERVAL IN MINUTES
JUDITE 2400 STARTING DATE
JUTIME 2400 STARTING TIME
  54 IN
                  SUBBASIN RUNOFF DATA
                    SUBBASIN CHARACTERISTICS
TAREA, 0.04 SUBBASIN APEA
  BI BA
                    PRECIPITATION DATA
                           STORM
                                          7.46 BASIN TOTAL PRECIPITATION
  56 PB
                    UNIFORM LOSS RATE
  82 LU
                                     0.20 INITIAL LOSS
0.06 UNIFORM LOSS RATE
                           STRTL
                           CNSTL
                                          57.84 PERCENT IMPERVIOUS AREA
                    INPUT UNITGRAPH, 93
4.3 9.9
89.4 91.5
                                                            VOLUME = 1.00
  83 UI
                                          91 ORDINATES.
                                                  16.1
90.4
                                                               21.7
85.6
                                                                           29.6
76.0
                                                                                                                56.8
                                                                                        37.7
                                                                                                    46.8
                                                                                                    58.6
23.3
                                                                                                                53.3
21.5
                                                                                                                             47.2
20.0
                                                                                                                                         43.3
18.7
                          89.4
39.2
17.3
                                      35.8
                                                   32.6
15.2
                                                               29.8
14.2
                                                                           27.5
                                                                                        25.2
                                                                                        12.5
                                                                                                    11.8
                                                                                                                 11 3
                                                                                                                             10.8
                                                                                                                                         10.3
                                                                                                                  7.0
                                                                                                                              6.7
                                                                                                                                          6.4
                                                   8.9
5.6
3.5
                           9.8
                                       9.3
5.8
                                                                8.4
5.3
                                                                            8.1
5.0
                                                                                         4.8
                                                                                                     4.5
                                                                                                                 4.4
                                                                                                                              4.2
2,6
                           3.8
                                       3.6
                                                                3.3
                                                                            3.1
                                                                2.1
                                                                            2.0
                                                                                         1.9
                                                                                                     1.8
                                                    2.2
                                                                                                                 1.7
                                                                                                                              2.7
                                                                                                                                          1.6
                                       1.4
                                                   1.4
```

\*\*\*

HYDROGRAPH AT STATION B

7.46, TOTAL LOSS = 1.84. TOTAL EXCESS = 5.63 TOTAL RAINFALL » MAXIMUM AVERAGE FLOW PEAK PLOW TIME 249.10-HR 6-HR 24 - FR (HR) (CFS) (CFS) 3.329 5.617 (INCHES) 1.251 (AC-PT) 5.

> 0.04 SQ MI CTEMULATIVE AREA =

¢

95 IN TIME DATA FOR INPUT TIME SERIES

60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE JYMIN JXDATE 2400 STARTING TIME JXTIME

SUBBASIN RUNOFF DATA

SUBBASIN CHARACTERISTICS
TAREA, 0.06 SUBBASIN AREA 122 BA

1.2

PRECIPITATION DATA

7.46 BASIN TOTAL PRECIPITATION 97 98 STORM

UNIFORM LOSS RATE 123 LU 0.20 INITIAL LOSS STRTL

122 III

0.06 UNIFORM LOSS RATE 56.96 PERCENT IMPERVIOUS AREA RTIMP

INPUT UNITGRAPH, 114 ORDINATES, 19.4 102.1 E2.9 26.2 15.1 64.3 75.7 3.6 74.3 8.6 85.7 13.9 96.7 24.6 32.0 24.6 103.8 49.4 24.5 14.2 9.6 6.6 4.6 3.1 2.2 103.1 45.7 23.2 13.7 93.3 39.3 20.6 12.7 8.6 84.5 36.6 19.5 12.2 100.8 42.2 22.0 34.0 18.5 68.0 31.8 17.5 63.1 29.8 58.2 27.9 15.8 13.1 9.0 6.2 4.3 11.8 16,8 10.0 6.8 4.8 3.2 2.3 9,3 6,4 4,4 11.3 10.4 10.8 5.9 4.1 2.8 5.7 7.4 5.1 3.5 5.5 3.9 3.8 5.3 4.9 3.3 3.0 2.1 1.5 2.9 2.0 1.4 2.0 2.5 1.7 1.2 2.4 1.6 1.1 2.5 1.7 1.5

HYDROGRAPH AT STATION C

5.57 1.89, TOTAL EXCESS = TOTAL RAINFALL = 7.46, TOTAL LOSS =

MAXIMUM AVERAGE FLOW PEAK FLOW TIME 249 10-RR 24-HR 72-HR (CFS) (HR) (CFS) 153.02 (INCHES) 3.301 5.563 1.241 2,310 (AC-FT) 4.

> CUMULATIVE AREA = 0.06 SQ MI

\*\*\*

\*\*\*

137 KK D

24-25

```
TIME DATA FOR INPUT TIME SERIES
138 IN
                                   60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE
2400 STARTING TIME
                        JXMIN
JXDATE
                        JXTIME
                SUBBASIN RUNOFF DATA
                  SUBBASIN CHARACTERISTICS
165 BA
                                       0.05 SUBBASIN AREA
                         TAREA.
                  PRECIPITATION DATA
                                      7.46 BASIN TOTAL PRECIPITATION
140 PB
                         STORM
                  UNIFORM LOSS RATE
166 LU
                                      0.20 INITIAL LOSS
                         STRTL
                                       0.07 UNIFORM LOSS RATE
                         CNSTL
                                      47.04 PERCENT IMPERVIOUS AREA
                         RTIMP
                  INPUT UNITGRAPH, 111 ORDINATES,
                                                       VOLUME = 1.00
165 UI
                                                                               25.6
79.4
33.5
17.1
                                                                                          31.2
76.0
                                                                                                     37.6
                                                                                                                 44.5
                                                                                                                            51.8
                        2,9
60.1
50.7
                                              11.2
77.9
42.5
                                                         15.4
79.9
                                    6.9
                                                                                                     69.2
28.9
                                                                                                                62.2
26.9
                                                                                                                            55.6
25.0
                                   69.3
46.9
                                                                    80.7
                                                         39.4
19.2
11.0
7.4
                                                                                          31.2
16.1
                                                                    36.5
                                                                                                                 14.4
9.0
6.1
                                                                                                                            13.6
                        23.4
                                   21.9
12.2
                                                                    18.1
                                              20.5
                                                                                            9.7
6.6
                                                                                                       9.1
6.3
                                              11.6
                                                                    10.5
                                                                                10.1
                                                                                6.8
4.6
                                                                                                                             5.9
                         8.3
5.7
3.9
                                    8.0
                                                                                            4.5
                                    5.4
                                               5.2
3.6
                                                          5.0
3.4
                                                                     4.9
                                                                     3.3
                                                                                                                  2.8
                                                                                                                             2.7
                                                                                 3.2
                                                                                                       3.0
                                                                                 2.1
                                                                                                                  1.9
                                                                                                                             1.9
                                    2.5
                                               2.4
1.7
                                                          2.3
1.6
                         2.6
                                                                     1.6
                                                                                1.5
                                                                                                                             1.3
                                                                                                       1.4
                                                                                                                  1.3
                         1.8
1.2
0.8
                                                                                                       1.0
                                               1.1
                                    1.2
                                                          1.1
                        ***
                                         ***
                           HYDROGRAPH AT STATION D
                                                2.41, TOTAL EXCESS =
                        7.46, TOTAL LOSS =
    TOTAL RAINFALL =
                                                 MAXIMUM AVERAGE FLOW
PEAK FLOW
                TIME
                                                                            249.10-HR
                                                                   72-HR
                                        6-HR
                                                    24-HK
                (HR)
  (CFS)
                            (CFS)
                                       6.
1.192
             153.02
      14.
                                                     2.145
                                                                                 5.052
                         (INCHES)
                          (AC-PT)
                                                                                   13.
                                                 0.05 SO MI
                          CUMULATIVE AREA .
180 KK
                  TIME DATA FOR INPUT TIME SERIES
181 IN
                                   60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE
2400 STARTING TIME
                        JXMIN
                        JXDATE
                       JXTIME
                SUBBASIN RUNOFF DATA
                  SUBBASIN CHARACTERISTICS
208 BA
                                   0.04 SUBBASIN AREA
                        TAREA.
                  PRECIPITATION DATA
                        STORM
                                       7.46 BASIN TOTAL PRECIPITATION
183 PB
                  UNIFORM LOSS RATE
209 LII
                                  0.20 INITIAL LOSS
0.06 UNIFORM LOSS RATE
                        STRTL
                        CNSTL
                        RTIMP
                                      60.77 PERCENT IMPERVIOUS AREA
                  INPUT UNITGRAPH.
                                      93 ORDINATES.
                                                       VOLUME = 1.00
208 UI
                                  8.3
77.9
                                              13.5
77.6
                                                         18.0
75.1
                                                                    24.8
67.2
                                                                               31.4
59.1
22.4
11.2
                       3.6
75.9
                                                                                           38 9
                                                                                                      47 3
                                                                                                                 56 5
                                                                                                                            67.1
                                                                                          51.6
20.7
10.5
                                                                                                      47.0
                                                                                                                 42.2
                                                                                                                            38.2
                                              29.0
13.5
                                                         26.5
12.8
                                                                    24.2
11.8
                                                                                                      19.1
9.9
                                                                                                                 17.8
9.6
                                                                                                                            16.6
9.1
                       15.4
8.7
5.5
                                  14.4
                                                                                6.9
4.3
2.7
                                                                                                       6.3
                                                          7.5
                                                                     7.2
4.5
                                                                                                                  6.0
                                                                                                                             5.7
                                   8.3
                                               7.9
                                                                                            6.5
                                                                                                                  3.8
                                                                                                                             3.6
                                               4.9
                                   5.2
                                                                     2.9
                                                                                                       2.5
                                   4.3
                                                          3.0
```

```
1.6
                                                                                    1.7
                                           2.0
1.3
0.8
                      2.1
1.4
0.9
                                 2.0
1.3
0.8
                                                                          1.8
                      ---
                                     ***
                         HYDROGRAPH AT STATION E
                       7.46, TOTAL LOSS =
                                              1.67, TOTAL EXCESS =
                                                                       5.80
   TOTAL RAINFALL =
                                             MAXIMUM AVERAGE PLOW
PEAK FLOW
              TIME
                                     6-HR
                                                24-HR
                                                             72-HR
  (CFS)
               {HR}
                          (CPS)
          153.00
     11.
                                                                          5.788
                                                2.386
                        (INCHES)
                                    1.258
                                                    5.
                        (AC-FT)
                                             0.04 SO MI
                        CUMULATIVE AREA =
大军者 医骨骨 电电子 化水平 大水石 大水石 大水石 化水子 化水子 化水子 化水子 化水子 化水子 化水子 化水子 化水子 化光光 大大水 大大水 大大水 大大水 大大水 大水子 大水子 大水子
221 KK
                 HYDROGRAPH COMBINATION
223 HC
                                       5 NUMBER OF HYDROGRAPHS TO COMBINE
                       ICOMP
                                                       ***
                         HYDROGRAPH AT STATION DUMMY1
                                              MAXIMUM AVERAGE PLOW
               TIME
PEAK FLOW
                                                 24-HR
                                                                      249.10-HR
               (HR)
  (CFS)
                          (CFS)
                                                                           4.
5.587
                                      41.
                                                   19.
             153,02
                                                 2.318
                                                             3.314
54.
                         (AC-FT)
                                      20.
                                                   38.
                        CUMULATIVE AREA =
                                             0.31 SQ MI
225 KK
 226 IN
                 TIME DATA FOR INPUT TIME SERIES
                                 60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE
2400 STARTING TIME
                      JXMIN
               SUBBASIN RUNOFF DATA
                 SUBBASIN CHARACTERISTICS
 253 BA
                                    0.05 SUBBASIN AREA
                 PRECIPITATION DATA
                                    7.46 BASIN TOTAL PRECIPITATION
                       STORM
228 PB
                 UNIFORM LOSS RATE
254 LU
                               0.20 INITIAL LOSS
                       STRTL
                       CNSTL
                                   0.07 UNIFORM LOSS RATE
49.51 PERCENT IMPERVIOUS AREA
                       RTTMP
                 INPUT UNITGRAPH, 98 ORDINATES, VOLUME = 1.00
253 UI
                                                                                    41.3
67.3
26.9
13.6
8.5
                                                               26.6
84.8
                                8.9
88.1
                                           14.4
89.8
                                                     19.2
88.7
                                                                          33.3
                       3.8
                                                                          76.2
28.9
14.7
8.9
5.7
                                                                                              59.3
24.8
12.9
                                                                                                         54.2
23.1
12.2
7.8
5.0
3.3
                                                                                                                   49.1
21.4
                      81.5
44.5
20.0
                                                     34.3
16.4
9.7
6.3
4.1
                                40.9
                                           37.1
17.5
                                                               31.5
                                18.8
10.6
6.8
4.4
                                                                                                                   11.5
7.4
                      11.1
                                           10.2
                                                                9.2
                                                                                                5.3
                                                                                                                    4.8
                                           6.5
                                                                                     5.5
3.6
                       4.6
```

```
2.3
1.5
1.0
                                                                                                                                           2.0
1.3
                                                                                         2.4
1.5
1.0
                           2.9
2.0
1.3
                                                                            1.6
                          ***
                             HYDROGRAPH AT STATION F
                           7.46, TOTAL LOSS =
                                                      2.34, TOTAL EXCESS =
   TOTAL RAINFALL =
                                                       MAXIMUM AVERAGE FLOW
PEAK FLOW
                 TIME
                                                                                     249.10-HR
                                             6-HR
                                                          24-HR
                 (HR)
  (CFS)
                              (CFS)
              153.00
      13.
                                                                         3.066
                                                                                          5.114
                                           1.197
                            (INCHES)
                                               3.
                                                       0.05 SO MI
                            CUMULATIVE AREA =
266 KK
                    TIME DATA FOR INPUT TIME SERIES

JXMIN 60 TIME INTERVAL IN MINUTES
JXDATE 31DEC99 STARTING DATE
JXTIME 2400 STARTING TIME
257 IN
                  SUBBASIN RUNOFF DATA
                    SUBBASIN CHARACTERISTICS
TAREA, 0.06 SUBBASIN AREA
294 BA
                    PRECIPITATION DATA
                                           7.46 BASIN TOTAL PRECIPITATION
                            STORM
269 PB
                    UNIFORM LOSS RATE
295 LU
                                        0.20 INITIAL LOSS
0.07 UNIFORM LOSS RATE
38.92 PERCENT IMPERVIOUS AREA
                            STRTL
CNSTL
                            RTIME
                                                                      = 1.00
27.1
                    INPUT UNITGRAPH, 109 ORDINATES.
294 UI
                                                                                                                  51.2
90.2
                                                                                                                               60.7
80.7
34.8
                                                                                                                                           70.5
72.1
32.6
                                                              20.9
107.1
51.4
24.9
14.4
                           3.9
82.1
66.3
30.4
16.7
                                       9.4
94.6
                                                   15.2
                                                                           107.6
47.4
23.5
13.6
                                                                                        105.5
43.7
22.2
                                                                                                      99.6
40.6
20.8
                                                                                                                  37.6
19.7
                                       61.1
28.5
15.9
                                                    55.2
                                                                                                                               18.6
                                                                                                                                            17.8
11.2
                                                    26.6
                                                                                                                   12.3
                                                                                                      12.7
                                                                                                                                             7.6
5.2
                                                                                                                                7.9
                                                                              9.2
6.2
4.2
                                       7.0
                                                    10.0
                                                                 9.6
6.6
                                                                                                                                5.4
3.6
2.5
                                                                                          6.0
4.1
2.7
                                                                                                       5.8
3.9
                                                                                                                    5.5
                            7.3
4.9
                                                                                                                   3.7
                                        4.8
                                                     4.6
3.1
                                                                 4.4
                                                                              2.8
                                                                                                       2.7
                            3.3
                                                                                                       1.8
                                                                                                                   1.7
                                                                                                                                1.7
1.1
                                                                                                                                             1.6
                            2.3
                                        2.2
1.5
                                                    2.1
1.4
                                                                 2.0
                                                                 1.4
                                                                              1.3
                                                                                           1.3
                              HYDROGRAPH AT STATION G
                                                     2.83. TOTAL EXCESS =
                           7.46, TOTAL LOSS =
    TOTAL RAINFALL =
                                                       MAXIMUM AVERAGE FLOW
PEAK FLOW
                  TIME
                                                                                     249.10-HR
                                             6-HR
                                                           24-HR
   (CFS)
                  (HR)
                                (CFS)
              153.02
      18.
                                                                                           4.625
                                                           2.007
                                                                          2.822
                            (INCHES)
                                            1.152
                                                                                             15.
                             (AC-FT)
                             CUMULATIVE AREA =
                                                      0.06 SQ MI
*** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** ***
```

308 KK

24-28

\* \*

TIME DATA FOR INPUT TIME SERIES

JEMIN 60 TIME INTERVAL IN MINUTES
JUDITE 310EC99 STARTING DATE
JUTINE 2400 STARTING TIME 309 IN SUBBASIN RUNOFF DATA SUBBASIN CHARACTERISTICS
TAREA, 0.11 SUBBASIN AREA 336 BA PRECIPITATION DATA 7.46 BASIN TOTAL PRECIPITATION STORM 311 PB 337 LU UNIFORM LOSS RATE 0.20 INITIAL LOSS 0.07 UNIFORM LOSS RATE STRTL CNSTL 46.94 PERCENT IMPERVIOUS AREA RTIMP VOLUME = 1.00 INPUT UNITGRAPH, 161 ORDINATES, 3.2 7.2 11.8 336 UI 43.8 128.4 38.0 50 3 30.9 16.6 81.1 128.5 21.8 89.7 122.0 26.1 3.2 57.5 132.2 80.7 11.8 130.8 120.1 98.3 54.1 99.5 114.2 110.0 64.8 132.3 76.3 106.3 91.0 51.5 130.9 67.0 40.1 63.9 38.3 60.6 33.3 36.5 34.9 23.1 31.9 30.5 46.5 44.1 28.2 41.7 21.6 15.6 20.7 25.9 18.0 24.9 17.4 27.1 16.8 16.0 18.5 13.9 10.7 16.5 19.9 14.8 11.3 19.4 12.2 9.4 7.1 5.5 9.1 11.6 14.4 13.6 10.4 1.3.3 8.8 10.1 7.8 6.0 9.6 7.3 5.7 9.9 7.5 8.1 6.1 4.7 6.9 8.6 8.4 8.1 6.3 5.4 5.8 4.2 3.2 2.5 4.3 4.0 5.1 4.9 4.5 3.2 3.1 2.4 3.5 2.7 2.1 3.7 3.4 3.9 3.6 2.8 2.6 3.0 3.0 1.8 2.2 2.2 1.7 2.1 1.5 1.8 \*\*\* \*\*\* HYDROGRAPH AT STATION H 7.46, TOTAL LOSS = 2.44, TOTAL EXCESS = 5.02 TOTAL RAINFALL = MAXIMUM AVERAGE FLOW TIME PEAK FLOW 249.10-HR 6-HR 24-KR (HR) (CFS) (CFS) 153.05 1. 5.015 (INCHES) 2.128 3.019 18. (AC-PT) 7. 13. CUMULATIVE AREA \* 0.11 SQ MI 香油子 不免者 食物等 医软 医软皮 医皮皮 医皮皮 医皮肤 医皮肤 医皮肤 医皮肤 有效的 有效的 有效的 医皮肤 化混合 化聚合 化物质 化物质 化化物 化化物 化化物 化化物 化水水 医外皮 化物质 使失失 356 KK r TIME DATA FOR INPUT TIME SERIES 60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE JXMIN JXDATE 2400 STARTING TIME SUBBASIN RUNOFF DATA SUBBASIN CHARACTERISTICS 0.08 SUBBASIN AREA TAREA, PRECIPITATION DATA 7.46 BASIN TOTAL PRECIPITATION STORM 359 PB 385 LU UNIFORM LOSS RATE 0.20 INITIAL LOSS 0.07 UNIFORM LOSS RATE 46.33 PERCENT IMPERVIOUS AREA STRTL CNSTL RTIMP

12.0

17.4

20.0

24.1

27.6

INPUT UNITGRAPH, 186 ORDINATES, VOLUME = 1.00 1.8 4.0 6.5 9.2 12

384 UI

```
68.5
                                                                                                                                           74.5
               34.9
84.7
66.6
39.3
                              39.0
86.1
                                              43.2
87.0
58.2
                                                                             52.6
                                                             47.9
                                                                             86.8
52.9
32.7
                                                                                            85.8
50.4
31.2
                                                                                                           84.5
47.6
                                                                                                                           80.1
                                                                                                                                           75.7
                                                              87.6
80.1
                                                                                                                           44.8
28.5
                                                                                                                                           43.0
27.3
                                                             55.4
34.1
22.5
71.2
                              62.2
37.3
                                                                                                            29.9
41.2
                                                                                                            20.0
                                                                                                                           19.3
                                                                                                                                           18.7
26.4
18.1
               25.3
17.4
                              24.2
16.8
12.1
                                              23.4
                                                                                             14.7
11.0
8.7
6.9
                                                                                                                                            13.3
                                              16.2
                                                              15.7
                                                                             15.2
11.2
                                                                                                                            13.9
                                                                                                            14.4
                                                                                                            10.8
8.5
6.7
                                                                                                                            10 5
                                                                                                                                            10.3
               12.6
13.0
                                                                                                                             8.3
                                                                                                                                             8.1
5.4
                9.8
                                9.6
                                               9.3
                                                               9.1
7.2
                                                                               8.9
                                                                               7.1
5.6
 7.9
                                                                                                                                             5.1
4.1
                                               5.8
4.6
3.7
 6.3
                6.2
4.9
                                6.0
                                                               5.7
                                                                                              5.4
                                                               4.5
                                                                               4.4
3.6
                                                                                                                              4.2
                                                                                              4.4
                                                                                                              4.3
                                                                                              3.5
                                                                                                                              3.3
                                                                                                                                             3,2
  4.0
                 3.9
                                3.8
                                               2.9
2.3
1.9
1.5
                                3.0
                                                               2.8
2.3
                                                                               2.8
                                                                                                             2.7
                                                                                                                             2.6
                                                                                                                                             2,5
 3.2
2.5
2.0
1.6
1.3
                 3.1
                                                                                                                             2.1
1.7
1.3
                                                                                                                                             2 1
                 2.4
                                1.9
                                                               1.8
                                                                               1.8
                                                                                               1.8
                                                                               1.4
                                                                                                             1.4
                                                                                                                                             1.3
                 1.6
                 1.2
                                1.2
                                                                1.2
                 1.0
                                                                               0.9
                                                                 ***
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#### HYDROGRAPH AT STATION I

TOTAL RAINFALL = 2.42. TOTAL EXCESS = 5.05 7.46, TOTAL LOSS \* MAXIMUM AVERAGE FLOW TIME 249.10-HR 6-HR 24-HR (CFS) (HR) (CFS) 153.08 23 (TNCHES) 3.038 5.043 1.178 2.146 23. (AC-FT)

CUMULATIVE AREA =

DIX XXV DIE CER CEP JEG XET DIG JEG ARD GOD MAN SEN VOC VEN HIN DER DER AUG DER BEG BEG KER KER KER BER KER KER

406 KK \* J \*

407 IN TIME DATA POR INPUT TIME SERIES

JXMIN 60 TIME INTERVAL IN MINUTES
JXDATE 31DEC99 STARTING DATE
JXTIME 2400 STARTING TIME

0.08 SQ MI

SUBBASIN RUNOFF DATA

434 BA SUBBASIN CHARACTERISTICS

TAREA, 0.09 SUBBASIN AREA

PRECIPITATION DATA

409 PB STORM 7.46 BASIN TOTAL PRECIPITATION

435 LU UNIFORM LOSS RATE

STRTL 0.20 INITIAL LOSS
CNSTL 0.06 UNIFORM LOSS RATE
RTIMP 75.17 PERCENT IMPERVIOUS AREA

434 UI INPUT UNITGRAPH, 119 ORDINATES, VOLUME = 1.00

11.0 25.1 30.9 40.9 49.1 59.2 69.8 81.4 4.5 137.5 61.6 31.9 139.5 133.1 122.1 93.3 99.7 122.4 135.0 138.1 107.5 84.1 77.7 38.2 70.9 36.0 65.3 33.8 49.7 53.3 27.0 17.0 46.3 25.7 43.2 22.2 14.6 10.2 7.1 24.4 23.2 17.5 21.0 20.0 19.0 18.3 14.1 12.2 11.7 16.4 9.8 9.5 6.6 8.8 8.5 10.9 10.5 9.1 8.2 6.2 4.2 5.9 5.7 7.6 7.3 7.9 4.9 3.4 2.4 4.7 3.4 2.3 5.5 3.8 2.7 4.0 5.3 3.7 5.2 3.5 4.4 4.1 4.5 3.3 3.2 3.0 2.1 2.9 2.8 2.0 2.5 2.6 1.9 1.7 1.7 1.6 1.5 1.5 1.5

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#### HYDROGRAPH AT STATION J

TOTAL RAINFALL = 7.46, TOTAL LOSS = 1.02, TOTAL EXCESS = 6.44

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
6-HR 24-HR 72-HR 249.10-HR
(CFS) (HR)

```
0.09 SQ MI
                             CUMULATIVE AREA =
                    OFF-N
449 KK
                                85
                    TIME DATA FOR INPUT TIME SERIES

JXMIN 60 TIME INTERVAL IN MINUTES
JXDATE 31DEC99 STARTING DATE
JXTIME 2400 STARTING TIME
450 IN
                  SUBBRASTN RUNOPP DATA
                    SUBBASIN CHARACTERISTICS
477 BA
                                            0.64 SUBBASIN AREA
                            TAREA,
                    PRECIPITATION DATA
                                             7.46 BASIN TOTAL PRECIPITATION
                            STORM
452 PB
                    UNIFORM LOSS RATE
478 LU
                            STRTL
                                             0.20 INITIAL LOSS
                                             0.07 UNIFORM LOSS RATE
2.00 PERCENT IMPERVIOUS AREA
                            CNSTL
                            RTIMP
                    INPUT UNITGRAPH, 472 ORDINATES,
477 UI
                                                                                                        23.5
66.2
                                                                                           19.4
62.7
                                                                                                                     27 5
                                                                                                                                  31.B
                                                                                                                                               36.0
                                       5.6
44.5
                                                     8.4
49.1
                                                                              15.4
                           2.8
                                                                 11.3
                                                                                                                                              77.5
135.7
                                                                                                                                  73.1
                                                                                                                     69.6
                                                                  53.8
                                                                             58.4
107.4
                                                                                          112.5
175.1
                                                                                                       117.5
                                                                                                                    123.2
                                                                                                                                 129.4
                                      90.2
148.4
218.9
                          83.9
142.0
                                                   96.5
155.0
                                                                102.3
                                                                                                        182.3
                                                                                                                                              204.2
                                                                161.6
234.5
                                                                             168.1
                                                                                                                                 279.5
                                                                                          252.1
335.3
                                                                                                       260.8
                                                                                                                    270.1
                                                   226.2
                          211.5
                                                                                                                     339.4
                                                                                                                                 341.5
                                                                                                                                              342.7
                                       307.0
                                                    315.6
                                                                324.2
                                                                             332.7
                                                                                                                                  337.1
                                                                             343.7
304.8
                                                                 344.8
                                                                                           342.5
                                                                                                        341.3
                                                                                                                    339.2
                          343.8
                                       344.9
                                                    346.0
                                                                                                                                 276.6
216.7
                                                                                           297.8
                                                                                                                     283 7
                                                                                                                                               269.5
                                       325.3
                                                   318.5
                                                                311.7
                          332.1
                                                    248.4
                                                                             236.0
193.0
                                                                                           229.7
                                                                                                        224.5
                                                                                                                     220.6
                                       255.2
                          262.4
                                                                                                        183.9
152.6
                                                                                                                    179.3
                                                                                                                                 175.9
                                                                                                                                               173.0
                          208.9
                                       205.0
167.4
                                                    201.1
                                                                 197.3
                                                                                                                    149.6
125.0
                                                                                                                                               143.5
                                                   164.5
136.6
                                                                 1€1.6
                                                                              158.6
                                                                                           155.7
                          170.2
                                                                                           129.6
108.3
                                                                                                        127.3
106.9
                                                                                                                                               120.8
                                                                             131.9
                                                                                                                                  122.9
                          141.1
118.8
                                       138.9
                                                                 124.3
                                                                                                                                  104.0
                                                                                                                                               102.5
                                       116.7
                                                                 112.5
                                                                             110.3
                                                                                            93.0
79.6
                                                                                                        91.6
78.6
                                                                                                                                                87.4
                                                                  95.7
                                                                               94.3
                                                                                                                      90.2
                                                                                                                                   88.8
                          100.8
                                        99.0
                                                     97.3
                                                                                                                      77.5
                                                                                                                                                75.5
65.7
                                                                                                                                   76.5
                                        94.6
73.6
                                                     83.4
                                                                  £2.1
71.7
                                                                               80.8
                           86.0
                                                                                                                                   66.6
                                                                               70.6
                                                                                            69.5
                                                                                                         68.4
                           74.6
                                                                                                         60.0
                                                                                                                      59.2
                                                                                                                                   58.4
                                                                                                                                                57.8
                           64.8
57.3
                                        64.0
56.7
                                                     63.2
56.1
                                                                  62.4
                                                                               61.6
                                                                               54.4
47.5
43.2
                                                                                                                                                51.2
                                                                                                         52.6
                                                                  55.3
                                                                                            53.5
                                                                                            47.2
                                                                                                         46.8
42.6
                                                                                                                      46.5
                                                                                                                                   46.1
                                                                                                                                                45.5
                                                     49.1
                                        49.9
44.2
                                                                  48.3
                           50.7
                                                                                                                      42.2
                                                                                                                                                41.3
                                                     43.7
                                                                  43.5
                           44.9
                                                                                                                                   38.0
                                                                  40.0
                                                                                            39.2
                                                                                                         38.8
                                                                                                                      38.4
                           40.9
                                        40.6
                                                                                                                      34.9
31.7
                                                                                                                                   34.6
                                                                                                                                                34.3
                                                     36.5
33.3
                                                                                            35.4
                                        36.8
                                                                  36.1
                                                                               35.8
                                                                               32.6
29.9
                                                                                            32.3
                                                                                                         32.0
                           34.0
                                        33.7
                                                                                                         29.3
26.7
                                                                                                                      29.0
                                                                                                                                   28.7
                                                                                                                                                28.4
                                        30.8
                                                     30.5
27.8
                                                                  30.2
                                                                                                                                                26.1
                                                                  27.6
25.1
                                                                               27.4
                                                                                            27.0
                                        28.0
                           28.2
                                                                                                                                                23.9
                                                                                            24.5
                                                                                                         24.4
22.2
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                                                                                                                                   24.1
                                                     25.4
                           25.9
                                        25.7
                                                                                                                                   21.8
                                                                                                                                                21.6
                                                     23.0
                                                                  22.8
                                                                               22.6
                           23.6
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                                                                                            20.8
                                                                                                                      20.2
                                                                                                                                   20.0
                                                                  21.1
                                                                                                         20.5
                           21.4
                                        21.2
                                                                                                                      18.4
                                                                                                                                   18.2
                                                                                                                                                18.0
                                        19.4
17.7
                                                     19.3
17.6
                                                                  19.1
                                                                               18.9
                                                                                                                                   16.8
                                                                  17.4
15.9
                                                                               17.3
                                                                                            17.2
15.7
                                                                                                         17.0
                           17.8
                                                                                                                      15.4
14.1
                                                                                                                                                15.2
                                                                               15.8
                                                                                                         15.6
                                                                                                                                   15.3
                           16.4
                                        16.3
                                                     16.1
                                        14.9
13.6
12.4
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                                                                  14.6
                                                                                                         14.2
                                                                               14.5
                                                                                            14.4
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                                                                               13.2
                                                                                            13.0
                                                                                                                      32.9
                                                                                                                                   12.8
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                           13.7
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                                                     12.2
                                                                  12.0
                                                                               11.9
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                           12.5
                                                                                                                                   10.5
                                                                                                                                                 10.4
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                                                                                                         10.7
                                                                                                                      10.6
                                                                  10.9
                           11.2
                                        11.1
                                                                                                                                                  9.5
8.6
                                                     10.1
9.3
8.5
7.9
7.1
                                                                                              9.9
                                        10.2
                                                                  10.0
                                                                                9.9
                                         9.3
8.6
7.9
                                                                                 9.1
                                                                                              9.0
                                                                                                           8.9
                                                                                                                       8.8
                            9.4
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7.7
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                                                                                                                                    8.2
7.5
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                                                                                                                                                  8.1
                            8.6
                                                                   8.5
                                                                                 8.4
                                                                   7.8
                                                                                 7 R
                                                                                                                                    6.8
                                                                                                                                                  6.8
                                                                                                                        5.9
                                         7.2
                            7.3
                                                                                                           6.3
                                                       6.6
                                                                   6.5
                                                                                 5.4
                                                                                              5.4
```

6.439

HYDROGRAPH AT STATION OFF-N

6.0 5.5 5.1 4.6

4.2

3.9

6.1

5.1

4.0

3.6

5.8

5.4

4.5

4.2

3.8

\*\*\*

5.4 4.9 4.5

4.2

3.8

\*\*\*

5.9

5.4 5.0

4.6

3.9

(CFS)

(INCHES)

(AC-FT)

153.02

26.

12

б.

1.319

2.580

12.

3,740

5.5

5.1

4.3

3.6

5.7

4.8

4.1

5.3 4.9

4.2

5.7

4.8

4.3

4.1

3.6

5.6

5.2 4.7

4.3

3.6

```
7.46. TOTAL LOSS = 4.55, TOTAL EXCESS =
                                                                                    2.92
    TOTAL RAINFALL =
                                                      MAXIMUM AVERAGE FLOW
PEAK PLOW
                 TIME
                                                                                   249.10-HR
                                            6-HR
                                                         24-HR
                                                                        72-HR
                  (HR)
   (CPS)
                               (CFS)
                                                                        15.
1.969
     162.
               153.62
                                                                                        2.916
                                                          1.484
                            (INCHES)
                                           0.945
                                                            67.
                                                                                         131.
                             (AC-FT)
                             CUMULATIVE AREA -
                                                      0.84 SO MI
528 KK
                    HYDROGRAPH COMBINATION
530 HC
                           ICOMP
                                               6 NUMBER OF HYDROGRAPHS TO COMBINE
                             HYDROGRAPH AT STATION DUMMY2
                                                      MAXIMUM AVERAGE FLOW
                 TIME
PEAK PLOW
                                                                                   249.10-HR
                                            6-HR
                                                         24-HR
                                                                        72-HR
                 (HR)
  (CFS)
                               (CFS)
               153.17
                                            134
                                                           56.
                                                                          26.
                                                                                          12.
                                                                                        3.663
                            (INCHES)
                                           1.010
                             (AC-FT)
                                             65.
                                                          112.
                                                                         154.
                            CIMULATIVE AREA =
                                                      1.23 SO MI
532 KK
                   TIME DATA FOR INPUT TIME SERIES

JIMIN 60 TIME INTERVAL IN MINUTES

JXDATE 31DEC99 STARTING DATE
533 IN
                          JXTIME
                                           2400 STARTING TIME
                 SUBBASIN RUNOFF DATA
                    SUBBASIN CHARACTERISTICS
560 BA
                                          0.06 SUBBASIN AREA
                           TAREA,
                    PRECIPITATION DATA
535 PB
                           STORM
                                          7,46 BASIN TOTAL PRECIPITATION
                   UNIFORM LOSS RATE
561 LU
                                        0.20 INITIAL LOSS
                          STRIL
                                        0.06 UNIFORM LOSS RATE
47.94 PERCENT IMPERVIOUS AREA
                          RTIMP
                   INPUT UNITGRAPH, 151 ORDINATES,
                                                           VOLUME = 1.00
560 UI
                                                                                                              24.8
77.8
52.0
28.9
17.7
                         2.0
                                     4.7
                                                 7.7
48.1
                                                              10.8
53.5
                                                                          14.1
59.8
                                                                                      16.7
66.5
                                                                                                  20.5
72.9
                                                                                                                           28.5
79.3
                                                                                                                                       33.1
                                                                                                                                        80.1
                                                 76.3
38.4
22.3
                                                                                                  56.3
30.6
                                     78.5
40.5
                                                                          66.3
34.1
                                                                                      61.2
32.3
                                                                                                                           49.2
                         79.7
                                                              71.3
                                                                                                                                        46.4
                         43.3
24.6
15.5
10.6
                                                              36.3
                                                                                                                           27.4
17.0
                                                                                                  18.4
12.2
8.9
6.6
5.0
                                     23.5
                                                              21.3
                                                                          20.3
                                                                                      19.3
                                                                                                                                        16.3
                                                              13.8
9.7
7.3
5.5
                                                                          13.3
9.4
7.1
5.3
                                                                                                               11.8
8.6
6.5
4.9
                                                 14.3
                                                                                      9.2
                                     7.7
                                                                                                                             8.3
                                                                                                                                        8.1
                          7.9
                                                                                       6.8
                                                                                                                                        6.1
4.6
                                      5.8
                                                  5.6
                          4.5
3.4
2.5
1.9
                                      4.3
                                                  4.2
                                                               4.1
3.1
                                                                           4.0
                                                                                       3.9
2.9
                                                                                                   3.8
                                                                                                                                        3.5
                                      2.4
                                                  2.4
                                                               2.3
                                                                           2.3
                                                                                       2.2
                                                                                                    2.1
                                                                                                               2.1
                                                                                                                            2.0
                                                                                                                                        2.0
                                                                                                                                        1,5
                                                               1.8
                          1.5
1.1
0.8
                                                                                                   1.2
                                      1.4
                                                                           1.3
                                                                                                                1.2
                                                                                                                            1.2
                                                                                                                                        1.1
```

1.4

1.3

1.3

HYDROGRAPH AT STATION K

2.31, TOTAL EXCESS = 7.45. TOTAL LOSS = TOTAL RAINFALL =

MAXIMUM AVERAGE FLOW PEAK FLOW TIME 249.10-HR 6-HR 24-HR 72-HR (CFS) (HR) (CFS)

2. 3.094 153.05 18. 2.184 (INCHES) 1.196 17. (AC-PT)

> CUMILATIVE AREA = 0.06 SQ MI

579 KK

TIME DATA FOR INPUT TIME SERIES 580 IN

60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE
2400 STARTING TIME JXMIN JXDATE

JXTIME

SUBBASIN RUNOFF DATA

SUBBASIN CHARACTERISTICS 607 BA 0.03 SUBBASIN AREA

TAREA,

PRECIPITATION DATA

STORM 7.46 BASIN TOTAL PRECIPITATION 582 PB

UNIFORM LOSS RATE 608 LU

0.20 INITIAL LOSS 0.06 UNIFORM LOSS RATE CNSTL 70.00 PERCENT IMPERVIOUS AREA

INPUT UNITGRAPH, 6 6.4 14.7 67 ORDINATES. VOLUME - 1.00 607 UI 91.6 23.9 10.3 5.4 2.8 76.2 33.6 12.6 6.6 3.5 1.9 22.9 57.2 23.6 49.1 45.9 43.4 59.7 38.0 13.7 7.0 3.7 26.7 11.0 5.8 3.0 66.3 16.2

6.4 79.6 21.5 9.6 5.1 2.7 29.7 11.7 6.1 3.2 1.7 17.7 8.5 4.5 2.4 9.0 4.8 2.5 4.2 4.0 2.0 1.1 1.4 1.3 1.2

HYDROGRAPH AT STATION L

7.46, TOTAL LOSS = 1.29, TOTAL EXCESS = 6.18 TOTAL RAINFALL =

PEAK FLOW TIME MAXIMUM AVERAGE FLOW 249.10-ER 6-HR 24-HR (HR) (CFS) 153.00 1. 6.168 3.603 (AC-FT) 2.

0.03 SQ MI

TIME DATA FOR INPUT TIME SERIES

JXMIN 60 TIME INTERVAL IN MINUTES

JXDATE 31DEC99 STARTING DATE 618 IN

CUMULATIVE AREA =

2400 STARTING TIME TXTTME

SUBBASIN RUNOFF DATA

SUBBASIN CHARACTERISTICS 645 BA 0.07 SUBBASIN AREA TAREA,

PRECIPITATION DATA

7.46 BASIN TOTAL PRECIPITATION STORM 620 PB

UNIFORM LOSS RATE 646 LU

0.20 INITIAL LOSS STRTL 0.04 UNIFORM LOSS RATE CNSTL

95.00 PERCENT IMPERVIOUS AREA RTIMP

INPUT UNITGRAPH, 160 ORDINATES, WOLDER = 1 00 645 UI 15.8 60.4 26.6 30.5 13.2 54.4 18.8 23.1 4.4 39.3 79.7 7.2 44.2 78.8 10.0 1.9 34.9 66.8 72.8 58.8 77.6 54.4 79.0 49.2 77.4 51.0 29.2 73.1 38.3 68.4 36.3 79.8 34.2 32.4 19.9 30.8 48.4 45.7 26.4 42.7 40.2 25.0 24.0 15.5 22.9 21.8 14.9 10.4 7.9 14.4 13.6 13.4 13.0 12.4 17.5 16.9 11.5 16.2 11.0 9.6 7.3 9.4 7.1 9.9 7.5 5.7 9.1 10.8 8.1 6.2 4.8 7.7 5.9 6.9 8.6 6.5 5.0 8.3 6.4 4.9 3.7 8.9 5.4 4.1 5.3 6.1 4.6 4.5 3.5 4.4 4.3 5.1 3.4 3.3 3.2 3.1 4.0 3.9 3.7 2.4 2.5 2.9 2.2 1.7 1.3 2.8 2.7 2.6 3.0 2.0 2.0 1.9 2.2 1.4 1.5 1.5 1.6 1.8 1.8 1.6 1.6 1.2 1.2 1.1 1.3 1.2 1.1 1.4 1.3 0.9 0.8 1.0 1.0 1.0 1.0

HYDROGRAPH AT STATION M

7.46, TOTAL LOSS -0.17, TOTAL EXCESS = 7.30 TOTAL RAINFALL =

MAXIMUM AVERAGE FLOW TIME PEAK PLOW 6-BR 249.10-HR 24-HR (HR) (CPS) (CFS) 153.05 10. 20. (INCHES) 1.378 4.154 7,286 (AC-FT) 5. 10. 15.

0.07 SO MX CUMULATIVE AREA =

\*\*\*

664 KK

665 IN

TIME DATA FOR INPUT TIME SERIES

JXMIN 60 TIME INTERVAL IN MINUTES

JXDATE 31DEC99 STARTING DATE JXTIME 2400 STARTING TIME

SUBBASIN RUNOFF DATA

SUBBASIN CHARACTERISTICS

0.04 SUBBASIN AREA TAREA,

PRECIPITATION DATA

STORM 7.46 BASIN TOTAL PRECIPITATION 667 PB

693 LU UNIFORM LOSS RATE

0.20 INITIAL LOSS STRTL 0.07 UNIFORM LOSS RATE 43.11 PERCENT IMPERVIOUS AREA CNSTL

RTIMP

INPUT UNITGRAPH, 117 ORDINATES, VOLUME = 1.00 692 UI 2.0 42.0 42.9 11.2 59.8 33.4 13.9 18.3 36.5 4.9 48.4 8.0 60.4 26.5 13.7 61.1 30.7 61.4 28.6 55.0 57.7 52.8 47.8 24.6 23.0 21.4 36.4 39.2 18.7 17.5 10.1 12.3 11.6 16.5 15.5 14.5 13.1 11.1 9.5 9.1 7.1 6.8 6.5 4.5 6.3 6.1 5.8 5.6 5.5 5.2 5.0 3.9 3.8 3.7 3.5 4.9 3.4 3.1 2.6 2.5 3.2 3.0 2.9 2.8 2.4 1.9 1.9 1.8

```
1.5
1.0
0.7
                                                                             1.4
1.0
0.7
                                                                                                      1.3
0.9
0.6
                           1.6
1.1
0.8
                                                    1.5
1.0
0.7
                                                                                         1.4
                                        1.5
                                                                  ***
                              HYDROGRAPH AT STATION N
                                                      2.60, TOTAL EXCESS -
                            7.46, TOTAL LOSS =
    TOTAL RAINFALL =
                                                       MAXIMUM AVERAGE FLOW
PEAK FLOW
                  TIME
                                             6-ER
                                                           24-HR
                                                                                    249.10-HR
                  (HR)
   (CFS)
                                (CFS)
               153.02
      11.
                                                                          2.941
                                                                                          4.856
                            (INCRES)
                                                           2.083
                                            1.173
                             (AC-FT)
                             CUMULATIVE AREA =
                                                       0.04 SQ MI
707 KK
                    TIME DATA FOR INPUT TIME SERIES
708 IN
                                        60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE
2400 STARTING TIME
                          JXMIN
JXDATE
                          TXTIME
                 SUBBASIN RUNOFF DATA
                    SUBBASIN CHARACTERISTICS
735 BA
                                          0.04 SUBBASIN AKEA
                           TAREA,
                    PRECIPITATION DATA
                                          7.46 BASIN TOTAL PRECIPITATION
710 PB
                    UNIFORM LOSS RATE
736 LU
                           STRTL
CNSTL
                                         0.20 INITIAL LOSS
0.07 UNIFORM LOSS RATE
                           RTIMP
                                          50.00 PERCENT IMPERVIOUS AREA
                    INPUT UNITGRAPH, 93 ORDINATES.
735 UI
                                                             VOLUME = 1.00
                                                                                        32.7
63.8
24.3
12.1
7.4
4.7
                                      8,6
82.0
                                                  14.0
82.1
                                                               18.7
                                                                           25.8
72.3
                                                                                                     40.4
55.8
22.3
11.3
                                                                                                                 49.1
50.5
                                                                                                                              58.6
45.7
                                                                                                                                          69.6
41.1
                          79.8
                                                                                                                 20.7
10.7
6.7
4.3
2.7
                                      34.0
15.5
8.9
                                                                           26.1
12.8
7.7
4.9
                          37.6
16.7
                                                               28.6
13.7
                                                                                                                              19.1
10.3
                                                   31.3
                                                                                                                                          17.9
                                                                                                                                           9.8
                                                   14.6
                                                   8.5
5.3
3.4
2.1
                                                                                                                               6.5
4.1
2.6
1.7
                           9.4
5.9
3.7
2.3
                                                                8.1
5.1
                                       3.6
                                                                3.3
                                                                                         3.0
                                                                                                      2.8
                                                                             3.1
                                                                                                                                           2.5
                                                                                         1.9
                           1.5
                                       1.4
                                                                1.3
                                                                             1.3
                                                                                                                                           1.0
                             HYDROGRAPH AT STATION O
   TOTAL RAINFALL =
                           7.46, TOTAL LOSS =
                                                      2.32, TOTAL EXCESS =
                                                                                     5.15
                                                      MAXIMUM AVERAGE FLOW
                                            6-HR
                                                                                    249.10-HR
                                                         24 - HR
                                                                        72-HR
  (CFS)
                 (HR)
                              (CFS)
     12.
             153.00
                                                         2.167
                                                                        3.076
                                                                                         5.135
                                           1.199
                            (AC-FT)
                           CUMULATIVE AREA =
                                                      0.04 SQ MI
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24-35

\*\*\*\*\*

OPERATION

STATION

PLOW

PEAK

6-HOUR

24-HOUR

72-HOUR

TIME DATA FOR INPUT TIME SERIES

JXMIN 60 TIME IN 749 IN 60 TIME INTERVAL IN MINUTES
31DEC99 STARTING DATE TYDATE JXTIME 2400 STARTING TIME SUBBASIN RUNOFF DATA SUBRASIN CHARACTERISTICS
TAREA, 0.03 SUBBASIN AREA 776 BA PRECIPITATION DATA STORM 7.46 BASIN TOTAL PRECIPITATION 751 PB UNIFORM LOSS RATE 777 LU 0.20 INITIAL LOSS 0.06 UNIFORM LOSS RATE 56.38 PERCENT IMPERVIOUS AREA STRTL CNSTL RTIMP INPUT UNITGRAPH, 102 ORDINATES, VOLUME = 1.00 776 UI 28.3 52.4 34.2 46.3 19.4 10.1 10.0 64.3 29.0 13.7 7.8 13.4 64.5 26.5 18.2 63.1 40.5 47.7 2.6 6.2 62.7 38.1 58.5 20.8 22.6 17.9 34.4 15.6 31.5 9.6 8.9 5.8 12.8 7.5 12.0 11.3 7.2 6.6 6.3 6.9 8.6 8.1 4.0 2.6 1.7 4.3 5.1 3.3 2.2 4.9 3.2 2.1 4.5 5.6 5.3 3.5 3.0 1.8 1.8 2.3 1.5 1.0 1.6 2.4 1.6 1.0 1.5 1.3 1.3 0.8 0.8 0.7 \*\*\* HYDROGRAPH AT STATION P 1.90. TOTAL EXCESS = 5.56 7.46, TOTAL LOSS = TOTAL RAINFALL = MAXIMUM AVERAGE FLOW PEAK PLOW TIME 249.10-HR 72-HR S-HR 24-HR (HR) (CFS) (CFS) 153.02 10. 1.245 2.313 5.562 (INCHES) 10. (AC-FT) CUMULATIVE AREA = 0.03 SO MI 食分子 食物质 食物水 大食工 大大者 少年的 法有效 全角化 全体化 大學工 黄油金 金板木 大学的 电影性 生物的 电影 放射 大大学 工作的 光明化 医外虫 电电子 经外帐 化分析 电电子 生物化 电电子 电电子 \* DUMMY3 \* 790 KK 792 HC HYDROGRAPH COMBINATION 6 NUMBER OF HYDROGRAPHS TO COMBINE ICOMP \*\*\* HYDROGRAPH AT STATION DUMMY3 MAXIMUM AVERAGE PLOW PEAR FLOW TIME 6-HR 249.10-HR (CFS) (HR) (CFS) 37. 18. 153.02 81. 1.255 5.799 (TNCHES) 2.376 3.415 35. (AC-FT) 0.27 SQ MI CUMULATIVE AREA = 1 RUNOFF SUMMARY FLOW IN CUBIC FEET PER SECOND TIME IN HOURS, AREA IN SQUARE MILES BASIN AVERAGE FLOW FOR MAXIMUM PERIOD MUMIXAM PEAK TIME OF TIME OF

MAX STAGE

AREA

STACE

| + | HYDROGRAPH AT | A      | 33.  | 153.07 | 16.        | 7.         | 4.  | 0.12 |
|---|---------------|--------|------|--------|------------|------------|-----|------|
| + | HYDROGRAPH AT | B      | 13.  | 153.00 | 6.         | 3.         | 1.  | 0.04 |
| + | HYDROGRAPH AT | c      | 18.  | 153.02 | 8.         | 4.         | 2.  | 0.06 |
| ÷ | HYDROGRAPH AT | D      | 14.  | 153.02 | 6.         | 3.         | 1.  | 0.05 |
|   | HYDROGRAPH AT | E      | 11.  | 153.00 | 5.         | 2.         | 1.  | 0.04 |
| + | 5 COMBINED AT | DUMMY1 | 89.  | 153.02 | 41.        | 19.        | 9.  | 0.31 |
| • | HYDROGRAPH AT | F      | 13.  | 153.00 | 6.         | 3.         | 1   | 0.05 |
| + | HYDROGRAPH AT | G      | 18.  | 153.02 | 8.         | 3.         | 2.  | 0.06 |
| + | hydrograph at | н      | 31.  | 153.05 | 14.        | 6.         | 3.  | 0.11 |
|   | HYDROGRAPE AT | I      | 23.  | 153.08 | 11.        | 5.         | 2.  | 0.08 |
|   | HYDROGRAPH AT | J      | 26.  | 153.02 | 12.        | 6.         | 3.  | 0.09 |
| + | HYDROGRAPH AT | opp-n  | 162. | 153.62 | 86.        | 34.        | 15. | 0.84 |
|   | 6 COMBINED AT | DUMMY2 | 252. | 153.17 | 134.       | 56.        | 26. | 1.23 |
| + | HYDROGRAPH AT | ĸ      | 18.  | 153.05 | 8.         | 4.         | 2.  | 0.06 |
| + | HYDROGRAPH AT | L      | 10.  | 153.00 | 5.         | 2.         | 1.  | 0.03 |
|   | HYDROGRAPH AT | ж      | 20.  | 153.05 | 10.        | 5 <i>.</i> | 2.  | 0.07 |
| • | HYDROGRAFH AT | N      | 11.  | 153.02 | <b>5</b> . | 2.         | 1.  | 0.04 |
| • | HYDROGRAPH AT | 0      | 12.  | 153.00 | 5.         | 2.         | 1.  | 0.04 |
|   | HYDROGRAPH AT | P      | 10.  | 153.02 | 5.         | 2.         | 1.  | 0.03 |
|   | 6 COMBINED AT | DUMMY3 | 81.  | 153.02 | 37.        | 18.        | 8.  | 0.27 |
|   |               |        |      |        |            |            |     |      |

<sup>\*\*\*</sup> NORMAL END OF HEC-1L \*\*\*

## **Ultimate Conditions HEC-RAS Model**

#### 100year 24hour Model 25

HEC-RAS Version 3.1.3 May 2005 U.S. Army Corp of Engineers Hydrologic Engineering Center 609 Second Street Davis, California

| x   | х            | XXXXXX                                 | XX  | XX |     | ХX | XX | X      | x | XXXX  |
|-----|--------------|--|-----|----|-----|----|----|--------|---|-------|
| x   | х            | x                                      | x   | Х  |     | x  | х  | х      | x | x     |
| ж   | ж            | x                                      | x   |    |     | ж  | х  | x      | x | x     |
| XXX | XXXXXXX XXXX |  | x   |    | XXX | XX | XX | XXXXXX |   | XXXX  |
| X   | х            | x                                      | х   |    |     | х  | x  | x      | x | x     |
| x   | x            | x                                      | х   | x  |     | х  | x  | x      | x | x     |
|     | -            | ************************************** | *** | ~~ |     | ~  | *  | ¥      | ¥ | YYYYY |

PROJECT DATA
Project Title: GREENBRIAR PARMS Project File: GB.prj Run Date and Time: 7/14/2005 3:37:39 PM

Project in English units

Project Description:

Project Description:
References:

1) Offsite Drainage Improvements-Metro Air Park, Exhibit D-2
(Offsite improved channels and Interstate 5 crossing)
2) 100yr-10day &
10yr-10day, STA 0+00, West Drain Stages, Mark Kubik & Mead & Hunt Inc.

### PLAN DATA

Plan Title: P3-100YR24HR-DEVELOP

Plan File : j:\Jobs\1116-GreenbriarFarms\1116-GreenbriarFarms\Civil\Docs\Report\HEC-RAS\GB.p03

Geometry File : j:\Jobs\1116-GreenbriarFarms\1116-GreenbriarFarms\Civil\Docs\Report\EEC-RAS\GB.g01

Flow Title

Plan Summary Information:
Number of: Cross Sections = 207
Culverts = 6 Multiple Openings = Inline Structures = Lateral Structures =

Computational Information
Water surface calculation tolerance = 0.01
Critical depth calculation tolerance = 0.01
Maximum number of iterations = 20
Maximum difference tolerance = 0.3

Computation Options
Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Subcritical Flow

Profile Output Table - Concise Table 1

| River   |          | Reach | River Sta | Profile | Q Total<br>(cfs) | Min Ch El<br>(ft) | W.S. Elev<br>(ft) | E.G. Elev<br>(ft) | Vel Chnl<br>(ft/s) | Flow Area<br>(sq ft) |
|---------|----------|-------|-----------|---------|------------------|-------------------|-------------------|-------------------|--------------------|----------------------|
| WEST DE | ETENTION | 1     | 5540      | Max WS  | 5.89             | 11.00             | 14.90             | 14.90             | 0.00               | 1472.20              |
| WEST DE | ETENTION | 1     | 5460      | Max WS  | 5.88             | 11.00             | 14.90             | 14.90             | 0.00               | 1351.94              |
| WEST DE | ETENTION | 1     | 5438      | Max WS  | 5.88             | 11.00             | 14.90             | 14.90             | 0.01               | 628.37               |
| WEST DE | ETENTION | 1     | 5412      | Max WS  | 5.88             | 11.00             | 14.90             | 14.90             | 0.01               | 531.02               |
| WEST DE | ETENTION | 1     | 4950      | Max WS  | 5.87             | 11.00             | 14.90             | 14.90             | 0.01               | 514.07               |
| WEST DE | ETENTION | 1     | 4.907     | Max WS  | 5.87             | 11.00             | 14.90             | 14.90             | 0.01               | 671.81               |
| WEST DE | ETENTION | 1     | 4611      | Max WS  | 9.41             | 11.00             | 14.90             | 14.90             | 6.01               | 659.33               |
| WEST DE | ETENTION | 1     | 4537      | Max WS  | 11.83            | 11.00             | 14.90             | 14.90             | 0.02               | 514.64               |
| WEST DE | RTENTION | 1     | 3571      | Max WS  | 11.83            | 11.00             | 14.90             | 14.90             | 0.02               | 512.48               |
| WEST DE | TENTION  | 1     | 3570      |         | Culvert          |                   |                   |                   |                    |                      |
| WEST DE | RTENTION | 1     | 3417      | Max WS  | 11.67            | 11.00             | 14.87             | 14.87             | 0.02               | 508.82               |
| WEST DE | ETENTION | 1     | 3400      | Max WS  | 11.67            | 11.00             | 14.87             | 14.87             | 0.02               | 508.48               |
| WEST DE | ETENTION | 1     | 3383      | Max WS  | 13.96            | 11.00             | 14.87             | 14.87             | 0.03               | 509.83               |
| WEST DE | TENTION  | 1     | 2760      | Max WS  | 16.03            | 11.00             | 14.87             | 14.87             | 0.03               | 507.98               |
| WEST DE | CTENTION | 1     | 2722      | Max WS  | 18.58            | 11.00             | 14.87             | 14.87             | 0.02               | 909.49               |
| WEST DE | TENTION  | 1     | 2635      | Max WS  | 18.58            | 11.00             | 14.67             | 14.87             | 0.02               | 916.87               |
| WEST DE | TENTION  | 1     | 2586      | Max WS  | 18.58            | .11.00            | 14.87             | 14.87             | 0.01               | 1301.49              |
| WEST DE | TENTION  | 1     | 2545      | Max WS  | 18.57            | 11.00             | 14.87             | 14.87             | 0.01               | 1301.91              |

| WEST DETENTION  | 1        | 2507 | Max WS | 18.57      | 11.00 | 14.87 | 14.87 | 0.02 | 925.62  |
|-----------------|----------|------|--------|------------|-------|-------|-------|------|---------|
| WEST DETENTION  | ī        | 2402 | Max WS | 18.57      | 11.80 | 14.87 | 14.87 | 0.02 | 914.81  |
| WEST DETENTION  | î.       | 2367 | Max WS | 21.74      | 11.00 | 14.87 | 14.87 | 0.04 | 519.80  |
| WEST DETENTION  | ī        | 1987 | Max WS | 21.73      | 11.00 | 14.87 | 14.87 | 0.04 | 510.69  |
| WEST DETENTION  | ī        | 1986 |        | Culvert    |       |       |       |      |         |
| WEST DETENTION  | î        | 1922 | Max WS | 21.70      | 11.00 | 14.79 | 14.79 | 0.04 | 497.47  |
| WEST DETENTION  | ī        | 1891 | Max WS | 21.70      | 11.00 | 14.79 | 14.79 | 0.04 | 496,93  |
| WEST DETENTION  | i        | 1815 | Max WS | 23.76      | 11.00 | 14.79 | 14.79 | 0.02 | 1052.61 |
| SOUTH DETENTION | 3        | 1636 | Max WE | 49.37      | 11.00 | 14.79 | 14.79 | 0.03 | 1451.36 |
| SOUTH DETENTION | 3        | 1561 | Max WS | 49.37      | 11.00 | 14.79 | 14.79 | 0.05 | 991.54  |
| SOUTH DETENTION | 3        | 1153 | Max WS | 55.95      | 11.00 | 14.79 | 14.79 | 0.05 | 1212.08 |
| SOUTH DETENTION | 3        | 1080 | Max WS | 55.95      | 11.00 | 14.79 | 14.79 | 0.05 | 1045.94 |
| SOUTH DETENTION | 3        | 1012 | Max WS | 61.46      | 11.00 | 14.79 | 14.79 | 0.04 | 1598.14 |
| SOUTH DETENTION | ã        | 945  | Max WS | 61.45      | 11.00 | 14.79 | 14.79 | 0.05 | 1123.51 |
| SOUTH DETENTION | 3        | 942  |        | Inl Struct |       |       |       |      |         |
| SOUTH DETENTION | 3        | 940  | Max WS | 61.45      | 2.70  | 14.79 | 14.79 | 8.62 | 4385.12 |
| SOUTH DETENTION | 3        | 930  | Max WS | 61.46      | 2.70  | 14,79 | 14.79 | 0.02 | 4385.12 |
| SOUTH DETENTION | 3        | 500  |        | Culvert    |       |       |       |      |         |
| SOUTH DETENTION | 3        | 150  | Max WS | 61.43      | 2.20  | 8.84  | 8.84  | 0.63 | 1919.15 |
| SOUTH DETENTION | 3        | 100  | Max WS | 61.25      | 2.20  | 6.84  | 8.84  | 0.03 | 1919.15 |
| SOUTH DETENTION | 3        | 90   | Max WS | 61.22      | 2,20  | 8,84  | 8.84  | 0.03 | 1919.15 |
| OFFSITE         | RS NORTH | 5350 | Max WS | 402.66     | 9.00  | 15.70 | 15.82 | 2,72 | 147.89  |
| OFFSITE         | RS NORTH | 1100 | Max WS | 383.17     | 5.00  | 8.84  | 9.82  | 7.97 | 48.09   |
| OFFSITE         | RE NORTH | 1050 | Max WS | 386.23     | 2.30  | 9.03  | 9.08  | 1.66 | 232.12  |
| OFFSITE         | RS NORTH | 100  | Max WS | 384.32     | 2.20  | 8.84  | 8.88  | 1.70 | 226.60  |
| OFFSITE         | RS SOUTH | 3500 | Max WS | 445.54     | 2,20  | 8.84  | 8.90  | 1.97 | 225.60  |
| OFFSITE         | RS SOUTH | 3450 | Max WS | 445.51     | 2,20  | 6.85  | 8.89  | 1.52 | 293.71  |
| OFFSITE         | RE SOUTH | 3300 |        | Culvert    |       |       |       |      |         |
| OFFSITE         | RE SOUTH | 3100 | Max WS | 444,62     | 2.00  | 8.46  | 8.49  | 1.58 | 281.07  |
| OFFSITE         | RS SOUTH | 100  | Max WS | 181.03     | 1.80  | 7.56  | 7.58  | 0.98 | 184.16  |
| EAST DETENTION  | 2        | 5600 | Max WS | -0.89      | 11.00 | 14.90 | 14.90 | 0.00 | 1472.54 |
| EAST DETENTION  | 2        | 5560 | Max WS | -0.89      | 11.00 | 14.90 | 14.90 | 0.00 | 1464.29 |
| EAST DETENTION  | 2        | 5520 | Max WS | -0.89      | 11.00 | 14.90 | 14.90 | 0.00 | 1362.87 |
| EAST DETENTION  | 2        | 5480 | Max WS | -0.89      | 11.00 | 14.90 | 14.90 | 0.00 | 624.64  |
| EAST DETENTION  | 2        | 5455 | Max WS | -0.89      | 11.00 | 14.90 | 14.90 | 0.60 | 514.64  |
| EAST DETENTION  | 2        | 4920 | Max WS | -0.91      | 11.00 | 14.90 | 14.90 | 0.00 | 513.99  |
| EAST DETENTION  | 2        | 4880 | Max NS | -0.91      | 11.00 | 14.90 | 14.90 | 0.00 | 898.34  |
| EAST DETENTION  | 2        | 4850 | Max WS | -0.92      | 11.00 | 14.90 | 14.90 | 0.00 | 2129.66 |
| EAST DETENTION  | 2        | 4775 | Max WS | 5.92       | 11.00 | 14.90 | 14.98 | 0.01 | 965.98  |
| EAST DETENTION  | 2        | 4653 | Max WS | 8.67       | 11.00 | 14.90 | 14.90 | 0.02 | 553.84  |
| EAST DETENTION  | 2        | 4126 | Max WS | 8.66       | 11.00 | 14.90 | 14.90 | 0.02 | 515.17  |
| EAST DETENTION  | 2        | 3563 | Max WS | 12.39      | 11.00 | 14.90 | 14.90 | 0.02 | 513.52  |
| EAST DETENTION  | 2        | 3562 |        | Culvert    |       |       |       |      |         |
| EAST DETENTION  | 2        | 3414 | Max WS | 11.88      | 11.00 | 14.86 | 14.86 | 0.02 | 507.39  |
| EAST DETENTION  | 2        | 3335 | Max WS | 11.88      | 11.00 | 14.86 | 14.86 | 0.03 | 464.78  |
| EAST DETENTION  | 2        | 3282 | Max WS | 14.06      | 11.00 | 14.86 | 14.86 | 0.06 | 221.68  |
| EAST DETENTION  | 2        | 2946 | Max WS | 20.50      | 11.00 | 14.86 | 14.86 | 0.10 | 195.65  |
| EAST DETENTION  | 2        | 2945 |        | Culvert    |       |       |       |      |         |
| EAST DETENTION  | 2        | 2855 | Max WS | 20.38      | 11.00 | 14.79 | 14.79 | 0.09 | 229,22  |
| EAST DETENTION  | 5        | 2804 | Max WS | 20.38      | 11.00 | 14.79 | 14.79 | 0.08 | 254.88  |
| EAST DETENTION  | 2        | 1864 | Max WS | 25.61      | 11.00 | 14.79 | 14.79 | 0.03 | 809.85  |
| EAST DETENTION  | 2        | 1800 | Max WS | 25.61      | 11.00 | 14.79 | 14.79 | 0.02 | 1318.29 |
| DUMMY           | 4        | 1    | Max WS | 5.00       | 11.00 | 14.90 | 14,90 | 0.01 | 337.64  |
| DUMMY           | 4        | 0    | Max WS | 5.00       | 11.00 | 14.90 | 14.90 | 0.01 | 339.48  |
|                 |          |      |        |            |       |       |       |      |         |

Profile Output Table - ChannelVolume

| River           | Reach | River Sta | Profile | Volume     |
|-----------------|-------|-----------|---------|------------|
|                 |       |           |         | (acre-ft)  |
|                 |       |           |         |            |
| WEST DETENTION  | 1     | 5540      | Max WS  | 57.07      |
| WEST DETENTION  | 1     | 5460      | Max WS  | 54.64      |
| WEST DETENTION  | 1     | 5438      | Max WS  | 52.39      |
| WEST DETENTION  | 1     | 5412      | Max WS  | 52.01      |
| WEST DETENTION  | 1     | 4950      | Max WS  | 45.45      |
| WEST DETENTION  | 1     | 4907      | Max WS  | 45.70      |
| WEST DETENTION  | 1     | 4611      | Max WS  | 41.03      |
| WEST DETENTION  | 1.    | 4537      | Max WS  | 40.07      |
| WEST DETENTION  | 1     | 3571      | Max WS  | 28.59      |
| WEST DETENTION  | 1     | 3570      |         | Culvert    |
| WEST DETENTION  | 1.    | 3417      | Max WS  | 26.86      |
| WEST DETENTION  | 1     | 3400      | Max WS  | 26.66      |
| WEST DETENTION  | 1     | 3383      | Max WS  | 26.48      |
| WEST DETENTION  | 1     | 2760      | Max WS  | 19.28      |
| WEST DETENTION  | 1     | 2722      | Max WS  | 18.30      |
| WEST DETENTION  | 1     | 2635      | Max WS  | 16.47      |
| WEST DETENTION  | 1     | 2586      | Max WS  | 14.58      |
| WEST DETENTION  | 3.    | 2545      | Mack WS | 13.37      |
| WEST DETENTION  | 1     | 2507      | Max WS  | 11.73      |
| WEST DETENTION  | 1     | 2402      | Max WS  | 9.41       |
| WEST DETENTION  | 1     | 2367      | Max WS  | 8.39       |
| WEST DETENTION  | 1.    | 1987      | Max WS  | 3.89       |
| WEST DETENTION  | 1     | 1986      |         | Culvert    |
| WEST DETENTION  | 1     | 1922      | Max WS  | 3.15       |
| WEST DETENTION  | 1     | 1891      | Max WS  | 2.79       |
| WEST DETENTION  | 1     | 1815      | Max WS  | 1.44       |
| SOUTH DETENTION | 3     | 1636      | Max WS  | 80.12      |
| SOUTH DETENTION | 3     | 1561      | Max WS  | 78.00      |
| SOUTH DETENTION | 3     | 1153      | Max WS  | 67.68      |
| SOUTH DETENTION | 3     | 1080      | Max WS  | 65.79      |
| SOUTH DETENTION | 3     | 1012      | Max WS  | 63.73      |
| SOUTH DETENTION | 3     | 945       | Max WS  | 61.64      |
| SOUTH DETENTION | 3     | 942       |         | Inl Struct |
| SOUTH DETENTION | 3     | 940       | Max WS  | 61.32      |
|                 |       |           |         |            |

| SOUTH DETENTION | 3        | 930  | Max WS | 60.32   |
|-----------------|----------|------|--------|---------|
| SOUTH DETENTION | 3        | 500  |        | Culvert |
| SOUTH DETENTION | 3        | 150  | Max WS | 3.87    |
| SOUTH DETENTION | 3        | 100  | Max WS | 1.67    |
| SOUTH DETENTION | 3        | 90   | Max WS | 1.23    |
| OFFSITE         | RS NORTH | 5350 | Max WS | 17.46   |
| OFFSITE         | RS NORTH | 1100 | Max WS | 5.42    |
| OFFSITE         | RS NORTH | 1050 | Max WS | 5.26    |
| OFFSITE         | RE NORTH | 100  | Max WS | 0.26    |
| OFFSITE         | RB SOUTH | 3500 | Max WS | 18.78   |
| OFFSITE         | R8 SOUTH | 3450 | Max WS | 18.48   |
| OFFSITE         | R8 SOUTH | 3300 |        | Culvert |
| OFFSITE         | RE SOUTH | 3100 | Max WS | 16.17   |
| OFFSITE         | RS SOUTH | 100  | Max WS |         |
| EAST DETENTION  | 2        | 5600 | Max WS | 60.85   |
| EAST DETENTION  | 2        | 5560 | Max WS | 59.64   |
| EAST DETENTION  | 2        | 5520 | Max WS | 58.23   |
| EAST DETENTION  | 2        | 5480 | Hax WS | 55.94   |
| EAST DETENTION  | 2        | 5455 | Max WS | 55.49   |
| EAST DETENTION  | 2        | 4920 | Max WS | 49.17   |
| EAST DETENTION  | 2        | 4880 | Max WS | 48.19   |
| EAST DETENTION  | 2        | 4850 | Max WS | 42.39   |
| EAST DETENTION  | 2        | 4775 | Max WS | 35.26   |
| EAST DETENTION  | 2        | 4653 | Max WS | 33.14   |
| EAST DETENTION  | 2        | 4126 | Max WS | 26.65   |
| EAST DETENTION  | 2        | 3563 | Max WS | 20.02   |
| EAST DETENTION  | 2        | 3562 |        | Culvert |
| EAST DETENTION  | 2        | 3414 | Max WS | 18.27   |
| EAST DETENTION  | 2        | 3335 | Max WS | 17.39   |
| RAST DETENTION  | 2        | 3282 | Max WS | 16.97   |
| EAST DETENTION  | 2        | 2945 | Max WS | 35.36   |
| EAST DETENTION  | 2        | 2945 |        | Culvert |
| EAST DETENTION  | 2        | 2855 | Max WS | 14.92   |
| EAST DETENTION  | 2        | 2804 | Max WS | 14.63   |
| EAST DETENTION  | 2        | 1864 | Max WS | 3.15    |
| EAST DETENTION  | 2        | 1800 | Max WS | 1.59    |
| DOMENTY         | 4        | 1    | Max WS | 0.10    |
| DUMMY           | 4        | 0    | Max WS | 0.02    |

#### 100year 10day Model 25

HEC-RAS Version 3.1.3 May 2005 U.S. Army Corp of Engineers Hydrologic Engineering Center 609 Second Street Davis, California

| x | x | XXXXXXX | XX  | ж  |     | XX | ХX | 3   | ЭX  | XXXX  |
|---|---|---------|-----|----|-----|----|----|-----|-----|-------|
| x | x | x       | x   | X  |     | X  | x  | x   | x   | x     |
| x | x | x       | x   |    |     | x  | x  | х   | x   | ж     |
|   |   | XXXX    | X X |    | XXX | XX | XX | XXX | XXX | XXXX  |
| x | x | x       | x   |    |     | Х  | X  | x   | х   | х     |
| x | x | x       | х   | х  |     | X  | х  | x   | x   | x     |
| Y | Y | XXXXXX  | XX  | XX |     | x  | x  | x   | x   | XXXXX |

PROJECT DATA PROJECT DATA
Project Title: GREENBRIAR FARMS
Project File: GB.prj
Run Date and Time: 7/14/2005 9:49:06 AM

Project in English units

Project Description:

References: Net of State Drainage Improvements-Metro Air Park, Exhibit D-2 (Offsite improved channels and Interstate 5 crossing)
2) 100yr-10day & 10yr-10day, STA 0+00, West Drain Stages, Mark Kubik @ Mead & Hunt Inc.

#### PLAN DATA

Plan Title: P1-100YR10DAY-DEVELOP

Plan File : j:\Jobs\1116-GreenbriarFarms\1116-GreenbriarFarms\Civi1\Docs\Report\HEC-RAS\GB.p01

Geometry Title: DEVELOP

Geometry File : j:\Jobs\1116-GreenbriarFarms\1116-GreenbriarFarms\Civil\Docs\Report\EEC-RAS\G8.g01

Plow Title Flow File

Plan Summary Information:

Number of: Cross Sections = 207 Multiple Openings > Culverts = 6 Inline Structures > Bridges = 0 Lateral Structures =

Computational Information

putational Information
Water surface calculation tolerance = 0.01
Critical depth calculation tolerance = 0.01
Maximum number of iterations = 20
Maximum difference tolerance = 0.3
Flow tolerance factor = 0.001

puration Options
Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Subcritical Flow

Profile Output Table - Concise Table 1

| River  |           | Reach | Ríver Sta | Profile | Q Total<br>(cfs) | Min Ch El<br>(ft) | W.S. Elev<br>(ft) | E.G. Elev<br>(ft) | Vel Chnl<br>(ft/s) | Plow Area<br>(sq ft) |
|--------|-----------|-------|-----------|---------|------------------|-------------------|-------------------|-------------------|--------------------|----------------------|
| WEST D | DETENTION | 1     | 5540      | Max WS  | 6.79             | 11.00             | 14.87             | 14.87             | 0.00               | 1461.31              |
| WEST D | DETENTION | 1     | 5460      | Max WS  | 6.77             | 11.00             | 14.87             | 14.87             | 0.01               | 1341.81              |
| WEST D | DETENTION | 1     | 5438      | Max WS  | 6.76             | 11.00             | 14.87             | 14.87             | 0.01               | 623.47               |
| WEST D | ETENTION  | 1     | 5412      | Max WS  | 6.75             | 11,00             | 14.87             | 14.87             | 0.01               | 526.81               |
| WEST D | ETENTION  | 1     | 4950      | Max WS  | 6.72             | 11.00             | 14.87             | 14.87             | 0.01               | 510.06               |
| WEST D | ETENTION  | 1     | 4907      | Max WS  | 6.71             | 11.00             | 14.87             | 14.87             | 0.01               | 666.52               |
| WEST D | ETENTION  | 1     | 4611      | Max WS  | 9.19             | 11.00             | 14.87             | 14.87             | 0.01               | 654.24               |
| WEST D | ETENTION  | 1     | 4537      | Max WS  | 10,90            | 11.00             | 14.87             | 14.87             | 0.02               | 510.62               |
| WEST D | ETENTION  | 1     | 3571      | Max WS  | 10.81            | 11.00             | 14.87             | 14.87             | 0.02               | 508.48               |
| WEST D | ETENTION  | 1     | 3570      |         | Culvert          |                   |                   |                   |                    |                      |
| WEST D | ETENTION  | 1     | 3417      | Max WS  | 9.75             | 11.00             | 14.84             | 14.84             | 0.02               | 505.40               |
| WEST D | ETENTION  | 1     | 3400      | Max WS  | 9.75             | 11.00             | 14.84             | 14.84             | 0.02               | 505.06               |
| WEST D | ETENTION  | 1     | 3383      | Max WS  | 11.25            | 11.00             | 14.84             | 14.84             | 0.02               | 506.40               |
| WEST D | ETENTION  | 1     | 2760      | Max WS  | 12.95            | 11.00             | 14.84             | 14.84             | 0.03               | 504.55               |
| WEST D | ETENTION  | 1     | 2722      | Max WS  | 14.85            | 11.00             | 14.84             | 14.84             | 0.02               | 903.57               |
| WEST D | ETENTION  | 1     | 2635      | Max WS  | 14.85            | 11.00             | 14.84             | 14.84             | 0.02               | 910.91               |
| WEST D | ETENTION  | 1     | 2586      | Max WS  | 14.84            | 11.00             | 14.84             | 14.84             | 0.01               | 1293.13              |
| WEST D | ETENTION  | 1     | 2545      | Max WS  | 14.83            | 11.00             | 14.84             | 14.84             | 0.01               | 1293.55              |
| WEST D | ETENTION  | 1     | 2507      | Max WS  | 14.83            | 11.00             | 14.84             | 14.84             | 0.02               | 919.60               |

| WEST DETENTION  | 1        | 2402         | Max WS           | 14.82        | 11.00          | 14.84          | 14.84          | 0.02 | 908.85            |
|-----------------|----------|--------------|------------------|--------------|----------------|----------------|----------------|------|-------------------|
| WEST DETENTION  | ī        | 2367         | Max WS           | 17.26        | 11.00          | 14.84          | 14.84          | 0.03 | 516.29            |
| WEST DETENTION  | 1        | 1987         | Max WS           | 17.24        | 11.00          | 14.84          | 14.84          | 0.03 | 507.23            |
| WEST DETENTION  | 1        | 1986         |                  | Culvert      |                |                |                |      |                   |
| WEST DETENTION  | 1        | 1922         | Max WS           | 15.26        | 11.00          | 14.80          | 14.80          | 0.03 | 498.95            |
| WEST DETENTION  | 1        | 1891         | Max WS           | 15.26        | 11.00          | 14.80          | 14.80          | 0.03 | 498.42            |
| WEST DETENTION  | ī        | 1815         | Max WS           | 17.30        | 11.00          | 14.80          | 14.80          | 0.02 | 1055.66           |
| SOUTH DETENTION | 3        | 1636         | Max WS           | 42.53        | 11.00          | 14.80          | . 14.80        | 0.03 | 1455.50           |
| SOUTH DETENTION | 3        | 1561         | Max WS           | 42.53        | 11.00          | 14.80          | 14.80          | 0.04 | 994,38            |
| SOUTH DETENTION | 3        | 1153         | Max WS           | 53.13        | 11.00          | 14.80          | 14.80          | 0.04 | 1215.51           |
| SOUTH DETENTION | 3        | 1080         | Max WS           | 53.12        | 11.00          | 14.80          | 14.80          | 0.05 | 1048.91           |
| SOUTH DETENTION | 3        | 1012         | Max WS           | 61.47        | 11.00          | 14.80          | 14.80          | 0.04 | 1602.65           |
| SOUTH DETENTION | 3        | 945          | Max WS           | 61.46        | 11.00          | 14.80          | 14.80          | 0.05 | 1126.79           |
| SOUTH DETENTION | 3        | 942          |                  | Inl Struct   |                |                |                |      |                   |
| SOUTH DETENTION | 3        | 940          | Max WS           | 61.46        | 2.70           | 14.80          | 14.80          | 0.02 | 4389.69           |
| SOUTH DETENTION | 3        | 930          | Max WS           | 61.46        | 2.70           | 14.80          | 14.80          | 0.02 | 4389.69           |
| SOUTH DETENTION | 3        | 500          |                  | Culvert      |                | *              |                |      |                   |
| SOUTH DETENTION | 3        | 150          | Max WS           | 46.18        | 2.20           | 11.21          | 11.21          | 0.02 | 2906.49           |
| SOUTH DETENTION | 3        | 100          | Max WS           | 46.18        | 2.20           | 11.21          | 11.21          | 0.02 | 2906.49           |
| SOUTH DETENTION | 3        | 90           | Max WS           | 46.18        | 2.20           | 11.21          | 11.21          | 0.02 | 2906.49           |
| OFFSITE         | RS NORTH | 5350         | Max WS           | 251.59       | 9.00           | 14.18          | 14.27          | 2.46 | 102.28            |
| OFFSITE         | RS NORTH | 1100         | Max WS           | 19.48        | 6.00           | 11.21          | 11.21          | 0.18 | 110.05            |
| OFFSITE         | R8 NORTH | 1050         | Max WS           | 19.48        | 2.30           | 11.21          | 11.21          | 0.06 | 345.95            |
| OFFSITE         | RS NORTH | 100          | Max WS           | 19.46        | 2.20           | 11.21          | 11.21          | 0.06 | 350.01            |
| OFFSITE         | RS SOUTH | 3500         | Max WS           | 65.63        | 2.20           | 11.21          | 11.21          | 0.19 | 350.01            |
| OFFSITE         | RS SOUTH | 3450         | Max WS           | 65.63        | 2.20           | 11.21          | 11.21          | 0.15 | 440.12            |
| OPPSITE         | RB SOUTH | 3300         |                  | Culvert      |                |                |                |      |                   |
| OFFSITE         | R8 SOUTH | 3100         | Max WS           | 65,63        | 2.00           | 11.20          | 11.20          | 0.15 | 449.24            |
| OFFSITE         | RS SOUTH | 100          | Max WS           | 63.33        | 1.80           | 11.19          | 11.19          | 0.17 | 365.14<br>1461.65 |
| EAST DETENTION  | 2        | 5600         | Max WS           | -1.79        | 11.00          | 14.87          | 14.87          | 0.00 | 1453.45           |
| EAST DETENTION  | 2        | 5560         | Max WS           | -1.80        | 11.00          | 14.87          | 14.87<br>14.87 | 0.00 | 1352.68           |
| EAST DETENTION  | 2        | 5520         | Max WS           | -1.80        | 11.00          | 14.87          | 14.87          | 0.00 | 619.76            |
| EAST DETENTION  | 2        | 5460         | Max WS           | -1.82        | 11.00          | 14.87          | 14.87          | 0.00 | 510.62            |
| EAST DETENTION  | 2        | 5455         | Max WS           | -1.82        | 11.00          | 14.87          | 14.87          | 0.00 | 509.97            |
| EAST DETENTION  | 2 .      | 4920         | Max WS           | -1.87        | 11.00          | 14.87<br>14.87 | 14.87          | 0.00 | 891.37            |
| EAST DETENTION  | 2        | 4880         | Max WS           | -1.88        | 11.00<br>11.00 | 14.67          | 14.87          | 0.00 | 2113.88           |
| EAST DETENTION  | 2        | 4850         | Max WS           | -1.92        | 11.00          | 14.87          | 14.87          | 0.01 | 958.63            |
| EAST DETENTION  | 2        | 4775         | Max WE           | 6.48         | 11.00          | 14.67          | 14.87          | 0.01 | 549.49            |
| EAST DETENTION  | 2        | 4653         | Max WS           | 7.42<br>7.36 | 11.00          | 14.87          | 14.67          | 0.01 | 511.14            |
| EAST DETENTION  | 2        | 4126         | Max WS           | 10.82        | 11.00          | 14.87          | 14.87          | 0.02 | 509.49            |
| EAST DETENTION  | 2        | 3563         | Max WS           | Culvert      | 77.00          | 14.07          | 14.07          | 0.04 | 202,27            |
| EAST DETENTION  | 2        | 3562         | M MC             | 8.84         | 11.00          | 14.84          | 14.84          | 0.02 | 504.30            |
| EAST DETENTION  | 2        | 3414         | Max WS<br>Max WS | 8.84         | 11.00          | 14.84          | 14.84          | 0.02 | 461.92            |
| EAST DETENTION  | 2        | 3335         | Max WS           | 10.38        | 11.00          | 14.84          | 14.84          | 0.05 | 220.17            |
| EAST DETENTION  | 2        | 3282         |                  | 16.11        | 11.00          | 14.84          | 14.84          | 0.08 | 194.30            |
| EAST DETENTION  | 2        | 2946         | Max WS           | Culvert      | 44,00          | ****           |                | 4    |                   |
| EAST DETENTION  | 2        | 2945<br>2855 | Max WS           | 15.55        | 11.00          | 14.80          | 14.80          | 0.07 | 229.97            |
| EAST DETENTION  | 2        | 2855         | Max WS           | 15.55        | 11.00          | 14.80          | 14.80          | 0.06 | 255.70            |
| EAST DETENTION  | 2        |              | Max WS           | 25.24        | 11.00          | 14.80          | 14.80          | 0.03 | 812.18            |
| EAST DETENTION  | 2        | 1864<br>1800 | Max WS           | 25.23        | 11.00          | 14.80          | 14.80          | 0.02 | 1322.08           |
| EAST DETENTION  | 2        | 1800         | Max WS           | 5.00         | 11.00          | 14.87          | 14.87          | 0.01 | 334.52            |
| DUMMY           | 4        | ė            | Max WS           | 5.00         | 11.00          | 14.87          | 14.87          | 0.01 | 336.36            |
| DUMMY           | 4        | U            | MON WE           | 5.00         |                | ~              |                |      |                   |

Profile Output Table - ChannelVolume

| River           | Reach | River Sta | Profile | Volume     |
|-----------------|-------|-----------|---------|------------|
|                 |       |           |         | (acre-ft)  |
|                 |       |           |         |            |
| WEST DETENTION  | 1     | 5540      | Max WS  | 56.70      |
| WEST DETENTION  | 1     | 5460      | Max WS  | 54.28      |
| WEST DETENTION  | 1     | 5438      | Max WS  | 52.05      |
| WEST DETENTION  | 1     | 5412      | Max WS  | 51.67      |
| WEST DETENTION  | 1     | 4950      | Max WS  | 46.15      |
| WEST DETENTION  | 1     | 4907      | Max WS  | 45.41      |
| WEST DETENTION  | 1     | 4611      | Max WE  | 40.77      |
| WEST DETENTION  | 1     | 4537      | Max WS  | 39.82      |
| WEST DETENTION  | 1     | 3571      | Max WS  | 28.53      |
| WEST DETENTION  | 1     | 3570      |         | Culvert    |
| WEST DETENTION  | 1     | 3417      | Max WS  | 26.72      |
| WEST DETENTION  | 1     | 3400      | Max WS  | 26.51      |
| WEST DETENTION  | 1     | 3383      | Max WS  | 26.33      |
| WEST DETENTION  | 1     | 2760      | Max WS  | 19.18      |
| WEST DETENTION  | 1.    | 2722      | Max WS  | 18.22      |
| WEST DETENTION  | 1     | 2635      | Max WS  | 16.39      |
| WEST DETENTION  | 1     | 2586      | Max WS  | 14,52      |
| WEST DETENTION  | 1     | 2545      | Max WS  | 13.31      |
| WEST DETENTION  | 1     | 2507      | Max WS  | 11.68      |
| WEST DETENTION  | 1     | 2402      | Max WS  | 9.38       |
| WEST DETENTION  | 1     | 2367      | Max WS  | 8.37       |
| WEST DETENTION  | 1     | 1987      | Max WS  | 3.90       |
| WEST DETENTION  | 1     | 1986      |         | Culvert    |
| WEST DETENTION  | 1     | 1922      | Max WS  | 3.16       |
| WEST DETENTION  | 1     | 1891      | Max WS  | 2.80       |
| WEST DETENTION  | 1     | 1815      | Max W5  | 1.44       |
| SOUTH DETENTION | 3     | 1636      | Max WS  | 91.06      |
| SOUTH DETENTION | 3     | 1561      | Max WS  | 88.93      |
| SOUTH DETENTION | 3     | 1153      | Max WS  | 78.58      |
| SOUTH DETENTION | 3     | 1080      | Max WS  | 76.68      |
| SOUTH DETENTION | 3     | 1012      | Max WS  | 74.62      |
| SOUTH DETENTION | 3     | 945       | Max WS  | 72.52      |
| SOUTH DETENTION | 3     | 942       |         | Inl Struct |
| SOUTH DETENTION | 3     | 940       | Max WS  | 72.20      |
| SOUTH DETENTION | 3     | 930       | Max WS  | 71.20      |

| SOUTH DETENTION | 3        | 500  |        | Culvert |
|-----------------|----------|------|--------|---------|
| SOUTH DETENTION | 3        | 150  | Max WS | 5.87    |
| SOUTH DETENTION | 3 .      | 100  | Max WS | 2.54    |
| SOUTH DETENTION | 3        | 90   | Max WS | 1.87    |
| OFFSITE         | R8 NORTH | 5350 | Max WS | 18.01   |
| OFFSITE         | RS NORTH | 1100 | Max WS | 8.25    |
| OFFSITE         | R8 NORTH | 1050 | Max WS | 7.99    |
| OFFSITE         | R8 NORTH | 100  | Max WS | 0.40    |
| OFFSITE         | R8 SOUTH | 3500 | Max WS | 32.09   |
| OFFSITE         | R8 SOUTH | 3450 | Max WS | 31.64   |
| OFFSITE         | R8 SOUTH | 3300 |        | Culvert |
| OFFSITE         | RE SOUTH | 3100 | Max WS | 28.07   |
| OFFSITE         | R8 SOUTH | 100  | Max WS |         |
| EAST DETENTION  | 2        | 5600 | Max WS | 60.54   |
| EAST DETENTION  | 2        | 5560 | Max WS | 59.35   |
| EAST DETENTION  | 2        | 5520 | Max WS | 57.95   |
| EAST DETENTION  | 2        | 5480 | Max WS | 55.68   |
| EAST DETENTION  | 2        | 5455 | Max WS | 55.23   |
| EAST DETENTION  | 2        | 4920 | Max WS | 48.96   |
| EAST DETENTION  | 2        | 4880 | Max ₩S | 47.98   |
| EAST DETENTION  | 2        | 4850 | Max WS | 42.23   |
| EAST DETENTION  | 2        | 4775 | Max WS | 35.15   |
| EAST DETENTION  | 2        | 4653 | Max WS | 33.04   |
| EAST DETENTION  | 2        | 4126 | Max WS | 26,62   |
| EAST DETENTION  | 2        | 3563 | Max WS | 20.03   |
| EAST DETENTION  | 2        | 3562 |        | Culvert |
| EAST DETENTION  | 2        | 3414 | Max WS | 18.29   |
| EAST DETENTION  | 2        | 3335 | Max WS | 17.42   |
| EAST DETENTION  | 2        | 3282 | Max WS | 17.00   |
| EAST DETENTION  | 2        | 2946 | Max WS | 15.41   |
| EAST DETENTION  | 2        | 2945 |        | Culvert |
| EAST DETENTION  | 2        | 2855 | Max WS | 14.96   |
| EAST DETENTION  | 2        | 2804 | Max WS | 14.68   |
| EAST DETENTION  | 2        | 1864 | Max WS | 3.16    |
| EAST DETENTION  | 2        | 1800 | Max WS | 1.59    |
| DOMMY           | 4        | 1    | Max WS | 0.10    |
| DEMMEY          | 4        | G    | Max WS | 0.02    |

#### 10year 24hour Model 25

HEC-RAS Version 3.1.3 May 2005 U.S. Army Coxp of Engineers Hydrologic Engineering Center 609 Second Street Davis, California

| x  |    |       | XX   | СХХ |     | XXXX |    | XX     |   | XXXX  |
|----|----|-------|------|-----|-----|------|----|--------|---|-------|
| x  | X  | X     | x    | X   |     | X    | x  | x      | x | x     |
| x  | ×  | x     | x    |     |     | X    | х  | x      | x | x     |
|    |    | XXXX  | x xx |     | XXX | XX   | XX | XXXXXX |   | XXXX  |
| x  | x  | x     | X    |     |     | X    | X  | x      | х | x     |
| x  | ×  | x     | x    | х   |     | ж    | ж  | x      | x | x     |
| 35 | ** | ***** | 10   | CVY |     | ×    | x  | х      | х | XXXXX |

PROJECT DATA Project Title: GREENBRIAR FARMS
Project File: GB.prj
Run Date and Time: 7/15/2005 10:41:24 AM Project in English units Project Description: Project Description:
References:

1) Offsite Drainage Improvements-Metro Air Park, Exhibit D-2
(Offsite improved channels and Interstate S crossing)
2) 100yr-10day &
10yr-10day, STA 0+00, West Drain Stages, Mark Kubik @ Mead & Hunt Inc.

#### PLAN DATA

Plan Title: P4-10YR24HR-DEVELOP Plan File : j:\Jobs\1116-GreenbriarFarms\1116-GreenbriarFarms\Civil\Docs\Report\HEC-RAS\GB.p05

Geometry Title: DEVELOP Geometry File : j:\Jobs\1116-GreenbriarFarms\1116-GreenbriarFarms\Civil\Docs\Report\HEC-RAS\GB.g01

Flow Title Flow File

Plan Summary Information:
Number of: Cross Sections « 207 Multiple Openings = Culverts = 6 Inline Structures = Bridges = 0 Lateral Structures =

Computational Information

putational Information
water surface calculation tolerance = 0.01
Critical depth calculation tolerance = 0.01
Maximum number of iterations = 20
Maximum difference tolerance = 0.3
Flow tolerance factor = 0.001

Computation Options
Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only

Friction Slope Method: Computational Flow Regime: Average Conveyance Subcritical Flow

Profile Output Table - Concise Table 1

| River          | Reach | River Sta | Profile | Q Total<br>(cfs) | Min Ch El<br>(ft) | W.S. Elev<br>(ft) | E.G. Blev<br>(ft) | Vel Chnl<br>(ft/s) | Flow Area<br>(sq ft) |
|----------------|-------|-----------|---------|------------------|-------------------|-------------------|-------------------|--------------------|----------------------|
| WEST DETENTION | 1     | 5540      | Max WS  | 5.83             | 11.00             | 13.54             | 13.54             | 0.01               | 950.13               |
| WEST DETENTION | 1     | 5460      | Max WS  | 5.83             | 11.00             | 13.54             | 13.54             | 0.01               | 867.68               |
| WEST DETENTION | 1     | 5438      | Max WS  | 5.83             | 11.00             | 13.54             | 13.54             | 0.01               | 397.43               |
| WEST DETENTION | 1     | 5412      | Max WS  | 5.83             | 11.00             | 13.54             | 13.54             | 0.02               | 333.77               |
| WEST DETENTION | 1     | 4950      | Max WS  | 5.82             | 11.00             | 13.54             | 13.54             | 0.02               | 325.08               |
| WEST DETENTION | ī     | 4907      | Max WS  | 5.82             | 11.00             | 13.54             | 13.54             | 0.01               | 426.32               |
| WEST DETENTION | ī     | 4611      | Max WS  | 9.27             | 11.00             | 13.54             | 13.54             | 0.02               | 418.73               |
| WEST DETENTION | 1     | 4537      | Max WS  | 11,61            | 11.00             | 13.54             | 13.54             | 0.04               | 325.44               |
| WEST DETENTION | 1     | 3571      | Max WS  | 11.60            | 11.00             | 13.54             | 13,54             | 0.04               | 323.91               |
| WEST DETENTION | 1     | 3570      |         | Culvert          |                   |                   |                   |                    |                      |
| WEST DETENTION | 1     | 3417      | Max WS  | 11.38            | 11.00             | 13.50             | 13,50             | 0.04               | 318.96               |
| WEST DETENTION | ĭ     | 3400      | Max WS  | 11.38            | 11.00             | 13.50             | 13.50             | 0.04               | 318.63               |
| WEST DETENTION | 1     | 3383      | Max WS  | 13.61            | 11.00             | 13.50             | 13.50             | 0.04               | 319.72               |
| WEST DETENTION | 1     | 2760      | Max WS  | 15.56            | 11.00             | 13.50             | 13.50             | 0.05               | 318.28               |
| WEST DETENTION | ï     | 2722      | Max WS  | 17.94            | 11.00             | 13.50             | 13.50             | 0,03               | 578.20               |
| WEST DETENTION | 1     | 2635      | Max WS  | 17.93            | 11.00             | 13.50             | 13.50             | 0.03               | 582.88               |
| WEST DETENTION | 1     | 2586      | Max WS  | 17.93            | 11.00             | 13.50             | 13.50             | 0.02               | 831.71               |
| WEST DETENTION | î     | 2545      | Max WS  | 17.93            | 11.00             | 13.50             | 13.50             | 0.02               | 832.26               |

| WEST DETENTION  | 1        | 2507 | Max WS  | 17.93      | 11.00 | 13.50 | 13.50 | 0.03 | 588.23  |
|-----------------|----------|------|---------|------------|-------|-------|-------|------|---------|
| WEST DETENTION  | 1        | 2402 | Max WS  | 17.93      | 11.00 | 13.50 | 13.50 | 0.03 | 581,57  |
| WEST DETENTION  | 1        | 2367 | Max WS  | 20.91      | 11.00 | 13.50 | 13.50 | 0.06 | 325.70  |
| WEST DETENTION  | î        | 1987 | Max WS  | 20.91      | 11.00 | 13.50 | 13.50 | 0.07 | 320.13  |
| WEST DETENTION  | 1        | 1986 |         | Culvert    |       |       |       |      |         |
| WEST DETENTION  | î        | 1922 | Max WS  | 20.82      | 11.00 | 13.41 | 13.41 | 0.07 | 306.61  |
| WEST DETENTION  | 1        | 1891 | Max WS  | 20.81      | 11.00 | 13.41 | 13.41 | 0.07 | 306.21  |
| WEST DETENTION  | ì        | 1815 | Max WS  | 23.06      | 11.00 | 13.41 | 13.41 | 0.04 | 656.13  |
| SOUTH DETENTION | 3        | 1636 | Max WS  | 48.55      | 11.00 | 13.41 | 13.41 | 0.05 | 910.62  |
| SOUTH DETENTION | 3        | 1561 | Max WS  | 48.54      | 11.00 | 13.41 | 13.41 | 0.08 | 620.72  |
| SOUTH DETENTION | 3        | 1153 | Max WS  | 55.63      | 11.00 | 13.41 | 13.41 | 0.07 | 761.75  |
| SOUTH DETENTION | 3        | 1080 | Max WS  | 55.62      | 11.00 | 13.41 | 13.41 | 0.08 | 656.09  |
| SOUTH DETENTION | 3        | 1012 | Max WS  | 61.38      | 11.00 | 13.41 | 13.41 | 0.06 | 1003.90 |
| SOUTH DETENTION | 3        | 945  | Max WS  | 61.37      | 11.00 | 13.41 | 13.41 | 0.09 | 695.48  |
| SOUTH DETENTION | 3        | 942  |         | Inl Struct |       |       |       |      |         |
| SOUTH DETENTION | 3        | 940  | Max WS  | 61.37      | 2.70  | 13.40 | 13.40 | 0.02 | 3772.33 |
| SOUTH DETENTION | 3        | 930  | Maox WS | 61.37      | 2.70  | 13.40 | 13.40 | 0.02 | 3772.13 |
| SOUTH DETENTION | 3        | 500  |         | Culvert    |       |       |       |      |         |
| SOUTH DETENTION | 3        | 150  | Max WS  | 61.36      | 2.20  | 8.19  | 8.19  | 0.04 | 1710.23 |
| SOUTH DETENTION | 3        | 100  | Max WS  | 61.23      | 2.20  | 8.19  | 8.19  | 0.04 | 1710.23 |
| SOUTH DETENTION | 3        | 90   | Max WS  | 61.21      | 2,20  | 8.19  | 8.19  | B.04 | 1710.23 |
| OFFSITE         | RS NORTH | 5350 | Max WS  | 241.70     | 9.00  | 13.95 | 14.05 | 2.51 | 96.17   |
| OFFSITE         | RS NORTH | 1100 | Max WS  | 229.18     | 6.00  | 8.26  | 8.89  | 5.36 | 36.01   |
| OFFSITE         | RS NORTH | 1050 | Max WS  | 229.88     | 2.30  | 8.30  | 8.32  | 1.16 | 197.86  |
| OFFSITE         | RS NORTH | 100  | Max WS  | 229.04     | 2.20  | 8.19  | 8.21  | 1.16 | 196.88  |
| OFFSITE         | RE SOUTH | 3500 | Max WS  | 290.25     | 2.20  | 8.19  | 8.22  | 1.47 | 196.88  |
| OFFSITE         | RS SOUTH | 3450 | Max WS  | 290.23     | 2.20  | 8.20  | 8.22  | 1.13 | 257.17  |
| OFFSITE         | RS SOUTH | 3300 |         | Culvert    |       |       |       |      |         |
| OFFSITE         | RS SOUTH | 3100 | Max WS  | 290.09     | 2.00  | 7.99  | 8.01  | 1.14 | 255.17  |
| OPPSITE         | R8 SOUTH | 100  | Max WS  | 128.88     | 1.80  | 7.56  | 7.57  | 0.70 | 184.16  |
| EAST DETENTION  | 2        | 5600 | Max WS  | -0.83      | 11.00 | 13.54 | 13.54 | 0.00 | 950.30  |
| EAST DETENTION  | 2        | 5560 | Max WS  | -0.83      | 11.00 | 13.54 | 13.54 | 0.00 | 944.64  |
| EAST DETENTION  | 2        | 5520 | Max WS  | -0.83      | 11.00 | 13.54 | 13.54 | 0.00 | 876.14  |
| RAST DETENTION  | 2        | 5480 | Max WS  | -0.84      | 11.00 | 13.54 | 13.54 | 0.00 | 395.08  |
| EAST DETENTION  | 2        | 5455 | Max WS  | -0.84      | 11,00 | 13.54 | 13.54 | 0.00 | 325.47  |
| EAST DETENTION  | 2        | 4920 | Max WS  | -0.84      | 11.00 | 13.54 | 13.54 | 0.00 | 324.97  |
| EAST DETENTION  | 2        | 4880 | Max WS  | -0.85      | 11.00 | 13.54 | 13.54 | 0.00 | 569.95  |
| EAST DETENTION  | 2        | 4850 | Max WS  | -0.85      | 11.00 | 13.54 | 13.54 | 0.00 | 1374.82 |
| EAST DETENTION  | 2        | 4775 | Max WS  | 6.76       | 11 00 | 13.54 | 13.54 | 0.01 | 617.66  |
| EAST DETENTION  | 2        | 4653 | Max WS  | 8.65       | 11.00 | 13.54 | 13.54 | 0.02 | 349.80  |
| EAST DETENTION  | 2        | 4126 | Max WS  | 8.54       | 11.00 | 13.54 | 13.54 | 0.03 | 325.81  |
| EAST DETENTION  | 2        | 3563 | Max WS  | 12.18      | 11.00 | 13.54 | 13.54 | 0.04 | 324.71  |
| EAST DETENTION  | 2        | 3562 |         | Culvert    |       |       |       |      |         |
| EAST DETENTION  | 2        | 3414 | Max WS  | 11.15      | 11.00 | 13.50 | 13.50 | 0.04 | 317.97  |
| EAST DETENTION  | 2        | 3335 | Max WS  | 11.15      | 11.00 | 13.50 | 13.50 | 0.04 | 289.72  |
| EAST DETENTION  | 2        | 3282 | Max WS  | 13.33      | 11.00 | 13.50 | 13.50 | 0.10 | 132.23  |
| EAST DETENTION  | 2        | 2946 | Max WS  | 19.77      | 11.00 | 13.50 | 13.50 | 0.17 | 116.24  |
| EAST DETENTION  | 2        | 2945 |         | Culvert    |       |       |       |      |         |
| EAST DETENTION  | 2        | 2855 | Max WS  | 19.76      | 11.00 | 13.41 | 13.41 | 0.15 | 135.99  |
| EAST DETENTION  | 2        | 2804 | Max WS  | 19.76      | 11.00 | 13.41 | 13.41 | 0.13 | 152.17  |
| EAST DETENTION  | 2        | 1864 | Max WS  | 25.50      | 11.00 | 13.41 | 13.41 | 0.05 | 505.61  |
| EAST DETENTION  | 2        | 1800 | Max WS  | 25.49      | 11.00 | 13.41 | 13.41 | 0.03 | 823.79  |
| DUMMY           | 4        | 1    | Max WS  | 5.00       | 11.00 | 13.54 | 13.54 | 0.03 | 198.21  |
| DUMMY           | 4        | G    | Max WS  | 5.00       | 11.00 | 13.54 | 13.54 | 0.03 | 199.73  |
|                 |          |      |         |            |       |       |       |      |         |

Profile Output Table - ChannelVolume

| River           | Reach | River Sta | Profile | Volume     |
|-----------------|-------|-----------|---------|------------|
| ****            |       |           |         | (acre-ft)  |
|                 |       |           |         |            |
| WEST DETENTION  | 1     | 5540      | Max WS  | 36.06      |
| WEST DETENTION  | 1     | 5460      | Max WS  | 34.49      |
| WEST DETENTION  | 1     | 5438      | Max WS  | 33.06      |
| WEST DETENTION  | 1     | 5412      | Max WS  | 32.82      |
| WEST DETENTION  | 1     | 4950      | Max WS  | 29.31      |
| WEST DETENTION  | 1     | 4907      | Max WS  | 28.84      |
| WEST DETENTION  | 1     | 4611      | Max WS  | 25,87      |
| WEST DETENTION  | 1     | 4537      | Max W5  | 25.27      |
| WEST DETENTION  | 1     | 3571      | Max WS  | 18.07      |
| WEST DETENTION  | 1     | 3570      |         | Culvert    |
| WEST DETENTION  | 1     | 3417      | Max WS  | 16.92      |
| WEST DETENTION  | 1     | 3400      | Max WS  | 16.79      |
| WEST DEPENTION  | 1     | 3383      | Max WS  | 16.68      |
| WEST DETENTION  | 1     | 2760      | Max WS  | 12.17      |
| WEST DETENTION  | 1     | 2722      | Max WS  | 11.55      |
| WEST DETENTION  | 1     | 2635      | Max WS  | 10.38      |
| WEST DETENTION  | 1     | 2586      | Max WS  | 9.18       |
| WEST DETENTION  | 1     | 2545      | Max WS  | 8.41       |
| WEST DETENTION  | 1     | 2507      | Max WS  | 7.36       |
| WEST DETENTION  | 1     | . 2402    | Max WS  | 5.88       |
| WEST DETENTION  | 1     | 2367      | Max WS  | 5.24       |
| WEST DETENTION  | 1     | 1987      | Max WS  | 2.42       |
| WEST DETENTION  | 1     | 1986      |         | Culvert    |
| WEST DETENTION  | 1     | 1922      | Max WS  | 1.96       |
| WEST DETENTION  | 1     | 1891      | Max WS  | 1.74       |
| WEST DETENTION  | 1     | 1815      | Max WS  | 0.90       |
| SOUTH DETENTION | 3     | 1636      | Max WS  | 65.25      |
| SOUTH DETENTION | 3     | 1561      | Max WS  | 63.92      |
| SOUTH DETENTION | 3     | 1153      | Max WS  | 57.44      |
| SOUTH DETENTION | 3     | 1080      | Max WS  | 56.26      |
| SOUTH DETENTION | 3     | 1012      | Max WS  | 54.96      |
| SOUTH DETENTION | 3     | 945       | Max WS  | 53.66      |
| SOUTH DETENTION | 3     | 942       |         | Inl Struct |
| SOUTH DETENTION | 3     | 940       | Max WS  | 53.40      |
|                 |       |           |         |            |

| SOUTH DETENTION | 3        | 930  | Max WS | 52.53   |
|-----------------|----------|------|--------|---------|
| SOUTH DETENTION | 3        | 500  |        | Culvert |
| SOUTH DETENTION | 3        | 150  | Max WS | 3.45    |
| SOUTH DETENTION | 3        | 100  | Max WS | 1.49    |
| SOUTH DETENTION | 3        | 90   | Max WS | 1.09    |
| OFFSITE         | RS NORTH | 5350 | Max WS | 12.94   |
| OFFSITE         | RS NORTH | 1100 | Max WS | 4.55    |
| OFFSITE         | RS NORTH | 1050 | Max WS | 4.53    |
| OFFSITE         | RS NORTH | 100  | Max WS | 0.23    |
| OFFSITE         | RS SOUTH | 3500 | Max WS | 17.48   |
| OFFSITE         | RS SOUTH | 3450 | Max WS | 17.22   |
| OFFSITE         | RS SOUTH | 3300 |        | Culvert |
| OFFSITE         | RE SOUTH | 3100 | Max WS | 15.16   |
| OFFSITE         | R8 SOUTH | 100  | Max WS |         |
| EAST DETENTION  | 2        | 5600 | Max WS | 38.37   |
| EAST DETENTION  | 2        | 5560 | Max WS | 37.60   |
| EAST DETENTION  | 2        | 5520 | Max WS | 36.69   |
| EAST DETENTION  | 2        | 5480 | Max WS | 35.23   |
| EAST DETENTION  | 2        | 5455 | Max W5 | 34 - 94 |
| EAST DETENTION  | 2        | 4920 | Max WS | 30.94   |
| EAST DETENTION  | 2        | 4880 | Max WS | 30.32   |
| EAST DETENTION  | 2        | 4850 | Max WS | 26.60   |
| EAST DETENTION  | 2        | 4775 | Max WS | 22.01   |
| EAST DETENTION  | 2        | 4653 | Max WS | 20.56   |
| EAST DETENTION  | 2        | 4126 | Max WS | 16.56   |
| EAST DETENTION  | 2        | 3563 | Max WS | 12.36   |
| EAST DETENTION  | 2        | 3562 |        | Culvert |
| EAST DETENTION  | 2        | 3414 | Max WS | 11.26   |
| EAST DETENTION  | 2        | 3335 | Max WS | 10.71   |
| EAST DETENTION  | 2        | 3282 | Max WS | 10.45   |
| EAST DETENTION  | 2        | 2946 | Max WS | 9.50    |
| EAST DETENTION  | 2        | 2945 |        | Culvert |
| EAST DETENTION  | 2        | 2855 | Max WS | 9.23    |
| EAST DETENTION  | 2        | 2804 | Max WS | 9.06    |
| EAST DETENTION  | 2        | 1864 | Max WS | 1.97    |
| EAST DETENTION  | 2        | 1800 | Max WS | 1.00    |
| DUMMY           | 4        | 1    | Max WS | 0.06    |
| THE BANKY       | 4        | 0    | Max WS | 0.01    |



## 8. APPENDIX C -

**Existing Culvert Capacities** 

# AppC.TXT BOX CULVERT ANALYSIS COMPUTATION OF CULVERT PERFORMANCE CURVE

### July 15, 2005

| PROGRAM INP  | JT DATA   |                     |          |               |  |  |  |  |
|--|-----------|---------------------|----------|---------------|--|--|--|--|
| DESCRIPTION  |           |                     |          | VALUE         |  |  |  |  |
| Culvert Span (ft)  |           |                     |          | 8.0           |  |  |  |  |
| Culvert Rise (ft)  |           | *******             |          | 5.0<br>8<br>1 |  |  |  |  |
| FHWA Chart Number FHWA Scale Number (Type of Culvert Entrance)                               |           |                     |          |               |  |  |  |  |
| Manning's Roughness Coefficient (n-value).   |           | * * * * * * * * * * |          | 0.012         |  |  |  |  |
| Entrance Loss Coefficient of Culvert Openium   | 1g        |                     |          | 0.5<br>340.0  |  |  |  |  |
| Culvert Length (ft)  | ert (ft). |                     |          | 5.3           |  |  |  |  |
| Invert Elevation at Upstream end of Culver   | t (ft)    |                     |          | 5.5           |  |  |  |  |
| Culvert Slope (ft/ft)  |           | *******             |          | 0.0006        |  |  |  |  |
| Starting Flow Rate (cfs)   |           |                     |          | 301.0         |  |  |  |  |
| Starting Flow Rate (cfs)   |           |                     |          | 0.0           |  |  |  |  |
| Ending Flow Rate (cts)   |           |                     |          | 301.0         |  |  |  |  |
| Starting Tailwater Depth (ft)  |           | *******             |          | 7.0           |  |  |  |  |
| Starting Tailwater Depth (ft)  Incremental Tailwater Depth (ft)  Ending Tailwater Depth (ft) |           |                     |          | 4.2<br>11.2   |  |  |  |  |
| Ending Tailwater Depth (Ft)  |           |                     |          | 11.2          |  |  |  |  |
|  |           | · <del></del>       |          |               |  |  |  |  |
| COMPUTATION RESULTS  |           |                     |          |               |  |  |  |  |
| Flow Tailwater Headwater (ft)  | Normal    | Critical            | Depth at | Outlet        |  |  |  |  |
| Flow Tailwater Headwater (ft)<br>Rate Depth Inlet Outlet                                     | Depth     | Depth               | Outlet   | Velocity      |  |  |  |  |
| (cfs) (ft) Control Control   | (†t)      | (†t)                | (†t)     | (fps)         |  |  |  |  |

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Phone: (281)440-3787, Fax: (281)440-4742, Email: software@dodson-hydro.com
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8.83 13.03

5.73 5.73 5.0 5.0 5.0

7.53 7.53

3.53 3.53

7.0 11.2

301.0 301.0

Results and Discussion: Under existing conditions, the 100-year peak flow through the 3-8'x5' box culverts is 904cfs (see Table 1). The culvert was analyzed individually by prorating the flow.



## 9. APPENDIX D -

Gate Maximum Outflow Calculations

## Worksheet Worksheet for Broad Crested Weir

| Project Description  |               |      |       |           |  |  |
|----------------------|---------------|------|-------|-----------|--|--|
| Worksheet            | W             | /eir |       |           |  |  |
| Туре                 | Broad Crested |      |       |           |  |  |
|                      | Weir          |      |       |           |  |  |
| Solve For            | D             | ISC  | harge |           |  |  |
|                      |               |      | -     |           |  |  |
| Input Data           |               |      |       |           |  |  |
| Headwater            | 14.90         | ft   | •     |           |  |  |
| Elevation            |               |      |       |           |  |  |
| Crest Elevation      | 14.00         |      |       |           |  |  |
| Tailwater Elevation  | 11.20         | ft   |       |           |  |  |
| Crest Surface Type   |               |      |       |           |  |  |
|                      | d             | _    |       |           |  |  |
| Crest Breadth        | 6.00          |      |       |           |  |  |
| Crest Length         | 16.00         | π    |       |           |  |  |
|                      |               |      |       |           |  |  |
| Results              |               |      |       |           |  |  |
| Discharge            |               |      | 41.69 | cfs       |  |  |
| Headwater Height A   | bove          |      | 0.90  | ft        |  |  |
| Crest                | _             |      |       | ~         |  |  |
| Tailwater Height Abo |               | st   |       |           |  |  |
| Discharge Coefficier | nt            |      | 3.05  | US        |  |  |
| Submergence Factor   | r             |      | 1.00  |           |  |  |
| Adjusted Discharge   |               |      | 3.05  | US        |  |  |
| Coefficient          |               |      |       | <b>A2</b> |  |  |
| Flow Area            |               |      | 14.4  |           |  |  |
| Velocity             |               |      | 2.90  |           |  |  |
| Wetted Perimeter     |               |      | 17.80 |           |  |  |
| Top Width            |               |      | 16.00 | ft        |  |  |

## Result and Discussion:

During the peak stage, 14.9', in the pond, the Rubicon gate will close to reduce the total outflow. With the top of the gate at elevation 14.0', there will be weir flow above the gate and the total outflow was determined to be 42 cfs, which is less than the total allowable of 62 cfs.



## 10. APPENDIX E -

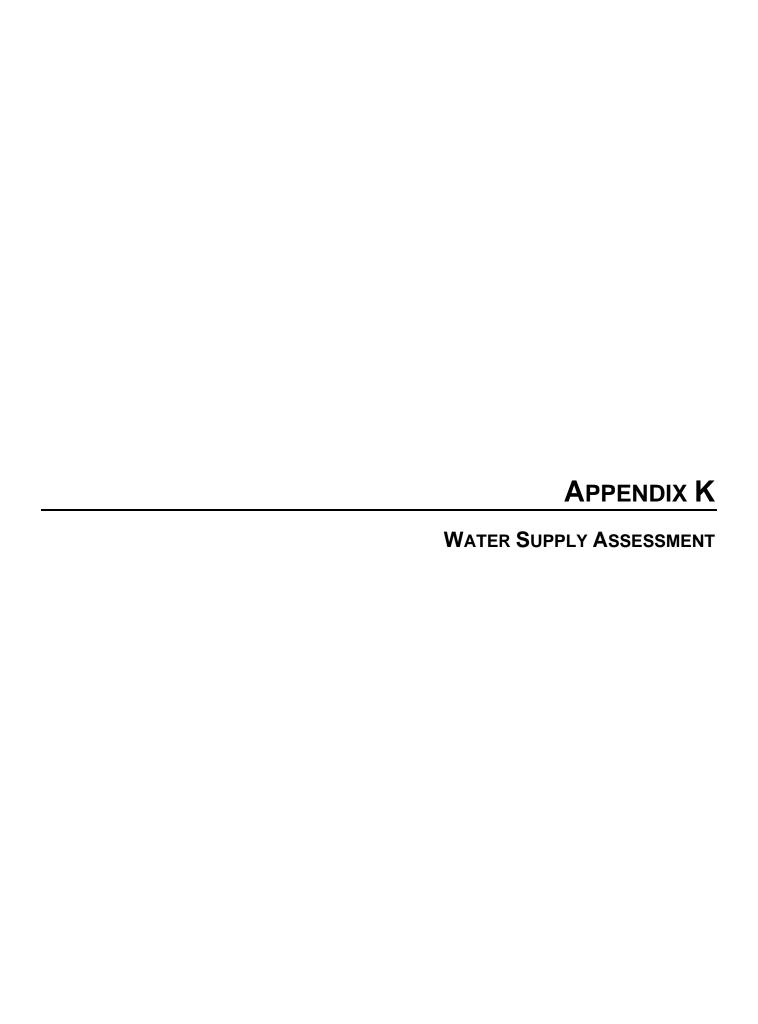
Onsite Drain Pipe Design

10-YEAR STORM EVENT ONSITE HYDRAULIC DESIGN SUMMARY

HGL CALCULATIONS - 10 YEAR

| Cover<br>(ft)   | 4ωων4 ω44νη 4ωω4υων4ων4ων4ωνανανανανανανα<br>Φωροφ4οναν τη 4 εθουνο 4ουν4ων 4 ωνανανανανανανανανανανανανανανανανανανα   |
|---|---|
| Submerg.  | 2.42<br>1.68<br>1.68<br>1.54<br>2.39<br>1.54<br>1.54<br>1.56<br>1.56<br>1.56<br>1.57<br>1.57<br>1.57<br>1.57<br>1.57<br>1.57<br>1.57<br>1.57  |
| Catc.<br>Cetta  | 1.67<br>0.96<br>0.96<br>0.96<br>0.74<br>1.47<br>1.06<br>1.06<br>1.06<br>1.16<br>0.23<br>2.08<br>2.18<br>2.18<br>2.18<br>2.18<br>2.18<br>2.18<br>2.18<br>2.1   |
| 0.5ff<br>Freeboard<br>ok?                                   | ***************   |
| Average 0.5ft Farget HGLIFreeboard Elev. ok? (ft)           | 18.0<br>15.0<br>15.0<br>15.0<br>15.0<br>15.0<br>16.0<br>16.0<br>16.0<br>16.0<br>16.0<br>16.0<br>16.0<br>16  |
| Average<br>Gutter<br>Elev.<br>(ft)                          | one that the second of the sec  |
| Average<br>Pad<br>Elev.<br>(ft)                             | gedran har en gran ger gran gran gran gran gran gran gran gra   |
| D/S<br>Crown<br>Elev.<br>(ft)                               | 13.48<br>13.08<br>13.08<br>13.00<br>12.55<br>13.56<br>12.56<br>12.56<br>12.56<br>12.56<br>12.56<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58<br>13.58 |
| D/S<br>HGL<br>(#)   | 15.10<br>15.82<br>15.82<br>15.82<br>14.85<br>14.15<br>14.15<br>14.15<br>14.15<br>14.15<br>14.15<br>14.15<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10<br>15.10 |
| Crown<br>Elev.  | 13.94<br>13.20<br>13.20<br>13.20<br>13.20<br>13.20<br>13.30<br>12.34<br>12.32<br>12.33<br>12.33<br>12.33<br>12.33<br>12.33<br>12.33<br>12.33<br>12.33<br>12.33<br>12.33<br>12.33<br>12.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33<br>13.33 |
| S Jo €  | 15.33<br>15.33<br>16.33<br>16.05<br>16.05<br>14.12<br>16.09<br>14.13<br>16.09<br>17.16<br>16.90<br>17.16<br>16.90<br>17.16<br>16.90<br>17.16<br>16.90<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16<br>17.16 |
| Pipe<br>Slope<br>(fVR)                                      | 0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.  |
| Head<br>Loss<br>(ff)  | 1,22<br>1,19<br>0,20<br>0,20<br>0,20<br>1,13<br>1,59<br>1,13<br>0,13<br>1,23<br>0,13<br>1,23<br>0,13<br>1,23<br>1,23<br>1,23<br>1,23<br>1,23<br>1,23<br>1,23<br>1   |
| HGL<br>Slope<br>(ft/ft)                                     | 0.0015<br>0.0015<br>0.0007<br>0.0007<br>0.0017<br>0.0017<br>0.0018<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019<br>0.0019  |
| Pipe-full<br>Flow<br>(cfs)                                  | 14.20<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28<br>25.28 |
| Pipe-full<br>Velocity<br>(fVs)                              | 202222222222222222222222222222222222222   |
| Design<br>Flow<br>(cfs)                                     |   |
| (u)   |   |
| Pipe<br>Area<br>(ft <sup>2</sup> )                          | 7.07<br>12.55<br>8.65<br>8.65<br>8.65<br>8.65<br>8.65<br>7.07<br>7.07<br>7.07<br>7.07<br>8.65<br>8.65<br>8.65<br>8.65<br>8.65<br>8.65<br>8.65<br>8.65   |
| Olameter<br>(in)  | en en en en en en en en en en en en en e  |
| Upstream Downstream (FROM) (TO) Flowline Flowline (fl) (fl) | 9.06<br>9.06<br>9.06<br>9.06<br>9.00<br>11.04<br>9.00<br>11.04<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>11.02<br>9.00<br>9.00<br>9.00<br>9.00<br>9.00<br>9.00<br>9.00<br>9   |
| Upstream (<br>(FROM)<br>Flowline<br>(fl)                    | 10.91<br>9.43<br>9.70<br>9.72<br>9.72<br>9.72<br>10.73<br>10.04<br>11.14<br>9.44<br>10.05<br>9.18<br>11.10<br>10.03<br>9.18<br>11.10<br>10.03<br>9.18<br>11.10<br>10.03<br>9.18<br>11.10<br>10.03<br>9.18<br>11.10<br>9.10<br>9.10<br>9.10<br>9.10<br>9.10<br>9.10<br>9.1   |
| NODE  | AND SERVICE TO SERVICE TO A SER  |
| FROM  | 200 3051 0355 0565  |
|   |   |

Ext. Pipe P01 Design Flow=Prorated flow from SacCalc peak flow



## Greenbriar Development Project Sacramento, California

# SB 610 Water Supply Assessment



Prepared for: City of Sacramento Environmental Planning Services



July 2006



## SB 610 Water Supply Assessment



### Prepared for:

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i

## 1 EXECUTIVE SUMMARY

A water supply assessment (WSA) was prepared pursuant to Senate Bill 610 (SB 610 Water Code, Section 10910 et. seq., Chapter 643, statutes of 2001) for the proposed Greenbriar development project in Sacramento County. The Greenbriar site is located adjacent to and west of the City of Sacramento (City) City limits and outside of the City's Sphere of Influence (SOI); as such the project applicant is seeking to annex the project site to the City. The Greenbriar project is a proposed residential development centered on a common water feature including a total of 3,473 housing units and approximately 28 acres of retail and commercial space.

The water supply for Greenbriar would come from the City's water rights and a 1957 settlement contract with the United States Bureau of Reclamation (USBR). Under the contract, the City is entitled to divert up to 326,800 acre-feet per year (AFY) in 2030. As a signatory of the Water Forum Agreement (WFA), the City has agreed to limitations on diversions from the American River during certain specified conditions. During the conference year scenario, analogous to extremely dry years, the WFA limits annual withdrawal from the American River to 50,000 AFY. However, the WFA does not limit withdrawal from the Sacramento River; therefore, entitled American River water may be diverted further downstream at the Sacramento River Water Treatment Plant (WTP) below the confluence of the American and Sacramento Rivers. The resulting annual limitation is a function of the annual treatment plant capacity at the Sacramento River WTP, resulting in a total supply of 230,000 AFY, a maximum daily supply of 260 mgd. The total supply during the conference year scenario can meet the anticipated annual water demand through buildout of the City's SOI (2030).

During conference years when low flow conditions occur, the WFA limits the diversion rate from the American River to 155 cubic feet per second (cfs) during June through August when the peak demand occurs. Assuming treatment at the reduced diversion rate from the American River and maximum treatment at the Sacramento River WTP, the total surface water supply available to the City of Sacramento is 260 mgd. The projected maximum day demand within the City of Sacramento would exceed 260 mgd in 2015 by 4.6 mgd. However, groundwater sources supply 30 mgd in addition to available surface water supplies and would ensure maximum day demand in dry years is met through 2030. The additional demand from the proposed project would not significantly alter this timeline. The City is already undertaking studies to evaluate an additional Sacramento River diversion and treatment facility. While the City has sufficient water supplies through 2030, continued efforts to secure additional treatment capacity on the Sacramento River would ensure that the City has sufficient time to provide reliable delivery of water for the proposed project and future demand past 2030.

### This WSA finds:

- ► The City has sufficient water to serve the proposed project and projected future demands over the next twenty years.
- ▶ Under normal water years, the City has sufficient capacity within its WTPs to serve the proposed project and projected future demands over the next twenty years.
- ▶ During conference years the City has sufficient supply to serve the average daily demands of the proposed project and projected future demands if the WTPs operate at maximum production capacity.
- ▶ During conference years, under a peak demand scenario, the City's peak demands would exceed available capacity of the WTPs by the year 2015 due to limitations in the summer months of the production capacity of the City's WTPs,
- ► Available groundwater supply (30 mgd) would provide additional supply to meet peak demands during conference years.

## 2 INTRODUCTION

This report presents the WSA prepared pursuant to Senate Bill 610 (SB 610 Water Code, Section 10910 et. seq., Chapter 643, statutes of 2001) for the proposed Greenbriar development project in Sacramento County. The Greenbriar site is located adjacent and west of the City of Sacramento (City) limits and outside of the City's Sphere of Influence (SOI); as such the project applicant is seeking to annex the project site to the City. Annexation will require approval of pre-zoning entitlements from the City, approval of an amendment to the City's SOI and annexation approval from the Sacramento County Local Formation Commission (LAFCo). The Greenbriar development is a residential development centered on a common water feature with a total of 3,473 housing units and approximately 28 acres of retail and commercial space.

The City is proceeding with environmental review of the project in conformance with the requirements of the California Environmental Quality Act (CEQA). The environmental review for the proposed project includes an assessment of the available water supply to serve the project, and a WSA is required under SB 610. Greenbriar would be annexed to the City and would be the water supplier. The City, as the water supplier is required to make a determination through the WSA whether sufficient water supplies are available to meet project demands under normal, single-dry, and multiple-dry water years over a 20-year planning horizon. Assuming that the WSA makes this determination, the City would adopt the WSA as part of the CEQA documentation prepared for the project.

### **2.1 SENATE BILL 610**

SB 610 became effective January 1, 2002. The purpose of SB 610 is to strengthen the process by which local agencies determine the adequacy and sufficiency of current and future water supplies to meet current and future demands. SB 610 amended the California Public Resources Code to incorporate Water Code requirements within the CEQA process for certain types of projects. SB 610 also amended the Water Code to broaden the types of information included in Urban Water Management Plans (UWMP) (Water Code Section 10620 et. seq.).

### **2.1.1 WATER CODE PART 2.10**

Water Code Part 2.10 clarifies the roles and responsibilities of the Lead Agency under CEQA and the water supplier (i.e., public water system) with respect to describing current and future supplies compared to current and future demands, it defines the projects that are required to prepare a WSA, and the Lead Agency's responsibilities related to the WSA. A WSA is required for:

- 1. A proposed residential development of more than 500 dwelling units;
- 2. A proposed shopping center or business establishment employing more than 1,000 persons or having more than 500,000 square feet of floor space;
- 3. A proposed commercial office building employing more than 1,000 persons or having more than 250,000 square feet of floor space;
- 4. A proposed hotel or motel, or both, having more than 500 rooms;
- 5. A proposed industrial, manufacturing, or processing plant, or industrial park planned to house more than 1,000 persons, occupying more than 40 acres of land, or having more than 650,000 square feet of floor area;
- 6. A mixed-use development that includes one or more of the uses described above;
- 7. A development that would demand an amount of water equivalent to or greater than the amount of water required by a 500-dwelling-unit project; and

8. For Lead Agencies with fewer than 5,000 water service connections, any new development that will increase the number of water service connections in the service area by 10% or more.

Under Part 2.10, the Lead Agency must identify the affected water supplier and ask the water supplier whether the new demands associated with the project are included in the suppliers' UWMP. If the UWMP includes the demands it may be incorporated by reference in the WSA (Water Code Section 10910[C][2]). If there is no public water system to serve the project, the Lead Agency must prepare the WSA itself. (Water Code Section 10910[b]).

### 2.2 THE URBAN WATER MANAGEMENT PLANNING ACT

The Urban Water Management Planning Act requires a water supplier to document water supplies available during normal, single dry, and multiple dry water years during a 20-year projection and the existing and projected future water demand during a 20-year projection. The act requires that the projected supplies and demands be presented in 5-year increments for the 20-year projection (Water Code Section 10631).

### 3 GREENBRIAR DEVELOPMENT PROJECT

#### 3.1 PROJECT LOCATION

The Greenbriar project site encompasses 577 acres located at the northwest intersection of State Route 99 (SR 99) and Interstate 5 (I-5) in Sacramento County. The project site is located in the unincorporated portion of Sacramento County, adjacent to and west of the City of Sacramento (City). The project site is located outside the current SOI for the City of Sacramento (Exhibit 1).

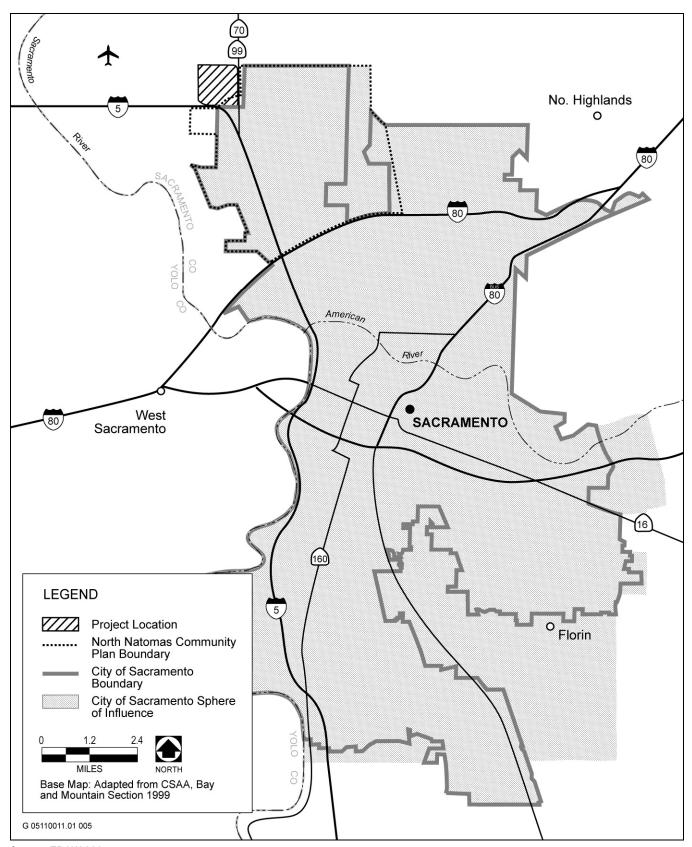
The project site is bordered by agricultural and rural residential land uses to the west and north, I-5 and agricultural lands to the south, and SR 99 and a new residential community currently under development within North Natomas to the east. The recently approved Metro Airpark development area is located adjacent to the western boundary of the project site, within Sacramento County and adjacent to the eastern boundary of the Sacramento International Airport. The Metro Airpark development area includes existing and proposed commercial, hotel, and recreational (i.e., golf course) land uses. The City's North Natomas Community Plan area is located adjacent to the eastern boundary of the project site and across SR 99.

#### 3.2 EXISTING LAND USE

The project site is currently undeveloped, fallow, and active farmlands. All farmlands on the property are irrigated with local groundwater wells. Existing water demands are limited to the water demands necessary for cross cultivating the property. Historic groundwater pumping volumes from the site are not available. There is currently no infrastructure on the property to deliver water to the property via the City's public water system.

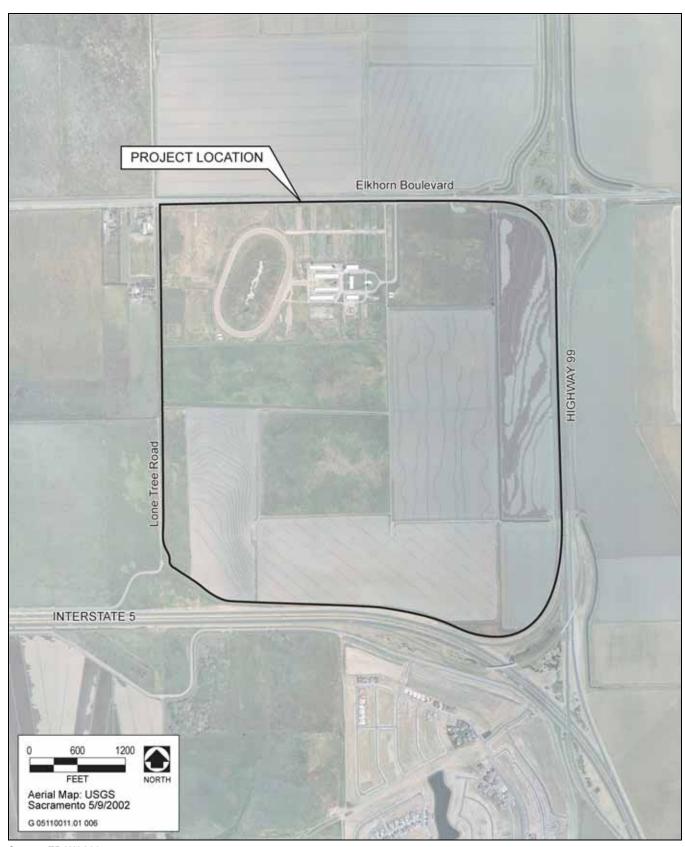
#### 3.3 PROPOSED DEVELOPMENT

The City is considering approval of a residential mixed-use development at the project site. The project includes the construction of a range of housing types (e.g., high, medium, low density) that would be located within close proximity to public transportation systems. The proposed land use plan is predominantly a residential development centered on a common water feature (approximately 39 acres) (Exhibit 2). A total of 3,473 housing units and approximately 28 acres of retail and commercial space would be provided on site. A 10-acre (net) elementary school would be provided in the southeastern portion of the project site and would serve the school demands of the project site. A total of 8 neighborhood parks (approximately 49 acres) would be provided throughout the community and would be connected by the central lake/detention basin and pedestrian paths and trails.



Source: EDAW 2005

Project Location Map Exhibit 1



Source: EDAW 2005

### **Aerial Map of the Project**

#### 3.4 WATER SUPPLY PLANNING FOR THE GREENBRIAR **DEVELOPMENT PROJECT**

The City's 2000 UWMP does not incorporate water demands for Greenbriar because Greenbriar is not currently located within the City's SOI. The City is currently in the process of preparing its 2005 UWMP, which would include demands associated with the Greenbriar project. Because the 2005 UWMP is not complete, this WSA uses the information provided in the 2000 UWMP as well as information provided by the City. Because the City's service area and water demands have grown since the 2000 UWMP was prepared and adopted, the City provided additional information related to this growth including updated water demand data. The 2000 UWMP and updated information provided by the City are the most recent and best information available addressing existing and future water demands, supplies, and facilities within the City of Sacramento.

The City is a signatory to the Water Forum Agreement (WFA). The WFA is a plan that provides for the effective longterm management of the Sacramento region's water resources. The WFA was developed by a diverse group of stakeholders known as the Water Forum, which consisted of water agencies, business groups, agricultural interests, environmentalists, citizen groups, and local governments and was formulated based on the two coequal objectives: 1) provide a reliable and safe water supply for the region's economic health and planned development through the year 2030; and 2) preserve the fishery, wildlife, recreational, and aesthetic values of the Lower American River.

As a signatory party to the WFA, the City has agreed to withdrawal limitations from the American River. These limitations have been and will continue to be incorporated into water supply planning for future development in the City limits, including the Greenbriar development and are described in greater detail in Section 4.4, "Supply Reliability Analysis."

#### 3.5 EXISTING AND PROJECTED GREENBRIAR PROJECT WATER **DEMANDS**

Average daily water demand for the proposed Greenbriar development was calculated to be approximately 2.39 million gallons per day (mgd), or 2,680 acre-feet (AF) per year at full project build out (Table 1) (Wood Rodgers 2005). Maximum daily demand (MDD) is estimated to be 4.3 mgd. The MDD was determined by applying a factor of 1.8 to the Average Daily Demand (ADD) estimates. Buildout of the project is expected to be complete approximately 5–10 years after construction begins.

| Wate         | r Demand                          | Table 1 Projections  | for Greenbr  | iar  |  |   |
|--------------|-----------------------------------|--|--|--|--|---|
| Tot          | al                                | ADD Unit Water Demand  |  |  | Demand   |   |
| Acrost (not) | Dwelling                          | anmlac   | apm/du   | Averaç   | ge Daily   | Average   |
| Acres (net)  | Units                             | уршас  | gpii/du —  | gpm  | mgd  | Annual (AF)   |
| 81           | 671                               | _  | 0.44   | 295  | 0.42   | 476   |
| 145          | 2,215                             | _  | 0.44   | 975  | 1.40   | 1,573   |
| 30           | 587                               | 2.48   | _  | 74   | 0.11   | 119   |
| 28           | _                                 | 1.86   | _  | 52   | 0.07   | 84  |
| 51           | _                                 | 2.6  |  | 133  | 0.19   | 215   |
| 10           | _                                 | 1.55   | _  | 16   | 0.02   | 26  |
| 345          | 3,473                             | _  | _  | 1,545  | 2.22   | 2,493   |
| _            | _                                 | _  | _  | 116  | 0.17   | 187   |
| _            |                                   | _  |  | 1,661  | 2.39   | 2,680   |
|              | Tot Acres¹ (net)  81 145 30 28 51 | Total       Acres¹ (net)     Dwelling Units       81     671       145     2,215       30     587       28     —       51     —       10     — | Water Demand Projections           Total         ADD Unit Water           Acres¹ (net)         Dwelling Units         gpm/ac           81         671         —           145         2,215         —           30         587         2.48           28         —         1.86           51         —         2.6           10         —         1.55 | Water Demand Projections for Greenbr           Total         ADD Unit Water Demand           Acres¹ (net)         Dwelling Units         gpm/ac         gpm/du         —           81         671         —         0.44           145         2,215         —         0.44           30         587         2.48         —           28         —         1.86         —           51         —         2.6         —           10         —         1.55         — | Water Demand Projections for Greenbriar           Total         ADD Unit Water Demand           Acres¹ (net)         Dwelling Units         gpm/ac         gpm/du         Average gpm           81         671         —         0.44         295           145         2,215         —         0.44         975           30         587         2.48         —         74           28         —         1.86         —         52           51         —         2.6         —         133           10         —         1.55         —         16           345         3,473         —         —         1,545           —         —         —         116 | Water Demand Projections for Greenbriar           Total         ADD Unit Water Demand         Demand           Acres¹ (net)         Dwelling Units         gpm/ac         gpm/du         Average Daily gpm         mgd           81         671         —         0.44         295         0.42           145         2,215         —         0.44         975         1.40           30         587         2.48         —         74         0.11           28         —         1.86         —         52         0.07           51         —         2.6         —         133         0.19           10         —         1.55         —         16         0.02           345         3,473         —         —         1,545         2.22           —         —         —         116         0.17 |

Notes: gpm = gallons per minute, mgd = million gallons per day Net acreage does not include street right of way.

Source: Wood Rodgers 2005

# 3.6 EXISTING AND PROJECT WATER DEMANDS FOR THE CITY OF SACRAMENTO

The City's historical surface and groundwater deliveries for the last five years are shown in Table 2. The total water supplied by the City from June 2003 to July 2004 was 143,784 AF. Over the past seven years, 17% of the delivered water has been supplied from groundwater (i.e., average of 20,454 AFY).

|                 | City                                       | of Sacramento                           | Table 2<br>Historical Wate             |  | leet Demand                              |                  |                     |
|-----------------|--|---|--|--|--|------------------|---------------------|
|                 | Surface Water                              |   |  | Groundwater                              | Total Water Delivered                    |                  |                     |
| Year            | Annual Surface<br>Water Delivered<br>(AFY) | Maximum Day<br>Water Delivered<br>(mgd) | Maximum Day to<br>Average Day<br>Ratio | Annual<br>Groundwater<br>Delivered (AFY) | Total Annual<br>Water Delivered<br>(AFY) | Average<br>(mgd) | Percent<br>Increase |
| 1997–98         | 92,031                                     | 191                                     | 1.71                                   | 22,053                                   | 114,034                                  | 99.9             | _                   |
| 1998–99         | 102,180                                    | 213                                     | 1.58                                   | 24,630                                   | 126,810                                  | 111.1            | 11.15               |
| 1999-00         | 112,547                                    | 220                                     | 1.61                                   | 24,149                                   | 136,696                                  | 119.8            | 7.8                 |
| 2000-01         | 114,172                                    | 213                                     | 2.10                                   | 23,578                                   | 137,750                                  | 122.7            | 0.77                |
| 2001-02         | 113,979                                    | 215                                     | 1.57                                   | 24,271                                   | 138,250                                  | 123.41           | 0.36                |
| 2002-03         | 111,539                                    | 227                                     | 2.35                                   | 23,997                                   | 135,536                                  | 120.7            | -1.96               |
| 2003-04         | 128,412                                    | 223                                     | 2.33                                   | 15,372                                   | 143,784                                  | 128.31           | 6.09                |
| 2004-05         | 116,305                                    | _                                       | _                                      | 19,271                                   | 135,576                                  | 120.7            | -5.71               |
| Average         | 111,396                                    | 214.57                                  | 1.89                                   | 22,165                                   | 133,561                                  | 117.09           | 2.64                |
| Source: City of | of Sacramento 1998,                        | 1999, 2000, 2001, 2                     | 2002, 2003, 2004, 200                  | )5                                       |  |                  |                     |

The City has identified current and future water demands through buildout of their service area. The demand analysis includes projects that have been recently approved but not fully constructed as well as projects that have pending development applications with the City and are within the City's SOI. Table 3 presents the City's projected demands through build out (2030). Average annual demands are presented to determine whether or not the City has adequate water supply to meet its demands. Peak or maximum day demand estimates are presented to determine if the WTPs have adequate capacity to handle peak day demands.

| Table 3 Projected 2030 Annual and Maximum Day Demand for the City of Sacramento |                        |                     |                             |  |  |
|---|------------------------|---------------------|-----------------------------|--|--|
| Area  | Annual Demand<br>(AFY) | Annual Demand (mgd) | Maximum Day<br>Demand (mgd) |  |  |
| Development within Existing City Limits   | 193,497                | 139                 | 250.2                       |  |  |
| SMUD Cogeneration Facility  | 622                    | 0.56                | 1.0                         |  |  |
| Panhandle Annexation <sup>a</sup>   | 4,199 <sup>d</sup>     | 3.00                | 5.4                         |  |  |
| Airport/Metro Air Park Wholesale Wheeling Assessment                            | 6,538                  | 6.50                | 11.7                        |  |  |
| SSWD Wholesale b,c  | 26,064                 | 16.67               | 30.0                        |  |  |
| Cal Am Parkway Wholesale Agreement  | 2,580                  | 0.61                | 1.1                         |  |  |
| Zone 40 Wheeling Service  | 10,000                 | 6.11                | 11.0                        |  |  |
| Total   | 243,500                | 172                 | 310                         |  |  |

Notes: <sup>a</sup> This includes the demands within the County's Northgate system and the proposed Panhandle development. <sup>b</sup> SSWD does not take City wholesale water during times of Hodge restrictions. <sup>c</sup> SSWD has the option to contract for up to 10 mgd of additional firm or non-firm capacity in addition to the 20 mgd of firm capacity under the Wholesale Agreement. <sup>d</sup> Assumes a conservation rate of 7.5%. Source: Peifer, pers. comm., 2005

The City's projected water demands in 2030 were estimated to be 243,500 AFY with a average daily demand of 172 mgd and a maximum day demand of 310 mgd.

The 2030 projected water demands do not include the increased demand associated with the Greenbriar project. Therefore, the project would increase the City's 2030 water demands by 2,680 AFY, or approximately 1.4 % of the projected 2030 demand. The City's total 2030 water demands with the project would be 195,818 AFY with a projected average daily demand of 174.8 and a maximum day demand of 314.7 mgd.

# 4 WATER SUPPLY ASSESSMENT FOR THE GREENBRIAR PROJECT

#### 4.1 INTRODUCTION

#### 4.1.1 RESPONSIBILITIES OF THE LEAD AGENCY

The City of Sacramento is the CEQA Lead Agency responsible for evaluating the environmental impacts of the project in compliance with CEQA, certifying the EIR, and issuing the associated entitlements.

The City would be the retail water provider for the project and would be the agency responsible for preparation and approval of the WSA. In preparing the WSA, The City must do the following:

- ▶ Determine the sufficiency of the supply to meet the project demands under normal, single dry and multiple dry years over a 20-year projection.
- ▶ Identify existing water supply entitlements and water rights for the proposed project and quantify water received in prior years pursuant to these existing entitlements and rights.
- ▶ Describe the groundwater basin from which the proposed project will be supplied, if applicable. The description must include information regarding overdraft in the basin. The amount and location of groundwater pumped by the City must be quantified, based on reasonably available information.
- ▶ Describe and analyze the amount and location of groundwater projected to be pumped by the City from the basin from which the project will be supplied. The assessment must include an analysis of the sufficiency of groundwater from the basin to meet the projected water demand associated with the proposed project.
- ▶ Provide information related to capital outlay programs for financing delivery of water supply.
- ► Provide information on federal, state, and local permits for construction of necessary infrastructure and regulatory requirements associated with delivery of the water supply.

### 4.2 REQUIREMENTS OF THE WSA

SB 610, as described in California Water Code Sections 10910–10915 requires that a WSA for a project include the following information:

- ► A description and quantification of the existing and planned water sources.
- A description of the reliability and vulnerability of the water supply to seasonal or climatic shortages in the average water year, single dry water year, and multiple dry water year during a 20-year projection.
- ► Contingency plans including demand management and conjunctive use potential.

- ► A description of current and projected water demands.
- A description of all water supply projects and water supply programs that may be undertaken by the City to meet the total projected water use.

In addition, because the City uses groundwater as one of its supply sources, the WSA should include:

- A description of any groundwater basin (or basins) from which the City pumps groundwater.
- ▶ Information that characterizes the condition of the groundwater basin and a description of the measures currently being taken by the City to minimize any potential for overdraft conditions to occur.
- A detailed description and analysis of the amount and location of groundwater pumped by the City for the past five years from any groundwater basin from which the proposed project will be supplied.
- ► An analysis of the location, amount, and sufficiency of the groundwater from the basin or basins from which the proposed project will be supplied to meet the projected water demand associated with the proposed project.

The following analysis presents the WSA for the Greenbriar project in compliance with the requirements of SB 610.

#### 4.3 COMPLIANCE WITH PROVISIONS OF THE WATER CODE

# 4.3.1 DETERMINE WHETHER PROJECT IS SUBJECT TO THE CALIFORNIA ENVIRONMENTAL QUALITY ACT (CEQA) [WATER CODE SECTION 10910(A)]

The City has made the determination that the Greenbriar project is subject to CEQA and is a "project" as defined by Water Code Section 10912(a) because it would result in the construction of greater than 500 dwelling units, as well as commercial and retail office space. All criteria for projects requiring a WSA apply to the project.

# 4.3.2 IDENTIFY THE PUBLIC WATER SYSTEM THAT WILL SUPPLY WATER FOR THE PROJECT [WATER CODE SECTION 10910(B)]

The property where the proposed Greenbriar project would be located would be annexed to the City and served by the City's Utilities Department. The Utilities Department is a public water agency that served 131,745 connections as of June 2004. The City operates two water treatment plants (WTP). The Sacramento River WTP is located on the east bank of the Sacramento River, about one half mile downstream of the confluence of the American and Sacramento Rivers and the E.A. Fairbairn WTP (formally American River WTP) is located adjacent to the American River between the H Street and Howe Avenue bridges, approximately seven miles upstream of the confluence of the American and Sacramento Rivers. The city has 34 municipal drinking water wells; of these 23 are active and nine are on standby (Sherry, pers. comm., 2005).

# 4.3.3 IS THERE AN ADOPTED URBAN WATER MANAGEMENT PLAN (UWMP) [WATER CODE SECTION 10910(C)]

As described above, the City completed and adopted its 2000 UWMP (City of Sacramento 2001). Because the Greenbriar development is not currently within the City limits, the plan does not incorporate demands associated with the Greenbriar project. The City is currently preparing its 2005 UWMP, which would address water demands associated with Greenbriar. This document is anticipated to be adopted in early 2006. Because the 2005 UWMP is

not complete, this WSA relies on the information provided in the 2000 UWMP and other relevant water supply information provided by the City including, water demand data, and existing operational constraints.

# 4.3.4 ARE THE PROJECTED WATER DEMANDS ASSOCIATED WITH THE PROPOSED PROJECT ACCOUNTED FOR IN THE MOST RECENTLY ADOPTED URBAN WATER MANAGEMENT PLAN [WATER CODE SECTION 10910(c)]

The most recently adopted UWMP (City of Sacramento 2001) does not account for projected water demands associated with the proposed Greenbriar project because the Greenbriar property was not within the City of Sacramento's sphere of influence (SOI) or under their planning jurisdiction at the time of preparation.

# 4.3.5 IDENTIFY EXISTING WATER SUPPLIES FOR THE PROJECT [WATER CODE SECTION 10910(D)]

Water Code Section 10910(d)(1) requires identification of existing water supply entitlements, water rights, or water service contracts relevant to the Greenbriar project and a description of the quantities of water obtained by the City pursuant to these water supply entitlements, water rights, or water service contracts in previous years.

The City would be the retail water purveyor for the project. The water supplies for the project have been addressed in existing City water supply plans and agreements including:

- ► Water Forum Agreement (City-County Office of Metropolitan Water Supply Planning)
- ▶ 2000 Urban Water Management Plan (City of Sacramento 2001)

#### CITY OF SACRAMENTO SURFACE WATER SUPPLIES

The City has a permanent water right settlement contract with the USBR that limits the City's annual surface water diversion to 81,800 AF from the Sacramento River, and 245,000 AF from the American River. The maximum total combined water supply from both the Sacramento and American River by the year 2030 is 326,800 AF (Table 4). The projected incremental increases are shown in Table 4.

| Table 4 City of Sacramento USBR Contracted Annual Surface Water Entitlements (AFY) |         |         |         |         |         |         |
|--|---------|---------|---------|---------|---------|---------|
| Source   | 2005    | 2010    | 2015    | 2020    | 2025    | 2030    |
| American River   | 123,200 | 145,700 | 170,200 | 196,200 | 222,200 | 245,000 |
| Sacramento River   | 81,800  | 81,800  | 81,800  | 81,800  | 81,800  | 81,800  |
| Total  | 205,000 | 227,500 | 252,000 | 278,000 | 304,000 | 326,800 |

### **Sacramento and American River Diversion Rights**

The City has used surface water since 1854 and claims pre-1914 rights to divert 75 cubic feet per second (cfs) from the Sacramento River. Currently, the City holds five water right permits: one for diversion of Sacramento River water and four for diversion of American River water. The Sacramento River permit, Permit 992, has a priority date of March 20, 1920. Permits 11358 through 11361, on the American River, have priorities ranging from October 1947 to September 1954. The water right permits are on file with the City of Sacramento Utilities Engineering Department.

The Sacramento River permit and two of the American River permits (11358 and 11361) authorize direct diversion. The other two permits (11359 and 11360) authorize rediversion and consumptive uses of American River tributary water stored and released at SMUD's Upper American River Project power development reservoirs. The reservoirs (Union Valley, Ice House, Rubicon, Rockbound, Loon Lake and Gerle) are located in the Crystal Basin area of the Sierra Nevada Mountains east of Sacramento and north of U.S. Highway 50.

In 1957, USBR and the City entered into a permanent water rights settlement contract which provides, among other things, that:

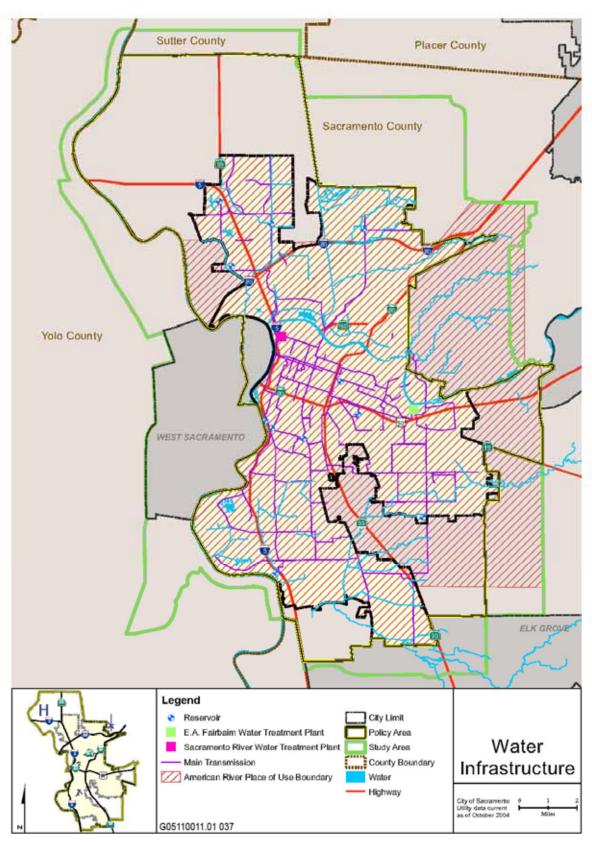
- ▶ USBR agreed to regulate flows at Folsom Reservoir to ensure the City's ability to divert up to 245,000 AFY under the City's American River water rights and to operate CVP reservoirs so that they do not interfere with the City's exercise of its Sacramento River water rights.
- The City agreed to:
  - 1. Limit its total diversion rates to 225 cfs of Sacramento River water and 675 cfs of American River water; and
  - 2. Limit its total diversion of Sacramento and American River water to 326,800 AFY (81,800 AF of Sacramento River water and 245,000 AF of American River water per year).
- The City is not required to take pro-rata reductions in dry years.

The City's water right permits allow authorized water diversions to be used within specified areas described as authorized places of use (POU). Permit 992 designates lands within the City of Sacramento as the authorized place of use. Permits 11358 and 11361 designate a 79,500 acre area within and adjacent to the City as the authorized POU. Permits 11359 and 11360 designate a 96,000-acre area within and adjacent to the City as the POU. Exhibit 3 illustrates the City's Water Service Area, showing the 96,000-acre authorized POU and current City limits. The Greenbriar project is adjacent to the City's POU, but will become part of the POU under Permit 992 if the area is annexed to the City.

As a signatory of the 2000 WFA, the City has agreed to reduce its diversions from the American River when flows are below Hodge flow criteria. Hodge flow criteria were defined as a result of *Environmental Defense Fund et al. v. East Bay Municipal Utility District (EBMUD)* which addressed the ability of EBMUD to divert water from the lower American River at the Folsom South Canal. Hodge flows are named after the judge presiding over the case and are minimum flow values in the Lower American River which must be met as a condition of EBMUD's diversion of contracted water. These flows are set at 2,000 cfs October 15–February; 3,000 cfs March–June; and 1,750 cfs July–October 14. The City agreed in the WFA to reduce its diversion from the American River during conference years and when flows bypassing the City's diversion are below the Hodge flow criteria. The City's authorized diversions with and without the WFA diversion restrictions are listed in Table 5. As shown in the table, under dry year conditions the City would not be subject to reductions in entitlement volumes only diversion rates.

# Water Code Section 10910(d)(2)(A) requires information related to written contracts or other proof of entitlements to the water supplies identified to serve the project.

As described above, the City has existing surface water entitlements and maintains active groundwater wells which would supply the proposed project. At build-out in 2030, the USBR contract provides the City with a maximum annual diversion of 326,800 AFY. Copies of the City's permits and the USBR Contract are available for review at the City of Sacramento, Utilities Department.



Source: City of Sacramento 2005

Water Infrastructure Exhibit 3

| Table 5 City of Sacramento Surface Water Entitlements with Water Forum Agreement |                                 |              |                  |  |  |
|--|---------------------------------|--------------|------------------|--|--|
| Permit   | Authorized Diversion            | Maximum Perm | itted Diversion  |  |  |
| i cinit  | Authorized Diversion            | AFY          | cfs              |  |  |
|  | American River                  | 245,000      | 675              |  |  |
| 1957 USBR 2030 Contractual Maximum <sup>a</sup>                                  | Sacramento River                | 81,800       | 225              |  |  |
|  | <b>Total Combined Diversion</b> | 326,800      | 900              |  |  |
|  | American River                  | 245,000      | 310 <sup>b</sup> |  |  |
| 2000 WFA Maximum   | Sacramento River                | 81,800       | 290°             |  |  |
|  | <b>Total Combined Diversion</b> | 326,800      | 900              |  |  |

#### Notes:

- <sup>a</sup> Based on permits 00922, 011358, 011359, 011360, and 011361.
- <sup>b</sup> 310 cfs is a maximum withdrawal rate, additional restrictions apply.
- There is no maximum withdrawal rate from the Sacramento River in the WFA. However, the total maximum withdrawal rate from the American and Sacramento rivers can not exceed 900 cfs. The Sacramento WTP is below the confluence the American and Sacramento Rivers.

Sources: City of Sacramento and Sacramento City-County Office of Metropolitan Water Planning

# Water Code Section 10910(d)(2)(B) requires information related to copies of the capital outlay program for financing the delivery of the identified water supply.

The infrastructure necessary to deliver water to the project site would be funded from the 2005–2010 Capital Improvement Program (CIP). A copy of the CIP is available for viewing at City of Sacramento Utilities Department. In summary, the 2005-2010 CIP totals \$366.8 million from all funding sources. The General Fund portion of the five-year program is \$12.4 million or 3% of the total. The first year of the CIP, the FY2005/06 CIP Budget totals \$105.4 million. These appropriations will add to currently active project appropriations of approximately \$1 billion. Expenditures are planned in the following major program areas: General Government; Public Safety; Convention, Culture and Leisure; Parks and Recreation; Transportation and Utilities. The bulk of the project budgets are for Utilities and Transportation projects supported by the Water, Sewer, Drainage, Measure A Sales Tax, Gas Tax, and Major Street Construction Funds.

The project would connect into the City's existing water distribution network. No new water treatment or diversion structures would be required to serve the project. The project includes the preparation of the Greenbriar Finance Plan. A summary of the Greenbriar Finance Plan is provided in Appendix C of the Greenbriar EIR. This plan would ensure the project applicants pay their fair share portion of necessary infrastructure costs (e.g., water supply infrastructure) necessary for delivering water to the project.

# Water Code Section 10910(d)(2)(C) requires information related to federal, state, and local permits for construction of infrastructure necessary for delivering the water supply.

As described above the City has sufficient water rights and entitlements to meet existing and future water demands within City over a 20-year period. All water supply infrastructure necessary to meet existing demands is constructed and all necessary approvals for the delivery and use of this water within City have been secured.

The City is pursuing construction of a new water treatment plant along the Sacramento River near Elverta Road (northeast of the project site). This treatment plant would provide additional treatment capacity to ensure the

provision of water to City customers beyond 2025. Permits and authorizations that may be required for construction of the new water treatment plant are listed below in Table 6.

| Table 6 Possible Required Permits and Authorizations for Water Supply Infrastructure |  |  |  |  |  |
|--|--|--|--|--|--|
| Federal  | State  | Local  |  |  |  |
| U.S. Army Corps of Engineers – Section 404 Permit                                    | California Department of Fish and Game (DFG) -<br>Streambed Alteration Agreement   | Department of Health<br>Services review and approval |  |  |  |
| U.S. Fish and Wildlife Service  – Endangered Species Act  Consultation               | Regional Water Quality Control Board - Section 401<br>Water Quality Certification, National Pollutant Discharge<br>Elimination System Construction Stormwater Permit |  |  |  |  |
| U.S. Bureau of Reclamation – Review and approval                                     | Sacramento Metropolitan Air Quality Management<br>District – Authority to Construct  |  |  |  |  |

The project would not require any additional water supply infrastructure above and beyond what is currently available or planned for by the City. The project would be required to extend water conveyance infrastructure to the site, which is being evaluated as part of the EIR. No additional permits are needed.

# Water Code Section 10910(d)(2)(D) requires information related to any regulatory approvals required for delivery of the water supply.

No regulatory approvals would be required to deliver water to the Greenbriar project site. The City has secured all water supply entitlements and regulatory approvals necessary to distribute groundwater and surface water within its service area.

# 4.3.6 IDENTIFY PARTIES DEPENDENT ON PROPOSED SUPPLY. [WATER CODE SECTION 10910(E)]

The intent of this section is to identify any potential conflicts that may arise from the exercise of water supply entitlements, water rights, or water service contracts to serve a proposed project if such water supply entitlements, water rights, or water service contracts have not been previously exercised.

The proposed project would be served by the City through its existing water supply entitlements and groundwater supplies. The City's surface water entitlements and contracts have all historically been exercised, and groundwater has been historically pumped. There are no unexercised water service contracts that will be used to serve the proposed project and therefore no potential conflicts would arise from supplying water to the proposed project.

# 4.3.7 DOES THE SUPPLY INCLUDE GROUNDWATER AS A SOURCE? [WATER CODE SECTION 10910(F)]

A portion of the water demand from the proposed project would be met with groundwater. Consequently, Section 10910(f) requires the following additional information.

## Water Code Section 10910(f)(1) requires a review of groundwater data contained in the UWMP.

The City maintains 34 wells for potable and non-potable use. Of these wells, 32 potable wells are north of the American River, and two are south of the American River (Peifer, pers. comm.., 2005). The current groundwater

system can supply 30 mgd and produce approximately 33,600 AFY. Historical average annual groundwater use for the period 1997-98 through 2003-04 was 20,454 AFY (Table 2).

# Water Code Section 10910(f)(2) requires a description of the groundwater basin and the efforts being taken to prevent long-term overdraft.

The City is located in the 548-square mile North American Groundwater Subbasin (Department of Water Resources 2003). The Subbasin's boundaries are the Feather and Sacramento Rivers on the west, the Bear River to the north, the American River on the south, and the Sierra Nevada on the east. The underlying geology of the basin consists of a variety of geologic formations that make up the water bearing units. There are two aquifer systems: an upper unconfined system consisting of the Victor, Fair Oaks, and Laguna Formations, and a lower, semi-confined system in the Mehrten Formation. These geologic formations are composed of lenses and layers of inter-bedded sand, silt, and clay with coarsegrained stream channel deposits. The groundwater contained in the upper aquifer system of the Victor, Fair Oaks and Laguna Formations is of superior quality compared to that in the lower semi-confined system, mainly because the water in the Mehrten Formation is higher in iron and manganese, and requires additional treatment. The upper unconfined system only requires chlorination treatment to be potable (Sacramento Groundwater Authority 2003).

The City is a member of the Sacramento Groundwater Authority (SGA). The SGA is a joint powers authority created in 1998 by a coordinated effort between the Sacramento Metropolitan Water Authority and the WFA to manage the region's North Area Groundwater Basin, a sub-region of the North American Subbasin. The signatory participants are managing the basin in a cooperative fashion by allowing representatives from the local water purveyors, the agricultural community, and other groundwater pumpers to serve on the Board of the SGA. The goal of the SGA is the responsible management of the groundwater basin through a commitment to not exceed the negotiated sustainable yield of the basin, which is approximately 131,000 AFY according to the WFA. The SGA developed a Groundwater Management Plan (GMP) to ensure a safe, reliable water supply for the rapidly growing northern Sacramento County area. Within this program the SGA will continually assess the status of the groundwater basin and make appropriate management decisions to sustain the basin.

The City and other SGA members, in accordance with the WFA, have implemented a conjunctive use program to responsibly manage and use the groundwater system. The program accounts for the annual climatic variability of the region, whereby in normal or wet years of precipitation the water providers will divert more surface water and reduce or eliminate groundwater use, allowing the groundwater system to recharge. In dry years when Lower American River flows must be maintained, groundwater will be pumped and used to supplement the reduced diversions from the river systems (Sacramento Groundwater Authority 2003).

# Water Code Section 10910(f)(3) requires a description of the volume and geographic distribution of groundwater extractions from the basin for the last five years.

The City's historical average annual groundwater use for the period 1997-98 through 2003-04 was 20,454 AFY (Table 2). The City's active municipal groundwater wells are located primarily in the northern areas of the City. Thirty-two of the wells are located north of the American River and the two wells are south of the river.

#### 4.4 SUPPLY RELIABILITY ANALYSIS

The WFA is important to consider when discussing water supplies and reliability within the Sacramento region. The WFA is an agreement between multiple stakeholders of the Sacramento metropolitan area and lower foothill regions. After seven years of meetings, sub-committee negotiations and small group operations, the Water Forum members established a working agreement that provides water quality and reliability for all participants. The WFA's coequal goals were to (1) provide a reliable and safe water supply for the region's economic health and planned development through to the year 2030, and (2) preserve the fishery, wildlife, recreational and aesthetic values of the Lower American River (Sacramento City-County Office of Metropolitan Water Planning 2000).

From these coequal goals, the Water Forum signatories determined seven major elements that must be implemented during the next thirty years if the agreement is to be successful. The elements specific to water supply reliability include:

- ▶ Increased Surface Water Diversions,
- ▶ Actions to Meet Customers' Needs While Reducing Diversion Impacts in Drier Years,
- Water Conservation.
- ► Groundwater Management and the Water Forum Successor Effort.

Each of these elements plays a vital role in the Water Forum's coequal objectives. As a signatory of the WFA, the City's Utilities department is actively participating in all seven elements.

The City is continuing to develop a water supply consistent with the WFA. Public Law 106-554 authorized the preparation of the Sacramento River Water Reliability Study, which includes a feasibility study for the construction of a second Sacramento River diversion. The Sacramento River Water Reliability Study includes development of water supply alternatives, an environmental evaluation, and consultation with federal and state agencies regarding potential impacts. The Draft Planning report is scheduled for review in early 2006.

The WFA places flow restrictions on diversions from the American River when flow is below the Hodge flows as defined in *Environmental Defense Fund et al. v. East Bay Municipal Utility District* (flow levels of 2,000 cfs from October 15 through February; 3,000 cfs from March through June; and 1,750 cfs from July to October 14). The City's WFA diversion limits change seasonally and are listed in Table 7. Approximately 59% of the years will experience Hodge flow conditions during the peak months of June through August based on historic operations of Folsom Reservoir.

| Restr     | ates      |                       |
|-----------|-----------|-----------------------|
| Month —   | Diversion | on Limit <sup>a</sup> |
| WOIGH     | cfs       | AF                    |
| January   | 120       | 7,400                 |
| February  | 120       | 6,700                 |
| March     | 120       | 7,400                 |
| April     | 120       | 7,100                 |
| May       | 120       | 7,400                 |
| June      | 155       | 9,200                 |
| July      | 155       | 9,500                 |
| August    | 155       | 9,500                 |
| September | 120       | 7,100                 |
| October   | 100       | 6,100                 |
| November  | 100       | 6,000                 |
| December  | 100       | 6,100                 |

#### Notes

The Sacramento River WTP has a capacity of 160 mgd (179,200 AFY). Fairbairn WTP has a treatment capacity of 200 mgd (224,000 AFY), equal to the maximum diversion rate allowed in the WFA. If both plants operated at their maximum production, the combined theoretical output would be approximately 360 mgd.

<sup>&</sup>lt;sup>a</sup> Restriction occurs when the flow passing the WTP is below the Hodge flow condition. Source: Sacramento City-County Office of Metropolitan Water Planning 2000

To account for future growth past 2030, and increased reliability, the City is evaluating the construction of a 145 mgd (225 cfs) WTP on the Sacramento River near Elverta Road, north of the Sacramento International Airport. The proposed water treatment plant is anticipated to be operational within the next 6 to 10 years. With the addition of the new Sacramento River WTP, the City's combined maximum production would be 505 mgd (an additional 145 mgd) and the dry year or Hodge Flow conditions production would be 405 mgd (the 100 mgd reduction at the American River because of dry year conditions would result in an additional 45 mgd of treatment capacity). Maximum day production before and after completion of a 145 mgd Sacramento WTP is shown in Table 8.

|                                       | Table 8 Maximum Day Production                               |  |
|---------------------------------------|--|--|
| Source                                | Production Limit with Flows Above<br>Hodge Criteria<br>(mgd) | Production Limit with Flows Below<br>Hodge Criteria<br>(mgd) |
| Fairbairn WTP                         | 200  | 100  |
| Sacramento WTP                        | 160  | 160  |
| Groundwater                           | 30   | 30   |
| Total                                 | 390  | 290  |
| New Sacramento WTP                    | 145  | 145  |
| Total with new WTP                    | 535  | 435  |
| Source: Sacramento City-County Office | e of Metropolitan Water Planning 2000                        |  |

During years when the projected unimpaired inflow to Folsom Reservoir is less than 400,000 AF, the WFA limits all diversions from the American River to 50,000 AFY. The WFA has labeled the extremely low flow conditions as a "conference year" where signatories will meet to discuss water management strategies. A conference type year scenario has a 1.8% probability of occurring and did occur in 1924 and in 1977. The WFA does not restrict diversion of American River entitlements from a Sacramento River diversion point; therefore normal year and dry year supplies are identical for the City as shown in Table 9. However, annual surface water diversions are limited by the diversion capacity from the Sacramento River. Assuming 50,000 AFY from the Fairbairn WTP and a maximum production from the Sacramento WTP of 179,000 AFY, the current drought limiting scenario would allow for a theoretical maximum surface water production of 230,000 AFY.

| 2005 Annual  | Ta<br>Surface Water Suppli<br>Consecutive Confere |                                     |                                      | ·                                   |  |  |
|--|---|-------------------------------------|--------------------------------------|-------------------------------------|--|--|
| 2005 City of 2005 to 2007 Dry Year Supply <sup>a</sup> |   |                                     |                                      |                                     |  |  |
| Source   | Sacramento Surface Water Rights (AFY)             | First Conference<br>Year 2005 (AFY) | Second Conference<br>Year 2006 (AFY) | Third Conference<br>Year 2007 (AFY) |  |  |
| American River   | 123,200   | 50,000                              | 50,000                               | 50,000                              |  |  |
| American River diverted from Sacramento River          |   | 73,200                              | 77,700                               | 82,200                              |  |  |
| Sacramento River                                       | 81,800  | 81,800                              | 81,800                               | 81,800                              |  |  |
| Total <sup>b</sup>                                     | 205,000   | 205,000                             | 209,500                              | 214,000                             |  |  |

#### Notes:

Source: City of Sacramento

<sup>&</sup>lt;sup>a</sup> Diversion capacity from Sacramento River is 180,000 AFY, allowing a drought year production of 230,000 AFY.

b Total supply increases pursuant to USBR contract.

The theoretical maximum "conference year" production of 230,000 AFY over estimates the current drought year production, because the existing Sacramento WTP could not operate at maximum capacity of 160 mgd in the winter months. In the winter months, demand is less than the maximum treatment capacity of 160 mgd and no storage is available to store excess treated water. Therefore, the treatment plant would operate at maximum demand, which is some increment less than maximum capacity.

#### COMPARISON OF AVAILABLE WATER SUPPLIES VERSUS DEMAND

#### **ANNUAL SUPPLY AND DEMAND**

The City's 2004 water demand of 143,764 AFY was below the current USBR contracted entitlements of 200,000 AFY. The City's projected (2030) annual water demand remains approximately 59% of the USBR contracted annual entitlements. Water demands were estimated for the City from 2005 to 2030 by assuming a constant linear growth rate in water demands between 2005 and 2030 (Table 10). The project's total demand of 2,680 AFY would result in an increase in total demand in 2030 equal to 195,818 AFY. The table shows that under normal year types, sufficient water supplies are available to meet the project and City projected future demands under a 25 year planning horizon.

| City of Sacramento Supply a       | and Demand | Table<br>Comparison ( |         | Il Year Types | 2005 through | 2030 (AFY) |
|-----------------------------------|------------|-----------------------|---------|---------------|--------------|------------|
|                                   | 2005       | 2010                  | 2015    | 2020          | 2025         | 2030       |
| Surface Water Supply              |            |                       |         |               |              |            |
| American River                    | 123,200    | 145,700               | 170,200 | 196,200       | 222,200      | 245,000    |
| Sacramento River                  | 81,800     | 81,800                | 81,800  | 81,800        | 81,800       | 81,800     |
| <b>Total Surface Water Supply</b> | 205,000    | 227,500               | 252,000 | 278,000       | 304,000      | 326,800    |
| Demand                            | 161,342    | 167,714               | 174,073 | 180,432       | 186,791      | 193,138    |
| Project Demand                    | 0          | 2,680                 | 2,680   | 2,680         | 2,680        | 2,680      |
| <b>Total Demand</b>               | 161,342    | 170,394               | 176,753 | 183,112       | 189,471      | 195,818    |
| Additional Water Supply           | 43,658     | 57,106                | 75,247  | 94,888        | 114,529      | 130,982    |

The WFA limits the driest year diversion to 50,000 AFY from the American River, but does not limit the diversion for the American River entitlement from the Sacramento River. Therefore, the City would not be subjected to reductions in contracted deliveries for single or multiple dry years. Annual supply is only limited by diversion and treatment capacity of the Sacramento River during dry year conditions. Current theoretical maximum production during the conference years is approximately 230,000 AFY. Table 11 shows a comparison of supply and demand during conference years. As shown in the table, at maximum production rates sufficient water is available to meet project demands during conference years (i.e., single dry and multiple dry years) in addition to existing and projected future demands over a 25-year planning period. In dry years, the City's total water demands are reduced because the city does not supply water to Sacramento Suburban Water District (SSWD). However, because demand would not be equal to maximum production capacity and no storage is available, the conference year production estimate of 230,000 AFY may over estimate the current drought supply. Therefore, it is important that maximum day demand is also evaluated as described below.

| Table 11 Supply and Demand Comparison during Conference Years |         |         |         |         |         |         |
|---|---------|---------|---------|---------|---------|---------|
|   | 2005    | 2010    | 2015    | 2020    | 2025    | 2030    |
| Surface Water Supply  |         |         |         |         |         |         |
| American River  | 50,000  | 50,000  | 50,000  | 50,000  | 50,000  | 50,000  |
| American River diverted from the Sacramento River             | 73,200  | 95,700  | 120,200 | 146,200 | 172,200 | 179,000 |
| Sacramento River  | 81,800  | 81,800  | 81,800  | 81,800  | 81,800  | 81,800  |
| Total Surface Water Supply <sup>a</sup>                       | 205,000 | 227,500 | 252,000 | 278,000 | 304,000 | 310,800 |
| Demand <sup>b</sup>   | 135,576 | 157,036 | 178,496 | 199,957 | 221,417 | 242,877 |
| Project Demand  | 0       | 2,680   | 2,680   | 2,680   | 2,680   | 2,680   |
| Total Demand  | 135,576 | 159,716 | 181,176 | 202,637 | 224,097 | 245,557 |
| Additional Water Supply                                       | 69,424  | 67,784  | 70,824  | 75,363  | 79,903  | 65,243  |

Notes: Conference Year, as defined by the WFA, when the projected unimpaired inflow to Folsom Reservoir is less than 400,000 AF.

Source: City of Sacramento

### **Maximum Day Demand**

Because of diversion limitations during Hodge flow conditions, the maximum peak day demand should also be considered when comparing supply to demand. Table 12 shows the maximum day surface water supply and demand under normal flow conditions. Table 13 shows the maximum day surface water supply and demand under Hodge flow conditions. Table 12 shows that the City would meet the anticipated peak day demands under normal flow conditions through the year 2030, even without the new WTP. Table 13 shows that during Hodge flow conditions, treatment capacity at Fairbairn is reduced from 200 mgd to 100 mgd, resulting in a total treatment capacity of 260 mgd. Peak day demands under Hodge flow conditions would be met through 2010 with available surface water treatment capacity. The City currently can pump up to 30 mgd of groundwater which would supplement the available surface water. The City's surface and groundwater supplies would provide adequate supplies to meet peak daily demands during a conference year through 2030.

|                                   | 2005 | 2010 | 2015 | 2020 | 2025 | 2030 |
|-----------------------------------|------|------|------|------|------|------|
| <b>Surface Water Supply</b>       |      |      |      |      |      |      |
| American River <sup>a</sup>       | 200  | 200  | 200  | 200  | 200  | 200  |
| Sacramento River <sup>a</sup>     | 160  | 160  | 160  | 160  | 160  | 160  |
| <b>Total Surface Water Supply</b> | 360  | 360  | 360  | 360  | 360  | 360  |
| Demand                            | 218  | 234  | 251  | 267  | 283  | 300  |
| Project Demand                    | -    | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  |
| Total demand                      | 218  | 238  | 255  | 271  | 287  | 304  |
| Additional Water Supply           | 142  | 122  | 105  | 89   | 73   | 56   |

<sup>&</sup>lt;sup>a</sup> Total surface water supply shown is based on USBR contracted deliveries and not maximum dry year treatment and diversion capacity of 230,000 AFY

b Dry/Conference year demand reduced because City does not provide water to SSWD in dry years.

| Table 13 Peak Day Surface Water Supply and Demand Comparison during Hodge Flow Conditions (mgd) |       |        |        |        |       |       |  |
|---|-------|--------|--------|--------|-------|-------|--|
|   | 2005  | 2010   | 2015   | 2020   | 2025  | 2030  |  |
| Surface Water Supply  |       |        |        |        |       |       |  |
| American River <sup>a</sup>   | 100   | 100    | 100    | 100    | 100   | 100   |  |
| Sacramento River b  | 160   | 160    | 160    | 160    | 160   | 160   |  |
| <b>Total Surface Water Supply</b>   | 260   | 260    | 260    | 260    | 260   | 260   |  |
| Demand <sup>c</sup>   | 239.3 | 251.94 | 260.16 | 268.38 | 276.6 | 280.4 |  |
| Project Demand  | -     | 4.3    | 4.3    | 4.3    | 4.3   | 4.3   |  |
| <b>Total Demand</b>   | 239.3 | 256.2  | 264.5  | 272.7  | 280.9 | 284.7 |  |
| Surplus   | 20.7  | 3.8    | -4.5   | -12.7  | -20.9 | -24.7 |  |
| Groundwater   | 30    | 30     | 30     | 30     | 30    | 30    |  |
| Additional Water Supply   | 50.7  | 33.8   | 25.5   | 17.3   | 9.1   | 5.3   |  |

#### Notes:

Source: City of Sacramento

### SUPPLY RELIABILITY ASSESSMENT

The City's has sufficient water supplies to meet their existing and projected future demands in addition to the proposed project through 2030. During normal water years, the City would be able to meet its anticipated demands by using available surface water supplies and surface water treatment capacity. During conference years, or when flows are below Hodge conditions, the City's peak daily demands, including the proposed project, could be met with available surface water treatment capacity through 2015 and through 2030 with combined use of available surface water and groundwater supplies.

The City is a partner in the Sacramento River Water Reliability Study, which is investigating alternatives for an additional diversion on the Sacramento River. The environmental documents for the alternatives analysis are scheduled to be complete in 2006. The proposed 145 mgd diversion facility and WTP included in the Sacramento River Water Reliability Study would provide additional assurance for the delivery of the entitled water for the City, as well as all wholesale and wheeling agreements past 2030.

#### This WSA finds:

- ► The City has sufficient water supplies to serve the proposed project and projected future demands over the next 25 years.
- ▶ Under normal year types, the City has sufficient capacity within its existing WTPs to serve the proposed project and projected future demands over the next 25 years.

<sup>&</sup>lt;sup>a</sup> American River diversion is limited to 100 mgd during Hodge flow conditions.

<sup>&</sup>lt;sup>b</sup> Sacramento WTP peak day supply is based on plant capacity.

<sup>&</sup>lt;sup>c</sup> Dry/Conference year demand reduced because City does not provide water to SSWD in dry years.

- ▶ During conference years (analogous to dry years and multiple dry years) the City has sufficient supply to serve the proposed project and projected future demands if the WTPs operate at maximum production capacity.
- ▶ During conference years, under a peak demand scenario, with limitations in production capacity of the WTPs (whereby demands do not equal maximum capacity), the City's peak demands would exceed available capacity of the WTPs by the year 2020. However, the City's existing groundwater supplies (up to 30 mgd) would ensure peak demands would be met through 2030.
- ► The City's proposed 145-mgd diversion and WTP on the Sacramento River near Elverta Road would provide additional flexibility for managing water supplies, especially with respect to meeting peak demand during dry years.

### **REFERENCES**

- City of Sacramento. 1998–2005. Operational Statistics Annual Report. Sacramento, CA.
- City of Sacramento. 2005. City of Sacramento General Plan Update. Map of Water Infrastructure. http://www.sacgp.org/. Map last updated October 2004. Accessed October 2005.
- City of Sacramento. 2000 (December). 2000 Urban Water Management Plan. Sacramento, CA.
- Peifer, Jim. Utilities Department, City of Sacramento, CA. November 22, 2005—telephone conversation with Diane Wagner of EDAW regarding Water Supply Assessment preparation.
- Sherry, Dan. Water supervising engineer. Utilities Department, City of Sacramento, CA. August 12, 2005—telephone conversation with Diane Smith of EDAW regarding Water Supply Assessment preparation.
- Sacramento Groundwater Authority (SGA). 2003 (December). Groundwater Management Plan. Sacramento, CA.
- United States Bureau of Reclamation. 2005 (March). Sacramento River Water Reliability Study. Initial Alternatives Report. Sacramento, CA.
- Wood Rodgers Engineering. 2005 (July). *Greenbriar Water Study Prepared for City of Sacramento*. Sacramento, CA.
- Sacramento City-County Office of Metropolitan Water Planning. 2000 (January). *Water Forum Agreement*. Sacramento, CA.

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### **Acronyms**

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### Greenbriar CLUP Analysis - Safety Zone Compliance Overview

#### 8/15/2005

| Greenbriar Land Uses Identified in CLUP       | CLUP Compatibility* | Description                        |
|---|---------------------|------------------------------------|
| Single-family detached Mulfi-family dwellings | Yes**<br>Yes**      | See "persons per hour detail" Same |
| Streets, roads and Highways                   | Yes*                | Game                               |
| Light rail lines: passenger                   | Yes*                |                                    |
| Passenger terminals and stations              | No                  | "Over-ride" needed                 |
| Parking lots                                  | Yes*                | _                                  |
| Grocery stores                                | Yes**               | See "persons per hour detail"      |
| Eating and Drinking                           | Yes**               | Same                               |
| Miscellaneous Retail Trade                    | Yes**               | Same                               |
| Neighborhood shopping centers                 | Yes**               | Same                               |
| Neighborhood parks                            | Maybe               |                                    |
| Open space, natural and water areas           | Yes*                |                                    |

<sup>\*</sup> As per the Sacramento International Airport CLUP, amended January 1994

### Conclusion:

The Greenbriar project complies with the Sacramento International Airport CLUP in all instances except for the light rail station. The project complies with the spirit and intent of the CLUP as it relates to parks, by siting "Regional-serving" larger parks outside of the safety zone. However, park consistency with the CLUP may require some attention due to a footnote in the CLUP stating that the parks may not contain any "structured playgrounds, ballfields or picnic pavilions."

<sup>\*\*</sup> As per CLUP "concentration" guidelines - see attached analyses

### **Greenbriar Safety Zone Densities - Summary**

### 8/15/2005

### 25 Persons Per Acre Per Average Hour:

| Gross Persons Within Safety Zone Per "Average Hour" Allowable Persons Within Safety Zone Per "Average Hour" |       |  |  |  |
|---|-------|--|--|--|
| Persons Per Acre Per Average Hour Within Safety Zone  | 21    |  |  |  |
| Allowable Persons Per Acre Per Average Hour Within Safety Zone  | 25    |  |  |  |
| 50 Persons Per Acre Maximum:  |       |  |  |  |
| Gross Persons Within Safety Zone At Any Given Time  | 12543 |  |  |  |
| Allowable Persons Within Safety Zone At Any Given Time  | 20250 |  |  |  |
| Maximum Average Persons Per Acre Within Safety Zone At Any Given Time                                       | 31    |  |  |  |
| Maximum Allowable Average Persons Per Acre Within Safety Zone At Any Given Time                             | 50    |  |  |  |

| Greenbriar Safety Zone Densities - Persons per Hour | Explanation per April 29 submission of "formal" development application per CLUP, page 36 and Appendix A-1  | number came from Jim McDonald, LRP - from historical 10-year City of Sac census info number came from Jim McDonald, LRP - from historical 10-year City of Sac census info number came from Jim McDonald, LRP - from historical 10-year City of Sac census info 2099 total detached units x 2.86 (1119 LDR, 1005 MDR) 225 total multi-family units x 1.9 | For purposes of "averaging" - assume people at home 18 hours per day, on average                  | Area Factor Occ. Load 58.500 30 1,950 "Factor" is population factor - persons per square foot maximums as set forth in 6,500 300 122 Table 10-A of the 2001 California Building Code (2001 is current edition).  17.840 15 1,189 Occupancy Load #s are "maximum" persons per square foot derived from CA Building Code 4,480 200 22.3  38,250 30 1275 Not shown on "Conceptual Plan," but included here to be conservative and provide flexibility later. 6,750 300 22.5  4,481 Only those commercial uses that fall within the safety line are analyzed in this section. | 2,800 200 14 21,250 30 708 "Conceptual Pian* shows 14,700 sf; more analyzed here to be conservative and provide flexibility later 3,750 300 13 15,000 100 150 1632 For purposes of "averaging" - assume commercial units empty for 10 hours per day   | Population totals attributable to parks have no noticeable impact on overall density evaluation, due to the siting of "Regional" parks outside of the safety line. See footnote below. | per April 29 submission of formal development application   |
|---|---|---|---|---|---|--|---|
| Greenbr 8/15/2005                                   | <u>25 Persons Per Acre Per Average Hour</u> Gross acreage within safety zone Allowable persons per acre per "average hour" 25 Total allowable persons within safety zone ("on average") | Assumptions: Assumptions: Persons per household - single family detached* Persons per household - wo-four-plex* Persons per household - 5-plex+ (apartments)* Calculations: Single-family households - total # of persons Multi-family households - total # of persons 428  | Total Maximum Persons Occupying Residential Units 6431 Occupied an average of 75% of the day 4823 | COMMERCIAL           Large Commercial Area:         Use         %           Area         Store         90%           Shore         Store         10%           Shops         45,000         Store           Total Max Occupancy Load         Storage         15%  | Meister Way Commercial:         Dinning         80%           Restaurant         14,000         Kitchen         20%           Shops         25,000         Store         85%           Office         15,000         Office         15%           Total Max Occupancy Load         Office         100%           Total Maximum Persons Occupying Commercial Units         6112           Occupied for 14 hours per day         3545 | PARKS** TOTAL PERSONS PER AVG HOUR WITHIN SAFETY ZONE TOTAL ALLOWABLE PERSONS WITHIN SAFETY ZONE TOTAL PERSONS PER ACRE PER AVG HOUR WITHIN SAFETY ZONE                                | TOTAL ALLOWABLE PERSONS PER ACRE PER AVG HOUR WITHIN SAFETY ZON 25  50 Persons Per Acre Maximum Gross acreage within safety zone Allowable persons Total maximum allowable persons within safety zone at any given time 20250 |

| per analysis above                                |   | Population totals attributable to parks have no noticeable impact on overall density evaluation, | doe to the sking of hegional parks outside of the safety line. See roomore below.                     |
|---|---|--|---|
| 6431  | 6112  |  | 12543<br>20250  |
| Total Maximum Persons Occupying Residential Units | COMMERCIAL Total Maximum Persons Occupying Commercial Units | PARKS*   | TOTAL MAXIMUM PERSONS WITHIN SAFETY ZONE AT ANY GIVEN TIME TOTAL ALLOWABLE PERSONS WITHIN SAFETY ZONE |

• 4 4 5

TOTAL PERSONS PER ACRE WITHIN SAFETY ZONE AT ANY GIVEN TIME

TOTAL MAXIMUM ALLOWABLE PERSONS PER ACRE WITHIN SAFETY ZONE

50

The only parks sited within the safety zone are neighborhood parks. In other words, people using those parks come primarily from within the project area and thus those population numbers are already captured in the analysis above. There will be no lighted ballifield "complexes" within the safety zone. While there is the potential for one or two ballifields on the 5 or 7 acre park, maximum "occupancy" on those fields would probably be 300 to 400 persons on the busiest days. Those rumbers are not nearly large enough to make a difference in the overall calculation.

<sup>\*</sup>Census data: I used the more conservative of two estimates on household population assumptions. The 2000 U.S. Census Bureau states that for the City of Sacramento, Total Average Houshold Size is 2.57 persons/house.

The detail states that of that, "Owner Occupied" (probably a good surrogage for single-family detached) is 2.65 persons/house and "Renter Occupied" is 2.50 persons/house. \*\* Parks



# **DRAFT**

# Patterns of Winter Avian Abundance in Rice Fields and Urban Lakes in the Natomas Basin

Sacramento County, California



Prepared for: RWI Investments

Date: February, 2006

Prepared by:



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#### 1.1 Purpose

This study was designed to compare winter avian use of rice fields and urban lakes in the Natomas Basin of Sacramento County, California, and to assess the relative degree to which each of these habitat types may attract birds that pose a risk to aircraft.

#### 1.2 Background

The Natomas Basin is located in California's Sacramento Valley, one of the most important wintering and migratory areas for waterfowl and other bird species in North America. Approximately 60 percent or more of the waterfowl population in the Pacific Flyway winter in or migrate through the Sacramento Valley (Ducks Unlimited 1995a). These waterfowl and other bird species pose a hazard to aircraft using the Sacramento International Airport, located at the heart of the Natomas Basin (**Figure 1**).

The location of the Sacramento International Airport along the Pacific Flyway poses a significant challenge to airport operators attempting to minimize the risk of aircraft bird strikes (Larson 2003). Aircraft bird strikes present a significant human safety risk and cost to the airline industry. The Federal Aviation Administration (FAA) estimates that wildlife strikes cost the U.S. civil avaition industry \$500 million annually. Approximately 6,100 strikes were reported at civil airports in 2003 alone (Wildlife Services 2004). The level of bird aircraft strike risk at Sacramento International Airport has warranted full-time assistance from USDA to manage wildlife hazards (Wildlife Services 2004).

Changing land use patterns have altered the landscape of the Natomas Bain significantly, although a large proportion of this historic floodplain has continued to provide waterfowl habitat. The Natomas Basin is a low-lying area located along the east side of the Sacramento River, upstream of its confluence with the American River. Prior to 1914, this basin consisted of an alluvial plain with several large lakes and sloughs that provided surface drainage to the American River and habitat for an abundance of waterfowl (Hinds 1952, USFWS 2003; see **Appendix A**, 1908 Land Cover). After 1914, reclamation efforts such as construction of canals, levees, and pumping stations converted much of the Natomas Basin to agricultural production, primarily rice (USFWS 2003). As the natural wetlands were converted to ricelands, waterfowl wintering in the basin came to rely on winter flooded rice. Indeed, because of the limited amount of natural wetlands remaining, the large numbers of waterfowl wintering in California could not be supported without small-grain production such as commercial rice (Ducks Unlimited 1995b).

More recently, approximately 11% of the Natomas Basin has been converted from agricultural to urban uses (City of Sacramento, Sutter County, NBC 2002). Urban lakes have been constructed and are planned for construction in these urbanizing areas to provide surface storage for flood control purposes and conjunctive uses such as recreation and storm water pollution prevention.

1

The FAA discourages land uses that increase aircraft strike hazards by attracting birds into airport overflight zones. Urban lakes such as those constructed in the Natomas Basin may attract waterfowl including geese, gulls, and other species known to be involved in aircraft strikes. However, as described above, the Natomas Basin has historically supported waterfowl because of its low position in the watershed, itstendency to flood. In assessing the impacts of constructing urban lakes, one must make a comparison with pre-project conditions. This study was designed to compare the level of aircraft strike risk posed by these urban lakes as compared with pre-urbanization conditions (i.e., flooded agriculture).

Figure 1: Study Area and Study Sites

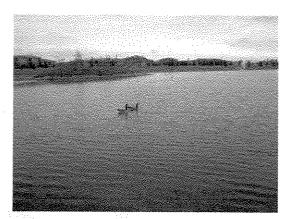


### 2.1 Study Area

Missing

The study area was the Natomas Basin, located in Sacramento County in the northern Sacramento Valley (Figure 1). Three man-made lakes were surveyed within the study area: these are described below and their locations in relation to the Natomas Basin are shown on Figure 1:

1. Northborough Lake is a large, L-shaped lake at the corner of Truxel Road and North Park Drive. It has gently sloping sides of approximately 25 degrees and consisted of round boulders of varying sizes. It has two islands that have similar sides as the periphery of the lake and small shrubs and willow trees.



2. Alleghany Lake is just east of the corner of Truxel Road and Terracina Drive. Like Northborough Lake, it has gently sloping sides of approximately 25 degrees. It has one island that also has similar sides as the periphery of the lake and has small shrubs and willow trees.



3. Gateway North Lake is in the middle of Gateway North subdivision and is just east of El Centro Road and north of Arena Boulevard on the west side of Interstate 5 freeway. It has 90 degree rock sides and the lakeside homes abut the lakeshore.



Rice fields were surveyed along on a driving route that was chosen based on presence of flooded agriculture, lack of disturbance such as hunting pressure, and accessibility of the survey points. The survey route started at Sankey Road near Pacific Road, then east to east levee road, then south to west Elverta Road and to the Interstate 5 freeway (**Figure 1**).





**Elverta Road Ricef Field** 

East Levee Road Rice Field



Sankey Road Rice Field

#### 2.2 Survey Method

A standard 10-minute point count method was used, by which the observer recorded all birds seen and heard from a single point (survey point) during a 10 minute period (Howe et al. 1997, Ralph et al. 1993). The surveys for both urban lakes and rice fields started at ten minutes after sunrise, and ended no later than three hours after sunrise. The same observer surveys both the lakes and rice fields to avoid observer biases. At each point count, the observer recorded the number of birds observed for each species. For numbers between 100 and 200, the observer estimated to the nearest 10. For numbers between 200 and 1,000, the observer estimated to the nearest 50. For numbers greater than 1,000, the observer estimated to the nearest 100.

At the lake sites, survey points were spaced to maximize visibility of the entire lake without double-counting. Due to its L-shape, Northborough Lake had to be surveyed from two points to view the entire lake. The entirity of Alleghany Lake could be surveyed from one point. Due to the lakeshore homes of Gateway Lake, it could only be surveyed from two points, one point at the east side of the lake and one at the west side. Survey points at the rice fields were spaced 200 meters apart to maximize coverage and avoid double-counting. The observer would drive to each survey point and walk to the edge of the rice field for the point count.

### 2.3 Data Analysis

Assuming the number of birds per point count does not follow a Gaussian distribution, a nonparametric test was used to compare the total number of birds per point count in rice fields and urban lakes. A Mann-Whitney U-test was applied and significance was assessed at a 99% confidence interval. P-values  $\leq 0.01$  were considered statistically significant. Data were also summarized by species observed at rice fields vs. urban lakes, and the range of numbers of individuals per species at rice fields vs. lakes. Species observed were lumped into various categories consistent with the categories used in the FAA National Wildlife Strike Database (e.g., ducks, geese, gulls . . .: FAA 2000) . Data was then summarized by the mean number of birds observed per survey site per species category.

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## 3.1 Bird Abundance in Urban Lakes and Rice Fields

The number of birds observed per point count was significantly higher for rice fields than for urban lakes (**Table 1:** U = 224, P < 0.0001). For rice fields, the total number of birds observed per point count ranged from 1 to 2,652, while for urban lakes, the total number ranged from 0 to 37. The mean number of birds per point count was 224.12 ( $SD \pm 428.69$ ) for rice fields and 12.12 ( $SD \pm 11.55$ ) for urban lakes.

Table 1: Median Number of Birds per Point Count

| Rice Field  | 48              | 70 P | 83 | 224  |
|-------------|-----------------|------|----|------|
| Urban Lakes | 50              |      | 10 | 2176 |
|             | Mann-Whitney U: | 224  |    |      |

## 3.2 Species Observed

The diversity of bird species observed was higher at rice fields than at urban lakes: there were 18 species observed at rice fields and 10 at urban lakes (**Table 2**). Species observed at rice fields that were not observed at urban lakes were American widgeon, black-necked stilt, curlew, double-crested cormorant, green-winged teal, northern pintail, northern shoveller, phalarope, snow goose, snowy egret, sandpiper sp, white-faced ibis, and western grebe. Species observed at urban lakes but not at rice fields included Canada goose, common merganser, green heron, and western grebe.

Table 2: Species Observed at Rice Fields and Urban Lakes

| Species                  | Rice Fields | Urban Lakes | Group      |  |
|--------------------------|-------------|-------------|------------|--|
| American coot            | 0-1,000     | 0 - 6       | Other      |  |
| American widgeon         | 0 - 44      | 0           | Ducks      |  |
| Black-necked stilt       | 0 - 32      | 0           | Shorebirds |  |
| Canada goose             | 0           | 0 - 23      | Geese      |  |
| Common grebe             | 0 - 2       | 0 - 3       | Other      |  |
| Common merganser         | 0           | 0 - 18      | Ducks      |  |
| Curlew                   | 0 - 47      | 0           | Shorebirds |  |
| Double-crested Cormorant | 0 - 4       | 0           | Other      |  |

Table 3: Species Observed at Rice Fields and Urban Lakes-Continued

| Species                 | Rice Fields | Urban Lakes | Group         |
|-------------------------|-------------|-------------|---------------|
| Great blue heron        | 0 - 2       | 0 - 1       | Herons/egrets |
| Great egret             | 0 - 12      | 0 - 2       | Herons/egrets |
| Greater yellowlegs      | 0 - 4       | 0           | Shorebirds    |
| Green heron             | 0           | 0-4         | Herons/egrets |
| Green-winged teal       | 0 - 32      | 0           | Ducks         |
| Mallard                 | 0 - 39      | 0-22        | Ducks         |
| Northern pintail        | 0 - 950     | 0           | Ducks         |
| Northern Shoveller      | 0 - 26      | 0           | Ducks         |
| Phalarope               | 0 - 19      | 0           | Shorebirds    |
| Snow goose              | 0 - 450     | 0           | Geese         |
| Snowy egret             | 0 - 22      | .0          | Herons/egrets |
| Gull                    | 0 - 130     | 0 – 9       | Gulls         |
| Sandpiper spp.          | 0 - 80      | 0           | Shorebirds    |
| White-faced ibis        | 0 - 33      | 0           | Other         |
| White fronted goose     | 0 - 750     | 0           | Geese         |
| Western grebe           | 0           | 0 – 1       | Other         |
| Total # Species present | 18          | 10          |               |

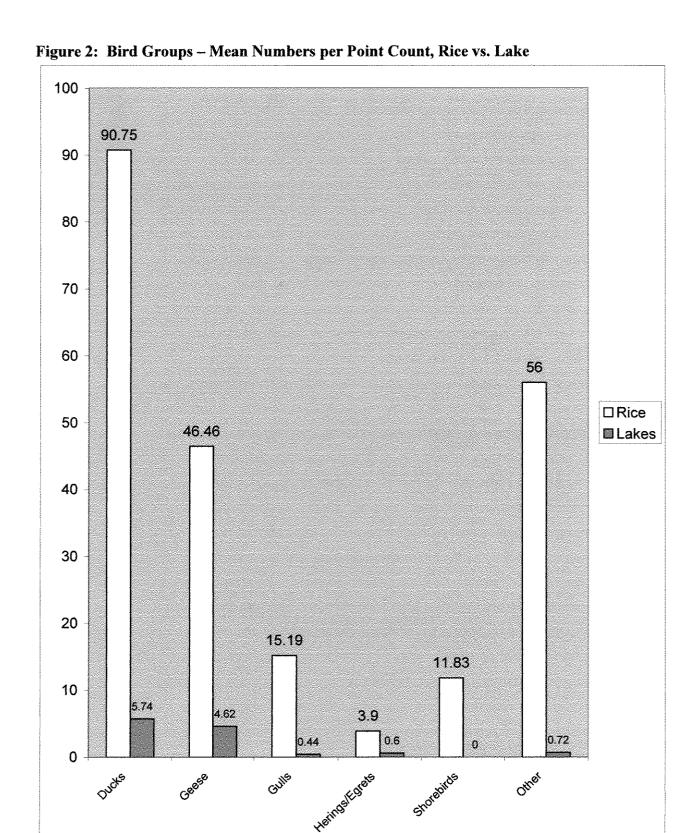
## 3.3 Number of Birds per Species Group

The mean number of birds per point count were higher at rice fields than at urban lakes for all groups (**Table 4**). Although Canada geese were present only at urban lakes, large flocks of snow geese and white fronted geese were observed at rice fields, so that birds in the geese group were much more abundant in rice fields than at the urban lakes.

Although the mean number of birds per point count per group were quite variable between sites, they were consistently higher at rice fields than urban lakes (**Figures 3,4**). Gateway Lake differed from the other two lakes in that it had no ducks or geese, but had a higher number of gulls than the other two lakes. Gateway Lake also had a moderate number of birds lumped as "other".

Table 4: Mean Number Birds per Group

| Group         | Habitat | Location                       | Total<br>Birds | Mean<br>Number* | Mean # when<br>Observed*<br>(dropping<br>zeros) |
|---------------|---------|--------------------------------|----------------|-----------------|---|
| Ducks         | Rice    | Elverta Rd.                    | 3281           | 68.35           | 121.52  |
| 20010         |         | Levee Rd.                      | 730            | 15.2            | 91.25   |
|               |         | Sankey Rd.                     | 345            | 7.18            | 38.33   |
|               | Lake    | Alleghany lake<br>Northborough | 110            | 2.2             | 10  |
|               |         | lake                           | 177            | 3.54            | 8.85  |
|               |         | Gateway Lake                   | 0              | 0               | null  |
| Geese         | Rice    | Elverta Rd.                    | 1180           | 24.58           | 393.33  |
|               |         | Levee Rd.                      | 0              | 0               | null  |
|               |         | Sankey Rd.                     | 1050           | 21.88           | 350   |
|               | Lake    | Alleghany lake<br>Northborough | 98             | 1.96            | 16.33   |
|               |         | lake                           | 133            | 2.66            | 11.08   |
|               |         | Gateway Lake                   | 0              | 0               | null  |
| Gulls         | Rice    | Elverta Rd.                    | 562            | 11.71           | 40.14   |
|               |         | Levee Rd.                      | 57             | 1.1875          | 57  |
|               |         | Sankey Rd.                     | 110            | 2.3             | 27.5  |
|               | Lakes   | Alleghany lake<br>Northborough | 0              | 0               | null  |
|               |         | lake                           | 8              | 0.16            | 8   |
|               |         | Gateway Lake                   | 14             | 0.28            | 7   |
| Herons/Egrets | Rice    | Elverta Rd.                    | 167            | 3.48            | 6.42  |
|               |         | Levee Rd.                      | 10             | 0.21            | 3.33  |
|               |         | Sankey Rd.                     | 10             | 0.21            | 5   |
|               | Lake    | Alleghany lake<br>Northborough | 5              | 0.1             | 1   |
|               |         | lake                           | 25             | 0.5             | 1.92  |
|               |         | Gateway Lake                   | 0              | 0               | 0   |
| Shorebirds    | Rice    | Elverta Rd.                    | 447            | 9.3125          | 34.38   |
|               |         | Levee Rd.                      | 50             | 1.04            | 50  |
|               |         | Sankey Rd.                     | 71             | 1.48            | 17.75   |
|               | Lake    | Alleghany lake<br>Northborough | 0              | 0               | nuli  |
|               |         | lake                           | 0              | 0               | null  |
|               |         | Gateway Lake                   | 0              | 0               | null  |
| Other         | Rice    | Elverta Rd.                    | 1614           | 33.63           | 67.25   |
|               |         | Levee Rd.                      | 1074           | 22.38           | 214.8   |
|               |         | Sankey Rd.                     | 0              | 0               | <u>null</u>                                     |
|               | Lake    | Alleghany lake<br>Northborough | 9              | 0.18            | 1.29  |
|               |         | lake                           | 23             | 0.46            | 2.09  |
|               |         | Gateway Lake                   | 13             | 0.26            | 1.86  |



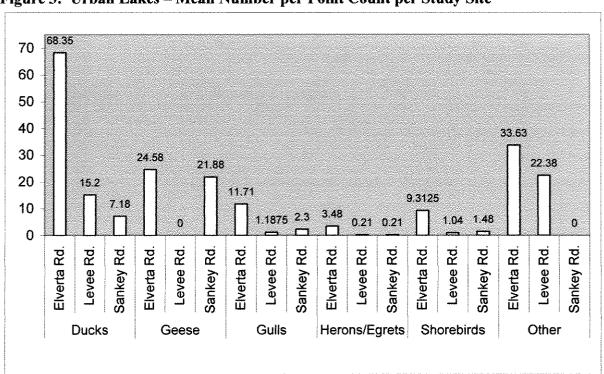
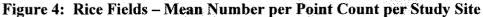
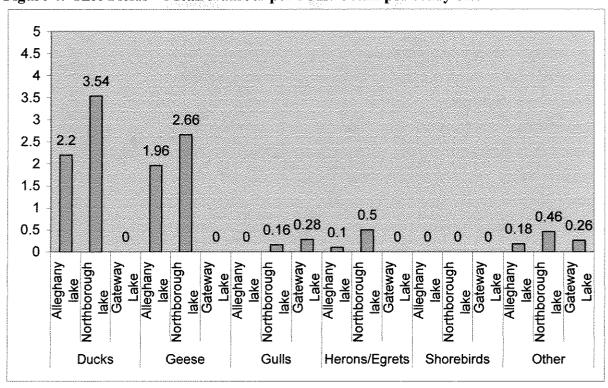


Figure 3: Urban Lakes - Mean Number per Point Count per Study Site





Species grouped as "other" were those that did not fit into any of the categories in the FAA National Wildlife Strike Database. However, because of the large number of birds lumped into this category found in rice fields, and the relatively large proportion of lake birds designated as "other", this category was broken down further in assessing the relative proportions of different bird types present.

At both urban lakes and rice fields, ducks made up the highest proportion of total birds observed (**Figure 5**, **Figure 6**). Geese were the second most abundant group at urban lakes, while coots were the second most abundant group at rice fields, although geese also made up a large proportion of birds observed at rice fields. For both rice and urban lakes, the remaining categories made up less than 25% of total birds observed.



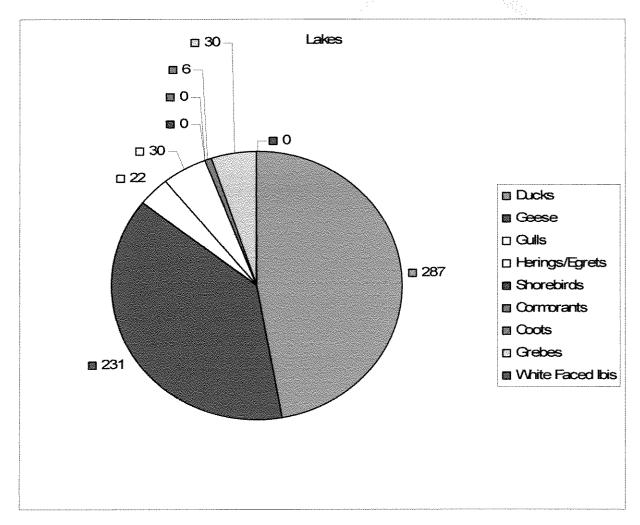
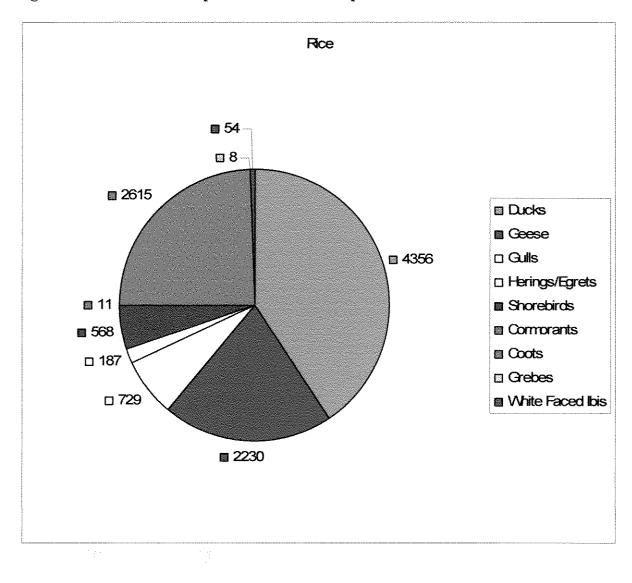


Figure 6: Rice Fields - Proportion of Each Group



## 3.4 Aircraft Hazard Levels

The FAA National Wildlife Strike Database (FAA) ranks various groups of birds in terms of relative hazard to aircraft as shown on Table 5.

Table 5: FAA Database - Wildlife Hazards to Aviation in the U.S.

| Species              | Relative hazard (1-100) | This study: lakes                         | This study: rice fields |
|----------------------|-------------------------|---|-------------------------|
| Vultures             | 63                      | 0   | O                       |
| Geese                | 52                      | X   | X                       |
| Cranes               | 48                      | O jakibas                                 | 0                       |
| Osprey               | 50                      | 0   | 0                       |
| Pelicans             | 44                      | 0   | 0                       |
| Ducks                | 37                      | X   | X                       |
| Hawks                | 25                      | 0   | O THE SEC               |
| Eagles               | 1                       | 0   | <b>O</b> \$355.         |
| Rock dove            | 24                      | 0   | 0                       |
| Gulls                | 22                      | X   | X                       |
| Herons               | 22                      | X   | X                       |
| Mourning dove        | 17                      | 0   | 0                       |
| Owls                 | 16                      | O Philips                                 | 0                       |
| American kestrel     | 14                      | 0   | 0                       |
| Shorebirds           | 12                      | AO 11 11 11 11 11 11 11 11 11 11 11 11 11 | X                       |
| Crows/ravens         | 12                      | 0   | 0                       |
| Blackbirds/starlings | 9                       | O   | 0                       |
| Sparrows             | 4                       | 0   | 0                       |
| Swallows             | 2                       | 0   | О                       |

High risk species categories in **Table 4** and found at both urban lakes and rice fields are geese, ducks, gulls, and herons (grouped with egrets). Shorebirds, also idenfied as an aircraft hazard, were found only at rice fields and not urban lakes. As described in section 3.3, for all groups identified above as an airstrike hazard, greater numbers were found at rice fields than at urban lakes.

Additionally, based on data compiled from 1990 to 1992 (Cleary et al. 2003), the top 20 bird species causing damage to civil aircraft in the United States were listed (**Table 6**). **Table 6** shows that four of the species identified in the top 20 were observed at urban lakes, while five of these species were observed at rice fields. Among these top 20 species, the number of birds observed per point count ranged higher at rice fields than at urban lakes. The species ranked highest in terms of aircraft hazard, Canada goose, was observed at urban lakes and not at rice fields.

Table 6: Data Comparison with Top 20 Bird Species Causing Damage to Aircraft

| A.<br>Rank | 6: Data Comparison wi<br>B. Species |           |       | oorted dam: |             | D.<br>Total | E.<br>Urban                            | F.<br>Rice |
|------------|-------------------------------------|-----------|-------|-------------|-------------|-------------|--|------------|
| Kank       |                                     | Destroyed | Minor | Uncertain   | Substantial | TOTAL       | Lakes <sup>1</sup>                     | Fields     |
| 1          | Canada goose                        | 1         | 163   | 64          | 111         | 339         | 0 - 23                                 | 0          |
| 2          | Rock dove                           |           | 49    | 16          | 54          | 119         | 0                                      | 0          |
| 3          | Turkey vulture                      | 1         | 42    | 18          | 32          | 93          | 0                                      | 0          |
| 4          | Red-tailed hawk                     |           | 33    | 14          | 24          | 71          | 0                                      | 0          |
| 5          | Mallard                             |           | 29    | 7           | 29          | 40          | 0 - 22                                 | 0 – 39     |
| 6          | Mourning dove                       |           | 15    | 15          | 20          | 50          | 0                                      | 0          |
| 7          | European starling                   |           | 24    | 8           | 15          | 47          | 0                                      | 0          |
| 8          | Herring gull                        |           | 7     | 4           | 29          | 40          | 02                                     | 0          |
| 9          | Snow goose                          |           | 11    | 5           | 7           | 33          | 0                                      | 0 - 450    |
| 10         | Ring-billed gull                    |           | 7     | 5           | 12          | 24          | 0-93                                   | 0 - 130    |
| 11         | American crow                       |           | 10    | 1           | 7           | 18          | 0                                      | 0          |
| 12         | Great blue heron                    |           | 11    | 4           | 3           | 18          | 0-1                                    | 0-2        |
| 13         | Bald eagle                          |           | 13    | 2           | 2           | 17          | 0                                      | 0          |
| 14         | Osprey                              |           | 8     | 1           | 7           | 16          | 0                                      | 0          |
| 15         | Sandhill crane                      |           | 10    |             | 6           | 16          | 0                                      | 0          |
| 16         | Killdeer                            |           | 7     | 6           | 2           | 15          | 0                                      | 0          |
| 17         | Double-crested cormorant            |           | 4     | 2           | 5           | 11          | 0                                      | 0-4        |
| 18         | Brown pelican                       | 1         | 7     | 2           | 1           | 11          | 0                                      | 0          |
| 19         | American kestral                    |           | 1     | 3           | 6           | 10          | 0                                      | 0          |
| 20         | Barn owl                            |           | 2     | 1           | 7           | 10          | 0                                      | 0          |
|            | 101 other species                   | O         | 92    | 26          | 111         | 229         | ************************************** |            |

<sup>&</sup>lt;sup>1</sup> Numbers in these E and F represent the range of total # of birds of a given species observed during a single point count.

<sup>&</sup>lt;sup>2</sup> Although gull data was not recorded to species, herring gulls are not known to occur in the Sacramento area.

<sup>&</sup>lt;sup>3</sup> Gull data was not recorded to species – these numbers are for all gull species observed.

### 4.1 Avian use of Rice Fields

Waterfowl arriving in the Central Valley require a diet rich in carbohydrates to replenish fat reserves lost during fall migration. Rice crops are eaten by many species of waterfowl because they are widespread, easily accessible, and provide high levels of carbohydrates. Historically, migratory waterfowl were viewed as major rice pests by farmers because of the amount of pre-harvest rice seed they consumed.

After harvest, up to 300 pounds of rice can remain on each acre of a rice field (Ducks Unlimited 1995b). This is a tremendous food resource for many forms of wildlife, especially when coupled with the variety of aquatic and terrestrial weeds found in rice fields. The seeds from all of these plants, along with the invertebrates commonly found there, provide a varied diet for a broad range of waterbirds. Waterfowl are among the most numerous of the species that are known to use rice fields. During fall and winter, after rice fields have been harvested, tens-of-thousands of ducks, geese, and swans can be seen resting and feeding in rice fields throughout the Sacramento Valley. Later, once grain and weed seeds are depleted, waterfowl and shorebirds still use fields to continue feeding on the insects and snails that occur on the decaying straw.

California has lost 90-95 percent of its original wetlands and the majority of these drained wetlands have been converted to rice fields (Ducks Unlimited 1995a). These rice fields are flooded in the spring and summer during the growing season and now have become surrogate wetlands for the locally breeding waterfowl like mallards. Ducklings need escape cover from predators and the rice stalks provide this needed habitat type. Moreover, the rice stalks provide a perfect substrate for invertebrates to cling to and feed on and the shallow water in rice fields provides a constant warm temperature for many invertebrate species.

All species of waterbirds have increased protein requirements during molt and egg laying. Agricultural fields flooded through late winter provide critical invertebrate food resources that provide the needed protein for molting and prelaying females (Ducks Unlimited, 1995b; Brouder, and Hill 1995). Rice fields provide about 250 pounds per acre of naturally occurring food sources such as small invertebrates, macroinvertebrates, tubers, edible shoots, and seeds. In addition, after harvest an average of 350 pounds per acre of rice is available to waterfowl. Rice fields managed as wetlands can provide as much as 600 pounds of food per acre, or 80 percent of the amount of food found in natural wetlands (Brouder and Hill, 1995). It is believed the reason for this is rice fields have a tremendous food base for waterbirds. Microinvertebrates are an important food base for waterfowl and shorebirds and are present in large numbers in rice fields.

Dabbling ducks are the most prevalent duck in the Central Valley. These include mallards, northern pintails, greenwing teal, northern shovelers, and American widgeon. When feeding in water, these birds as well as all the goose species, feed by tipping up in shallow

water. Therefore they only have access to food resources that are not deeper than their outstretched necks when tipping. Typically, 4-10 inches is the preferred feeding depth for dabbling ducks and this is the depth that rice fields are kept during spring and summer growing seasons and during the winter when farmers flood their rice fields for straw decomposition. Farmers need to dispose of the rice straw to make way for the next years crop. Burning traditionally was the preferred method but in 1991, the Legislature passed the Rice Straw Burning Reduction Act which gradually reduced the amount of acres that could use burning to dispose of the straw. Now, only 1/4 of the cropland can use the burn disposal method and only the farmer can prove that a disease is prevalent. Many farmers now flood their fields in the fall to help decompose the rice straw and they keep the water levels shallow for maximum oxygen and soil incorporation with the straw. This helps the straw rot and break down and also provides great habitat for shallow water loving species like waterfowl, shorebirds and wading birds.

The rice fields that were surveyed were also heavily used by shorebirds, including sandpipers, phalaropes, curlews, and dowitchers. These shorebirds also need shallow water to feed. Rice fields provide excellent habitat for invertebrates that are important for shorebirds and waterfowl (Wildlife Habitat Management Institute 2000). These invertebrate species include water boatman, backswimmers, water scorpions, giant water beetles, water beetles, dragonfly nymphs, and larva of mosquitoes, flies, midges, crane flies, soldier flies, dance flies, snipe flies, horse flies, and brineflies. Shorebirds prefer depths between 1-6 inches to forage for these prey invertebrate prey items.

Many wading birds such as egrets and herons were also observed in the rice fields. These wading birds also prefer shallow water for foraging and will feed in water up to 15 inches (Colwell and Taft 2000). These wading birds prefer larger macroinvertebrates like crayfish and vertebrates like rodents that frequent rice fields.

### 4.2 Avian Use of Urban Lakes

The man-made lakes that were surveyed are deeper than the water in the flooded rice fields and therefore these birds cannot feed efficiently in the lakes. Additionally, the water levels in the manmade lakes do not fluctuate for seed germination of emergent vegetation. The emergent vegetation seeds need exposed mud flats to germinate and grow, while the manmade lake levels are managed for a constant level.

Waterfowl use the man-made lakes primarily for loafing, and they are not found in large numbers in this habitat type. Gradually sloped sides like those of Allegheny and Northborough lakes in our survey appear to be more attractive to waterfowl because this allows the birds to climb out of the water to rest and preen. This behavior was observed in our surveys. The lakes that had sloping sides had more birds and the birds observed on these waters were frequently seen resting out of the water. Gateway North Lake, which has 90 degree sides that prevent waterfowl from exiting to rest and preen had virtually no waterfowl during our surveys.

## 4.3 Aircraft Strike Hazard: Urban Lakes versus Rice Fields

The results of this study indicate that not only are total numbers of birds higher at rice fields than at urban lakes, but numbers of birds belonging to species known to pose a hazard to aircraft are also higher in rice fields. Indeed, numbers were higher at rice fields than urban lakes for all species groups.

#### 4.4 Canada Geese

Canada goose, the species identified in **Table 6** as the greatest hazard to aircraft, was observed only at urban lakes and not at rice fields. While the numbers of Canada geese observed at urban lakes were low (0 to 23 per point count) compared with other geese such as snow geese (0-450) at rice fields, the increasing numbers of Canda geese in the United States is a concern to the USDA in their efforts to minimize wildlife strikes hazards (pers. comm. Scott Beckerman, USDA, January 13, 2005).

The number of Canada geese that nest and/or reside predominantly within the conterminous United States has increased dramatically in the past 20 years. The total number of Canada geese counted during winter in North America has increased from 980,000 in 1960 to 3,734,500 in 2000 (Mid-winter Survey unpublished reports), and Canada geese are now thought to be more abundant in the United States than at any time in history (USFWS 2005). Recent surveys suggest that the Nation's resident breeding population now exceeds 1 million birds in both the Atlantic and the Mississippi Flyways and is continuing to increase. In the Mississippi Flyway alone, the 1998 spring Canada geose population estimate exceeded 1.1 million birds, an increase of 21 percent from 1997. Data collected on California populations of Canada geese between 1970 and 1999, however, indicate that populations have not been increasing along the Pacific Flyway as dramatically as along the Atlantic and Mississippi Flyways (USFWS 2005).

The increase in resident Canada goose populations in the United States is partially attributed to increasing urban and suburban development which has resulted in the creation of ideal goose habitat; that is, parklike open areas with short grass adjacent to small bodies of water. Urban lakes may therefore pose a risk to aircraft by attracting Canada geese, and if population levels grow along the Pacific Flyway as they have been along the Atlantic and Mississippi Flyways, the risk may increase over time. However, a number of design and management measures can be implemented to minimize attraction of Canada geese to urban lakes. The following are among a variety of measures frequently used to make property less attractive to geese:

- Post signs prohibiting feeding of geese.
- Do not plant grass along the lakeshore, leave a 20-30 foot barrier strip of tall grass (6 inches or more) adjacent to lakeshore, or place fencing or other barriers between the lakeshore and surrounding grasslands.
- Plant dense hedges or erect fencing near lakeshore areas to reduce access to your lawn

• Check property frequently for nest building activity in the spring, and remove any nesting materials found



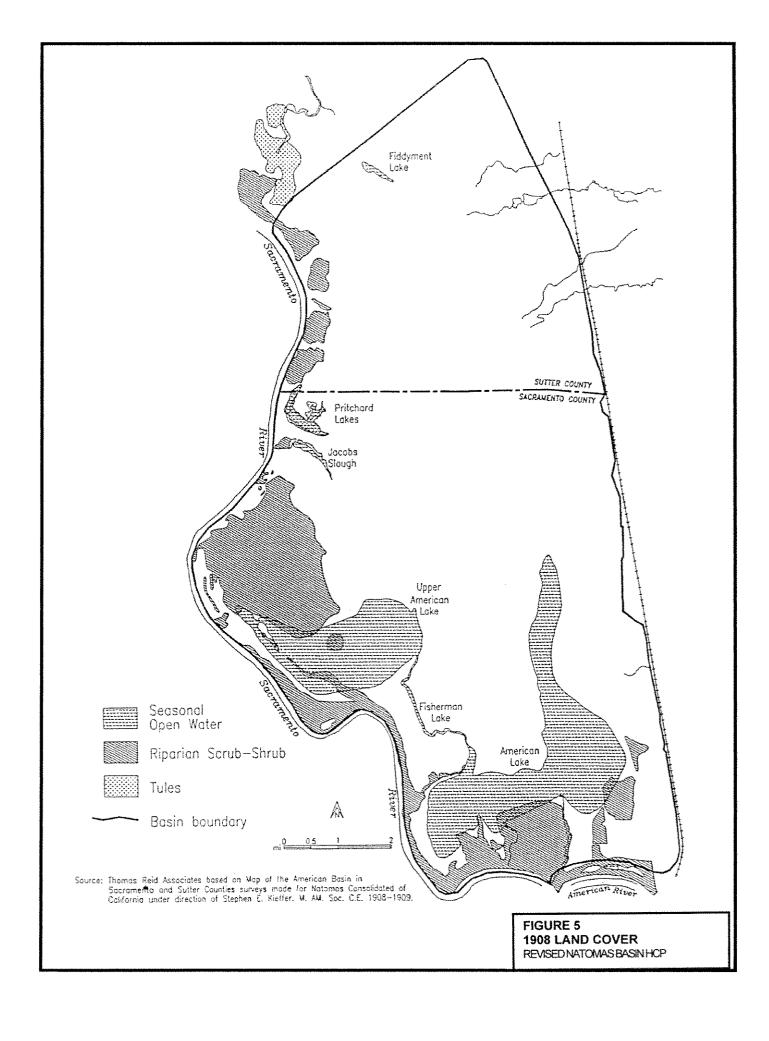
## 5.0 CONCLUSION

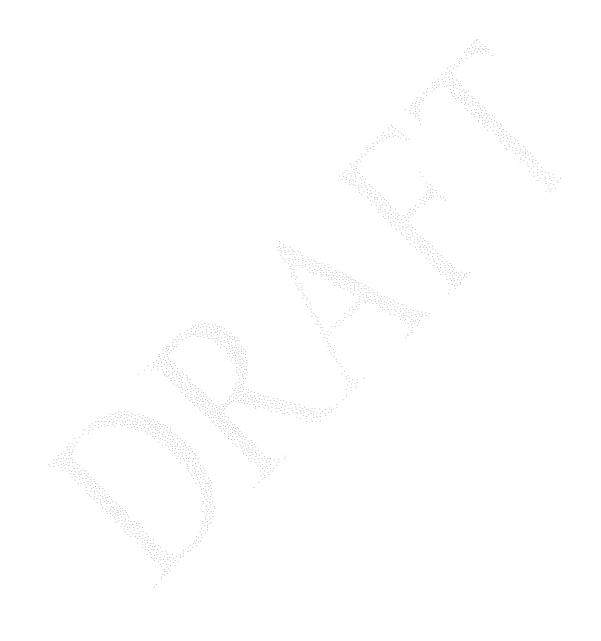
In conclusion, the results of this study indicate that winter rice fields in the Natomas Basin attract a greater number of birds that pose a risk to aircraft than do urban lakes in the Natomas Basin. Although the urban lakes observed supported a greater quantity of Canada geese (a high-risk species for aircraft strikes) than rice fields, the low numbers of these geese found at urban lakes indicate that the overall degree of hazard presented by urban lakes is lower than rice fields. While Canada goose populations are believed to be increasing in the coterminous United States and therefore could pose a greater future risk, a number of design and management measures can be implemented at urban lakes to minimize attractants. The data suggests that replacement of flooded agriculture in the Natomas Basin with urban lakes is expected to reduce risk of aircraft strikes at the Sacramento International Airport.

- Brouder, S. M. and J. E. Hill. 1995. Winter Flooding of Ricelands Provides Waterfowl Habitat. California Agriculture, 49, pp. 58.
- City of Sacramento, Sutter County, and Natomas Basin Conservancy. 2002. Draft Natomas Basin Habitat Conservation Plan. Prepared in association with Reclamation District 1000 and Natomas Central Mutual Water Company. Prepared for US Fish and Wildlife Service and California Department of Fish and Game. July 2002.
- Cleary, E.C., R.A. Dolbeer, and S.E. Wright. 2003. Federal Aviation Administration National Wildlife Strike Database Serial Report Number 9.
- Colwell, MA; Taft, OW. 2000. Waterbird Communities in Managed Wetlands of Varying Water Depth. Waterbirds. Vol. 23, no. 1, pp. 45-55.
- Ducks Unlimited, Inc. 1995a. Wildlife Resources of the Central Valley, California Birds Part II: Winter Residents and Transients.
- Ducks Unlimited, Inc. 1995b. Enhancing Agricultural Fields for Waterfowl.
- Federal Aviation Administration. 2000. Airport Wildlife Management: Most Hazardous Species. Airport Wildlife Management Bulletin #26 Spring, 2000
- Hinds, N.E.A. 1952. Evolution of the California Landscape. California Division of Mines Bulletin No. 158, 240 pp.
- Howe et al. (Howe, R.W., G.J. Niemi, S.J. Lewis, and D.A. Welsh. 1997. A standard method for monitoring songbird populations in the Great Lakes Region. Passenger Pigeon 59(3):183-194.).
- Larson, M. 2003. "Airport's aim: Say 'bye-bye' to the birdies." Sacramento Business Journal. August 15.

- Ralph, C.J., G.R. Geupel, P. Pyle, P.T. Martin, and D.F. DeSante. 1993. Handbook of field methods for monitoring landbirds. Gen. Tech. Rep. PSW-GTR-144. Albany, CA:
   Pacific Southwest Research Station, Forest Service, U.S. Department of Agriculture; 41pp.
- USFWS 2005. Final Environmental Impact Statement, Resident Canada Goose Management. USFWS Division of Migratory Bird Management.
- US Fish and Wildlife Service. 2003 Intra-Service Biological and Conference Opinion on Issuance of a Section 10(a)(1)(B) Incidental Take Permit to the City of Sacramento and Sutter County for Urban Development in the Natomas Basin, Sacramento and Sutter Counties, California. June 24. #1-1-03-F-0225.
- Wildlife Services 2004. FY 2003 Accomplishments under the Government Performance and Results Act. USDA
- Wildlife Habitat Management Institute. 2000, July. Fish and Wildlife Habitat Leaflet, Number 17, Shorebirds.

# Appendix A – 1908 Land Cover





|         |        | Natomas Man-made Wa                     | terbird Survey Poin         | t Counts                               |                       |
|---------|--------|---|-----------------------------|--|-----------------------|
| Survey# | Date   | Survey Point                            | Species Detected            | Number                                 | Total per Point Count |
| 1       | 2-Jan  | East side of Northborough lake          | Mallard                     | 8                                      | 21                    |
|         |        |   | Canada Goose<br>Green Heron | 9<br>4                                 |                       |
| 2       | 2-Jan  | West side of Northborough lake          | Mallard                     | 12                                     | 26                    |
| •       |        | 110000000000000000000000000000000000000 | Canada Goose                | 12                                     | 2.0                   |
|         |        |   | Common Grebe                | 2                                      |                       |
| 3       | 2-Jan  | West side of Gateway lake               |                             | ······································ | 0                     |
| 4       | 2-Jan  | East side of Gateway lake               |                             |  | 0                     |
| 5       | 2-Jan  | Alleghany lake                          | Canada Goose                | 23                                     | 37                    |
| •       | 04     | , and griderity reason                  | Maliard                     | 13                                     | <i>3.</i>             |
|         |        |   | Western Grebe               | 1                                      |                       |
| 6       | 4-Jan  | East side of Northborough lake          | Mallard                     | 8                                      | 32                    |
|         |        | •                                       | Canada Goose                | 16                                     |                       |
|         |        |   | American Coot               | 6                                      |                       |
|         |        |   | Green Heron                 | 2                                      |                       |
| 7       | 4-Jan  | West side of Northborough lake          | Maliard                     | 5                                      | 8                     |
|         |        |   | Common Grebe                | 2                                      |                       |
|         |        |   | Common Merganser            | 1                                      |                       |
| 8       | 4-Jan  | West side of Gateway lake               | Common Grebe                | 1                                      | 1                     |
| 9       | 4-Jan  | East side of Gateway lake               |                             |  | 0                     |
| 10      | 4-Jan  | Alleghany lake                          | Mallard                     | 11                                     | 29                    |
| 10      | 4-5011 | rategrially lance                       | Canada Goose                | 15                                     | 29                    |
|         |        |   | Great Blue Heron            | 1                                      |                       |
|         |        |   | Common Merganser            | 1                                      |                       |
|         |        |   | Green Heron                 | 1                                      |                       |
| 11      | 7-Jan  | East side of Northborough lake          | Mallard                     | 9                                      | 17                    |
|         |        |   | Canada Goose                | 8                                      |                       |
| 12      | 7-Jan  | West side of Northborough lake          | Mallard                     | 8                                      | 10                    |
| 12      | roals  | West side of Morthborodgi take          | Canada Goose                | 2                                      | 10                    |
| 13      | 7-Jan  | West side of Gateway lake               | Common Grebe                | 1                                      | 1                     |
|         |        |   |                             |  |                       |
| 14      | 7-Jan  | East side of Gateway lake               |                             |  | 0                     |
| 15      | 7-Jan  | Alleghany lake                          | Mallard                     | 16                                     | 33                    |
|         | . Jan  | · moderness mass                        | Canada Goose                | 16                                     | 50                    |
|         |        |   | Western Grebe               | 1                                      |                       |
| 16      | 8-Jan  | East side of Northborough lake          | Mallard                     | 7                                      | 10                    |
|         |        | _                                       | Great Blue Heron            | 1                                      |                       |
|         |        |   | Green Heron                 | 2                                      |                       |
| 17      | 8-Jan  | West side of Northborough lake          | Mallard                     | 11                                     | 20                    |
|         |        | _                                       | Unknown Gull Species        | 8                                      |                       |
|         |        |   | Western Grebe               | 1                                      |                       |

| 18 | 8-Jan    | West side of Gateway lake                           |                                  |         | 0     |
|----|----------|---|----------------------------------|---------|-------|
| 19 | 8-Jan    | East side of Gateway lake                           |                                  |         | 0     |
| 20 | 8-Jan    | Alleghany lake                                      | Mallard                          | 8       | 22    |
|    |          | <i>• .</i>  | Canada Goose                     | 12      |       |
|    |          |   | Common Grebe                     | 2       |       |
| 21 | 10-Jan   | East side of Northborough lake                      | Maliard                          | 22      | 23    |
| _; | 10-0411  | Last side of Moletoorough take                      | Common Grebe                     | 1       | in V  |
| 22 | 10-Jan   | West side of Northborough lake                      | Mallard                          | 4       | 10    |
|    |          |   | Common Grebe                     | 3       |       |
|    |          |   | Western Grebe                    | 1       |       |
|    |          |   | Great Egret                      | 2       |       |
| 23 | 10-Jan   | West side of Gateway lake                           | Unknown Gull Species             | 5       | 6     |
|    |          | •   | Common Grebe                     | 1       |       |
| 24 | 10-Jan   | East side of Gateway lake                           |                                  |         | 0     |
|    | 10 0001  | more order of overlent deliv                        |                                  |         | _     |
| 25 | 10-Jan   | Alleghany lake                                      | Mallard                          | 9       | 28    |
|    |          | g,  | Common Merganser                 | 18      | ==    |
|    |          |   | Common Grebe                     | 1       |       |
| 26 | 11-Jan   | East side of Northborough lake                      | Mallard                          | 6       | 13    |
|    | , , Jun  | more access on chart of specific personal is saying | Great Blue Heron                 | 1       |       |
|    |          |   | Common Merganser                 | 2       |       |
|    |          |   | Green Heron                      | 4       |       |
| 27 | 11-Jan   | West side of Northborough lake                      | Maliard                          | 12      | 26    |
|    | i i ouri | Troot side of troid borough take                    | Canada Goose                     | 14      | 20    |
|    |          |   |                                  |         |       |
| 28 | 11-Jan   | West side of Gateway lake                           |                                  |         | 0     |
| 29 | 11-Jan   | East side of Gateway lake                           |                                  |         | 0     |
| 30 | 11-Jan   | Alleghany lake                                      | Green Heron                      | 1       | 2     |
|    |          | <b>,</b>  | Common Grebe                     | 1       | _     |
| 31 | 13-Jan   | East side of Northborough lake                      | Great Egret                      | 2       | 28    |
|    |          | •   | Canada Goose                     | 18      |       |
|    |          |   | Mallard                          | 8       |       |
| 32 | 13-Jan   | West side of Northborough lake                      | Common Grebe                     | 2       | 12    |
|    |          | -   | Mallard                          | 10      |       |
| 33 | 13-Jan   | West side of Gateway lake                           |                                  |         | 0     |
|    |          |   |                                  |         |       |
| 34 | 13-Jan   | East side of Gateway lake                           |                                  |         | 0     |
|    |          |   |                                  |         |       |
| 35 | 13-Jan   | Alleghany lake                                      | Mallard<br>Canada Goose          | 6<br>18 | 32    |
|    |          |   | Canada Goose<br>Common Merganser | 10<br>8 |       |
|    |          |   | Common Mergansel                 | U       |       |
| 36 | 14-Jan   | East side of Northborough lake                      | Mallard                          | 14      | 17    |
|    |          |   | Common Grebe                     | 2       | • • • |
|    |          |   | Great Blue Heron                 | 1       |       |
|    |          |   |                                  |         |       |
| 37 | 14-Jan   | West side of Northborough lake                      | Maliard                          | 8       | 20    |
| 37 | 14-Jan   | West side of Northborough lake                      | Mallard<br>Canada Goose          | 8<br>10 | 20    |

| 38 | 14-Jan | West side of Gateway lake      |  |        | 0  |
|----|--------|--------------------------------|--|--------|----|
| 39 | 14-Jan | East side of Gateway lake      |  |        | 0  |
| 40 | 14-Jan | Alleghany lake                 | Canada Goose   | 14     | 15 |
|    |        |                                | Green Heron  | 1      |    |
| 41 | 16-Jan | East side of Northborough lake | Canada Goose   | 12     | 20 |
|    |        |                                | Mallard  | 8      |    |
| 42 | 16-Jan | West side of Northborough lake | Canada Goose   | 8      | 11 |
|    |        |                                | Great Blue Heron<br>Green Heron  | 1<br>2 |    |
|    |        |                                |  |        |    |
| 43 | 16-Jan | West side of Gateway lake      | Common Grebe   | 1<br>9 | 10 |
|    |        |                                | Unknown Gull Species   | 9      |    |
| 44 | 16-Jan | East side of Gateway lake      |  |        | 0  |
| 45 | 16-Jan | Alleghany lake                 | Maliard  | 12     | 15 |
|    |        |                                | Green Heron  | 1      |    |
|    |        |                                | Common Grebe   | 2      |    |
| 46 | 17-Jan | East side of Northborough lake | Western Grebe  | 1      | 17 |
|    |        |                                | Canada Goose   | 16     |    |
| 47 | 17-Jan | West side of Northborough lake | Mallard  | 14     | 25 |
|    |        |                                | Canada Goose   | 8      |    |
|    |        |                                | Great Blue Heron<br>Common Grebe   | 1<br>2 |    |
| 48 | 17-Jan | West side of Gateway lake      |  |        | 0  |
| 49 | 17-Jan | East side of Gateway lake      | ant-summer and a second second second second second second second second second second second second second se |        | 0  |
| 50 | 17-Jan | Alleghany lake                 | Mallard<br>Common Grebe  | 8<br>1 | 9  |

| Natomas Rice Field Waterbird Survey Point Counts |         |   |  |                     |                      |  |  |
|--|---------|---|--|---------------------|----------------------|--|--|
| irvey#   | Date    | Survey Point                                      | Species Detected                                 | Number              | Total per Point Cour |  |  |
| 1  | 2-Jan   | Sankey Rd., half way between Pacific and E. levee | Black-necked stilt                               | 16                  | 64                   |  |  |
|  |         |   | Unknown Gull Species                             | 1<br>39             |                      |  |  |
|  |         |   | Mallard<br>Northern Pintail                      | 3 <del>9</del><br>1 |                      |  |  |
|  |         |   | Greenwing Teal                                   | 2                   |                      |  |  |
|  |         |   | Greater Yellow leg                               | 4                   |                      |  |  |
|  |         |   | Great Blue Heron                                 | 1                   |                      |  |  |
| 2  | 2-Jan   | Levee Rd., Dewit Farms                            | American Coot                                    | 250                 | 707                  |  |  |
|  |         |   | Unknown Gull Species                             | 57                  |                      |  |  |
|  |         |   | Northern Pintail                                 | 360                 |                      |  |  |
|  |         |   | Mallard<br>Greenwing Teal                        | 8<br>32             |                      |  |  |
|  |         | Clouds Dd. Marsachad are such aids of sead        |  |                     | neo                  |  |  |
| 3  | 2-Jan   | Elverta Rd., Near shed on south side of road      | Northern Pintail<br>Unknown Gull Species         | 950<br>18           | 968                  |  |  |
| 4  | 2-Jan   | Elverta Rd., 200 Meters west of last point        | Northern Pintail                                 | 95                  | 221                  |  |  |
|  |         |   | Unknown Gull Species                             | 126                 |                      |  |  |
| 5  | 2-jan   | Elverta Rd., 200 Meters west of last point        | Northern Pintail                                 | 76                  | 102                  |  |  |
|  |         |   | Northern Shoveler                                | 26                  |                      |  |  |
| 6  | 2√Jan   | Elverta Rd., 200 Meters west of last point        | American Coot                                    | 1000                | 2652                 |  |  |
|  |         |   | White-fronted goose                              | 750                 |                      |  |  |
|  |         |   | Northern Pintail                                 | 900                 |                      |  |  |
|  |         |   | Great Egret                                      | 2                   |                      |  |  |
| 7  | 2-Jan   | Elverta Rd., 200 Meters west of last point        | American Coot                                    | 95                  | 98                   |  |  |
|  |         |   | Double-crested Cormorant                         | 3                   |                      |  |  |
| 8  | 2-Jan   | Elverta Rd., 200 meters west of last point        | Common Grebe                                     | 1                   | 86                   |  |  |
|  |         |   | Unknown Gull Species                             | 82                  |                      |  |  |
|  |         |   | Curlew   | 3                   |                      |  |  |
| 9  | 2-Jan   | Eiverta Rd., 200 Meters west of last point        | Unknown Gull Species                             | 8                   | 140                  |  |  |
|  |         |   | Great Egret                                      | 1                   |                      |  |  |
|  |         |   | Northern Pintail Double-crested Cormorant        | 127<br>4            |                      |  |  |
| 10   | 2-Jan   | Elverta Rd., 200 Meters west of last point        | Great Egret                                      | 4                   | 4                    |  |  |
|  | ~~~~~   |   |  |                     |                      |  |  |
| 11   | 2-Jan   | Elverta Rd., 200 Meters west of last point        | Great Egret<br>Curlew                            | 1<br>47             | 178                  |  |  |
|  |         |   | Unknown Gull Species                             | 130                 |                      |  |  |
| 12   | 2-Jan   | Elverta Rd., 200 Meters west of last point        | Great Blue Heron                                 | 1                   | 1                    |  |  |
| 13   | 4-Jan   | Sankey Rd., half way between Pacific and E. levee | White-fronted Goose                              | 250                 | 451                  |  |  |
| 1.0  | 77-J@11 | Comey Mu., non may be meet if acide and E. 18966  | Northern Pintail                                 | 120                 | ועד                  |  |  |
|  |         |   | Black-necked Stilt                               | 32                  |                      |  |  |
|  |         |   | Unknown Gull Species                             | 49                  |                      |  |  |
| 14   | 4-Jan   | Levee Rd., Dewit Farms                            | American Coot                                    | 300                 | 487                  |  |  |
| 1-4  | 4-1211  | Levee No., Dewa Faillis                           | Northern Pintail                                 | 180                 | 401                  |  |  |
|  |         |   | Great Blue Heron                                 | 1                   |                      |  |  |
|  |         |   | Great Egret                                      | 5                   |                      |  |  |
|  |         |   | Common Grebe                                     | 1                   |                      |  |  |
| 15   | 4-Jan   | Elverta Rd., Near shed on south side of road      | Northern Pintail                                 | 83                  | 117                  |  |  |
|  |         |   | Great Egret                                      | 2                   |                      |  |  |
|  |         |   | Northern Shoveler<br>Mallard                     | 26<br>6             |                      |  |  |
|  | 4.      | Di Books  |  |                     | 2.1                  |  |  |
| 16   | 4-Jan   | Elverta Rd., 200 Meters west of last point        | Unknown Gull Species<br>Double-crested Cormorant | 12<br>2             | 14                   |  |  |
|  |         |   |  |                     |                      |  |  |
| 17   | 4-Jan   | Elverta Rd., 200 Meters west of last point        | Northern Pintail                                 | 135                 | 257                  |  |  |
|  |         |   | American Coot<br>American Wigeon                 | 78<br>44            |                      |  |  |
| 10   | A 1     | Chrosin Dd. 200 Males and of last as Co.          | American Coot                                    | 67                  | 76                   |  |  |
| 18   | 4-Jan   | Elverta Rd., 200 Meters west of last point        | American Coot<br>Great Egret                     | 6 <i>1</i><br>9     | (0                   |  |  |

| 19       |                |  |  |   |           |
|----------|----------------|--|--|---|-----------|
|          | 4-Jan          | Elverta Rd., 200 Meters west of last point   | Great Blue Heron   | 1   | 1         |
| 20       | 4-Jan          | Elverta Rd., 200 Meters west of last point   | Mallard  | 22  | 123       |
| 4-0      | , ,            | Errored For the State of the Control | American Wigeon  | 44  |           |
|          |                |  |  | 56  |           |
|          |                |  | American Coot  |   |           |
|          |                |  | Common Grebe   | 1   |           |
| 21       | 4-Jan          | Elverta Rd., 200 Meters west of last point   | Curlew   | 47  | 68        |
|          |                |  | Snowy Egret  | 21  |           |
| 22       | 4-Jan          | Elverta Rd., 200 Meters west of last point   | Northern Pintail   | 98  | 134       |
|          |                |  | Northern Shoveler  | 17  |           |
|          |                |  | American Coot  | 19  |           |
| 23       | 4-Jan          | Elverta Rd., 200 Meters west of last point   | Unknown Gull Species   | 39  | 70        |
|          |                |  | Curlew   | 31  |           |
| 24       | 4-Jan          | Elverta Rd., 200 Meters west of last point   | Great Blue Heron   | 1   | 4         |
|          |                |  | Common Grebe   | 2   |           |
|          |                |  | Double-crested Cormorant   | 1   |           |
| 25       | 7-Jan          | Sankey Rd., half way between Pacific and E. levee  | Unknown Gull Species   | 31  | 56        |
| 2.9      | i "Jai!        | Odenicy 134, 11dn 144y Dollectit F done and E. levee   |  | 19  | JU        |
|          |                |  | Phallarope   |   |           |
|          |                |  | Maliard  | 6   |           |
| 26       | 7-Jan          | Levee Rd., Dewit Farms   | American Coot  | 400   | 496       |
|          |                |  | Northern Pintail   | 92  |           |
|          |                |  | Mallard  | 4   |           |
| 27       | 7-Jan          | Elverta Rd., Near shed on south side of road   | White-fronted Goose  | 180   | 630       |
|          |                |  | Snow Goose   | 250   |           |
|          |                |  | Northern Pintail   | 200   |           |
| 28       | 7-Jan          | Elverta Rd., 200 Meters west of last point   | Great Egret  | 9   | 43        |
|          |                | ,  | Great Blue Heron   | 1   |           |
|          |                |  | Northern Pintail   | 33  |           |
| 29       | 7-Jan          | Elverta Rd., 200 Meters west of last point   | American Coot  | 48  | 48        |
|          |                |  |  |   |           |
| 30       | 7-Jan          | Elverta Rd., 200 Meters west of last point   | Snowy Egret  | 22  | 23        |
|          |                |  | Common Grebe   | 1   |           |
| 31       | 7-Jan          | Elverta Rd., 200 Meters west of last point   | White-faced Ibis   | 33  | 114       |
|          |                |  | Black-necked Stilt   | 14  |           |
|          |                |  | American Coot  | 67  |           |
| 32       | 7-Jan          | Elverta Rd., 200 Meters west of last point   | Unknown Guli Species   | 48  | 91        |
|          |                |  | Curlew   | 31  |           |
|          |                |  | Great Egret  | 12  |           |
| 33       | 7-Jan          | Elverta Rd., 200 Meters west of last point   | Great Egret  | 7   | 42        |
|          |                |  | Snowy Egret  |   |           |
|          |                |  | Showy Egiet  | 15  |           |
|          |                |  |  |   |           |
|          |                |  | Great Blue Heron<br>Unknown Gull Species   | 15<br>2<br>18   |           |
| 34       | ** from        | ·  | Great Blue Heron<br>Unknown Gull Species   | 2<br>18   | 106       |
| 34       | 7-Jan          | Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gulf Species Unknown Gulf Species   | 2<br>18<br>5  | 196       |
| 34       | 7-Jan          | ·  | Great Blue Heron Unknown Gull Species Unknown Gull Species Northern Pintail  | 2<br>18<br>5<br>130   | 196       |
| 34       | 7-Jan          | ·  | Great Blue Heron Unknown Gull Species Unknown Gull Species Northern Pintail American Wigeon  | 2<br>18<br>5<br>130<br>26   | 196       |
| 34       | 7-Jan          | ·  | Great Blue Heron Unknown Gull Species Unknown Gull Species Northern Pintail American Wigeon Mallard  | 2<br>18<br>5<br>130<br>26<br>12                                       | 196       |
|          | _              | Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species Unknown Gull Species Northern Pintail American Wigeon Mallard Northern Shoveler  | 2<br>18<br>5<br>130<br>28<br>12<br>23                                 |           |
| 34       | 7-Jan<br>7-Jan | ·  | Great Blue Heron Unknown Gull Species  Unknown Gull Species  Northern Pintail American Wigeon Mailard Northern Shoveler  Double-crested Cormorant  | 2<br>18<br>5<br>130<br>26<br>12<br>23                                 | 196<br>45 |
|          | _              | Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species  Unknown Gull Species Northern Pintail American Wigeon Mailard Northern Shoveler  Double-crested Cormorant Great Egret   | 2<br>18<br>5<br>130<br>26<br>12<br>23                                 |           |
|          | _              | Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species  Unknown Gull Species  Northern Pintail American Wigeon Mailard Northern Shoveler  Double-crested Cormorant  | 2<br>18<br>5<br>130<br>26<br>12<br>23                                 |           |
|          | _              | Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species  Unknown Gull Species  Northern Pintail American Wigeon Mallard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron   | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>11<br>33                |           |
| 35       | 7-Jan          | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species Unknown Gull Species Northern Pintail American Wigeon Mallard Northern Shoveler  Double-crested Cormorant Great Egret Curlew   | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>11<br>33                | 45        |
| 35<br>36 | 7-Jan<br>7-Jan | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species Unknown Gull Species Northern Pintail American Wigeon Mallard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron Unknown Gull Species  | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>1<br>11<br>33           | 45<br>7   |
| 35       | 7-Jan          | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species  Unknown Gull Species Northern Pintail American Wigeon Mallard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron Unknown Gull Species  White-fronted Goose  | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>11<br>33<br>1<br>6      | 45        |
| 35<br>36 | 7-Jan<br>7-Jan | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species Unknown Gull Species Northern Pintail American Wigeon Mailard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron Unknown Gull Species  White-fronted Goose Snow Goose  | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>11<br>33<br>1<br>6      | 45<br>7   |
| 35<br>36 | 7-Jan<br>7-Jan | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species  Unknown Gull Species Northern Pintail American Wigeon Mallard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron Unknown Gull Species  White-fronted Goose Snow Goose Mallard   | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>11<br>33<br>1<br>6      | 45<br>7   |
| 35<br>36 | 7-Jan<br>7-Jan | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species  Unknown Gull Species Northern Pintail American Wigeon Mallard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron Unknown Gull Species  White-fronted Goose Snow Goose Mallard Northern Pintail                                  | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>1<br>11<br>33<br>1<br>6 | 45<br>7   |
| 35<br>36 | 7-Jan<br>7-Jan | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species  Unknown Gull Species Northern Pintail American Wigeon Mailard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron Unknown Gull Species  White-fronted Goose Snow Goose Mailard Northern Pintail American Wigeon                  | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>11<br>33<br>1<br>6      | 45<br>7   |
| 35<br>36 | 7-Jan<br>7-Jan | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species Unknown Gull Species Northern Pintail American Wigeon Mallard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron Unknown Gull Species  White-fronted Goose Snow Goose Mallard Northern Pintail American Wigeon Green-winged Teal | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>11<br>33<br>1<br>6      | 45<br>7   |
| 35<br>36 | 7-Jan<br>7-Jan | Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point  Elverta Rd., 200 Meters west of last point   | Great Blue Heron Unknown Gull Species  Unknown Gull Species Northern Pintail American Wigeon Mailard Northern Shoveler  Double-crested Cormorant Great Egret Curlew  Great Blue Heron Unknown Gull Species  White-fronted Goose Snow Goose Mailard Northern Pintail American Wigeon                  | 2<br>18<br>5<br>130<br>26<br>12<br>23<br>1<br>11<br>33<br>1<br>6      | 45<br>7   |

| 38 | 8-Jan | Levee Rd., Dewit Farms                       | American Coot              | 123 | 231 |
|----|-------|--|----------------------------|-----|-----|
|    |       |  | Great Egret                | 4   |     |
|    |       |  | Northern Pintail           | 46  |     |
|    |       |  | Mallard                    | 8   |     |
|    |       |  | Western or Least Sandpiper | 50  |     |
| 39 | 8-Jan | Elverta Rd., Near shed on south side of road | Northern Pintail           | 97  | 220 |
|    |       |  | American Coot              | 43  |     |
|    |       |  | Western or Least Sandpiper | 80  |     |
| 40 | 8-Jan | Elverta Rd., 200 Meters west of last point   | Uknown Gull Species        | 6   | 8   |
|    |       |  | Great Blue Heron           | 2   |     |
| 41 | 8-Jan | Elverta Rd., 200 Meters west of last point   | Northern Pintail           | 61  | 61  |
| 42 | 8-Jan | Elverta Rd., 200 Meters west of last point   | American Coot              | 34  | 50  |
|    |       | •  | Snowy Egret                | 7   |     |
|    |       |  | Great Egret                | 9   |     |
| 43 | 8-Jan | Elverta Rd., 200 Meters west of last point   | Phallarope                 | 12  | 79  |
|    |       |  | Black-necked Stilt         | 8   |     |
|    |       |  | Great Blue Heron           | 1   |     |
|    |       |  | Unknown Gull Species       | 58  |     |
| 44 | 8-Jan | Elverta Rd., 200 Meters west of last point   | Mallard                    | 6   | 30  |
|    |       |  | American Coot              | 24  |     |
| 45 | 8-Jan | Elverta Rd., 200 Meters west of last point   | Northern Pintail           | 33  | 44  |
|    |       |  | Mailard                    | 2   |     |
|    |       |  | Northern Shoveler          | 9   |     |
| 46 | 8-Jan | Elverta Rd., 200 Meters west of last point   | American Coot              | 11  | 35  |
|    |       |  | Great Blue Heron           | 1   |     |
|    |       |  | Common Grebe               | 2   |     |
|    |       |  | White-faced Ibis           | 21  |     |
| 47 | 8-Jan | Elverta Rd., 200 Meters west of last point   | Curlew                     | 36  | 66  |
|    |       |  | Snowy Egret                | 16  |     |
|    |       |  | Great Egret                | 8   |     |
|    |       |  | Unknown Gull Species       | 6   |     |
| 48 | 8-Jan | Elverta Rd., 200 Meters west of last point   | Western or Least Sandpiper | 80  | 105 |
|    |       |  | Curlew                     | 25  |     |



**LESA MODELING** 

| Soil Name                        | Map Symbol | Storie<br>Index | Acres | %               | Nonirrigtaed capability | Irrigated<br>capability       |
|----------------------------------|------------|-----------------|-------|-----------------|-------------------------|-------------------------------|
|                                  |            | Grade           |       |                 | classification          | classification classification |
| Clear Lake clay                  | 115        | 4               | 421.2 | 421.2 72.21% 3S | 38                      | 2S                            |
| Jacktone clay                    | 127        | 8               | 75.54 | 75.54 12.95% 3S | 38                      | 38                            |
| San Joaquin silt Ioam            | 137        | 5               | 9.61  | 1.65% 3S        | 38                      | 38                            |
| Consumnes silt loam              | 161        | 4               | 13.45 | 2.31% 3W        | 3W                      | 2W                            |
| Durixeralfs                      | 213        | 4               | 7.61  | 1.30% 48        | 4S                      | 4S                            |
| San Joaquin -Durixeralfs complex | 216        | 4               | 45.27 | 7.76% 4S        | 4S                      | unknown                       |
| San Joaquin-Xerarents complex    | 221        | 4               | 10.63 | 1.82% 3S        | 38                      | 38                            |
| TOTAL ACREAGE                    |            |                 | 583.4 |                 |                         |                               |

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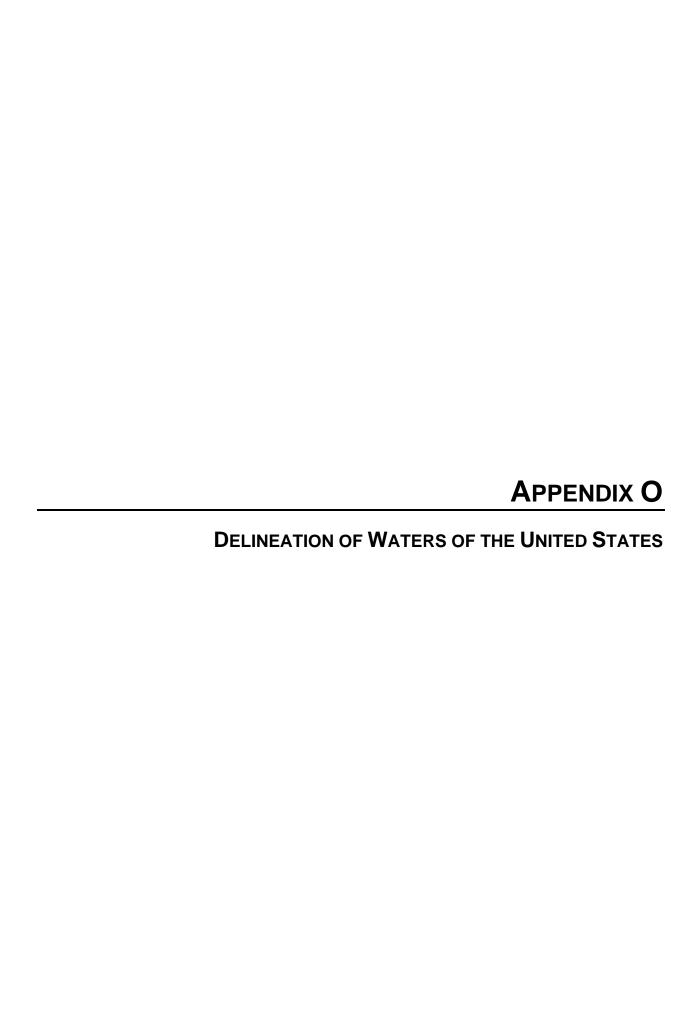
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|----------------------------------|---------------|------------|----|--------|--------|---|--------------|
| Soil Map Unit                    | בוסלפרו שכופס | ion odo i  |    | Rating |        |   | Score        |
| Clear Lake clay                  | 421.24        | 72.21%     |    | 09     |        | 4 | 2.89         |
| Jacktone clay                    | 75.54         | 12.95%     |    | 09     |        |   | 0.26         |
| San Joaquin silt Ioam            | 9.61          | 1.65%      |    | 9      |        | 5 | 0.08         |
| Consumnes silt loam              | 13.45         | 2.31%      |    | 09     |        | 4 | 60:0         |
| Durixeralfs                      | 7.61          | 1.30%      | 4S | 40     | 0.5218 | 4 | 0.05         |
| San Joaquin -Durixeralfs complex | 45.27         | 7.76%      |    | 40     |        | 4 | 0.31         |
| San Joaquin-Xerarents complex    | 10.63         | 1.82%      | 38 | 90     | 1.0933 | 4 | 0.07         |
|                                  | 583.35        | 100.00%    |    |        | 58.187 |   | 3.76         |

\* Based on nonirrigated capability classification

| Site Assessment Worksheet 1 | et 1                |                      | Site Ass           | Site Assessment Worksheet 2 | orksheet          | 8   | :                    |
|-----------------------------|---------------------|----------------------|--------------------|-----------------------------|-------------------|---|----------------------|
| LCC<br>Class I-II           | LCC Class LCC Class | LCC Class<br>IV-VIII | Project<br>Portion | Water<br>Resource           | Project<br>Area % | Project Water Project Water Portion Resource Area % v Score | Weighted Availabilit |
|                             | 421.24              |                      | -                  | irrigated 100%              | 100%              | 06  |                      |
|                             | 75.54               |                      | 2                  |                             |                   |   |                      |
|                             | 9.61                |                      | က                  |                             |                   |   |                      |
|                             | 13.45               |                      | 4                  |                             |                   |   |                      |
|                             |                     | 7.61                 | 5                  |                             |                   |   |                      |
|                             |                     | 45.27                | 9                  |                             |                   |   |                      |
|                             | 10.63               |                      |                    | Total Wa                    | iter Reso         | Total Water Resource Score                                  | 06                   |
| Total Acres                 | 530.47              | 52.88                |                    |                             |                   |   |                      |
| Project Size Scores         | 100                 | 20                   |                    |                             |                   |   |                      |
| Highest Project Size Score  | 100                 |                      |                    |                             |                   |   |                      |

| Size Scc      | roject Size Scoring Table |           |        |            |          |
|---------------|---------------------------|-----------|--------|------------|----------|
| Class I or II | or ==                     | Class III | ≡ s    | Class IV o | or Lower |
| age           | Points                    | Acreage   | Points | Acreage    | Points   |
| 8             | 100                       | >160      | 100    | >320       | 100      |
| 79            | 06                        | 120-159   | 06     | 240-319    | 80       |
| 59            | 80                        | 80-119    | 80     | 160-239    | 09       |
| 39            | 20                        | 62-09     | 20     | 100-159 40 | 40       |
| 10-19         | 30                        | 40-59     | 90     | 40-99      | 20       |
| ×             | 0                         | 20-39     | 30     | 40<        | 0        |
|               |                           | 10-19     | 10     |            |          |
|               |                           | 10<       | 0      |            |          |
|               |                           |           |        |            |          |

|          |               |            |                                |              |          |            |              |                             |                               |                         |      | FINAL LESA SCORE |  |
|----------|---------------|------------|--------------------------------|--------------|----------|------------|--------------|-----------------------------|-------------------------------|-------------------------|------|------------------|--|
| Weighted | Factor Scores |            | 14.55                          | 0.94         | 15.49    |            | 15           | 13.5                        | 1.5                           | 0                       | 30   | 45.49            |  |
| Factor   | Weight        |            | 0.25                           | 0.25         | 0.50     |            | 0.15         | 0.15                        | 0.15                          | 0.05                    | 0.50 |                  |  |
| Factor   | Scores        |            | 58.19                          | 3.76         |          |            | 100          | 06                          | 10                            | 0                       |      |                  |  |
|          |               | LE Factors | Land Capability Classification | Storie Index | LE Total | SA Factors | Project Size | Water Resource Availability | Surrounding Agricultural Land | Protected Resource Land |      |                  |  |



## **Delineation of Waters of the United States**

Greenbriar ±569-Acre Site and Associated Utility Alignments Sacramento County, California

Prepared for: U.S. Army Corps of Engineers

Contracted By: AKT Development Corporation

November 3, 2005



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## 1.0 INTRODUCTION

The purpose of this document is to present the results of a formal delineation of jurisdictional waters of the United States, including wetlands, on the  $\pm 569$ -acre Greenbriar site and utility alignments located in northwestern Sacramento County, California (**Figure 1**).

This report presents the results of Foothill Associates review of available literature, aerial photographs, soil surveys, and fieldwork on the site. These results are summarized to depict jurisdictional waters of the United States following the technical guidelines provided in the 1987 U.S. Army Corps of Engineers Wetlands Delineation Manual for identifying wetlands and distinguishing them from aquatic habitats and other nonwetlands.

The delineation methodology is described in this report, followed by the results of the delineation. Details regarding soils, topography, hydrology, and vegetation are summarized and routine wetland determination data forms are provided in **Appendix B**. A detailed delineation map illustrates waters of the U.S. on the site (**Figure 3**).

### 2.0 REGULATORY BACKGROUND

The U.S. Army Corps of Engineers (Corps) regulates discharge of dredged or fill material into waters of the United States under Section 404 of the Clean Water Act (CWA). "Discharges of fill material" is defined as the addition of fill material into waters of the U.S., including, but not limited to the following: placement of fill that is necessary for the construction of any structure, or impoundment requiring rock, sand, dirt, or other material for its construction; site-development fills for recreational, industrial, commercial, residential, and other uses; causeways or road fills; fill for intake and outfall pipes and subaqueous utility lines [33 C.F.R. §328.2(f)]. In addition, Section 401 of the CWA (33 U.S.C. 1341) requires any applicant for a federal license or permit to conduct any activity that may result in a discharge of a pollutant into waters of the United States to obtain a certification that the discharge will comply with the applicable effluent limitations and water quality standards.

### 2.1 Waters of the United States

Waters of the U.S. include a wide range of features such as lakes, rivers, streams (including intermittent streams), mudflats, sandflats, wetlands, sloughs and wet meadows as well as tributaries to such features. The term tributary generally refers to a feature which contributes its waters to another feature (example: a stream that flows into a larger river is a tributary to that river). Boundaries between jurisdictional waters and uplands are determined in a variety of ways depending on which type of water is present. Methods for delineating wetlands and non-tidal waters are described below.

Wetlands are defined as "those areas that are inundated or saturated by surface or groundwater at a frequency and duration sufficient to support and under normal circumstances do support, a prevalence of vegetation typically adapted for life in saturated soil conditions" [33 C.F.R. §328.3(b)]. Presently, to be a wetland, a site must exhibit positive indicators of three wetland criteria: hydrophytic vegetation, hydric soils, and wetland hydrology existing under the "normal circumstances" for the site.

The lateral extent of non-tidal waters is determined by delineating the ordinary high water mark (OHWM) [33 C.F.R. §328.4(c)(1)]. The OHWM is defined by the Corps as "that line on shore established by the fluctuations of water and indicated by physical character of the soil, destruction of terrestrial vegetation, the presence of litter and debris, or other appropriate means that consider the characteristics of the surrounding areas" [33 C.F.R. §328.3(e)].

#### 3.1 Site-Specific References

Available information pertaining to the natural resources of the region was reviewed. All references reviewed for this delineation are listed in Section 5.0. Pertinent site-specific reports and general references utilized concurrent with the delineation include the following:

- Environmental Laboratory. 1987. Corps of Engineers Wetlands Delineation Manual. U.S. Army Corps of Engineers Waterways Experiment Station. Vicksburg, MS;
- GretagMacbeth. 2000. Munsell Soil Color Charts. New Windsor, NY;
- Hickman, James C. 1993. The Jepson Manual: Higher Plants of California.
   University of California Press, Berkeley, CA;
- Reed, P.B., Jr. 1988. *National List of Plant Species That Occur in Wetlands: California (Region O)*; U.S. Fish & Wildlife Service;
- USDA, NRCS (Natural Resource Conservation Service). 1993. Soil Survey of Sacramento County, California. USDA, NRCS, in cooperation with the Regents of the University of California (Agricultural Experiment Station);
- USDA, NRCS. 2003. Field Indicators of Hydric Soils in the United States,
   Version 5.01. G.W. Hurt, P.M. Whited, and R.F. Pringle (Eds). USDA, NRCS in cooperation with the National Committee for Hydric Soils. Fort Worth, TX;
- USDA, NRCS (Natural Resource Conservation Service). 1937. Historic Aerial Photo Coverage of Sacramento County, California. USDA, NRCS;
- USDA, NRCS (Natural Resource Conservation Service). 1957. Historic Aerial Photo Coverage of Sacramento County, California. USDA, NRCS;
- U.S. Geological Survey. 1954. *Davis*, California. 7.5 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1905. *Davisville*, *California*. 15 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1967. *Taylor Monument, California*. 7.5 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1967. Photorevised 1975. Taylor Monument, California. 7.5 -minute series topographic quadrangle. U.S. Department of the Interior; and

 U.S. Geological Survey. 1967. Photorevised 1980. Taylor Monument, California. 7.5 -minute series topographic quadrangle. U.S. Department of the Interior.

#### 3.2 Research and Field Methodology

This delineation utilized the Corps 1987 three-parameter (vegetation, hydrology, and soils) methodology to delineate jurisdictional waters of the U.S., focusing specifically on jurisdictional wetlands. This methodology requires the collection of data on soils, vegetation, and hydrology at several locations to establish the jurisdictional boundary of wetlands. Additional methods to identify and delineate other waters of the U.S. (e.g. streams, drainages, lakes, etc.) were used as applicable.

A review of historic and current aerial photographs, topographic maps and soils survey data was conducted before delineating the site on December 28<sup>th</sup>, 2004 as well as concurrently with delineation work on January 4<sup>th</sup>, July 7<sup>th</sup>, August 15<sup>th</sup>, August 22<sup>nd</sup> and October 3<sup>rd</sup>, 2005. Wetland biologists visually inspected the entire site and collected data on vegetation and hydrology. Soils were also examined and correlations were developed between the three parameters to make wetland determinations. Specifically, data points were evaluated to determine the composition and identification of dominant plant species. The indicator status of all dominant plant species (as determined by the U.S. Fish and Wildlife Service National List of Plant Species that Occur in Wetlands: 1988 California (Region 0)) was applied and evaluated as part of the vegetation assessment portion of the wetland determination process. Additionally, immediate sub surface soils conditions were examined for hydric attributes or a lack thereof. Observations were made and recorded for both primary and secondary wetland hydrology indicators, if present. In addition to sampling representative wetland types, routine determination data points were collected within the interior portions of the site currently or historically used for agricultural activities in order to collect baseline data for all of the mapped soils types occurring on the site. The routine determination points were collected in January, July and August of 2005. The location of each data point is depicted in Figure 3 and corresponding routine wetland determination data forms are provided in **Appendix B**.

As part of the fieldwork, we also visually inspected several offsite areas to determine the surface hydrological connection between the ditches on the site. Several culverts and other water conveyance features were mapped during the delineation illustrated in **Figure 3**.

## 3.3 GPS Data Integration

Boundaries of wetlands and other waters of the U.S. within the site were surveyed and mapped with a Trimble GeoXT GPS (Global Positioning System) hand-held unit. This is a mapping-grade GPS unit capable of real-time differential correction and sub-meter accuracy. The GPS data were downloaded from the unit and differentially corrected utilizing Trimble Pathfinder Office software and appropriate base station data, and then converted to ESRI ® shape file format. Data are typically exported to the Geographic

Information System (GIS) software in the State Plane coordinate system (NAD 83) with units as "survey feet." Within the GIS, data are edited and linear features are built into polygons using recorded width information. All wetland shape files are merged to create a single wetland file with calculated acreages. These results are presented in **Figure 3**.

### 4.1 Study Area Description, Land Use

#### 4.1.1 Study Area Location

The ±569 acre site and associated utility alignments are located in northwestern Sacramento County, approximately two miles southeast of the Sacramento International Airport and two miles northeast of Sacramento River. The site is bound by Interstate 5 on the south, State Highways 70/99 on the east, and Elkhorn Boulevard on the north. The utility alignments include areas along the south edge of Elkhorn Boulevard, east to Natomas Boulevard and the east edge of the site, south along State Route 99. The site is bound on the west by rural residences and agricultural lands. The site is located within Townships 9 and 10 North, Range 4 East and occupies portions of sections 4 and 33 of the U.S.G.S. Taylor Monument 7.5' quadrangle map (**Figure 1**).

#### 4.1.2 Land Use

The site is currently in agricultural use, with dry farmed wheat. A portion of the site was in rice cultivation until 2002. A horse race track and an irrigated polo field were present in the northern portion of the site from approximately 1980 to the early 2000's. For several years the horse ranch subleased the northwest corner of the property to a highway construction company, who stored equipment there. For at least the last 20 years, the remainder of the property outside the horse ranch area has been in agricultural use (rice, sugar beets, wheat).

#### 4.1.3 Site History and Description

A review of historic aerial imagery indicates the site has been utilized for agricultural activities, mainly rice production, since 1937. The site was planted in rice as recently as 2002, according to review of aerial imagery. A conversation with the land manager confirmed that the site was planted with rice in 2003 and 2004, as well. In the 2005 growing season the site was planted with wheat (Johas, pers. comm.). At the cessation of this year's crop harvesting activities, the majority of the site was disced. Areas not disced within the site during the initial stage of the delineation include the following two locations: the northwestern portion of the site west of the equestrian track and north of ditch feature #14, west to the site boundary and continuing north to Elkhorn Boulevard; the northeastern portion of the site south of Elkhorn Boulevard and north and west of the ditch and canal segments labeled #13 and #21, respectively (Figure 3).

The natural hydrologic regime on the site has been altered to facilitate agricultural production processes since at least 1937 and is discussed in detail in section 4.2.4. The predominant features constructed on the site for water conveyance include ditches and canals. During past periods of rice cultivation, an extensive network of checks and berms

also existed on the site. These features were deconstructed in coincidence with the cessation of rice cultivating activities on the site which occurred as recently as 2004.

Soils on the site developed in an area that appears to have historically supported wetlands based on a review of the 1937 aerial photographs. Therefore, hydric soil indicators documented on the site may be the result of natural, historic conditions. However, the production of rice over a large portion of the site and over a long period of time has likely contributed to the current condition of soils on the site, potentially including the presence of secondary indicators of wetland hydrology and hydric soil indicators. Consequently, the soils may not be a reliable indicator of current conditions.

#### 4.2 Physical Features

#### 4.2.1 Soils

The Natural Resources Conservation Service (NRCS) has identified and mapped eight soils occurring on the site and associated utility alignments (Figure 2): Clear Lake clay, hardpan substratum, drained, 0 to 1 percent slopes, Cosumnes silt loam, partially drained, 0 to 2 percent slopes, Durixeralfs, 0 to 1 percent slopes, Jacktone clay, drained, 0 to 2 percent slopes, San Joaquin silt loam leveled, 0 to 1 percent slopes, San Joaquin-Durixeralfs complex, 0 to 1 percent slopes and San Joaquin-Xerarents complex, leveled, 0 to 1 percent slopes. General characteristics and properties associated with these soils are described below.

- Clear Lake clay, hardpan substratum, drained, 0 to 1 percent slopes: This deep to very deep artificially drained soil is located in basins between five to 30 feet above Mean Sea Level (MSL). A system of levees and large upstream dams has reduced the hazard of flooding. The construction of levees, drainage ditches and pumps has lowered the water table and altered the drainage of the soil. This soil formed from fine textured alluvium derived from mixed rock sources. Permeability is slow, available water capacity is moderate and runoff is very slow. This soil is subject to rare flooding and is typically used for irrigated crops such as rice, corn, tomatoes, sugar beets and wheat. Vegetation in uncultivated areas mainly consists of annual grasses and herbaceous species. The hydric soils list for Sacramento County identifies on type of hydric inclusion occurring within this soil type: Cosumnes, located on the low floodplain. The hydric soils list for Sacramento County also identifies one type of hydric component occurring within this soil type: Clearlake, located on basin floors.
- Cosumnes silt loam, partially drained, 0 to 2 percent slopes: This very deep, artificially drained soil is located on low floodplains at elevation between five to 20 feet above MSL. A system of levees and large upstream dams has reduced the hazard of flooding. Levees, open and closed drains and pumps have lowered the water table and altered the drainage of the soil. This soil formed in somewhat poorly drained alluvium derived from mixed rock sources. Permeability is slow, available water capacity is high and runoff is slow. This soil is subject to rare

flooding and is typically used for irrigated crops such as rice, corn, tomatoes, sugar beets and wheat. Vegetation in uncultivated areas mainly consists of annual grasses and herbaceous species. The hydric soils list for Sacramento County identifies three types of hydric inclusions occurring within this soil type: Clearlake, located on basin floors, Columbia, located on the low floodplain and Sailboat, located on the low floodplain. The hydric soils list for Sacramento County also identifies one type of hydric component occurring within this soil type: Cosumnes, located on the low floodplain.

- Durixeralfs, 0 to 1 percent slopes: This soil unit is a shallow or moderately deep, well drained, altered soil located on low terraces between 20-150 feet above MSL. Most or the entire original surface layer has been removed. The soils developed from alluvium derived from mixed granitic rocks. Slopes are plane due to artificial leveling. Water permeability is slow to very slow, available water capacity is very low or low and runoff is very slow. This soil unit is used for irrigated hay and pasture or for irrigated crops. Typically, vegetation in uncultivated areas within this soil unit consists of non-native annual grasses and herbaceous plant species. The hydric soils list for Sacramento County does not identify any hydric inclusions or components occurring within this soil unit.
- Jacktone clay, drained, 0 to 2 percent slopes: This moderately deep, artificially drained soil is located in high areas in basins between 10-25 feet above MSL. It is protected against flooding by a system of levees and large upstream dams. The construction of levees, drainage ditches and pumps has lowered the water table and altered the drainage of the soil. This soil formed in alluvium derived from mixed rock sources. Permeability is slow, available water capacity is moderate and runoff is very slow. This soil is subject to rare flooding. This soil is typically used for irrigated crops such as rice, barley, wheat and corn. Vegetation in uncultivated areas mainly consists of annual grasses and herbaceous species. The hydric soils list for Sacramento County identifies two types of hydric inclusions occurring within this soil type: Cosumnes, located on the low floodplain, and Clearlake, located on basin floors. The hydric soils list for Sacramento County also identifies one type of hydric component occurring within this soil type: Jacktone, located on basin rims.
- San Joaquin silt loam, leveled, 0 to 1 percent slopes: This soil unit is located on low terraces at an elevation of 20 to 125 feet above MSL. Slopes are plane due to land leveling processes. San Joaquin silt loam is a moderately deep, moderately well drained soil formed in alluvium derived from dominantly granitic rocks. Permeability is very slow, available water capacity is low and runoff is very slow. Vegetation typically found on this soil unit consists of non-native annual grasses and herbaceous plant species, and a few scattered native oaks (*Quercus* spp.). The hydric soils list for Sacramento County does not identify any hydric inclusions within this soil type.
- San Joaquin silt loam, 0 to 3 percent slopes: This soil unit is located on low terraces. San Joaquin silt loam is a moderately deep, moderately well drained soil

formed in alluvium derived from dominantly granitic rocks. Permeability is very slow, available water capacity is low and runoff is very slow. Vegetation typically found on this soil unit consists of non-native annual grasses and herbaceous plant species, and a few scattered native oaks (*Quercus* spp.). The hydric soils list for Sacramento County identifies one type of hydric inclusion occurring within this soil type: Galt, located within depressions.

- San Joaquin-Durixeralfs complex, 0 to 1 percent slopes: This soil complex is located on low terraces at elevations of 20 to 100 feet above MSL. Slopes are plane due to land leveling processes. The San Joaquin soil is a moderately deep, well drained soil formed in alluvium derived from granitic rock. Permeability is very slow, available water capacity is low and runoff is very slow. The Durixeralfs formed in alluvium derived from mixed granitic rocks and are shallow or moderately deep, well drained and altered. Permeability is slow or very slow in the Durixeralfs, available water capacity is very low or low and runoff is very slow. Vegetation typically associated with uncultivated portions of this soil complex is typically composed of annual grasses and herbaceous plant species. The hydric soils list for Sacramento County identifies one type of hydric inclusion occurring within this soil type: Galt, located within depressions.
- San Joaquin-Xerarents complex, leveled, 0 to 1 percent slopes: This soil complex is located on low terraces at elevations of 20 to 125 feet above MSL. Slopes are plane due to land leveling processes. The San Joaquin soil is a moderately deep, moderately well drained soil formed in alluvium derived from granitic rock. Permeability is very slow, available water capacity is low and runoff is very slow. The Xerarents are moderately deep to very deep, well drained and altered and formed in fill material mixed by leveling processes. The fill material is derived from mixed but predominantly granitic rock sources. Permeability is moderate to very slow in the Xerarents, available capacity is moderate or high and runoff is very slow. Prior to leveling, areas with these soils consisted of depressions and narrow channels along drainageways. Typically, areas with these soils are used for irrigated crop production. Vegetation associated with uncultivated portions of this soil complex is primarily composed of annual grasses and herbaceous plant species. The hydric soils list for Sacramento County identifies four types of hydric inclusions occurring within this soil type: Galt, located in depressions; Clearlake, located on basin floors; Columbia, located on low floodplains and Sailboat, located on low floodplains.

In summary, and according to the hydric soils list and soil survey for Sacramento County, the following hydric soil inclusions and/or components and the landform types they are associated with are listed as occurring within six of the eight soil types mapped by NRCS: Columbia hydric inclusions that are located on the low floodplain, Cosumnes hydric inclusions that are located on the low floodplain, Clearlake hydric inclusions that are located on basin floors, Galt hydric inclusions that are located in depressions, Sailboat hydric inclusions that are located on the low floodplain, hydric components of Clearlake that are located on basin floors, hydric components of Cosumnes that are located on the

low floodplain, hydric components of Jacktone that are located on basin rims and hydric components of Galt that are located within depressions.

### 4.2.2 Topography

The natural topography of the site has been altered to facilitate agricultural production processes. Historically, the site was largely flat and is located in an area that was part of the original floodplain of the Sacramento River. Throughout the past several decades, the site has been repeatedly leveled, drained and/or disced for the process of rice production and most recently for wheat production. Other common agricultural maintenance activities or practices influencing the topography and drainage on the site include ditching and mechanical harvesting processes. The slopes throughout the site range from approximately 0 to 2 percent. The elevation on the site ranges from approximately 11 to 22 feet above MSL.

## 4.2.3 Regional Hydrology

The site is located in the Natomas Basin approximately two miles northeast of Sacramento River within the northern Sacramento Valley portion of the Great Central Valley. Historically, the Sacramento River and many of its main tributaries flooded seasonally, creating areas that remained inundated for substantial periods during the rainy season. As a result, large-scale flood-control projects, diversion dams, and water-control structures were built on tributary rivers entering the valley in the 1930's. As a result of the construction of these fortified structures, natural flooding events were reduced in frequency and intensity. As the demand for agricultural production processes in the region increased, the development of a complex system of canals and ditches to maximize water conveyance and storage ensued. A review of the U.S.G.S. Davisville topographic map of 1905 indicates that the site is within the former location of historic Bush Lake which was drained as a result of the construction of the Natomas Drainage Canal.

### 4.2.4 Site-Specific Hydrology

The site is within the historic 100-year floodplain (FEMA, 1996) of Sacramento River. The hydrologic regime on the site is supplemented by seasonal storm water run off and precipitation, primarily between November and March. The majority of seasonal surface run off is conveyed throughout the site via altered, leveled topography and/or artificial water conveyance features such as ditches and canals. The hydrology of the site has been altered for the conveyance of water to, from, and throughout the site via a network of ditches and canals in order to facilitate agricultural production processes. Hydrologic features identified and mapped within the site include the following: depressional seasonal wetland, depressional seasonal marsh, depressional perennial marsh, excavated pond and ditch/canal (**Figure 3**). Diagnostic characteristics of the features mapped on the site are defined and discussed in Section 4.4.

The ditches and canals on the site are physically connected to the West Drainage canal via a series of culverts, and the West Drainage Canal is tributary to Sacramento River.

However, not all the ditches appear to be functionally connected via natural flows to or from the West Drainage Canal, specifically features #46, #48 and #49. The ditches are man made and appear to constitute the remnants of artificial water conveyance facilities associated with past agricultural practices on the site. As a result, these features or a portion or portions thereof may be considered non-jurisdictional by the Corps.

The Final Natomas Basin Habitat Conservation Plan has identified and described the ditches/canals along the western, southern and eastern site boundary as part of a water *drainage* system, and the ditches within the interior site boundary are identified as part of a water *delivery* system. At no time was standing or flowing water observed within these interior, remnant ditches that are classified as part of a water delivery system.

The depressional seasonal wetlands on the site are characterized by saturation rather than inundation. The depressional seasonal marshes are seasonally inundated or saturated, but inundation/saturation persists for some period into the warm season. The depressional perennial marshes are depressions that typically remain inundated or saturated throughout the year. The excavated ponds are supplied by seasonal precipitation and are isolated from any other wetlands or waters.

#### 4.3 Vegetation

The vegetation assemblages and habitat types occurring on the site include the following: agricultural cropland, California annual grassland alliance, depressional seasonal wetland, depressional seasonal marsh and depressional perennial marsh.

#### 4.3.1 Agricultural Cropland

The majority of the site is composed of leveled agricultural cropland (wheat). According to the land manager, the wheat crop was planted in November of 2005 and harvested in July 2005.

## 4.3.2 California Annual Grassland Alliance

California annual grassland alliance consists of a myriad of native and non-native annual plant species and occurs in a majority of the state at elevations from sea level to approximately 4,000 feet above MSL. Composition of this vegetation community varies depending on distribution, geographic location and land use. Additional major influences on this vegetation community include soil type, annual precipitation and fall temperatures. Dominant plant species within the California annual grassland on the site include the following: Italian ryegrass (*Lolium multiflorum*), soft brome (*Bromus hordeaceus*), wild oat (*Avena* sp.), mouse-tail grass (*Vulpia myuros*), medusahead (*Taeniatherum caput-medusae*), long-beaked filaree (*Erodium botrys*), woodland geranium (*Geranium molle*), chick weed (*Stellaria media*), milk thistle (*Silybum marianum*), star thistle (*Centaurea solstitialis*), barley (*Hordeum murinum* ssp. *leporinum*), wild oat (*Avena* sp.), clover (*Trifolium* sp.) and shepherd's purse (*Capsella bursa-pastoris*). California annual grassland alliance occurs primarily in between the

leveled agricultural fields, along the berms above the ditches and canals on the site and along the maintenance roads as well as the upland areas outside of the agricultural fields.

#### 4.3.3 Seasonal Wetland

The depressional seasonal wetlands on the site support hydrophytic vegetation. Depressional seasonal wetlands are depressions within the topography that inundate or saturate for short periods of time following intense rains but do not maintain seasonal aquatic or saturated soils conditions for durations long enough for colonization by perennial, obligate plant species. As such, plant species in seasonal wetlands are generally of two types: species that can tolerate short periods of inundation but have not adapted to withstand sustained aquatic or saturated soils conditions, and short-lived (primarily annual) species that take advantage of ephemeral aquatic and/or saturated soils conditions. Plant species observed occurring within the seasonal wetlands on the site and in the associated utility alignments include Italian ryegrass, Mediterranean barley (Hordeum marinum ssp. gussoneanum), vernal pool buttercup (Ranunculus bonariensis var. trisepalus) and nutsedge (Cyperus esculentus). The depressional seasonal wetlands are concentrated in the northern and central portions of the site.

#### 4.3.4 Seasonal Marsh

Cattail alliance occurs throughout the state of California in brackish, alkali or freshwater marshes from sea level to approximately 6,500 feet above MSL. Typically, cattail alliance occurs in intermittently or permanently flooded wetlands, such as the depressional perennial marsh in the northwestern portion of the site. The diagnostic species of this vegetation alliance is cattail (*Typha latifolia*), which is a hydrophytic species. Associates vary widely depending on length of inundation/saturation during the year as well as seasonal temperatures and water chemistry. On the site, sand bar willow (*Salix exigua*) and smartweed (*Polygonum* sp.) are common associates of this alliance. This vegetation alliance also occurs within the depressional seasonal marsh located along the eastern site boundary.

#### 4.3.5 Perennial Marsh

The depressional perennial marshes on the site support hydrophytic vegetation. Depressional perennial marsh is located in the northwestern portion of the site within the center of the equestrian track. The marsh is supplied by a ditch which conveys water into the marsh via a subsurface conveyance feature and culverts. A review of historical photographs indicates that this feature was created on the site as part of the equestrian track design and/ or maintenance function. The dominant tree species in the marsh, which appears to have been red willow (*Salix laevigata*), had been recently cut down prior to conducting the wetland delineation. Sand bar willow is common along the boundary and within the margins of this feature. Emergent aquatic plant species such as cattail and floating aquatics such as duckweed (*Lemna* sp.) and knotweed also occur in this area. Dense interspersed stands of Himalayan blackberry (*Rubus discolor*) occur with regular frequency along the boundary of this feature, as well.

#### 4.4 Classification of Waters of the United States

As discussed previously in section 2.0, jurisdictional waters of the U.S. are classified into multiple types based on topography, edaphics (soils), vegetation and hydrologic regime. Primarily, the Army Corps of Engineers establishes two distinctions: wetland and non-wetland waters of the U.S. Non-wetland waters are commonly referred to as other waters. Potential jurisdictional wetland types mapped within the site include the following: depressional seasonal wetland, depressional seasonal marsh and depressional perennial marsh.

Potential other waters of the U.S. delineated within the site include the following: ditch/canal. In addition, the ponds on the site were identified as excavated in uplands and interpreted as potentially non jurisdictional features. A description of all of the features delineated within the site is provided in the following sections.

## 4.4.1 Depressional Seasonal Wetland

A total of **4.68** acres of depressional seasonal wetland have been delineated on the site. Depressional seasonal wetlands are defined by a hydrologic regime characterized by saturation rather than inundation. Depressional seasonal wetlands were identified on the site as topographic depressions with a hydrologic regime characterized by saturation and capable of supporting hydrophytic plant species and hydric soils. Plant species in depressional seasonal wetlands are adapted to withstand short periods of saturation or saturated soils conditions but will not withstand prolonged periods of inundation, as is common in vernal pools. The depressional seasonal wetlands on the site support wetland soils, vegetation, and hydrology, and would likely be regulated by the Corps. Depressional seasonal wetlands are located in the northern central portion of the site (**Figure 3**).

#### 4.4.2 Depressional Seasonal Marsh

A total of **0.31-**acre of depressional seasonal marsh has been delineated on the site. Depressional seasonal marshes are wetlands that are seasonally inundated or saturated, but inundation/saturation persists through the majority of the warm season. The persistence of inundation/saturation into the warm season permits the growth of primarily perennial herbaceous plant species capable of withstanding extended periods of inundation or saturated soil conditions. In the Great Central Valley, these features are typically located on the fringes of naturally occurring or artificially created impoundments, such as ponds or reservoirs. These features may also be associated with slow moving riverine systems where natural and/or artificial flows persist into the warm season. The depressional seasonal marsh on the site exhibits wetland characteristics.

#### 4.4.3 Depressional Perennial Marsh

A total of **1.34** acres of depressional perennial marsh have been delineated on the site. Depressional perennial marshes can occur as the result of natural and/or artificial water flows associated with agricultural or residential water uses. Depressional perennial

marshes are dominated by inundation. Typically, depressional perennial marshes remain inundated or saturated throughout the year. The persistence of inundation/saturation throughout the year permits the growth of warm-season wetland grasses and perennial herbaceous plant species. Within the Central Valley, depressional perennial marshes typically occur in association with the lowland terminus of local riverine watersheds or as the result of artificial excavation activities in low lying areas exhibiting historic hydric soils conditions, often resulting in artificially created impoundments, such as ponds or reservoirs.

The depressional perennial marsh is located within the abandoned equestrian racetrack in the northwestern portion of the site. It exhibits wetland characteristics and is connected via a series of culverts to a network of ditches/canals on the site which are connected to jurisdictional waters (Sacramento River) off site. The depressional seasonal marsh is therefore presumed to be a Corps jurisdictional wetland.

#### 4.4.4 Ditch/Canal

A total of 11.64 acres of ditch/canal have been delineated on the site. Non-tributary water conveyance features excavated in uplands and constructed for the transport and distribution of groundwater between agricultural fields are not jurisdictional features unless the Corps determines and claims jurisdiction on a case-by-case basis. Water conveyance features excavated in uplands and constructed for transport and distribution of surface water between agricultural fields may be jurisdictional features, specifically if they are tributary to known waters of the U.S.

An additional **0.72** acre of ditches/canals was delineated on the site and are not connected to any other water conveyance feature on or off of the site. At no time was standing or flowing water observed within the interior remnant ditches on the site. As a result, these features or a portion or portions thereof may be considered non-jurisdictional by the Corps. However, the Corps reviews these situations on a case-by-case basis. The ditches/canals are located throughout the interior of the site and along the eastern, western and southern site boundaries. Because of the lack of connectivity, we have identified these features as non-jurisdictional.

#### 4.4.5 Excavated pond

A total **0.34-**acre of excavated pond has been delineated on the site. There are two excavated ponds in the northern-central portion of the site. Ponds are typically the result of the deliberate impoundment of water through artificial damming. When stock ponds occur as the result of the construction of artificial impoundment features that restrict or stop the flow of jurisdictional waters of the U.S., the resulting pond becomes jurisdictional to the limits of the ordinary high water mark or wetland boundary. Conversely, ponds wholly excavated in uplands and supplied by surface run off or groundwater are not jurisdictional features. The ponds on the site are excavated and are not the result of the impoundment of a natural drainageway. Nor are the excavated ponds tributaries to or from any waters of the U.S. The hydrology of the ponds is supplied by

seasonal precipitation. Therefore, the Corps will not likely assert jurisdiction of these features.

**Table 1** below provides acreage per class and summarizes the total acreage of wetlands and waters on the site.

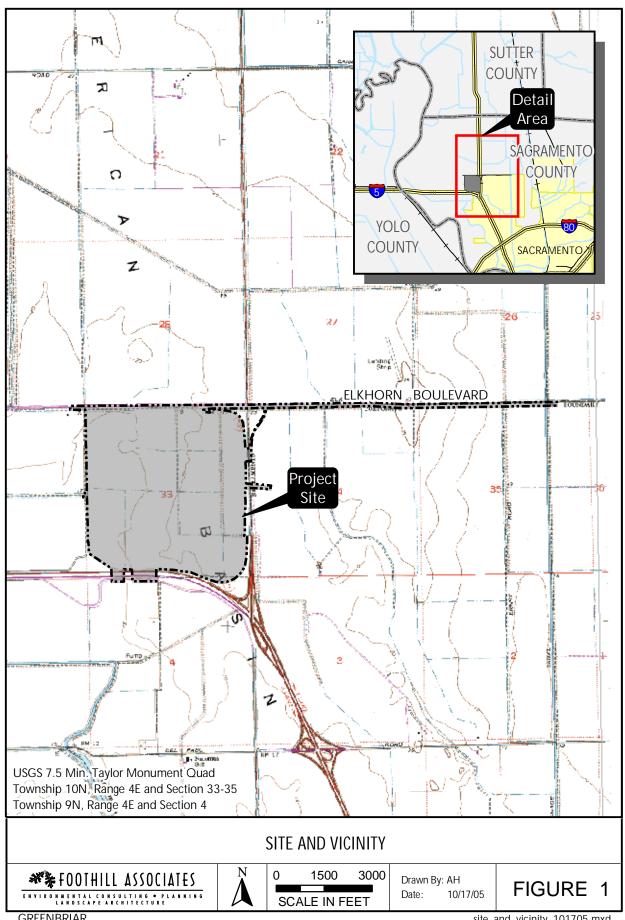
Table 1 — Waters of the U.S: Acreage According to Feature

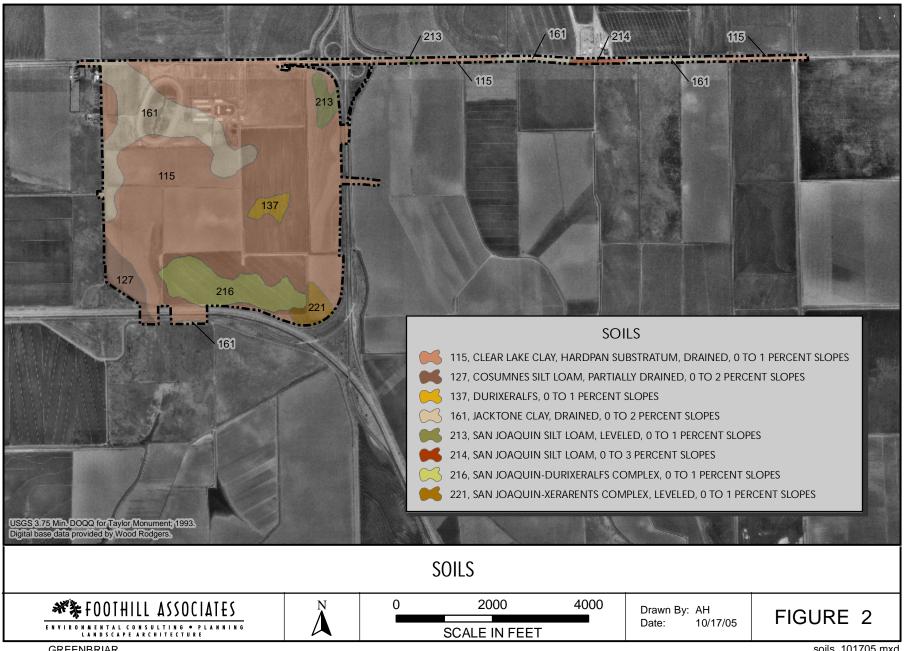
| CLASS                            | TOTAL<br>ACREAGE | JURISDITIONAL             | NON-<br>JURISDITIONAL |
|----------------------------------|------------------|---------------------------|-----------------------|
| Depressional Seasonal<br>Wetland | 4.68             | 4.68                      | 0.0                   |
| Depressional Seasonal<br>Marsh   | 0.31             | 0.31                      | 0.0                   |
| Depressional Perennial<br>Marsh  | 1.34             | 1.34                      | 0.0                   |
| Ditch/Canal                      | 12.36            | <b>11.64</b> <sup>1</sup> | 0.72                  |
| Excavated Pond                   | 0.34             | 0                         | 0.34                  |
| TOTAL                            | 19.03            | 17.97                     | 1.06                  |

<sup>&</sup>lt;sup>1</sup> Ditches and canals may not be jurisdictional.

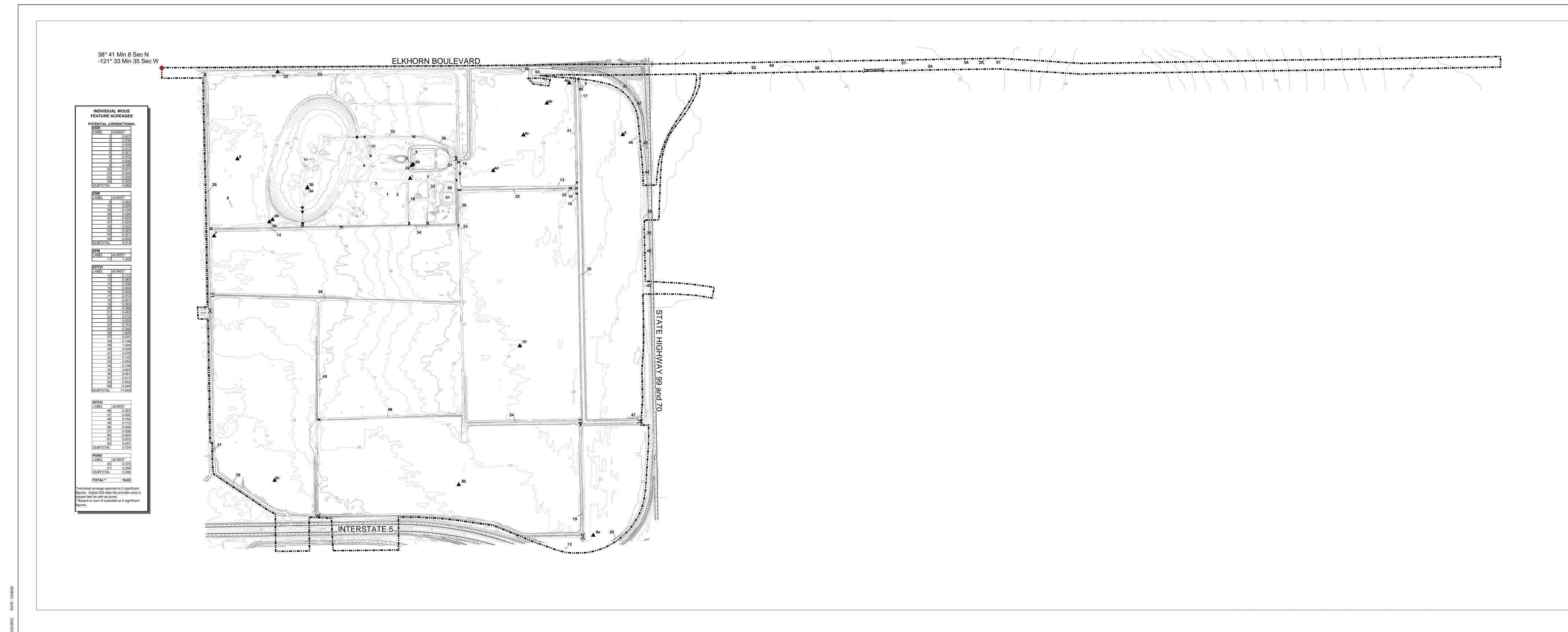
- City of Sacramento. 2003. <u>Errata to the Final Natomas Basin Habitat Conservation Plan.</u> Sacramento, CA;
- Environmental Laboratories. 1987. <u>Corps of Engineers Wetlands Delineation Manual</u>. U.S. Army Corps of Engineers Waterways Experiment Station. Vicksburg, MS;
- Federal Emergency management Agency (FEMA). 1996. National Flood Insurance Program Q3 Flood Data, Disc 1: California;
- Gretag Macbeth. 2000. Munsell Soil Color Charts. New Windsor, NY;
- Hickman, James C. 1993. <u>The Jepson Manual: Higher Plants of California</u>. University of California Press, Berkeley, CA;
- Hitchcock, A.S. 1935. Revised 1971. <u>Manual of the Grasses of the United States</u>. U.S. Department of Agriculture, Dover Publications, NY;
- Hitchcock, Leo C. and Arthur Cronquist. 1996. Flora of the Pacific Northwest. University of Washington Press, Seattle, WA;
- Mason, Herbert L. 1957. <u>A Flora of the Marshes of California</u>. University of California Press, Berkeley, California;
- Munz, Phillip A. 1968. <u>A California Flora and Supplement</u>. University of California Press, Berkeley, CA;
- Natural Resource Conservation Service (NRCS). March 1992. <u>Hydric Soils List for Sacramento County, California</u>. U.S. Department of Agriculture;
- Natural Resource Conservation Service (NRCS). 1993. <u>Soil Survey of Sacramento County, California</u>. U.S. Department of Agriculture;
- Reed, P.B., Jr. 1988. <u>National List of Plant Species That Occur in Wetlands: California (Region O)</u>; U.S. Fish & Wildlife Service;
- Sawyer, John O. and Todd Keeler-Wolf. 1995. <u>A Manual of California Vegetation</u>. California Native Plant Society (CNPS), Sacramento, CA;
- USDA, NRCS. 2003. <u>Field Indicators of Hydric Soils in the United States</u>, Version 5.01. G.W. Hurt, P.M. Whited, and R.F. Pringle (eds). USDA, NRCS in cooperation with the National Committee for Hydric Soils. Fort Worth, TX;
- USDA, NRCS. 1937. <u>Historic Aerial Photo Coverage of Sacramento County</u>, <u>California</u>. USDA, NRCS;

- USDA, NRCS. 1957. <u>Historic Aerial Photo Coverage of Sacramento County</u>, California. USDA, NRCS;
- U.S. Geological Survey. 1954. <u>Davis, California</u>. 7.5 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1905. <u>Davisville, California</u>. 15 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1967. <u>Taylor Monument, California</u>. 7.5 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1967. Photorevised 1975. <u>Taylor Monument, California</u>. 7.5 minute series topographic quadrangle. U.S. Department of the Interior; and
- U.S. Geological Survey. 1967. Photorevised 1980. <u>Taylor Monument, California</u>. 7.5 minute series topographic quadrangle. U.S. Department of the Interior.

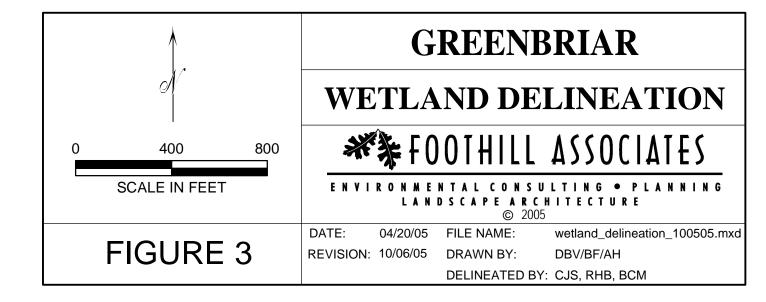




**GREENBRIAR** 



| JURISDICTIONAL WATERS OF CLASSIFICATION | OF THE U.S.<br>ACREAGE | NON JURISDICTIONA CLASSIFICATION | L ACREAGE<br>ACREAGE | TOTAL<br>ACREAGE | OTHER FEATURES                     | NOTES  |
|---|------------------------|----------------------------------|----------------------|------------------|------------------------------------|--|
| DEPRESSIONAL WETLANDS                   |                        |                                  |                      |                  | ▲ Data Points                      | Wetland delineation subject to U.S. Army Corps of Engineers verification.  |
| Seasonal Wetland                        | 4.68                   |                                  |                      | 4.68<br>0.31     | Direction of underground flow      | Digital base data provided by Wood Rodgers. Contour interval is 1 foot or less.  |
| Seasonal Marsh  Perennial Marsh         | 0.31<br>1.34           |                                  |                      | 1.34             | Culvert                            | <ul> <li>Eastern countours generated from 30M DEM, interval is 1 foot.</li> <li>The Hydrologic Unit Code for this site is 18020109.</li> </ul> |
| OTHER WATERS OF THE U.S.  Ditch/Canal   | 11.64                  | Ditch/Canal                      | 0.72                 | 12.36            | Off-Site Ditch/Canal Site Boundary | This wetland delineation utilizes the Corps' 1987 three-parameter methodology to delineate jurisdictional waters of the U.S.                   |
| TOTAL                                   | 17.97                  | Excavated Pond TOTAL             | 1.06                 | 19.03            | Site Boundary                      | Wetlands and other waters of the U.S. were mapped using a Trimble GP Global Positioning System).   |



## **Appendix A** — Contact Information

**Client Contact Information:** Niki Doan

AKT Development Corporation 7700 College Town Drive, Suite 101 Sacramento, CA 95826 -2397

**Delineation Conducted by**: Brian Mayerle, Biologist

Cristian Singer, Botanist

Foothill Associates

655 Menlo Drive, Suite 100 Rocklin, CA 95765-3718



# DATA FORM ROUTINE WETLAND DETERMINATION

| Is the site significantly disturbed (Atypical Situation)? Yes No Is the area a potential Problem Area? Yes No (If needed, explain on reverse.)    Dominant Plant Species   Stratum   Indicator   Associate Plant Species   Strature   S | y ID:<br>D: |
|--|-------------|
| Dominant Plant Species         Stratum         Indicator         Associate Plant Species         Stratum           1.         9.   |             |
| 1  |             |
| Remarks:  HYDROLOGY  |             |
| Recorded Data (Describe in Remarks): Stream, Lake, or Tide Gauge Aerial Photographs Other No Recorded Data Available  Field Observations:  Depth of Surface Water: Depth to Free Water in Pit: Depth to Saturated Soil:  Wetland Hydrology Indicators: Primary Indicators: Inundated Saturated in Upper 12 Inches Water Marks Drift Lines Sediment Deposits Drainage Patterns in Wetlands Secondary Indicators (2 or more required) Water-Stained Leaves Local Soil Survey Data FAC-Neutral Test Other (Explain in Remarks)  | ,           |

| ,                                | d Phase):  |                                 |                                  |   | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? | Yes | No |
|----------------------------------|--|---------------------------------|----------------------------------|---|---|-----|----|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                         |     | -  |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o  | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls  |     | -  |
| Remarks:                         |  |                                 |                                  |   |   |     |    |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
|  |                   |                |  |     |    |
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# DATA FORM ROUTINE WETLAND DETERMINATION

| Is the site significantly disturbed (Atypical Situation)? Yes No Is the area a potential Problem Area? Yes No (If needed, explain on reverse.)    Dominant Plant Species   Stratum   Indicator   Associate Plant Species   Strature   S | y ID:<br>D: |
|--|-------------|
| Dominant Plant Species         Stratum         Indicator         Associate Plant Species         Stratum           1.         9.   |             |
| 1  |             |
| Remarks:  HYDROLOGY  |             |
| Recorded Data (Describe in Remarks): Stream, Lake, or Tide Gauge Aerial Photographs Other No Recorded Data Available  Field Observations:  Depth of Surface Water: Depth to Free Water in Pit: Depth to Saturated Soil:  Wetland Hydrology Indicators: Primary Indicators: Inundated Saturated in Upper 12 Inches Water Marks Drift Lines Sediment Deposits Drainage Patterns in Wetlands Secondary Indicators (2 or more required) Water-Stained Leaves Local Soil Survey Data FAC-Neutral Test Other (Explain in Remarks)  | ,           |

| ,                                | d Phase):  |                                 |                                  |   | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? | Yes | No |
|----------------------------------|--|---------------------------------|----------------------------------|---|---|-----|----|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                         |     | -  |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o  | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls  |     | -  |
| Remarks:                         |  |                                 |                                  |   |   |     |    |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
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# DATA FORM ROUTINE WETLAND DETERMINATION

| Is the site significantly disturbed (Atypical Situation)? Yes No Is the area a potential Problem Area? Yes No (If needed, explain on reverse.)    Dominant Plant Species   Stratum   Indicator   Associate Plant Species   Strature   S | y ID:<br>D: |
|--|-------------|
| Dominant Plant Species         Stratum         Indicator         Associate Plant Species         Stratum           1.         9.   |             |
| 1  |             |
| Remarks:  HYDROLOGY  |             |
| Recorded Data (Describe in Remarks): Stream, Lake, or Tide Gauge Aerial Photographs Other No Recorded Data Available  Field Observations:  Depth of Surface Water: Depth to Free Water in Pit: Depth to Saturated Soil:  Wetland Hydrology Indicators: Primary Indicators: Inundated Saturated in Upper 12 Inches Water Marks Drift Lines Sediment Deposits Drainage Patterns in Wetlands Secondary Indicators (2 or more required) Water-Stained Leaves Local Soil Survey Data FAC-Neutral Test Other (Explain in Remarks)  | ,           |

| ,                                | d Phase):  |                                 |                                  |   | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? | Yes | No |
|----------------------------------|--|---------------------------------|----------------------------------|---|---|-----|----|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                         |     | -  |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o  | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls  |     | -  |
| Remarks:                         |  |                                 |                                  |   |   |     |    |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
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# DATA FORM ROUTINE WETLAND DETERMINATION

| Is the site significantly disturbed (Atypical Situation)? Yes No Is the area a potential Problem Area? Yes No (If needed, explain on reverse.)    Dominant Plant Species   Stratum   Indicator   Associate Plant Species   Strature   S | y ID:<br>D: |
|--|-------------|
| Dominant Plant Species         Stratum         Indicator         Associate Plant Species         Stratum           1.         9.   |             |
| 1  |             |
| Remarks:  HYDROLOGY  |             |
| Recorded Data (Describe in Remarks): Stream, Lake, or Tide Gauge Aerial Photographs Other No Recorded Data Available  Field Observations:  Depth of Surface Water: Depth to Free Water in Pit: Depth to Saturated Soil:  Wetland Hydrology Indicators: Primary Indicators: Inundated Saturated in Upper 12 Inches Water Marks Drift Lines Sediment Deposits Drainage Patterns in Wetlands Secondary Indicators (2 or more required) Water-Stained Leaves Local Soil Survey Data FAC-Neutral Test Other (Explain in Remarks)  | ,           |

| ,                                | d Phase):  |                                 | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? Yes No |   |                                       |  |   |
|----------------------------------|--|---------------------------------|--|---|---------------------------------------|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist)                                     | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc. |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o                                      | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls                                    |  | - |
| Remarks:                         |  |                                 |  |   |                                       |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
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# DATA FORM ROUTINE WETLAND DETERMINATION

| Is the site significantly disturbed (Atypical Situation)? Yes No Is the area a potential Problem Area? Yes No (If needed, explain on reverse.)    Dominant Plant Species   Stratum   Indicator   Associate Plant Species   Strature   S | y ID:<br>D: |
|--|-------------|
| Dominant Plant Species         Stratum         Indicator         Associate Plant Species         Stratum           1.         9.   |             |
| 1  |             |
| Remarks:  HYDROLOGY  |             |
| Recorded Data (Describe in Remarks): Stream, Lake, or Tide Gauge Aerial Photographs Other No Recorded Data Available  Field Observations:  Depth of Surface Water: Depth to Free Water in Pit: Depth to Saturated Soil:  Wetland Hydrology Indicators: Primary Indicators: Inundated Saturated in Upper 12 Inches Water Marks Drift Lines Sediment Deposits Drainage Patterns in Wetlands Secondary Indicators (2 or more required) Water-Stained Leaves Local Soil Survey Data FAC-Neutral Test Other (Explain in Remarks)  | ,           |

| ,                                | d Phase):  |                                 | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? Yes No |   |                                       |  |   |
|----------------------------------|--|---------------------------------|--|---|---------------------------------------|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist)                                     | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc. |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o                                      | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls                                    |  | - |
| Remarks:                         |  |                                 |  |   |                                       |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
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# DATA FORM ROUTINE WETLAND DETERMINATION

| Project/Site: Applicant/Owner: Investigator:   | Date:<br>County:<br>State:  |   |  |
|--|---|---|--|
| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation) Is the area a potential Problem Area? (If needed, explain on reverse.)   | Yes No<br>n)? Yes No<br>Yes No  | Community ID: Transect ID: Plot ID:   |  |
| /EGETATION   |   |   |  |
| Dominant Plant Species   | 9   | Stratum Indicator   |  |
| Recorded Data (Describe in Remarks):     Stream, Lake, or Tide Gauge     Aerial Photographs     Other     No Recorded Data Available  Field Observations:  Depth of Surface Water:(in.)  Depth to Free Water in Pit:(in.)  Depth to Saturated Soil:(in.) | Wetland Hydrology Indicator Primary Indicators: Inundated Saturated in Uppe Water Marks Drift Lines Sediment Deposit Drainage Patterns Secondary Indicators (2 Oxidized Root Che Water-Stained Lea Local Soil Survey FAC-Neutral Test Other (Explain in 1 | er 12 Inches  its is in Wetlands 2 or more required): hannels in Upper 12 Inches eaves y Data t |  |

| ,                                | d Phase):  |                                 | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? Yes No |   |                                       |  |   |
|----------------------------------|--|---------------------------------|--|---|---------------------------------------|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist)                                     | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc. |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o                                      | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls                                    |  | - |
| Remarks:                         |  |                                 |  |   |                                       |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
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# DATA FORM ROUTINE WETLAND DETERMINATION

| Project/Site: Applicant/Owner: Investigator:   | Date:<br>County:<br>State:  |   |  |
|--|---|---|--|
| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation) Is the area a potential Problem Area? (If needed, explain on reverse.)   | Yes No<br>n)? Yes No<br>Yes No  | Community ID: Transect ID: Plot ID:   |  |
| /EGETATION   |   |   |  |
| Dominant Plant Species   | 9   | Stratum Indicator   |  |
| Recorded Data (Describe in Remarks):     Stream, Lake, or Tide Gauge     Aerial Photographs     Other     No Recorded Data Available  Field Observations:  Depth of Surface Water:(in.)  Depth to Free Water in Pit:(in.)  Depth to Saturated Soil:(in.) | Wetland Hydrology Indicator Primary Indicators: Inundated Saturated in Uppe Water Marks Drift Lines Sediment Deposit Drainage Patterns Secondary Indicators (2 Oxidized Root Che Water-Stained Lea Local Soil Survey FAC-Neutral Test Other (Explain in 1 | er 12 Inches  its is in Wetlands 2 or more required): hannels in Upper 12 Inches eaves y Data t |  |

| ,                                | d Phase):  |                                 | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? Yes No |   |                                       |  |   |
|----------------------------------|--|---------------------------------|--|---|---------------------------------------|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist)                                     | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc. |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o                                      | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls                                    |  | - |
| Remarks:                         |  |                                 |  |   |                                       |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
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# DATA FORM ROUTINE WETLAND DETERMINATION

| Project/Site: Applicant/Owner: Investigator:   | Date:<br>County:<br>State:  |   |  |
|--|---|---|--|
| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation) Is the area a potential Problem Area? (If needed, explain on reverse.)   | Yes No<br>n)? Yes No<br>Yes No  | Community ID: Transect ID: Plot ID:   |  |
| /EGETATION   |   |   |  |
| Dominant Plant Species   | 9   | Stratum Indicator   |  |
| Recorded Data (Describe in Remarks):     Stream, Lake, or Tide Gauge     Aerial Photographs     Other     No Recorded Data Available  Field Observations:  Depth of Surface Water:(in.)  Depth to Free Water in Pit:(in.)  Depth to Saturated Soil:(in.) | Wetland Hydrology Indicator Primary Indicators: Inundated Saturated in Uppe Water Marks Drift Lines Sediment Deposit Drainage Patterns Secondary Indicators (2 Oxidized Root Che Water-Stained Lea Local Soil Survey FAC-Neutral Test Other (Explain in 1 | er 12 Inches  its is in Wetlands 2 or more required): hannels in Upper 12 Inches eaves y Data t |  |

| ,                                | d Phase):  |                                 | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? Yes No |  |                                       |  |  |
|----------------------------------|--|---------------------------------|--|--|---------------------------------------|--|--|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors (Munsell Moist)  | Mottle Abundance/<br>Size/Contrast   | Texture, Concretions, Structure, etc. |  |  |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-O | tions                           | Organic<br>Listed o<br>Listed o                                      | ions<br>ganic Content in Surface<br>Streaking in Sandy Soil<br>n Local Hydric Soils Lis<br>in National Hydric Soils L<br>Explain in Remarks) | ls                                    |  |  |
| Remarks:                         |  |                                 |  |  |                                       |  |  |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
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|  | State:  |   |
|--|---|---|
| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)? Is the area a potential Problem Area? (If needed, explain on reverse.)  | Yes No<br>Yes No<br>Yes No  | Community ID:<br>Transect ID:<br>Plot ID:   |
| EGETATION  |   |   |
| 1.       . | 9   | Stratum Indicator   |
| T  | Wetland Hydrology Indicator Primary Indicators: Inundated Saturated in Upper Water Marks Drift Lines Sediment Deposit Drainage Patterns Secondary Indicators (2: Oxidized Root Cha Water-Stained Lea Local Soil Survey I FAC-Neutral Test Other (Explain in F | er 12 Inches  ts s in Wetlands or more required): annels in Upper 12 Inches aves Data |

| ,                                |  |                                 |                                  |   | Drainage Class: Field Observations Confirm Mapped Type? Yes No |  |   |
|----------------------------------|--|---------------------------------|----------------------------------|---|--|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                          |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o  | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls   |  | - |
| Remarks:                         |  |                                 |                                  |   |  |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
|  |                   |                |  |     |    |
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|  | State:  |   |
|--|---|---|
| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)? Is the area a potential Problem Area? (If needed, explain on reverse.)  | Yes No<br>Yes No<br>Yes No  | Community ID:<br>Transect ID:<br>Plot ID:   |
| EGETATION  |   |   |
| 1.       . | 9   | Stratum Indicator   |
| T  | Wetland Hydrology Indicator Primary Indicators: Inundated Saturated in Upper Water Marks Drift Lines Sediment Deposit Drainage Patterns Secondary Indicators (2: Oxidized Root Cha Water-Stained Lea Local Soil Survey I FAC-Neutral Test Other (Explain in F | er 12 Inches  ts s in Wetlands or more required): annels in Upper 12 Inches aves Data |

| ,                                |  |                                 |                                  |   | Drainage Class: Field Observations Confirm Mapped Type? Yes No |  |   |
|----------------------------------|--|---------------------------------|----------------------------------|---|--|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                          |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o  | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls   |  | - |
| Remarks:                         |  |                                 |                                  |   |  |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
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| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)? Is the area a potential Problem Area? (If needed, explain on reverse.)  | Yes No<br>Yes No<br>Yes No  | Community ID:<br>Transect ID:<br>Plot ID:   |
| EGETATION  |   |   |
| 1.       . | 9   | Stratum Indicator   |
| T  | Wetland Hydrology Indicator Primary Indicators: Inundated Saturated in Upper Water Marks Drift Lines Sediment Deposit Drainage Patterns Secondary Indicators (2: Oxidized Root Cha Water-Stained Lea Local Soil Survey I FAC-Neutral Test Other (Explain in F | er 12 Inches  ts s in Wetlands or more required): annels in Upper 12 Inches aves Data |

| ,                                |  |                                 |                                  |   | Drainage Class: Field Observations Confirm Mapped Type? Yes No |  |   |
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| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                          |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o  | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls   |  | - |
| Remarks:                         |  |                                 |                                  |   |  |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
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|  | State:  |   |
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| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)? Is the area a potential Problem Area? (If needed, explain on reverse.)  | Yes No<br>Yes No<br>Yes No  | Community ID:<br>Transect ID:<br>Plot ID:   |
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| ,                                |  |                                 |                                  |   | Drainage Class: Field Observations Confirm Mapped Type? Yes No |  |   |
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| Remarks:                         |  |                                 |                                  |   |  |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
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| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)? Is the area a potential Problem Area? (If needed, explain on reverse.)  | Yes No<br>Yes No<br>Yes No  | Community ID:<br>Transect ID:<br>Plot ID:   |
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| ,                                |  |                                 |                                  |   | Drainage Class: Field Observations Confirm Mapped Type? Yes No |  |   |
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| Remarks:                         |  |                                 |                                  |   |  |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
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|  | State:  |   |
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| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)? Is the area a potential Problem Area? (If needed, explain on reverse.)  | Yes No<br>Yes No<br>Yes No  | Community ID:<br>Transect ID:<br>Plot ID:   |
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| ,                                |  |                                 |                                  |   | Drainage Class: Field Observations Confirm Mapped Type? Yes No |  |   |
|----------------------------------|--|---------------------------------|----------------------------------|---|--|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                          |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o  | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls   |  | - |
| Remarks:                         |  |                                 |                                  |   |  |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
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|  | State:  |   |
|--|---|---|
| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)? Is the area a potential Problem Area? (If needed, explain on reverse.)  | Yes No<br>Yes No<br>Yes No  | Community ID:<br>Transect ID:<br>Plot ID:   |
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| ,                                |  |                                 |                                  |   | Drainage Class: Field Observations Confirm Mapped Type? Yes No |  |   |
|----------------------------------|--|---------------------------------|----------------------------------|---|--|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                          |  | - |
| H<br>H<br>S<br>A<br>R            | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-C | tions                           | Organio<br>Listed o<br>Listed o  | tions<br>ganic Content in Surfac<br>: Streaking in Sandy Soi<br>in Local Hydric Soils List<br>on National Hydric Soils I<br>Explain in Remarks) | ls   |  | - |
| Remarks:                         |  |                                 |                                  |   |  |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
|--|-------------------|----------------|--|-----|----|
| Remarks:   |                   |                | •  |     |    |
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|  | State:  |   |
|--|---|---|
| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)? Is the area a potential Problem Area? (If needed, explain on reverse.)  | Yes No<br>Yes No<br>Yes No  | Community ID:<br>Transect ID:<br>Plot ID:   |
| EGETATION  |   |   |
| 1.       . | 9   | Stratum Indicator   |
| T  | Wetland Hydrology Indicator Primary Indicators: Inundated Saturated in Upper Water Marks Drift Lines Sediment Deposit Drainage Patterns Secondary Indicators (2: Oxidized Root Cha Water-Stained Lea Local Soil Survey I FAC-Neutral Test Other (Explain in F | er 12 Inches  ts s in Wetlands or more required): annels in Upper 12 Inches aves Data |

| ,                                |  |                                 |                                  |   | Drainage Class: Field Observations Confirm Mapped Type? Yes No |  |   |
|----------------------------------|--|---------------------------------|----------------------------------|---|--|--|---|
| Profile Des<br>Depth<br>(inches) | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors<br>(Munsell Moist) | Mottle Abundance/<br>Size/Contrast  | Texture, Concretions, Structure, etc.                          |  | - |
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| Remarks:                         |  |                                 |                                  |   |  |  |   |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
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| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)?                                       |  | 7   |
|--|--|---|
| Is the area a potential Problem Area? (If needed, explain on reverse.)   | Yes No<br>Yes No<br>Yes No   | Community ID:<br>Transect ID:<br>Plot ID:   |
| EGETATION  |  |   |
| 1.       9.         2.       10.         3.       11.         4.       12.         5.       13.         6.       14.         7.       15.  |  | Stratum Indicator   |
| Recorded Data (Describe in Remarks):  Stream, Lake, or Tide Gauge Aerial Photographs Other No Recorded Data Available  Field Observations: | etland Hydrology Indicator Primary Indicators: Inundated Saturated in Upper Water Marks Drift Lines Sediment Deposit: Drainage Patterns Secondary Indicators (2 of Charles of Ch | er 12 Inches  ts s in Wetlands or more required): annels in Upper 12 Inches aves Data |

| Map Unit Name (Series and Phase):  Taxonomy (Subgroup): |  |                                 |                                 | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? Yes No   |                                       |  |  |
|---|--|---------------------------------|---------------------------------|--|---------------------------------------|--|--|
| Profile Des<br>Depth<br>(inches)                        | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors (Munsell Moist)   | Mottle Abundance/<br>Size/Contrast   | Texture, Concretions, Structure, etc. |  |  |
| H<br>H<br>S<br>A<br>R                                   | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-O | tions                           | Organic<br>Listed o<br>Listed o | ions<br>ganic Content in Surface<br>Streaking in Sandy Soil<br>n Local Hydric Soils Lis<br>in National Hydric Soils L<br>Explain in Remarks) | ls                                    |  |  |
| Remarks:  |  |                                 |                                 |  |                                       |  |  |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
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| Do Normal Circumstances exist on the site? Is the site significantly disturbed (Atypical Situation)?                                       |  | 7   |
|--|--|---|
| Is the area a potential Problem Area? (If needed, explain on reverse.)   | Yes No<br>Yes No<br>Yes No   | Community ID:<br>Transect ID:<br>Plot ID:   |
| EGETATION  |  |   |
| 1.       9.         2.       10.         3.       11.         4.       12.         5.       13.         6.       14.         7.       15.  |  | Stratum Indicator   |
| Recorded Data (Describe in Remarks):  Stream, Lake, or Tide Gauge Aerial Photographs Other No Recorded Data Available  Field Observations: | etland Hydrology Indicator Primary Indicators: Inundated Saturated in Upper Water Marks Drift Lines Sediment Deposit: Drainage Patterns Secondary Indicators (2 of Charles of Ch | er 12 Inches  ts s in Wetlands or more required): annels in Upper 12 Inches aves Data |

| Map Unit Name (Series and Phase):  Taxonomy (Subgroup): |  |                                 |                                 | Drainage Class:<br>Field Observations<br>Confirm Mapped Type? Yes No   |                                       |  |  |
|---|--|---------------------------------|---------------------------------|--|---------------------------------------|--|--|
| Profile Des<br>Depth<br>(inches)                        | Horizon  | Matrix Color<br>(Munsell Moist) | Mottle Colors (Munsell Moist)   | Mottle Abundance/<br>Size/Contrast   | Texture, Concretions, Structure, etc. |  |  |
| H<br>H<br>S<br>A<br>R                                   | Indicators:<br>istosol<br>istic Epipedon<br>ulfidic Odor<br>quic Moisture F<br>educing Condi<br>leyed or Low-O | tions                           | Organic<br>Listed o<br>Listed o | ions<br>ganic Content in Surface<br>Streaking in Sandy Soil<br>n Local Hydric Soils Lis<br>in National Hydric Soils L<br>Explain in Remarks) | ls                                    |  |  |
| Remarks:  |  |                                 |                                 |  |                                       |  |  |

| Hydrophytic Vegetation Present?<br>Wetland Hydrology Present?<br>Hydric Soils Present? | Yes<br>Yes<br>Yes | No<br>No<br>No | Is this Sampling Point Within a Wetland? | Yes | No |
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# **Delineation of Waters of the United States** Supplemental Report

# **Regulatory #200500572**

Greenbriar ±577-Acre Site and Associated Utility Alignments Sacramento County, California

Prepared for: U.S. Army Corps of Engineers

Contracted By: AKT Development Corporation

February 27, 2006



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#### 1.0 INTRODUCTION

In response to the December 6, 2005 letter from the U.S. Army Corps of Engineers (Corps), this report provides supplemental information to the site's initial wetland delineation report, dated November 3, 2005, prepared by Foothill Associates. This report specifically addresses atypical situations versus normal circumstances on the site and includes three-parameter data gathered for the 36 Corps-requested data points along with updated three-parameter data for sample points 4A-10, which were initially evaluated as part of the site's original wetland delineation report. Additional data points were evaluated as warranted based on site conditions at the time of the field surveys, for example, to determine the wetland or upland status of uncertain areas. Based on the re-evaluation of the site, a revised wetland delineation map has been prepared and included in this report.

### 2.1 Site-Specific References

Available information pertaining to the natural resources of the region was reviewed. All references reviewed for this delineation are listed in Section 4.0 of this report. Pertinent site-specific reports and general references utilized concurrent with the delineation include the following:

- Environmental Laboratory. 1987. Corps of Engineers Wetlands Delineation Manual. U.S. Army Corps of Engineers Waterways Experiment Station. Vicksburg, MS;
- GretagMacbeth. 2000. Munsell Soil Color Charts. New Windsor, NY;
- Hickman, James C. 1993. The Jepson Manual: Higher Plants of California.
   University of California Press, Berkeley, CA;
- Reed, P.B., Jr. 1988. National List of Plant Species That Occur in Wetlands:
   California (Region O); U.S. Fish & Wildlife Service;
- USDA, NRCS (Natural Resource Conservation Service). 1993. Soil Survey of Sacramento County, California. USDA, NRCS, in cooperation with the Regents of the University of California (Agricultural Experiment Station); and
- USDA, NRCS. 2003. Field Indicators of Hydric Soils in the United States,
   Version 5.01. G.W. Hurt, P.M. Whited, and R.F. Pringle (Eds). USDA, NRCS in cooperation with the National Committee for Hydric Soils. Fort Worth, TX.

#### 2.2 Field Methodology

The Corps 1987 three-parameter (vegetation, hydrology, and soils) methodology to delineate jurisdictional waters of the U.S was utilized during the field surveys. This methodology requires the collection of data on soils, vegetation, and hydrology at several locations to establish the jurisdictional boundary of wetlands. In addition, the site was reevaluated according to atypical situation methodology according to the Corps' request.

Field surveys of the site were conducted by Foothill Associates on January 20 and 24, 2006; and February 13, 14, and 22, 2006. Each data point was evaluated to determine the composition and identification of dominant plant species. The indicator status of all dominant plant species (as determined by the U.S. Fish and Wildlife Service National List of Plant Species that Occur in Wetlands: 1988 California (Region 0)) was applied and evaluated as part of the vegetation assessment portion of the wetland determination process. The plant community within a five-foot radius surrounding each data point was evaluated to determine dominant vegetation. Given the herbaceous vegetation stratum

within the fields and the fact that the surveys were conducted near the beginning of the growing season, not all of the vegetation on the site was readily identifiable. All dominant species within each data point were keyed out to the extent possible. The state of the vegetation growth did not bias the results of the delineation in terms of which areas were identified as wetlands. The results were consistent under both normal and atypical methodologies. Any inaccuracies did not affect the results of this wetland delineation.

A soil pit was dug to a depth of 16-20 inches and the soil profile was examined for wetness characteristics. Observations were made and recorded for both primary and secondary wetland hydrology indicators, if present. In addition to sampling at the locations requested by the Corps, routine determination data points were collected in other areas of the site. The location of each data point is depicted in **Figure 2** and corresponding routine wetland determination data forms are provided in **Appendix B**.

As part of the fieldwork, all previously mapped ditches were re-inspected to determine the surface hydrological connection, if any, between the ditches on the site and their jurisdictional status was re-evaluated accordingly. Representative ground-level photographs on the site are included in **Appendix A**.

#### 2.3 GPS Data Integration

All data point locations and boundaries of wetlands and other waters of the U.S. within the site were surveyed and mapped with a Trimble GeoXT GPS (Global Positioning System) hand-held unit. This is a mapping-grade GPS unit capable of real-time differential correction and sub-meter accuracy. The GPS data were downloaded from the unit and differentially corrected utilizing Trimble Pathfinder Office software and appropriate base station data, and then converted to ESRI ® shape file format. Data were exported to the Geographic Information System (GIS) software in the State Plane coordinate system (NAD 83) with units as "survey feet." Within the GIS, data were edited and linear features were built into polygons using recorded width information. All wetland shape files were merged to create a single wetland file with calculated acreages. These results are presented in Figure 2.

### 3.1 Study Area Description, Land Use

### 3.1.1 Study Area Location

The ±577-acre site and associated utility alignments are located in northwestern Sacramento County, approximately two miles southeast of the Sacramento International Airport and two miles northeast of Sacramento River. The site is bound by Interstate 5 on the south, State Highways 70/99 on the east, and Elkhorn Boulevard on the north. The utility alignments include areas along the south edge of Elkhorn Boulevard, east to Natomas Boulevard and the east edge of the site, south along State Route 99. The site is bound on the west by rural residences and agricultural lands. The site is located within Townships 9 and 10 North, Range 4 East and occupies portions of sections 4 and 33 of the U.S.G.S. Taylor Monument 7.5' quadrangle map (Figure 1).

#### 3.1.2 Existing and Historic Land Use

With the exception of a small area in the northern portion of the site, the entire site is currently cultivated with dry farmed wheat. A portion of the site was in rice cultivation until 2002. A horse race track and an irrigated polo field were present in the northern portion of the site from approximately 1980 to the early 2000s. For several years the horse ranch subleased the northwest corner of the property to a highway construction company, who stored equipment there. For at least the last 20 years, the remainder of the property outside the horse ranch area has been in agricultural use (rice, sugar beets, wheat).

#### 3.1.3 Atypical Situation and Normal Circumstances

The site was evaluated as having normal circumstances because the vegetation conditions that were observed reasonably represent normal circumstances for the hydric soils and wetlands hydrology on the site. This is because the fields were seeded with wheat, an upland species, prior to the onset of the rainy season. Because wheat will not grow in wetlands as it cannot withstand wetland hydrology, the areas in which wheat has germinated and grown reflect non-wetland conditions. Since our observations were made during the normal wet period of the growing season, we were able to observe the vegetation before the planted community began to monopolize the site as we would expect to happen later during the year. We did observe a sorting of vegetation with wheat being either absent or not dominant from the areas that otherwise clearly had wetlands characteristics.

As requested by the Corps, we also evaluated the site as an atypical site. For the atypical evaluation, we were unable to determine what vegetation would have been present absent the agriculture use of the land (since that first took place over 60 years ago and appears to be relatively continuous since then), so we did a two-parameter delineation for the

atypical evaluation. For each data point, the atypical evaluation results in the same wetland determination as the normal circumstances assessment revealed.

#### 3.2 Vegetation

The vegetation assemblages and habitat types occurring on the site include agricultural cropland, depressional seasonal wetland, farmed wetland, and depressional seasonal marsh

### 3.2.1 Agricultural Cropland

As previously mentioned, nearly the entire site is currently cultivated with dry farmed, or non-irrigated, wheat. While wheat vastly dominates all other herbaceous vegetation on the site, other immature grasses were emerging within some of the data points. Since most of the non-wheat vegetation was observed prior to their flowering period and not readily identifiable, these species were keyed out to the extent possible. Aside from the wheat, the dominant herbaceous species observed within the data points are most likely annual bluegrass (*Poa annua*), Mediterranean barley (*Hordeum marinum*), ryegrass (*Lolium multiflorum*), and bur clover (*Medicago polymorpha*).

#### 3.2.2 Seasonal Wetland

The depressional seasonal wetlands on the site support hydrophytic vegetation. Depressional seasonal wetlands are depressions within the topography that inundate or saturate for short periods of time following intense rains but do not maintain seasonal aquatic or saturated soils conditions for durations long enough for colonization by perennial, obligate plant species. As such, plant species in seasonal wetlands are generally of two types: species that can tolerate short periods of inundation but have not adapted to withstand sustained aquatic or saturated soils conditions, and short-lived (primarily annual) species that take advantage of ephemeral aquatic and/or saturated soils conditions. Plant species observed occurring within the seasonal wetlands on the site and in the associated utility alignments include Italian ryegrass, Mediterranean barley (Hordeum marinum ssp. gussoneanum), vernal pool buttercup (Ranunculus bonariensis var. trisepalus) and nutsedge (Cyperus esculentus). The depressional seasonal wetlands are concentrated in the northern and central portions of the site.

#### 3.2.3 Farmed Wetland

Farmed wetlands on the site are basically seasonal wetlands that occur within agricultural croplands. Since wheat, an upland species, is currently in cultivation on the Greenbriar site, the cropland areas that are functioning as wetland habitat support a predominance of the non-wheat, herbaceous species discussed above for the agricultural cropland community.

#### 3.2.4 Seasonal Marsh

Cattail alliance occurs throughout the state of California in brackish, alkali or freshwater marshes from sea level to approximately 6,500 in elevation. Typically, cattail alliance occurs in intermittently or permanently flooded wetlands, such as perennial marshes. The diagnostic species of this vegetation alliance is cattail (*Typha latifolia*), which is a hydrophytic species. Associates vary widely depending on length of inundation/saturation during the year as well as seasonal temperatures and water chemistry. On the site, sand bar willow (*Salix exigua*) and smartweed (*Polygonum* sp.) are common associates of this alliance. This vegetation alliance also occurs within the depressional seasonal marsh located along the eastern site boundary.

# 3.3 Classification of Waters of the United States at the Greenbriar Site

Jurisdictional waters of the U.S. are classified into multiple types based on topography, edaphics (soils), vegetation and hydrologic regime. Primarily, the Corps establishes two distinctions: wetland and non-wetland waters of the U.S. Non-wetland waters are commonly referred to as other waters. Potential jurisdictional wetland types mapped within the site include depressional seasonal wetland, farmed wetland, and depressional seasonal marsh. Potential other waters of the U.S. delineated within the site include a portion of the networks of ditches and canals on-site. In addition, the ponds on the site were identified as excavated in uplands and interpreted as non-jurisdictional features. A description of all of the features delineated within the site is provided in the following sections.

### 3.3.1 Depressional Seasonal Wetland

A total of **0.18** acre of depressional seasonal wetland has been delineated on the site. Depressional seasonal wetlands are defined by a hydrologic regime characterized by saturation rather than inundation. Depressional seasonal wetlands were identified on the site as topographic depressions with a hydrologic regime characterized by saturation and capable of supporting hydrophytic plant species and hydric soils. Plant species in depressional seasonal wetlands are adapted to withstand short periods of saturation or saturated soils conditions but will not withstand prolonged periods of inundation, as is common in vernal pools. Depressional seasonal wetlands are located in the northern-central portion of the site and numbered 21-31 on **Figure 2**.

The depressional seasonal wetlands on the site support wetland soils, vegetation, and hydrology; however, they are isolated features and are exempt from Corps jurisdiction as they do not connect to waters of the United States.

#### 3.3.2 Farmed Wetland

A total of 9.75 acres of farmed wetlands have been delineated on the site. Similar to depressional seasonal wetlands, farmed wetlands are defined by a hydrologic regime characterized by saturation rather than inundation and support wetland soils, vegetation,

and hydrology. Farmed wetlands are located in the northern and western portions of the site and numbered 8-10 and 66-68 on **Figure 2**.

Wetlands 8-10 are adjacent to but hydrologically separated from Lone Tree Canal by a berm. These features have been identified in this delineation report as jurisdictional consistent with existing Corps policy and the decision of the Sixth Circuit of the United States Courts of Appeals in *Carabell v. United States*, 391 F.3d 704 (2004). The *Carabell* decision is now under review by the United States Supreme Court. The Supreme Court may reach a different conclusion regarding Corps jurisdiction over adjacent wetlands which may change the results of this delineation.

Wetland number 8 includes both wetland and upland characteristics. While the perimeter of the feature is relatively well defined, the interior portions contain small, irregularly shaped wetland and upland areas and are very difficult to map consistently. In order to determine the amount of wetland acreage encompassed within the feature, four east-west transects (perpendicular to existing cultivation furrows) were walked across the entire width of the feature. At every 25-foot interval along each transect, the determination of either upland or wetland characteristics (e.g., presence/absence of algal matting, wheat-dominated vegetation) were noted. Individual soil pits were not dug for any of the points within these transects. The percentage of all points that showed wetland characteristics was used to calculate the amount of wetland acreage within the mapped feature. Of the 33 points taken along the four transects, 14 showed wetland characteristics. Therefore, only 42 percent of Wetland 8 is a wetland.

Wetlands 66-68 are isolated and are exempt from Corps jurisdiction as they do not connect to waters of the United States.

### 3.3.3 Depressional Seasonal Marsh

A total of **1.65** acres of depressional seasonal marsh have been delineated on the site. Depressional seasonal marshes are wetlands that are seasonally inundated or saturated, but inundation/saturation persists through the majority of the warm season. The persistence of inundation/saturation into the warm season permits the growth of primarily perennial herbaceous plant species capable of withstanding extended periods of inundation or saturated soil conditions. In the Great Central Valley, these features are typically located on the fringes of naturally occurring or artificially created impoundments, such as ponds or reservoirs. These features may also be associated with slow-moving riverine systems where natural and/or artificial flows persist into the warm season. The depressional seasonal marshes occur in the northern and eastern portions of the site and are numbered 1 and 11-20 on **Figure 2**.

Marsh 1 was identified as a perennial wetland on the original wetland delineation map. This feature received year-round water from the equestrian facility when it was in operation. Given the lack of ponded water within this feature during our February 2006 field surveys and the fact that the equestrian facility is no longer in operation, this feature functions as a seasonal marsh and has been labeled on **Figure 2** accordingly.

#### 3.3.4 Ditch/Canal

A total of 12.37 acres of ditch/canal have been delineated on the site. Non-tributary water conveyance features excavated in uplands and constructed for the transport and distribution of groundwater between agricultural fields are not jurisdictional features unless the Corps determines and claims jurisdiction on a case-by-case basis. Water conveyance features excavated in uplands and constructed for transport and distribution of surface water between agricultural fields may be jurisdictional features, specifically if they are tributary to known waters of the U.S. Under the Corps policies implementing Section 404 of the Clean Water Act, non-tidal agricultural ditches constructed in uplands for the purpose of draining and irrigating agricultural farmland are normally non-jurisdictional. Based on this long-standing policy, the majority of agricultural ditches on the Greenbriar site are non-jurisdictional.

As stated in the earlier wetland delineation submitted, the site is approximately two miles northeast of the Sacramento River in the vicinity of the former Bush Lake. Large-scale flood control projects in the 1930s and demand for agricultural production in the region resulted in construction of a complex system of canals and ditches constructed to maximize water conveyance and storage. This system drained the area well prior to enactment of the Clean Water Act. On-site, the natural hydrologic regime was altered to facilitate agricultural production prior to 1937.

Lone Tree Canal is physically connected to the Western Drainage canal via a series of culverts, and the Western Drainage Canal is tributary to the Sacramento River. The Final Natomas Habitat Conservation Plan (2003) identified and described the ditches and canals along the western, southern, and eastern site boundary as part of the water drainage system, and the ditches within the interior site boundary are identified as part of the water delivery system. This system of irrigation and drainage ditches fed and drained the site for agricultural purposes. Water pumped through the irrigation ditches from a lift station located approximately half a mile north of the site artificially irrigated the site until 2003 when water to the site was shut off.

The original flood control structures in the Natomas region were constructed in the 1910s. These structures significantly changed the areas hydrologic regime. Subsequently, the system of irrigation canals and drainage ditches were constructed by the end of the 1930s to supply water for agricultural production and to drain excess water from fields. All of this occurred well prior to the enactment of the Clean Water Act in 1972. According to Corps policy and relevant case law, these conditions constitute the baseline environmental conditions and must be taken into account when determining jurisdiction over sites in this region. By 1972, virtually all of the Greenbriar site existed as uplands.

The irrigation ditches and the drainage ditches constructed on the site were constructed for the purpose of agricultural production. Since at least the 1930s, much of the Greenbriar site has been devoted to rice production. Crops continue to be grown on-site to this day. Rice was farmed on the site until as recently as 2004. Wheat, an upland crop, was planted for the 2005 growing season and again for the 2006 growing season.

As artificial irrigation of the site is no longer needed to grow rice, water delivery to the site from the pump station to the north has ceased. The on-site irrigation ditches are now dry. The site's natural hydrology supports the growth of wheat on the site. The underlying purpose and the current condition of the on-site irrigation ditches indicate that Ditches 32, 34-35, 37-40, and 42-56 are not subject to Corps jurisdiction.

There are isolated irrigation ditches on the site. These ditches were man-made and constitute remnants of artificial conveyance facilities associated with agricultural practices on site. They are not functionally connected by natural flow to Lone Tree Canal, the West Drainage Canal or the Sacramento River. At no time has standing or flowing water been observed in these interior, remnant ditches that are classified as part of a water delivery system. The isolated irrigation ditches ought to be exempt from Corps jurisdiction as they do not connect to waters of the United States. These non-jurisdictional irrigation ditches include Ditches 33, 36, and 41. Similarly, other on-site or roadside ditches with no connection to waters of the United States, including Ditches 57-63 are non-jurisdictional.

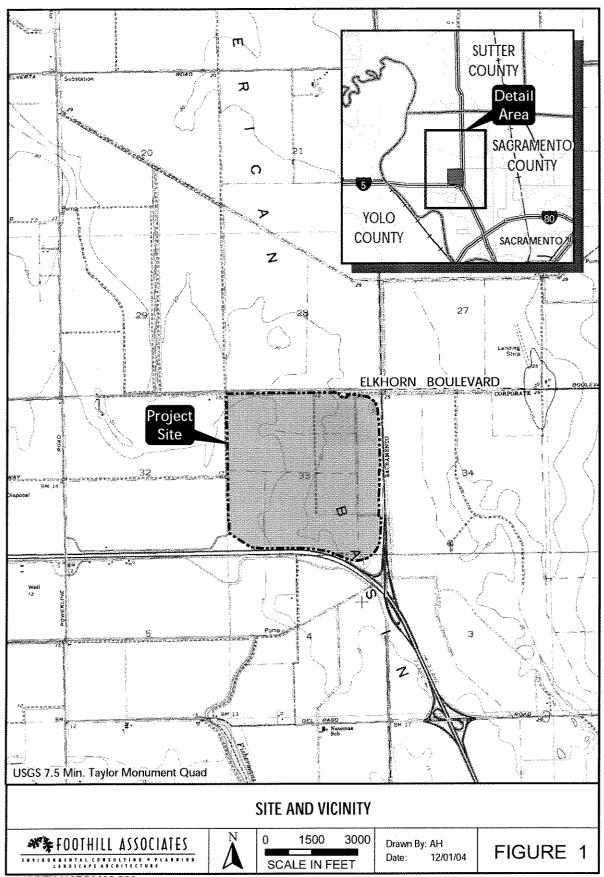
Other drainage ditches on the site that connect with Lone Tree Canal merely collect excess surface water from the site. Lone Tree Canal and other on-site drainages that eventually connect to the Sacramento River by way of Lone Tree Canal would be jurisdictional if they became tidal or extended the ordinary high water mark (OHWM). We understand that the exemption does not apply to a drainage ditch that extends the OHWM of a tributary otherwise subject to regulation.

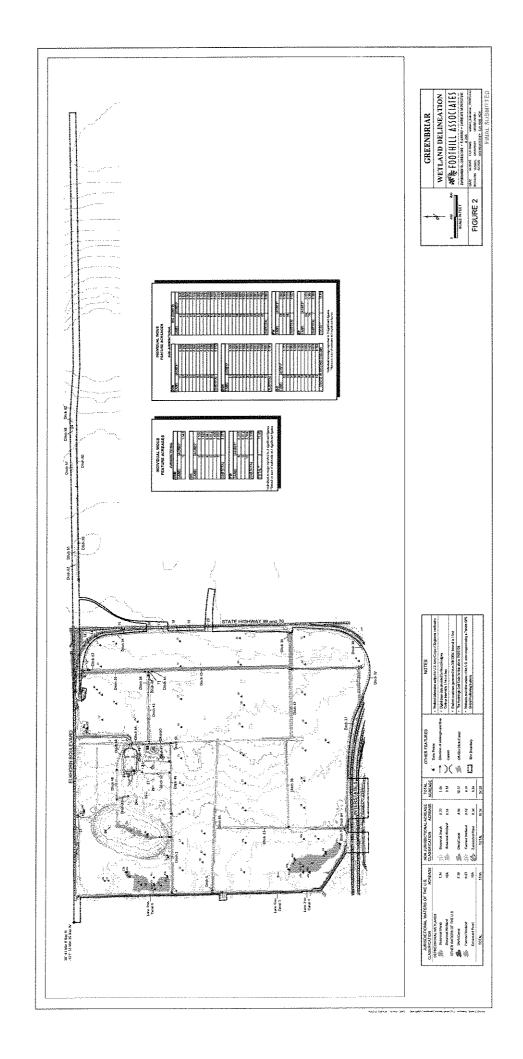
Lone Tree Canal (Ditches 3, 4, and 6) is likely a jurisdictional waters of the United States. This OHWM extends from Lone Tree Canal to other on-site drainage ditches with which it connects on site. These drainage ditches and any connecting irrigation ditches are jurisdictional to the extent of the OHWM or to the extent of adjacent wetlands. Ditches 5 and 7 connect with Lone Tree Canal and extend its OHWM. Ditch 7 extends the OHWM approximately 23 feet east from the culvert under I-5. Ditch 5 extends the OHWM approximately 11 feet east from its connection with Lone Tree Canal. Ditch 2 also extends the OHWM of Lone Tree Canal; however, because of its connection with Seasonal Marsh 1, it extends the Corps jurisdiction from Lone Tree Canal to the boundaries of the seasonal marsh.

Wetlands adjacent to jurisdictional waters of the United States extend the Corps' jurisdiction. However, the Corps lacks jurisdiction over on-site wetlands that are adjacent to exempt ditches. The jurisdictional ditches on the Greenbriar site include Lone Tree Canal (consisting of Feature 3, 4, and 6) and connecting drainage ditches 2, 5, and 7. Only wetlands adjacent to these features may be subject to Corps jurisdiction. Therefore, on-site wetlands that may be jurisdictional include Seasonal Marsh 1 and Farmed Wetlands 8-10. The remainder are non-jurisdictional based on their isolation from jurisdictional waters of the United States.

- City of Sacramento. 2003. Errata to the Final Natomas Basin Habitat Conservation Plan. Sacramento, CA;
- Environmental Laboratories. 1987. Corps of Engineers Wetlands Delineation Manual. U.S. Army Corps of Engineers Waterways Experiment Station. Vicksburg, MS;
- Federal Emergency Management Agency (FEMA). 1996. National Flood Insurance Program Q3 Flood Data, Disc 1: California;
- GretagMacbeth. 2000. Munsell Soil Color Charts. New Windsor, NY;
- Hickman, James C. 1993. *The Jepson Manual: Higher Plants of California*. University of California Press, Berkeley, CA;
- Hitchcock, A.S. 1935. Revised 1971. *Manual of the Grasses of the United States*. U.S. Department of Agriculture, Dover Publications, NY;
- Hitchcock, Leo C. and Arthur Cronquist. 1996. Flora of the Pacific Northwest. University of Washington Press, Seattle, WA;
- Mason, Herbert L. 1957. A Flora of the Marshes of California. University of California Press, Berkeley, California;
- Munz, Phillip A. 1968. *A California Flora and Supplement*. University of California Press, Berkeley, CA;
- Reed, P.B., Jr. 1988. National List of Plant Species That Occur in Wetlands: California (Region O); U.S. Fish & Wildlife Service;
- Sawyer, John O. and Todd Keeler-Wolf. 1995. A Manual of California Vegetation. California Native Plant Society (CNPS), Sacramento, CA;
- U.S. Department of Agriculture (USDA), Natural Resource Conservation Service (NRCS). 1937. Historic Aerial Photo Coverage of Sacramento County, California;
- USDA, NRCS. 1957. Historic Aerial Photo Coverage of Sacramento County, California;
- USDA, NRCS. March 1992. Hydric Soils List for Sacramento County, California;
- USDA, NRCS. 1993. *Soil Survey of Sacramento County, California*. USDA, NRCS, in cooperation with the Regents of the University of California (Agricultural Experiment Station); and

- USDA, NRCS. 2003. Field Indicators of Hydric Soils in the United States, Version 5.01. G.W. Hurt, P.M. Whited, and R.F. Pringle (eds). USDA, NRCS in cooperation with the National Committee for Hydric Soils. Fort Worth, TX;
- U.S. Geological Survey. 1954. *Davis, California*. 7.5 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1905. *Davisville, California*. 15 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1967. *Taylor Monument, California*. 7.5 -minute series topographic quadrangle. U.S. Department of the Interior;
- U.S. Geological Survey. 1967. Photorevised 1975. *Taylor Monument, California*. 7.5 minute series topographic quadrangle. U.S. Department of the Interior; and
- U.S. Geological Survey. 1967. Photorevised 1980. *Taylor Monument, California*. 7.5 minute series topographic quadrangle. U.S. Department of the Interior.

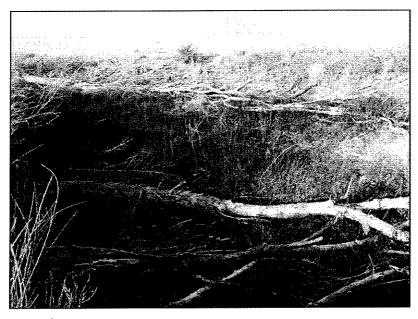




## **Appendix A** — **Ground-Level Photographs**



Greenbriar Seasonal Marsh #1 — Northern Portion Photo Date: February 22, 2006



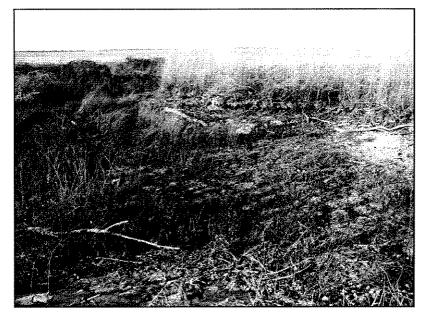
Greenbriar Seasonal Marsh #1 — Central Portion Photo Date: February 22, 2006

## **GROUND-LEVEL PHOTOGRAPHS**



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Appendix A



Greenbriar Seasonal Marsh #1 — Southern Portion Photo Date: February 22, 2006



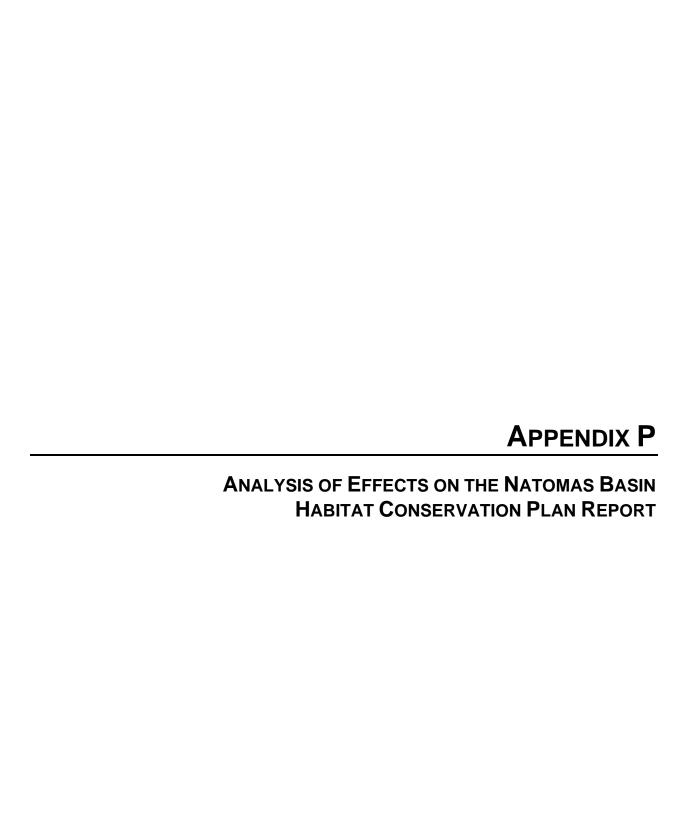
Greenbriar Seasonal Marsh #1 — Southern End Photo Date: February 22, 2006

## **GROUND-LEVEL PHOTOGRAPHS**



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Appendix A



## Greenbriar Development Project Sacramento, California

# Analysis of Effects on the Natomas Basin Habitat Conservation Plan Report



Prepared for: City of Sacramento Environmental Planning Services

July 19, 2006



Greenbriar Development Project Sacramento, California

# Analysis of Effects on the Natomas Basin Habitat Conservation Plan Report



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#### **EXECUTIVE SUMMARY**

#### **ES.1 INTRODUCTION**

This Analysis of Effects on the Natomas Basin Habitat Conservation Plan Report (effects analysis) (EDAW 2006) is an evaluation of the effects on each species covered by the Natomas Basin Habitat Conservation Plan (NBHCP), on the conservation strategy of the NBHCP, on specific conservation measures, and consequently on attainment of the NBHCP's goals and objectives as a result of implementing the proposed Greenbriar project. The U.S. Fish & Wildlife Service (Service) and the California Department of Fish & Game (Department) approved the NBHCP in the summer of 2003. The NBHCP establishes the overall conservation program for the development of a 17,500 acre-portion of the Natomas Basin. The Greenbriar site is located within the boundaries of the NBHCP plan area, but is not within an area permitted for development. This Effects Analysis is being released for public review in conjunction with the *Greenbriar Development Project Sacramento, California: Draft Environmental Impact Report* (DEIR) (EDAW 2006) because the EIR contains an evaluation of the Greenbriar project's effects on biological resources for purposes of CEQA review, as well as the evaluation of the project's effects on the NBHCP.

The Effects Analysis is organized in the following way:

- Section 1, Introduction
- Section 2, Evaluation Approach
- Section 3, Greenbriar Project's Alteration of Population and Habitat Attributes
- ► Section 4, Potential Effects of the Greenbriar Project on Covered Species
- ► Section 5, Potential Effects on the Conservation Strategy of the NBHCP
- ▶ Section 6, Potential Effects of the Greenbriar Project on NBHCP Goals and Objectives
- ► Section 7, Cumulative Effects
- ► Appendix A, Consistency of Greenbriar Project and NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts
- ► Appendix B, Change in Natomas Basin Land Cover in 2001–2004

#### **ES.2 OVERVIEW OF GREENBRIAR PROJECT**

As currently proposed, the Greenbriar project would:

- ▶ Develop 546 acres at the Greenbriar site;
- Avoid and preserve an on-site corridor (of 31 acres) along Lone Tree Canal;
- ► Create or enhance, preserve, and manage in perpetuity two proposed off-site reserves the Natomas 130 and Spangler properties (with a combined acreage of 266 acres).

As designed, the proposed project includes a package of measures to avoid, minimize, and mitigate impacts from the proposed development. In addition, the City of Sacramento, through the CEQA process, has proposed mitigation measures to reduce further the adverse effects of the proposed project. (Throughout this Effects

Analysis, "mitigation" refers to the measures proposed by the City of Sacramento in the Draft EIR for the Greenbriar project [City of Sacramento July 2006].) With the DEIR mitigation, the project's avoidance, minimization, and mitigation measures include:

- ► Avoidance of a 31 acre (250-foot wide) corridor along Lone Tree Canal;
- ▶ Measures to reduce or offset effects on the Lone Tree Canal corridor including barriers/fencing, creation of marsh habitat along the canal corridor, design of canal crossings to minimize obstacles to giant garter snake movement, and an assurance that aquatic habitat would be maintained in this section of the canal;
- ► Funding to manage the Lone Tree Canal corridor in perpetuity;
- ▶ Measures to avoid and minimize construction-related effects on covered species; and
- ► Creation or enhancement, preservation, and management in perpetuity of 315 acres of high quality habitat in addition to the corridor conserved along Lone Tree Canal.

#### **ES.3 SUMMARY OF FINDINGS**

To evaluate the proposed project's effects on the effectiveness of the NBHCP, this effects analysis performed an extensive analysis of the project's potential effects on the future condition of the Natomas Basin. This analysis used the 2001 land cover data that represents baseline conditions of the NBHCP, and also considered 2001–2004 changes in land cover, and 2005 conditions. Interpretations of the project's effects on the NBHCP were based on the sum of anticipated effects on the viability of populations of covered species using the Natomas Basin, on the effectiveness of the NBHCP's conservation strategy, and on attainment of the goals and objectives of the NBHCP.

Although the proposed project would cause a variety of adverse and beneficial effects, overall, the proposed project (with the DEIR mitigation) would not reduce the viability of covered species, the efficacy of the NBHCP conservation strategy, or adversely affect attainment of the NBHCP goals and objectives. In part, it would have this outcome because its conservation strategy includes a substantial investment in the creation, enhancement, and management in perpetuity of high quality habitat on the preserved land, and in the avoidance, minimization, and mitigation of effects on the Lone Tree Canal corridor. For most covered species, the increased habitat values on preserved lands offset the habitat values lost as a result of development at the Greenbriar site, and thus prevent a net loss in resources in the Natomas Basin for these species. The conservation of the Lone Tree Canal corridor, while costly and resulting in a small reserve that will be costly to manage, is essential for maintaining connectivity of aquatic habitat and movement of giant garter snakes between the southern and central Natomas Basin; without this connectivity, the effectiveness of the NBHCP's conservation strategy would be reduced.

The project's adverse and beneficial effects on the viability of populations of covered species using the Natomas Basin, on the effectiveness of the NBHCP's conservation strategy, and on attainment of the goals and objectives of the NBHCP are summarized in the following sections of text.

#### ES 3.1 EFFECT ON POPULATION VIABILITY OF COVERED SPECIES

The Greenbriar project would not affect five of the 15 animal species covered by the NBHCP: California tiger salamander, western spadefoot toad, vernal pool fairy shrimp, vernal pool tadpole shrimp, and midvalley fairy shrimp. None of these vernal pool-associated species are known from the vicinity of the Greenbriar or proposed reserve sites, nor does suitable habitat occur in the vicinity of these sites.

The project is also unlikely to affect valley elderberry longhorn beetle (VELB) because VELB is not known from the vicinity of the Greenbriar or proposed reserve sites, and riparian habitat that might contain elderberry bushes

is only present at and in the vicinity of the proposed Natomas 130 reserve; also, in the future, riparian habitat may recover and persist in the proposed reserve along Lone Tree Canal; preservation of these sites was considered unlikely to benefit VELB.

The Greenbriar project would cause a variety of beneficial and adverse effects on populations of nine species covered by the NBHCP. For these species, the overall effect on population viability is summarized below.

Three of these species are birds that do not nest in the Natomas Basin but forage in the Basin in winter or during migration: Aleutian Canada goose, white-faced ibis, and bank swallow. Based on 2001 land cover, the Greenbriar project (with the DEIR mitigation) would decrease the acreage of foraging habitat available for these species in the Natomas Basin by 1–3% and would preserve and enhance 0–2% of the foraging habitat in the Basin. Because the size of these populations is not limited by the availability of foraging habitat in winter, or during migration, and the Greenbriar project would not substantially alter the availability of such foraging habitat, the project's effect on foraging habitat would be unlikely to alter the viability of these populations. The project would also increase the acreage of nesting habitat for white-faced ibis, and this could increase the likelihood of white-faced ibis establishing a nesting colony in the Natomas Basin; while not discounted, this effect was not considered likely.

The Greenbriar project would cause both adverse and beneficial effects on burrowing owl and loggerhead shrike populations in the Natomas Basin, but effects due to the project would be insufficient to alter the viability of these populations. Based on 2001 land cover, the project would preserve approximately 345 and 141 acres of shrike and owl habitat, respectively, and this beneficial effect would at least partially offset the project's adverse effects on these species. Adverse effects would include a net loss of 141 acres of habitat for the shrike, and for both species a loss of occupied habitat, habitat fragmentation, and probably some increased mortality and habitat degradation adjacent to the Greenbriar site. However, the project's effects would be small relative to the quantity of habitat that would remain in the Natomas Basin (for example, the project would eliminate 1% of shrike habitat), and the Natomas Basin represents only a small portion of the habitat for and population of these species in the Central Valley; thus, the project is unlikely to measurably alter the viability of the loggerhead shrike and burrowing owl populations using the Natomas Basin.

The project (with the DEIR mitigation) could cause a small adverse or beneficial effect on tricolored blackbird use of the Natomas Basin, but in either case this effect is unlikely to alter the viability of the tricolored blackbird population using the Natomas Basin. Based on 2001 land cover, the Greenbriar project would increase the quantity of nesting habitat in the Natomas Basin (by 201 acres or about 9%), but would decrease the quantity of foraging habitat (by 598 acres or about 3%). This loss of foraging habitat would be partially (but not fully) offset by the preservation and enhancement of 135 acres of foraging habitat. Although currently, nesting habitat is more limited than foraging habitat in the Natomas Basin, under the future condition much more nesting habitat will exist, and thus the additional nesting habitat that would be provided by the project may not affect the tricolored blackbird population more than the loss of foraging habitat that would also result. However, because the project would only cause a small beneficial or adverse effect on tricolored blackbird use of the Natomas Basin, and because the Natomas Basin accounts for only a small portion of the habitat for and population of tricolored blackbird in the Central Valley, the Greenbriar project is unlikely to alter the viability of the tricolored blackbird population using the Natomas Basin.

The project with the mitigation proposed in the DEIR would result in both adverse and beneficial effects on the Swainson's hawk population nesting and foraging in the Natomas Basin, but these effects would be insufficient to alter the population's viability. Adverse effects would include a reduction in the total acreage of foraging habitat under the future condition (by 222 acres or 2%), fragmentation, and possibly degradation of habitat near the Greenbriar site, and a reduction in habitat available to hawks nesting at reserves near the Greenbriar site. Beneficial effects would include an overall increase in the acreage of high quality habitat, enhancing and preserving habitat within a mile of TNBC reserves, and possibly contributing to the connectivity of foraging habitat adjacent to proposed reserves and the mitigation site required by mitigation measure 6.13-2 of the DEIR.

Overall, the project would have a neutral effect. This interpretation is based on the USFWS interpretation of effects on Swainson's hawk due to the NBHCP (USFWS 2003). The availability of foraging habitat during April—August (the nesting period) is considered to limit the abundance and reproductive success of Swainson's hawk in the Natomas Basin (CH2M HILL 2003, USFWS 2003). Based on the methods used by CH2M HILL (2003) to evaluate availability of foraging habitat, the enhancement of habitat at the proposed reserves and mitigation sites would increase the availability of foraging habitat during these months. Using an alternative analysis developed by EDAW, this effects analysis estimated that during April—June the increase in foraging habitat values at the proposed reserve and mitigation sites would be about 6% greater than the habitat values lost by development at the Greenbriar site; during July—August, foraging values would not be fully offset, but foraging habitat values would be higher within the Natomas Basin as a whole at this time because of the harvesting of crops. Thus, based on these analyses, the project would not be expected to reduce the number of hawks nesting in the Natomas Basin or their reproductive success.

The project would cause both adverse and beneficial effects on the populations of giant garter snake and northwestern pond turtle that use canals, wetlands, and rice in the Natomas Basin; overall, the project would not adversely affect these populations. Beneficial effects would include preserving, creating, and enhancing habitat at the reserve sites, preserving and enhancing a 250-foot wide corridor along a portion of Lone Tree Canal, and contributing to the connectivity of habitat and existing TNBC reserves adjacent to or near the proposed reserves. Adverse effects would include a reduction in the total acreage of habitat by 204 acres, and possibly degradation of habitat near the Greenbriar site and reduced connectivity along Lone Tree Canal as a result of increased human disturbance and predation (which would result from narrowing the corridor of land along Lone Tree Canal, and placing residential development adjacent to it). The DEIR mitigation would reduce these adverse effects and ensure that connectivity of giant garter snake habitat was conserved along Lone Tree Canal at the Greenbriar site. For example, to minimize risks to connectivity due to human disturbance and predation, the DEIR mitigation includes requirements for fencing and barriers, and the creation of habitat along the canal.

The loss of habitat acreage would be offset by the increased habitat quality resulting from the preservation of habitat, and conversion of rice to marsh. The project (with the DEIR mitigation) also would conserve connectivity and habitat for giant garter snake along the affected section of Lone Tree Canal, which is an important waterway connecting the southern and central Natomas Basin, and proposed reserves would contribute to connectivity of habitats and reserves in the southern and central Basin.

Of the seven plant species covered by the NBHCP, the Greenbriar project would not affect the five vernal pool-associated species because these species are not known to occur in the vicinity of the Greenbriar or proposed reserve sites, nor is suitable habitat present at or near these sites. These plant species are: Boggs Lake hedge-hyssop, Sacramento Orcutt grass, slender Orcutt grass, Colusa grass and legenere. The other two covered plant species (delta tule pea and Sanford's arrowhead) are not known to occur at the Greenbriar or the proposed reserve sites, but suitable habitat for these species does occur at or near some of these sites, which have not been surveyed for these species. Overall, the project would increase the acreage of suitable habitat for these species (i.e., marsh and canal habitats) in the Natomas Basin. Nonetheless, because these species are not known to occur in the Natomas Basin, the project probably would not alter the viability of any of their populations.

#### ES 3.2 EFFECTS ON THE CONSERVATION STRATEGY OF THE NBHCP

The Greenbriar project (with the *DEIR* mitigation) would not reduce the effectiveness of the NBHCP's conservation strategy. In Section IV.C.1 (pages IV 5-15), the NBHCP describes the basis of the key components of the NBHCP's conservation strategy and how these components provide effective mitigation for 17,500 acres of urban development. These components are:

- ▶ basis for 0.5 to 1 mitigation ratio (Section IV.C.1.a),
- ▶ preparation of site specific management plans (Section IV.C.1.b),
- ▶ buffers within the reserve lands (Section IV.C.1.c),

- ► connectivity (Section IV.C.1.d),
- ▶ foraging habitat (Section IV.C.1.e), and
- ▶ 2,500-acre/400-acre minimum habitat block size requirements (Section IV.C.1.f).

In describing the basis for the 0.5:1 mitigation ratio, the NBHCP states that the ratio mitigates the impacts of the incidental take authorized under the NBHCP because much of the land to be developed does not provide habitat or provides only marginal habitat, and because the TNBC-managed reserves will provide habitat of higher quality than the eliminated habitat. Because the Greenbriar project would not alter the habitat value of land authorized for development under the NBHCP, and would not adversely affect the habitat value of TNBC reserves established under the NBHCP, the project would not affect the basis for the 0.5:1 mitigation ratio of the NBHCP. Although the project would result in the conversion of agricultural land and open space to urban development on an additional 546 acres of land in addition to the 17,500 acres of permitted development under the NBHCP, with the proposed mitigation, this conversion to urban development would result in a minimal change to the conditions in which the NBHCP conversation strategy is being implemented.

The Greenbriar site is not adjacent to existing TNBC reserves, and thus would not alter the effectiveness of the buffers within these reserve lands. Also, because under the future condition of the Natomas Basin resulting from the NBHCP, the Greenbriar site would already be bordered by urban development, highways or major roads on all sides, development of the Greenbriar site could cause only very limited effects on the effectiveness of buffers within future reserves, even if reserves were established on adjacent land to the north or southwest (i.e., adjacent land that would not be developed under the future condition of the Natomas Basin).

The development and reserves resulting from the Greenbriar project would, however, need to be considered in the development of site-specific management plans for existing and future reserves in their vicinity. Although the loss of raptor habitat at the Greenbriar site would be mitigated, there would still be less foraging habitat in the vicinity of some sites as a result of the project, which could alter site-specific plans. Also, the proposed reserves would provide additional options for management and future acquisitions that could alter the management plans of nearby TNBC reserves.

Overall, the project with the DEIR mitigations would not reduce connectivity of reserves or habitats within the Natomas Basin. The proposed reserve and mitigation sites would probably improve connectivity of habitats and TNBC reserves, and potential adverse effects on Lone Tree Canal would be minimized by measures included in the project design and additional mitigation measures in the DEIR. A comprehensive set of measures would be implemented to both reduce the project's effects on and to enhance the habitat in a 250-foot wide corridor along the Lone Tree Canal, which would provide garter snake habitat connectivity. These measures would prevent the project from reducing the connectivity of canal habitats and TNBC reserves, and also would prevent the project from subdividing the Basin's giant garter snake population into two smaller, and thus less viable, populations.

With the DEIR mitigation, the project would not reduce the availability of foraging resources for the Swainson's hawk in the Natomas Basin, and thus not affect reproduction or survival. Based on 2001 land cover, the Greenbriar project, however, would result in a net reduction of 253 acres of upland land cover providing habitat for covered species, it would enhance or create, and preserve, at least 135 acres of upland land cover types (plus 60 acres of upland components of created marshes). As a result, the upland habitats that would result from the project would provide foraging resources during the months of April—August (when Swainson's hawks are nesting in the Basin) comparable to the habitats that would be eliminated by the project. Based on the method CH2M HILL (2003) used to analyze effects of the NBHCP, the acreage of available foraging habitat would be increased by the project; based on the additional analysis conducted by EDAW for this effects analysis, the increase of habitat values resulting from enhancement would be greater than values lost at the Greenbriar site during April—June but not during July—August. Although the loss of values would not be fully offset during July—August, foraging resources increase in the Natomas Basin during those months from the harvesting crops, and therefore, Swainson's hawk is unlikely to be affected. (Both the mitigation and eliminated habitat would be within a mile of nesting habitat that is currently occupied.) By maintaining foraging resources during the critical April—

June period, the Greenbriar project would not compromise the NBHCP Operating Conservation Program, and thus actions such as those listed on pages IV-13 and IV-14 of the NBHCP would not be necessary.

Overall, the project would avoid, minimize and mitigate adverse effects of development by establishing large blocks of preserved habitat. It would enhance and preserve 296 acres of additional habitat adjacent to or near existing TNBC reserves and the *DEIR* mitigation would increase this benefit by requiring the preservation of at least an additional 49 acres of land. The project would adversely affect the preservation of large blocks of habitat by developing existing habitat at the Greenbriar site. Under the future condition of the Natomas Basin, this land would be surrounded by major roads and urban development, and the Greenbriar project includes design measures to preserve the most ecologically important portion of the site, the corridor of land along Lone Tree Canal.

#### ES 3.3 EFFECTS ON ATTAINMENT OF NBHCP GOALS AND OBJECTIVES

For many of the same reasons that viability of populations and the effectiveness of the NBHCP's conservation strategy would not be reduced, the Greenbriar project would not reduce the likelihood of attaining the goals and objectives of the NBHCP. Below, the overall effect resulting from the project (with the *DEIR* mitigations) is summarized for each goal or objective that could be affected.

**Overall Goal 1.** Establish and manage in perpetuity a biologically sound and interconnected habitat reserve system that mitigates impacts on Covered Species resulting from Covered Activities and provides habitat for existing, and new viable populations of Covered Species. (NBHCP, p. I-15)

The project (with its mitigation) would have an overall beneficial effect on the establishment and management of reserves for the NBHCP. Because the acreage of land in the Natomas Basin that is potentially available and suitable for preservation substantially exceeds the 8,750 acres that will be preserved by the NBHCP, the project would not preclude the preservation of sufficient land to attain the NBHCP's goals and objectives. It would provide reserve lands adjacent to or near existing reserves, increasing the connectivity of habitats and the resources available to covered species using reserves established by the NBHCP; in addition, it would conserve a portion of an important corridor of canal habitat along Lone Tree Canal. The project also would increase opportunities to establish new reserves, particularly to create larger reserves by preserving additional land adjacent to the project's proposed and existing TNBC reserves.

Although the project would cause a net reduction in the acreage of upland and wetland habitats, the preservation and enhancement of habitat by the project would adequately mitigate for its effects on upland and wetland habitats of covered species. Based on 2001 land cover mapping, the Greenbriar project would eliminate 388 acres of rice and 16 acres of canal habitats, but would increase the acreage of marsh by 201 acres, creating a net loss of 204 acres of these wetland land cover types and of the habitats they provide. An acre of marsh, however, provides a greater quantity and variety of habitat than does an acre of rice for several reasons. These reasons include:

- ► Giant garter snakes primarily use the margins of rice fields, whereas they use the full extent of managed marshes. These marshes are designed to provide open water, foraging habitat, dense cover, basking sites, and refugia in close proximity throughout the marsh. (For example, an acre of managed marsh provides several times the edge habitat than does a rice field.)
- ▶ Marshes provide habitat throughout the active period of the snake. Rice fields do not provide habitat during early and mid-spring, and are typically drained before the end of the snake's active period. Thus, for a portion of their active period, giant garter snakes must rely entirely on non-rice habitats. In the Natomas Basin, these habitats are canals and managed marsh. In contrast, managed marshes provide habitat year-round.
- ▶ Rice is fallowed periodically, and thus does not provide habitat in all years; in contrast, a managed marsh does provide habitat in all years.

Thus, the additional habitat values provided by the created marsh offsets the habitat values lost in the rice and canal land cover types. In addition, the project would preserve, and manage for its habitat values, the 201 acres of created marsh (i.e., about 1 acre for each acre lost), ensuring the long-term persistence of this habitat. Similarly, based on 2001 land cover, the Greenbriar project would cause a net reduction of 253 acres of upland land cover providing habitat for covered species, but would enhance and preserve 135 acres of upland habitats (plus 60 acres of upland components in created marshes for a total of 195 acres of upland habitat preserved). For most covered species associated with upland habitats, the additional habitat values resulting from this enhancement and preservation would offset the project's reduction of the acreage of upland habitats in the Natomas Basin. For example, during the months of April–August, when Swainson's hawks are nesting in the Basin, the enhancement of upland habitats that would result from the project would provide foraging resources comparable to the habitats that would be eliminated by the project.

As previously described, the potential effects (both adverse and beneficial) that would result from implementing the proposed project (including the DEIR mitigation) would be unlikely to alter the population viability of any of the covered species.

**Overall Goal 3.** Preserve open space and habitat that may also benefit local, non-listed and transitory wildlife species not identified within the NBHCP. (NBHCP, page I-16)

As described under Overall Goal 1 above, the project would have an overall beneficial effect on the TNBC reserve system. Furthermore, the project (with DEIR mitigation) would slightly increase the ratio of habitat preserved to habitat developed in the Natomas Basin by setting aside land at a ratio (0.6:1) that exceeds the 0.5:1 ratio required for development authorized by the NBHCP, and would include more extensive creation, enhancement, and management of habitat. For these reasons, the project (with the DEIR mitigation) would have an overall beneficial effect on the attainment of this goal.

**Overall Goal 4.** Ensure that direct impacts of Authorized Development upon Covered Species are avoided or minimized to the maximum extent practicable. (NBHCP, page I-16)

With the DEIR mitigation, the project would not adversely affect attainment of this goal because it would implement a comprehensive set of measures to avoid and minimize effects on covered species to the maximum extent practicable. The potential direct impacts are comparable to the potential direct impacts of the development authorized by the NBHCP. Thus, the Greenbriar project with the DEIR mitigation would include all of the applicable avoidance and minimization measures included in the NBHCP to avoid and minimize construction-related effects, and several more stringent minimization measures. The project also would include a set of measures to avoid and minimize effects on the Lone Tree Canal corridor. The Greenbriar project also would not alter the effectiveness of any NBHCP conservation measures for avoiding and minimizing the effects of development authorized by the NBHCP.

**Overall Objective 1.** Minimize conflicts between wildlife and human activities, including conflicts resulting from airplane traffic, roads and automobile traffic, predation by domestic pets, and harassment by people. (NBHCP, page I-16).

With the DEIR mitigation, the project would not adversely affect attainment of this objective because it would implement a comprehensive set of measures that would minimize human-wildlife conflicts. These measures include all of the applicable measures that were included in the NBHCP to avoid and minimize construction-related effects and to reduce human-wildlife conflicts, plus additional measures (e.g., fencing and barriers) to reduce human-wildlife conflicts along Lone Tree Canal. The Greenbriar project also would not alter the effectiveness of any NBHCP conservation measures for minimizing human-wildlife conflicts resulting from development authorized by the NBHCP.

**Overall Objective 3.** Ensure connectivity between TNBC reserves to minimize habitat fragmentation and species isolation. Connections between reserves will generally take the form of common property boundaries between

reserves, waterways (primarily irrigation and drainage channels) passing between reserves, and/or an interlinking network of water supply channels or canals. (NBHCP, page I-16)

The Greenbriar project would cause beneficial and adverse effects on the attainment of this objective through most of these mechanisms; its overall effect, however, would not be adverse. The main beneficial effects would be increased connectivity of habitats and TNBC reserves due to preservation, creation and enhancement of habitat at the project's proposed reserves, two of which are adjacent to or near (i.e., within a half mile of) existing TNBC reserves. Adverse effects would include reducing the foraging habitat within a mile of a TNBC reserve, fragmenting and reducing the connectivity of upland habitats adjacent to the Greenbriar site, and possibly reducing the connectivity of wetland habitats and TNBC reserves because of effects on Lone Tree Canal (despite preserving a corridor along the canal). The DEIR mitigation would reduce these adverse effects by incorporating additional measures to ensure that connectivity along Lone Tree Canal is sustained, and to preserve and enhance foraging habitat within a mile of existing TNBC reserve(s). (The connectivity of upland habitats, however, would still be reduced at the Greenbriar site.) In the absence of an adverse effect on connectivity along Lone Tree Canal, the project would cause only small effects on the attainment of this objective, and most of these effects would be beneficial.

**Wetland Species/Habitat Goal/Objective 1.** Acquire, enhance and create a mosaic of wetland habitats with adjacent uplands and connecting corridors to provide breeding, wintering, foraging, and cover areas for wetland species in the Plan Area. (NBHCP, page I-17)

For wetland land cover (i.e., rice, canal, and ponds and seasonally wet areas), the net reduction in acreage resulting from the development of the Greenbriar site would be offset by creating and managing marsh at the project's proposed reserves. Based on 2001 land cover mapping, the Greenbriar project would eliminate 388 acres of rice and 16 acres of canal habitats, but would increase the acreage of marsh by 201 acres, creating a net loss of 204 acres of these wetland land cover types and of the habitats they provide. An acre of marsh, however, provides a greater quantity and variety of habitat values than does an acre of rice, and thus the additional habitat provided by the created marsh offsets the habitat lost in the rice and canal land cover types. In addition, the project would preserve, and manage for its habitat values, the 201 acres of created marsh (i.e., about 1 acre for each acre lost), ensuring the long-term persistence of this habitat.

The project would not have an overall adverse effect, and might have a beneficial effect on, connectivity of wetland habitats. This overall effect on connectivity of wetland habitats is described under Overall Objective 1 above.

**Wetland Species/Habitat Goal/Objective 2.** Provide habitat to maintain, attract and sustain viable populations of the Covered Species. The habitat areas should be configured to encompass natural species migration areas, minimize species isolation, and prevent future habitat fragmentation. (NBHCP, page I-17)

The project would enhance and preserve habitat to offset its adverse effects and that would sustain populations of the covered species, and would not alter the population viability of any of the covered species. The habitat enhanced and preserved by the project and the project's effects on the TNBC reserve system are described under Overall Goal 1 above. The project's effect on the viability of each covered species is described under *Effects on Covered Species* above.

**Upland Species/Habitat Goal/Objective 1.** *Acquire, enhance and create a mosaic of upland habitat types for breeding, foraging, and cover for species dependent on upland habitats. (NBHCP, page I-17)* 

Overall, the project would not adversely and could beneficially affect this goal/objective. Because the acreage of upland habitat in the Natomas Basin that is potentially available and suitable for preservation is substantially more than the acreage of upland habitat that would be preserved and enhanced by the NBHCP, and the project would affect only a small percentage of this land, the project would not preclude the preservation of sufficient land to

attain the NBHCP's goals and objectives. The project would, however, increase opportunities to establish new and/or larger reserves, which would aid the attainment of this goal/objective.

**Upland Species/Habitat Goal/Objective 2.** Ensure reserve land connectivity with travel corridors for upland-dependent species. The habitat areas should encompass grasslands, agricultural croplands, riparian habitats, and shelter and nesting habitat areas (fence rows, clusters of shrubs and small trees), as well as wetland areas to provide a year-round source of water for upland species. The upland areas should be configured to enhance natural species migration, minimize species isolation, and prevent future habitat fragmentation. (NBHCP, page I-17)

A moderate level of uncertainty exists regarding the overall effect of the Greenbriar project on this goal/objective. The proposed changes at the Greenbriar site would have an uncertain effect on the movement and dispersal of upland species; also there is uncertainty regarding the project's contributions to connectivity elsewhere in the Basin because the location of the mitigation site that would account for much of upland habitat preserved has not been determined. However, because the project would cause adverse and beneficial effects that are similar in nature and magnitude, and would affect only a small portion of the Basin's land area, the project would have only a small overall effect on the attainment of this goal/objective, whether it was beneficial or adverse.

#### **ES.4 SUMMARY**

In summary, the Greenbriar project (with the DEIR mitigation) would not reduce the viability of populations of covered species using the Natomas Basin and would not reduce the effectiveness of the conservation strategy of the NBHCP. It also would have only small effects on the likelihood of attaining any of the goals and objectives of the NBHCP, and for most of these goals and objectives the overall effect would be neutral or beneficial.

#### 1 INTRODUCTION

This section presents the scope of the effects analysis, an overview of the proposed Greenbriar project, and the intended uses of this document. This section also summarizes the organization of the Effects Analysis.

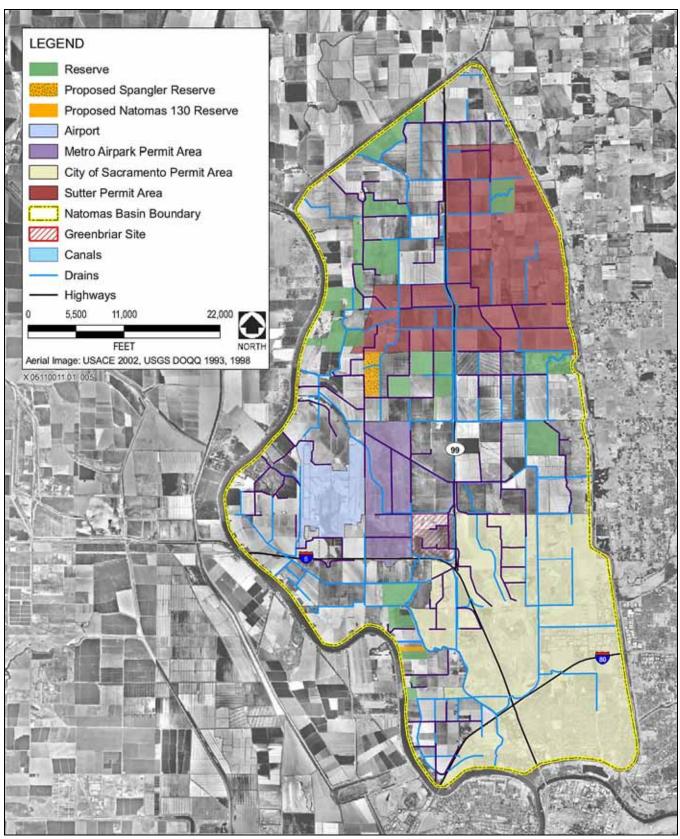
#### 1.1 INTRODUCTION

This analysis of effects of the Greenbriar project on the Natomas Basin Habitat Conservation plan (effects analysis) evaluates the effects of the Greenbriar project on each species covered by the Natomas Basin Habitat Conservation Plan (NBHCP), on the conservation strategy of the NBHCP, and on attainment of the NBHCP's goals and objectives. This project would include development at the Greenbriar site, which is located within the boundaries of the NBHCP plan area, but is not within an area permitted for development. The project also includes establishment of onsite and offsite reserves. The project could affect the population viability of species covered by the NBHCP, the conservation strategy of the NBHCP, or the attainment of the NBHCP's goals and objectives. The purpose of this evaluation is to document the potential effects of the Greenbriar project and evaluate its overall effect on the viability of populations of species covered by the NBHCP and on attainment of the goals and objectives of the NBHCP. Effects on the Metro Air Park Habitat Conservation Plan (MAP HCP) also were considered. However, the MAP HCP was designed to support and follow the regional conservation strategy of the NBHCP; its covered species are a subset of those covered by the NBHCP, and its biological goals and objectives largely represent a subset of the NBHCP's goals and objectives. (In fact, the MAP HCP has been superseded by the 2003 NBHCP.) Thus, the results of this effects analysis also document the project's potential effects on the MAP HCP's covered species and biological goals and objectives. Potential conflicts with and relationships to specific measures of the MAP HCP are also included in this evaluation.

The NBHCP was developed to satisfy the requirements of the Endangered Species Act for a permit for the incidental take of threatened and endangered species. It is intended to minimize and mitigate for the loss of habitat and the incidental take of covered species that could result from urban development and management of reserves in the Natomas Basin. The NBHCP authorizes 17,500 acres of development in the MAP, City of Sacramento, and Sutter County permit areas, and outside of these areas it preserves 8,750 acres in a reserve system surrounded by agricultural lands (Exhibit 1). The reserve system will consist of 4,375 acres of rice, 2,187 acres of created marsh, and 2,187 acres of upland habitat. In this reserve system, land will be managed to enhance its habitat values. The future condition of the Natomas Basin resulting from the NBHCP would provide fewer acres of habitat for covered species than existed in 2001. The U.S. Fish and Wildlife Service (USFWS) considers the reserve system with high quality habitat created by the NBHCP to adequately mitigate and offset the effects of this habitat loss because most of the lost habitat would be of lower quality (USFWS 2003). Consequently, most of the NBHCP's goals and objectives are related to creating a reserve system that provides high quality habitats and is likely to sustain populations of the covered species in the Natomas Basin for the foreseeable future. The NBHCP also includes numerous avoidance, minimization, and mitigation measures to reduce the effects of development on covered species and to ensure the creation and effective operation of the reserve system.

#### 1.2 OVERVIEW OF GREENBRIAR PROJECT

The Greenbriar project would develop the 577-acre Greenbriar site located northwest of the intersection of State Route 99 and Interstate 5 in Sacramento County (Exhibit 2). This site is bordered by agricultural land uses to the north and south, new residential development to the east, and the recently approved Metro Air Park development to the west. As currently proposed, the project would create a residential development with commercial and retail centers, an elementary school, neighborhood parks and a water feature (approximately 39 acres in size). A new east-west roadway, Meister Way, would be constructed through the center of the site. Along this roadway, a new light rail station is proposed to be eventually constructed by Sacramento Regional Transit near the center of the site that would connect the Greenbriar site to the Sacramento International Airport development to the west and to



Source: CH2M HILL, EDAW 2005

#### Location of Greenbriar Project in the Natomas Basin

Exhibit 1



Source: CH2M HILL, Ellen Berryman, Sacramento County 2002

### Project Boundary and Conservation Easement Locations at the Greenbriar Site

Exhibit 2

the North Natomas Community to the east across Highway 99 via a new proposed overpass over Highway 99. This development is adjacent to, but outside of, the areas of development permitted by the NBHCP.

Along with this development, the project would preserve, enhance, and create habitat in a 250-foot wide corridor along the site's western edge (occupying approximately 31 acres) and would preserve, enhance, and create habitats off-site at two proposed reserves: the Natomas 130 (30.2 acres, primarily of alfalfa and created marsh with smaller acreages of canal, riparian, and tree grove) and Spangler (235.4 acres, primarily of alfalfa and created marsh with a smaller acreage of canal) reserves.

Preserved lands would become part of reserve system operated by TNBC, or if necessary would be managed by another nonprofit entity. For each reserve, TNBC develops a site-specific management plan, and management activities include habitat management, monitoring, invasive plant control, domestic/feral animal control, and restricting public access and patrolling reserves to enforce restrictions. As part of its management, TNBC also implements a set of measures to avoid and/or minimize take of covered species. These measures are described on pages IV-29 through IV-38 of the NBHCP.

The fee title and an endowment would be provided to TNBC (or if necessary another nonprofit entity) by the project proponent. The endowment would provide for the restoration/enhancement, operation, maintenance, monitoring, and administration of the reserves. For the reserves proposed by the Greenbriar project, a larger endowment fee than that required for NBHCP mitigation may be necessary to provide for the required management. Additional details regarding Greenbriar's funding of these reserves will be developed through the HCP amendment or HCP process together with the development of reserve management plans. The reserve management plans will include details regarding effectiveness monitoring, adaptive management, and a schedule for acquisition of reserve uplands and implementation of all mitigation measures required through the Section 10(a)(1)(B) and Section 2081 permit processes. (For the proposed reserve along Lone Tree Canal, the management plan will include a legal agreement with the Natomas Mutual Water Company regarding vegetation management.) These reserve management plans will form the basis for calculating Greenbriar's endowment fee in consultation with the wildlife agencies.

In addition to the proposed reserves and measures incorporated as part of the proposed Greenbriar project, the City of Sacramento, through the CEQA process, has proposed mitigation measures for the project to reduce further the project's adverse effects. (Throughout this document, "mitigation" refers to these measures proposed by the City of Sacramento in the DEIR, unless otherwise noted as measures incorporated into the Greenbriar project's design.) These DEIR mitigation measures include the preservation of at least an additional 49 acres of land managed to provide high quality Swainson's hawk foraging habitat. This preserved land also would become part of TNBC reserve system. The location of this mitigation land has not yet been determined.

The Greenbriar site is outside of the area permitted for development; thus, the habitat loss, preservation and enhancement resulting from the project is in addition to that permitted by the NBHCP. Consequently, the project would alter the future condition of the Natomas Basin.

#### 1.3 USE OF THIS DOCUMENT

The Greenbriar EIR and Effects Analysis operate in tandem to evaluate the effects of implementation of the Greenbriar project on biological resources. The EIR satisfies the requirements of CEQA partly by considering these effects in light of the NBHCP, IA, and ITP requirements as analyzed in depth in the Effects Analysis (DEIR, Appendix P). The Greenbriar Project is located outside of the 17,500 acre permit area of the NBHCP. The NBHCP, Implementation Agreement, Biological Opinion and ITPs provide that because the NBHCP's Operating Conservation Plan is based upon the City limiting total development to 8,050 acres within the City's Permit Area, approval by the City of future urban development beyond the 8,050 acres or outside of its Permit Area would "constitute a significant departure from the NBHCP's OCP" and would trigger reevaluation of the NBHCP, a new effects analysis, potential amendments and/or revisions to the NBHCP and ITPs, a separate conservation strategy

and the need to obtain a new ITP by the Permittee for that additional development, and/or possible suspension or revocation of the City's ITP in the event the City were to violate such limitations without having completed the required reevaluation, and amendments or revisions if necessary, or having obtained a new permit. (See e.g., Implementation Agreement for the NBHCP, Section 3.1.1[a].) As part of this process, Greenbriar intends to file an application for a project-specific HCP.

This EIR evaluates the effects of the Greenbriar project in consideration of the NBHCP, IA and ITP requirements and is based upon an Effects Analysis prepared by the City's EIR consultant with biological resource information provided by Greenbriar's biologists. The purpose of this effects analysis is to support the analysis contained in the EIR and to provide the foundation for the preparation of an amendment to the NBHCP or a new HCP for the addition of the Greenbriar project to the City's permit area.

When the amendment to the NBHCP or new HCP process is initiated with USFWS and CDFG, the Effects Analysis will be reviewed by the USFWS and CDFG through the Section 10(a)(1)(B) and Section 2081 permit processes to assure the Greenbriar project's consistency with federal and state endangered species act requirements and to guide the wildlife agencies in their determinations as to the project's effects on the effectiveness of the NBHCP. Following development of an amendment to the NBHCP or new HCP, the City and/or the Greenbriar project applicant will be required to obtain amended or new ITPs from USFWS and CDFG authorizing incidental take of state and federally listed threatened and endangered species.

If LAFCo approves the proposed annexation of the Greenbriar Project to the City, then the City and/or Greenbriar project applicant will be required to initiate a new HCP or NBHCP amendment process with the wildlife agencies prior to final map approval. USFWS approval of the HCP/NBHCP amendment and issuance of the ITP/ITP amendment will be subject to review under NEPA. The Greenbrier EIR would provide a basis for consideration of environmental impacts under NEPA, and it is intended to provide the environmental information for CDFG action under CEQA. However, CDFG consideration of the HCP/HCP amendment and ITP/ITP amendment could result in subsequent environmental review under CEQA, if CDFG determines, on the basis of substantial evidence in light of the whole record, that there are substantial changes in the project or circumstances in which the project is undertaken, or new information indicates that new or substantially more severe significant environmental effects would occur than were covered in the Greenbriar EIR. Although incidental take would not occur until grading of the site occurs, issuance of the ITPs/amendments will be required prior to final map approval by the City of Sacramento to ensure that any adjustments to the subdivision map approvals (e.g., changes in site design) resulting from the HCP/ITP process occur prior to recordation of a final map.

#### 1.4 ORGANIZATION

This report presents the results of an analysis of the effects of the Greenbriar project (with the DEIR mitigation) on the future condition of the Natomas Basin, and how those changes would affect species covered by the NBHCP and attainment of the NBHCP's goals and objectives.

The Effects Analysis is organized in the following way:

- ▶ Section 1, Introduction
- Section 2, Evaluation Approach
- ► Section 3, Greenbriar Project's Alteration of Population and Habitat Attributes
- Section 4, Potential Effects of the Greenbriar Project on Covered Species
- ► Section 5, Potential Effects on the Conservation Strategy of the NBHCP
- ► Section 6, Potential Effects of the Greenbriar Project on NBHCP Goals and Objectives

- ► Section 7, Cumulative Effects
- ► Appendix A, Assessment of Avoidance and Minimization of Construction-related Effects and Human-Wildlife Conflicts
- ► Appendix B, Change in Natomas Basin Land Cover in 2001–2004

#### 2 EVALUATION APPROACH

#### 2.1 OVERVIEW

The Greenbriar project could affect covered species, effectiveness of the NBHCP conservation strategy, effectiveness of specific conservation measures, attainment of NBHCP goals and objectives, or cumulative effects by altering any of several population or habitat attributes. These attributes include:

- ► Construction-related effects on survival and reproduction,
- ► Zones with human-wildlife conflicts (i.e., areas adjacent to developed lands and roads),
- ► Acreage of habitat in Natomas Basin,
- ▶ Quality of habitat in the Natomas Basin,
- ► Connectivity of habitat in Natomas Basin,
- ► Connectivity of existing TNBC reserves,
- ► Habitat value of existing TNBC reserves,
- ▶ Water availability at TNBC reserves, and
- Opportunities to establish additional TNBC reserves.

For each of these attributes, alterations resulting from the Greenbriar project were analyzed. The findings of this effects analysis of the effects on covered species, effectiveness of the NBHCP conservation strategy, effectiveness of specific conservation measures, and NBHCP goals and objectives was based on the results of the analyses of the above attributes. The methodologies and the bases for the interpretations of effects on covered species and NBHCP goals and objectives are described below. In addition, this analysis of effects on covered species was also based on available information on the distribution of these species in the Natomas Basin and on their ecology.

Analyses of cumulative effects also were based on the results of these analyses together with additional analyses of land cover, and the compilation and review of projects proposed in the Natomas Basin.

#### 2.2 DESCRIPTION OF GREENBRIAR PROJECT

The analysis of the effects of the Greenbriar project is based on a description of the project (including the mitigation measures proposed as part of the project design) that was compiled from multiple sources. The primary source was the Greenbriar Draft Environmental Impact Report (DEIR) (EDAW 2005). Additional information was derived from the draft conceptual mitigation plan for the project (Wildlands, Inc. 2005), Greenbriar Draft Biological Assessment (BA) (Berryman Ecological 2005), and personal communications with project consultants. The draft conceptual mitigation plan describes the proposed Natomas 130 and Spangler reserves, and the proposed on-site reserve along Lone Tree Canal, and the proposed restoration of these areas to provide upland and wetland habitats. This conceptual mitigation plan also evaluated whether the proposed reserve sites met the TNBC's typical conditions for mitigation-land dedication. The draft BA includes proposed avoidance and minimization measures, and a description of the proposed preservation, restoration, and future management of habitat along Lone Tree Canal.

After the conceptual mitigation plan and draft BA were produced, several changes were made to the proposed habitat creation and enhancement at the Natomas 130 and Spangler sites. First, the proposed acreage of restored habitats was changed to 204.2 acres of managed marsh and associated canals (14.2 acres at Natomas 130 created from upland non-rice cropland and 190 acres at Spangler created from rice) and 59.6 acres of upland in alfalfa (14.2 acres at Natomas 130 and 45.4 acres at Spangler). The managed marsh would have 30% upland components. A revised conceptual mitigation plan that reflects these changes is under development. This effects analysis also assumed that development of an HCP for this project would result in mitigation providing habitat values comparable or greater than the proposed acreage of marsh and alfalfa evaluated in this effects analysis.

As indicated by the draft conceptual mitigation plan, and as explicitly required by the DEIR mitigation, the proposed reserves would be dedicated to TNBC, or another entity if necessary, with an endowment sufficient to pay for required restoration and management in perpetuity. The management of these reserves would be as described in sections VI-D, V-B, VI-E, VI-F, and VI-G of the NBHCP (Conservation Plan – Reserve/Management/Site Specific Management Plans; Take Avoidance, Minimization, and Mitigation; and Plan Implementation-Monitoring of the NBHCP, Adaptive Management, Annual Report, respectively) or that comparable management would be developed in consultation with USFWS and incorporated into an HCP for the project. As described in sections VI-D, V-B, VIE, VI-F, and VI-G of the NBHCP, this management would include:

- ▶ Development of a site-specific management plan;
- ► Implementation of measures to reduce take of covered species as a result of restoration and reserve management;
- ▶ Implementation of the NBHCP's conservation strategies for covered species on the reserves;
- ▶ Management activities that include invasive plant control, domestic/feral animal control, and restricting public access and patrolling reserves to enforce restrictions;
- ► Compliance and biological effectiveness monitoring; and
- An annual reporting and review meeting to cover progress toward meeting goals, implementation, monitoring, and adaptive management measures.

The dedication of the proposed reserves and their endowments would occur prior to entitlement of the project, and restoration would be initiated within one year of their dedication. Because of their specific management requirements (e.g., having uplands planted in alfalfa), greater proportion of managed marsh, and the potentially high maintenance costs for the small reserve proposed along Lone Tree Canal, this endowment may be greater per acre than the endowment for NBHCP mitigation lands.

Furthermore, in the DEIR, mitigation includes preservation and enhancement of Swainson's hawk foraging habitat, multiple measures to reduce effects on giant garter snake habitat and the snake's use of Lone Tree Canal as a movement corridor, and development and approval of a Habitat Conservation Plan (HCP) for compliance with the federal Endangered Species Act.

The DEIR mitigation for Swainson's hawk foraging habitat (mitigation measure 6.13-2) requires the preservation of an area of habitat that provides habitat values to the species comparable to the habitat eliminated at the Greenbriar site. This DEIR mitigation measure would require preservation of at least an additional 49 acres of land to be enhanced and managed to provide high quality Swainson's hawk foraging habitat. The actual acreage of this mitigation will be determined during development of an HCP for the project (as described in the DEIR), and will depend on the site attributes and future management that determine the level of habitat enhancement (as described in Section 2.3.4 *Quality of Habitat in the Natomas Basin*).

The DEIR mitigation for giant garter snake includes measures to reduce the project's effects on snakes use of Lone Tree Canal as a movement corridor. These measures include:

a. To ensure that the project does not diminish habitat connectivity for giant garter snake between the southwest and northwest zones identified in the NBHCP, approximately 30.6 acres along Lone Tree Canal shall be protected and managed as giant garter snake habitat. This on-site habitat preservation shall protect an approximately 250-foot wide corridor of giant garter snake habitat that includes the canal and approximately 200 feet of adjacent uplands. Uplands within the linear open space/buffer area shall be managed as perennial grassland as described below. Additional aquatic habitat for giant garter snake shall be created along the east

bank of Lone Tree Canal by construction and maintenance of a 2.7 acre tule bench. The habitat shall be managed in perpetuity as high-quality habitat for giant garter snake. Compliance and biological effectiveness monitoring shall be performed and annual monitoring reports prepared within six months of completion of monitoring for any given year. This monitoring, reporting, and adaptive management shall be performed as described in Section IV of the NBHCP.

- b. To ensure that the project does not diminish giant garter snake movement along Lone Tree Canal, all new road crossings of Lone Tree Canal shall be designed to minimize obstacles to giant garter snake movement. The use of culverts under new road crossings on Lone Tree Canal shall be prohibited unless it can be demonstrated that the culverts will not diminish the potential for giant garter snake movement through the section of Lone Tree Canal protected by the setback fence and conservation easement.
- c. Upland giant garter snake habitat within the Lone Tree Canal linear open space/buffer area shall be created and managed to provide cover, basking areas, and refugia during the winter dormant period. Hibernaculae would be constructed at regular intervals by embedding concrete or coarse rock in the bank or in a berm along the Lone Tree Canal corridor to provide additional winter refugia. Upland habitat with the linear open space/buffer areas shall be converted to native perennial grassland and managed, in perpetuity, as perennial grassland habitat.
- d. Aquatic habitat shall be maintained throughout the giant garter snake active season in Lone Tree Canal, in perpetuity. This is the legal responsibility and obligation of Metro Air Park property owners (MAP). The MAP HCP includes provisions for maintaining water in the canal such that the basic habitat requirements of the giant garter snake are met. The MAP HCP also provides a road map, through "Changed Circumstances", to address procedures to follow if water is not being maintained in the canal to meet these requirements. As described in the MAP HCP, the MAP is legally obligated to assure these requirements are met, and financial and procedural mechanisms are included in the MAP HCP to enforce this. It is, therefore, assumed that MAP will provide water to Lone Tree Canal, as required by the MAP HCP and ITP, in perpetuity. It is also assumed that USFWS will use all reasonable means available to it, to enforce this MAP HCP requirement. If water is not provided to Lone Tree Canal by the MAP to meet the habitat requirements of giant garter snake, as required by the MAP HCP, and USFWS exhausts its enforcement responsibilities, the project applicant shall assume the responsibility of providing suitable giant garter snake aquatic habitat throughout the section of Lone Tree Canal protected by the fence and conservation easement. However, as stated herein, the project applicant shall only assume this responsibility if it has been sufficiently demonstrated to the City that USFWS has exhausted all reasonable means to compel MAP to comply with the relevant conditions of the MAP ITP. Specific requirements related to ensuring suitable aquatic habitat in Lone Tree Canal is present, in perpetuity, throughout the giant garter snake active season shall be developed through consultation with DFG and USFWS, and included in the new or amended HCP for Greenbriar, and may include mechanisms, such as installation of a well, to assure water is provided in the canal to meet habitat requirements.
- e. A barrier shall be installed between the giant garter snake habitat linear open space/buffer area and the adjacent Greenbriar development to ensure that giant garter snakes do not enter the development area, and to prohibit humans and pets from entering the giant garter snake habitat. The design of this barrier shall be subject to USFWS and CDFG review and approval. The entire length of the barrier, which shall be bordered by yards rather than roadways, shall be maintained on the preserve side by a nonprofit land trust to ensure that vegetation or debris does not accumulate near the barrier and provide opportunities for wildlife and pets to climb over the barrier. On the development side, Covenants, Codes and Restrictions (CCRs) shall prohibit accumulation of vegetation or debris adjacent to the barrier. Chain link fencing shall be placed at both ends of the corridor, with locked gates permitting entry only by RD 1000 and NMWD for channel maintenance, and by the preserve manager for habitat monitoring and maintenance purposes.

- f. Specific requirements associated with the barrier shall be developed through consultation with USFWS and DFG, and may include the following and/or other specifications that DFG and USFWS consider to be equally or more effective:
  - Adequate height and below-ground depth to prevent snakes or burrowing mammals from providing a through-route for snakes by establishing burrows from one side to the other crossing;
  - ► Constructed using extruded concrete or block construction extending a minimum of 36-inches above ground level;
  - ▶ Maintenance to repair the barrier and to prevent the establishment of vegetation or collection of debris that could provide snakes with a climbing surface allowing them to breech the barrier;
  - A cap or lip extending at least two-inches beyond the barrier's vertical edge to prevent snakes from gaining access along the barrier's top edge; and
  - ▶ Signage to discourage humans and their pets from entering the area.
- g. The Lone Tree Canal linear open space/buffer area shall be protected in perpetuity under a conservation easement and managed to sustain the value of this area for giant garter snake habitat connectivity. Compliance and biological effectiveness monitoring shall be performed and annual monitoring reports prepared. This monitoring, reporting, and adaptive management shall be performed as described in Section IV of the NBHCP or following procedures developed in formal consultation with USFWS and DFG and contained in an ESA Incidental Take Permit for the Greenbriar project.

As a result of consultation with the USFWS, the HCP for the Greenbriar project could result in different mitigation than is described in the draft BA, conceptual mitigation plan, or the DEIR. The mitigation described in the DEIR, however, establishes a level of mitigation that will be met or exceeded in the HCP. Thus, the HCP will reduce effects to a comparable or lower level than the mitigation analyzed in this effects analysis.

## 2.3 METHODOLOGY FOR ANALYZING ALTERATIONS OF POPULATIONS AND HABITATS

#### 2.3.1 CONSTRUCTION-RELATED EFFECTS ON SURVIVAL AND REPRODUCTION

Information regarding the presence of covered species or potentially suitable habitat for these species at the Greenbriar site and adjacent lands was derived from the Greenbriar Draft Environmental Impact Report (DEIR) (EDAW 2005), Greenbriar Draft Biological Assessment (BA) (Berryman Ecological 2005), and a draft conceptual mitigation plan for the project (Wildlands, Inc. 2005). These documents, in turn, were based on site assessments by wildlife biologists and compilation and analysis of the best available data.

Each species was considered to be either likely, possibly, or not affected by construction-activities based on evidence of its presence and of the presence of potentially suitable habitat. Species documented recently (i.e., in the past 5 years) at or adjacent to the Greenbriar or proposed reserve sites were considered to still be using suitable habitat at that site; these species were considered likely to be affected by construction-related activities. The land area considered adjacent to the Greenbriar or proposed reserve sites differed among species according to their ecology (i.e., their territory and home range sizes, daily and seasonal movements, and their susceptibility to disturbance).

Species not recently documented at or adjacent to the Greenbriar site, but for which potentially suitable habitat has been documented at or adjacent to the site, were considered potentially present and thus individuals of those

species may be affected by construction activities. (These species were considered potentially present because surveys performed to date have not been adequate to determine absence of these species.)

Species not recently documented at or adjacent to the Greenbriar site, and for which no potentially suitable habitat was located on or adjacent to the site, were considered to not be affected by construction activities.

For species likely to be or possibly affected by construction-related activities, the avoidance and mitigation measures proposed for the Greenbriar project were evaluated. The extent of construction-related effects is reduced through appropriate avoidance and minimization measures. Where combinations of construction activities and affected species and habitats would be similar to those addressed by the NBHCP, this analysis considered the applicable avoidance and minimization measures in the NBHCP (Chapter V) that address construction-related effects to be a complete set of appropriate (and feasible) avoidance and minimization measures for comparable effects potentially caused by the Greenbriar project. Thus, a table of measures in the NBHCP was compiled, measures applicable to the project were identified, and inclusion of each measure in the project and its mitigation was evaluated based on the content of the BA and DEIR for the project. This table was used in evaluating the project's effects on attainment of NBHCP goals and objectives that address the implementation of avoidance and minimization measures. The analysis also considered the need for different measures to address effects that would be likely and that would differ from those addressed by the NBHCP, and the potential for the Greenbriar project to alter the efficacy of the NBHCP measures (Appendix A).

#### 2.3.2 Zones with Human-Wildlife Conflicts

Considerable conflicts between wildlife use and human activities (e.g., animal-vehicle collisions, harassment and predation by pets, degradation of water quality) normally occur in habitat areas adjacent to developed land uses and major roads. These effects diminish with distance, but the distance at which they are no longer significant is debatable.

In this document, the widths used to evaluate human-wildlife conflicts, alterations of vegetation and other habitat conditions, habitat fragmentation, and effects on existing reserves, were based on the ecological literature regarding effects on habitat adjacent to developed land uses and roads, and on the distances used in previous analyses related to the NBHCP or incorporated into the NBHCP itself, The effects of developed land uses on adjacent land diminish with distance. The different types of effects, however, extend different distances onto adjacent land; these distances can be from tens to thousands of feet, and differ not only among mechanisms but among sites as well (because of variation in site attributes such as the presence of barriers and the quantity of impervious surfaces). Thus, in a regional analysis, the use of a specific width only indicates the area within which effects of adjacent developed land are often sufficient to alter habitats.

In the GIS-based evaluations, two widths were used, 800 feet and one mile. The 800-foot width was used in evaluating zones where increased human disturbance, predation from cats and dogs, vehicle collisions, dumping, and alterations to soils, hydrology and vegetation were likely to occur. The one-mile width was used in evaluating the effects on foraging habitat for animals with large home ranges, such as raptors. Both widths are consistent with the ecological literature regarding these effects and the ecology of species in the Natomas Basin, and were previously used in comparable analyses supporting the NBHCP.

The Greenbriar project could cause human-wildlife conflicts in this zone by altering the acreage in the zone (because of an altered perimeter of development) or by altering the intensity of wildlife-human conflicts (because of the avoidance and minimization measures implemented or a change in land cover types in this zone). Change in the extent of the 800-foot wide zone was calculated from the acreage in this zone around the MAP, City of Sacramento and Sutter County permit areas for urban development from the Final NBHCP (City of Sacramento et al. 2003) and around these permit areas plus a developed Greenbriar site. Changes to the intensity of wildlife-human conflicts in the 800-foot wide zone were assessed by calculating changes in land cover types within these zones and by comparing the project's avoidance and minimization measures with those in the NBHCP that

address these conflicts. An increase in land cover providing higher quality habitat (or land cover more sensitive to human disturbance) would increase human-wildlife conflicts, while a decrease in such land cover types would reduce human-wildlife conflicts. Similarly, a less comprehensive or stringent set of measures would increase the intensity of conflicts, while a more comprehensive or stringent set of measures would reduce the intensity of conflicts. Any reduction in the efficacy of specific NBHCP measures addressing human-wildlife conflicts also could increase conflicts; potential effects on the efficacy of these measures were evaluated in Appendix A.

#### 2.3.3 ACREAGE OF HABITAT IN THE NATOMAS BASIN

A major component of the effects analysis in the NBHCP was an analysis of change in habitat acreage. For each covered species, the NBHCP analyzed the habitat that was available under baseline conditions and that would be available in the expected future condition of the Natomas Basin. The NBHCP documented baseline land cover in the Natomas Basin as of 2001. The data sources and methods used to do so are described in *Natomas Basin Conservation Plan Impacts to Proposed Covered Species* (CH2M HILL 2002) that was attached to the Final NBHCP as Appendix H. The Natomas Basin covers approximately 53,538 acres. The future condition evaluated was the result of developing an additional 17,500 acres of this land in the MAP, City of Sacramento, and Sutter County permit areas and establishing an 8,750–acre reserve system in the Natomas Basin outside of those permit areas. For each covered species, changes in habitat acreages were derived from the changes in the acreage of land cover types by identifying those land cover types that provide habitat for that species. Additional analyses were performed for Swainson's hawk that included assessment of changes in habitat within 1 mile of existing reserves and nests, quality of foraging habitat, and seasonal availability of foraging habitat.

The Greenbriar project would alter these future conditions by developing additional land and by preserving and enhancing additional land as part of the TNBC reserve system. Thus, for this project's effects analysis, for each covered species, the future condition of the Natomas Basin with the NBHCP and the Greenbriar project was compared to the future condition analyzed in the NBHCP and to the 2001 NBHCP baseline. For the Greenbriar and proposed reserve sites, these comparisons were based primarily on 2001 land cover to be consistent with and comparable to the NBHCP's effects analysis, and because 2001 conditions were used as the NBHCP baseline. These comparisons allow assessment of both the extent of future habitat under the future condition resulting from the NBHCP and under the future condition resulting from the NBHCP plus the Greenbriar project. These were GIS-based analyses. The land cover GIS data layer developed for the NBHCP was the data source for land cover. This was the available land cover data most applicable to this analysis.

Effects based on 2005 land cover were also quantified and considered. This was done by using aerial photography to update the land cover mapped in 2001 in a manner consistent with the 2001 mapping. This mapping used different criteria and was at a coarser scale than some of the land cover mapping in the BA and DEIR (which was based in part on site surveys by biologists). These differences did not lead to different conclusions regarding the efficacy of mitigation for the project's effects.

Land cover mapped by Jones & Stokes was also considered in our analyses (Jones & Stokes 2005; Jones & Stokes, unpublished data) (Appendix B). This mapping used different land cover classification and mapping methods from the 2001 mapping by CH2M HILL, which limited its applicability to this analysis. Nonetheless, a crosswalk between the CH2M HILL and Jones & Stokes land cover types was developed and a common classification was derived; after reclassifying both data sets, EDAW estimated land cover changes during 2001–2004, and used the results to assess overall changes in land cover, implementation of NBHCP conservation strategies on TNBC reserves, stability of agricultural land uses, and fallowing of rice in anticipation of development. This analysis is presented in Appendix B. Its results also were used in the cumulative effects analyses in Section 7 *Cumulative Effects*.

This assessment indicated that land cover changes since 2001 have occurred primarily within the MAP, City of Sacramento, and Sutter County permit areas for urban development, and at TNBC reserves; the primary land cover changes outside of these areas were an increase in the acreage of rice, a substantial decrease in the acreage

of non-rice crops and a corresponding increase in the acreage of fallowed and abandoned cropland. It did not indicate that fallowing of rice in anticipation of development was occurring. Although the dramatic changes in non-rice crop and idle cropland acreages affect the acreage of available habitat for just two covered species (burrowing owl and Aleutian Canada goose), they do illustrate that availability of agricultural habitats can change rapidly in the Natomas Basin; they also indicate that estimates of future availability of agricultural habitats in the NBHCP and in this report represent approximations based on assumptions that may not occur (i.e., that current patterns of agricultural land use are representative of future patterns).

Other GIS data layers used in the analyses included the locations of canals and drains, and the boundaries of the Natomas Basin, NBHCP permit areas, and of the Greenbriar and proposed reserve sites. In our analyses, canal habitats were analyzed differently than in the Final NBHCP. In the Final NBHCP, canals and drains were assigned to four categories (I-IV) based on the width of habitat they provided; of these, only category I canals were included in the land cover layer and categories II-IV were estimated separately. In contrast, we included all habitat along category I-IV waterways in the canal land cover type, Because these canal acreages were included in the canal land cover type in our analyses, the future acreages of land cover types differ somewhat from those presented in the NBHCP.

To assess the future condition of the Natomas Basin with the Greenbriar project, several assumptions were made regarding changes in land cover. These assumptions included the following.

- ▶ All land in the MAP, City of Sacramento, and Sutter County permit areas was assumed to be developed, or otherwise no longer providing habitat for covered species.
- ▶ Land at the Greenbriar site was assumed to be developed, or otherwise no longer providing habitat for covered species, except for a 250-foot wide corridor along the western edge of the Greenbriar site would be preserved. Land in this corridor would be converted to grassland, except for approximately 2.7 acres of tule marsh that would be created, and 1.4 acres of riparian habitat that was mapped in the conserved corridor in 2001 and would presumably recover and persist in the proposed reserve.
- ▶ All other areas were treated as in the effects analysis for the NBHCP, except that 8,750 acres (not including the project's proposed reserves) would be incorporated into a reserve system. The reserve system would be approximately 25% managed marsh, 50% rice and 25% upland land cover types. For estimating acreage changes, the managed marsh and rice was considered to come out of the baseline rice acreage.
- ▶ Under the future condition, land at the project's proposed reserve sites was assigned to land cover types based on the *Greenbriar Draft Conceptual Habitat Restoration Design* prepared by Wildlands, Inc. (2005), and subsequent revisions by the project applicant. The mitigation land required by Mitigation Measure 6.13-2 of the DEIR was not included in the GIS analysis because its location has not been determined.
- ► Preserved land would be dedicated to TNBC (or another nonprofit land trust) and an endowment would be provided for the enhancement, operations, maintenance, and administration of preserved land in perpetuity.)

Thus, the future condition that was analyzed assumes that the project, all development proposed under the NBHCP and all associated mitigation would occur, and that current agricultural land uses are representative of future agricultural land uses. These or comparable assumptions were also made in the effects analyses supporting the NBHCP (e.g., sections 3 and 4 of Appendix H of the NBHCP, and Section 2 of Appendix K).

Changes in the acreage of habitat for a covered species were the sum of changes in land cover types providing habitat for that species. The habitat-land cover relationships used in analyses supporting the NBHCP were also applied to analyses for the Greenbriar project. These relationships are summarized in Table 2-1. Vernal pool-associated species were not considered in these analyses because the Greenbriar and proposed reserve sites do not contain vernal pool habitats nor have vernal-pool associated species been documented in the vicinity of these sites.

Also, in addition to these analyses of Basin-wide GIS data sets, we also considered more detailed site-specific information provided in the DEIR, BA, and the most recent TNBC monitoring report (Jones & Stokes 2005).

| Table 2-1<br>Species Habitat-Land Cover Relationships |                  |         |        |           |          |      |                |            |          |       |         |                             |      |          |         |                      |             |       |
|---|------------------|---------|--------|-----------|----------|------|----------------|------------|----------|-------|---------|-----------------------------|------|----------|---------|----------------------|-------------|-------|
|   | Land Cover Types |         |        |           |          |      |                |            |          |       |         |                             |      |          |         |                      |             |       |
| Species   |                  | Alfalfa | Canals | Grassland | Highways | Idle | Non-rice Crops | Oak Groves | Orchards | Other | Pasture | Ponds and<br>Seasonally Wet | Rice | Riparian | Ruderal | Rural<br>Residential | Tree Groves | Urban |
| Giant garter snake                                    |                  |         | X      |           |          |      |                |            |          |       |         | X                           | X    |          |         |                      |             |       |
| Swainson's hawk (N)                                   |                  |         |        |           |          |      |                | X          |          |       |         |                             |      | X        |         |                      | X           |       |
| Swainson's hawk (F)                                   |                  | X       |        | X         |          | X    | X              |            |          |       | X       |                             |      |          | X       |                      |             |       |
| Burrowing owl   |                  | X       | X      | X         |          | X    |                |            |          |       | X       |                             |      |          | X       |                      |             |       |
| Loggerhead shrike                                     |                  | X       | X      | X         |          | X    | X              | X          | X        |       | X       | X                           |      | X        | X       | X                    | X           |       |
| Tricolored blackbird (F)                              |                  | X       |        | X         |          |      | X              |            |          |       | X       |                             | X    |          |         |                      |             |       |
| Aleutian Canada goose (F)                             |                  |         |        |           |          |      | X              |            |          |       | X       |                             | X    |          |         |                      |             |       |
| White-faced ibis                                      |                  | X       | X      |           |          |      |                |            |          |       |         | X                           | X    |          |         |                      |             |       |
| Bank swallow  |                  | X       | X      | X         |          |      | X              |            |          |       | X       | X                           | X    | X        |         |                      |             |       |
| Valley elderberry longhorn beetle                     |                  |         |        |           |          |      |                |            |          |       |         |                             |      | X        |         |                      |             |       |
| Northwestern pond turtle                              |                  |         | X      |           |          |      |                |            |          |       |         | X                           | X    | X        |         |                      |             |       |
| Sanford's arrowhead                                   |                  |         | X      |           |          |      |                |            |          |       |         | X                           |      |          |         | _                    |             |       |
| Delta tule pea  |                  |         | X      |           |          |      |                |            |          |       |         | X                           |      |          |         |                      |             |       |

#### 2.3.4 QUALITY OF HABITAT IN THE NATOMAS BASIN

Changes in habitat quality can result from changes in land cover, connectivity, adjacent land uses, and the preservation and management of land to enhance its habitat quality, changes in connectivity, and adjacent land uses. In this report, changes in the acreage of land cover types providing different quality habitat and changes in the acreage of land preserved and managed to enhance habitat quality were derived from the analyses of change in habitat acreages described in the preceding section (*Acreage of Habitat in the Natomas Basin*). Changes in habitat quality resulting from changes in connectivity or adjacent land uses were evaluated separately, and these evaluations are described in other sections.

For Swainson's hawk, the quality and seasonal availability of foraging habitat for Swainson's hawk were evaluated in a manner comparable to the effects analysis conducted by CH2M HILL for the NBHCP (CH2M HILL 2003). In addition, based on a quantitative model of the relative value of different foraging habitats, EDAW also analyzed the overall quantity of resources provided by foraging habitat in the Natomas Basin with and without the Greenbriar project. Though based largely on similar interpretations of existing information as the CH2M HILL analyses for the NBHCP, this model was developed by EDAW biologists for this effects analysis.

In the analysis conducted for the NBHCP, crops and other land cover types were placed in high, medium and low categories for habitat value. This was done on the basis of previous research (e.g., Estep 1989, Estep and Teresa 1992). Seasonal availability of prey was considered separately by calculating the "monthly availability of

potential foraging habitat." (This analysis of habitat availability was based on the assumption that for row and field crops, prey were only available to hawks at the time of harvest.) Because food resources for Swainson's hawk vary substantially among land cover and crop types, these analyses provided much more information than a simple tabulation of acres of potential foraging habitat. However, these analyses did not produce an estimate of total foraging resources that would indicate the overall change in habitat. Therefore, in addition to applying the same analysis as CH2M HILL conducted for the NBHCP, EDAW also estimated the total food resource potentially provided by foraging habitat.

In the analyses supporting the NBHCP, alfalfa and idle cropland were considered to be high value habitat; sugar beet, tomato, melons, squash and cucumber, beans, wheat, pastures (clover, unspecified or mixed) and ruderal land was considered moderate value habitat; Corn, safflower, onions and garlic, and unspecified row and field crops were considered low quality habitat.

The temporal availability of prey was also considered in an analysis conducted for the NBHCP. In this analysis, prey was considered inaccessible to Swainson's hawk during much of the spring and summer because of the dense (and high) cover of vegetation in cultivated fields. In contrast, crops, such as alfalfa, and other land cover types (e.g., grassland) were considered to provide accessible prey for longer periods because of frequent harvests or the vegetation's growth form. Thus, during the months of April–October, for the different crop types grown in the Natomas Basin, prey was assumed to be accessible only during the months when harvest predominantly occurs. These time periods were June for wheat, July–August for tomato and unspecified crops, August for safflower onions and garlic, September–October for sugar beet, and October for beans, melons, squash and cucumber. (Swainson's hawks have migrated out of the Natomas Basin by October, and thus crops harvested in October do not provide foraging habitat in the NBHCP analysis.) For crops harvested during periods of two months, the total acreage of these crops was divided by two to determine the acreage of foraging habitat available during each of those months. Grassland, ruderal, idle cropland, and pastures (including alfalfa) were considered to provide habitat throughout April–September.

These analyses regarding habitat value and temporal availability were applied to the Greenbriar project. For this analysis, the habitat value of the Greenbriar, proposed reserve, and DEIR mitigation sites was compared with and without the proposed development and proposed habitat creation, enhancement, and preservation.

For these analyses, the habitat value of the Greenbriar, proposed reserve and DEIR mitigation sites without the Greenbriar project was based on the same data sources as the analysis conducted for the NBHCP (i.e., 1993 DWR mapping of croplands and 2001 land cover mapping by CH2M HILL of the entire Natomas Basin).

The habitat value of the Greenbriar, proposed reserve and DEIR mitigation sites with the Greenbriar project was based on an assumed future condition derived from the project description and mitigation measure 6.13-2 of the DEIR for the project. For this assumed future condition, the acreages of habitats at these sites are presented in Table 2-2. For the Greenbriar site, these assumptions were that the 26.5 acres of preserved grassland that would be created and preserved along Lone Tree Canal would be low quality habitat (because of its proximity to development), and that the rest of the site would not provide any habitat for Swainson's hawk. For the proposed off-site reserves, these assumptions were that the 59.6 acres of upland at the Natomas 130 and Spangler sites would be alfalfa (or otherwise managed to provide high quality habitat) and that the 59.5 acres of upland components of created marsh would provide moderate quality habitat.

Mitigation measure 6.13-2 of the DEIR, which requires at least 49 acres of land be preserved, enhanced, and managed in perpetuity to provide high quality foraging habitat for Swainson's hawk so that the project's proposed mitigation plus this DEIR mitigation would provide equal or greater value to the species than the habitat present at the Greenbriar site in 2005. The location(s) and existing land cover of the Swainson's hawk foraging habitat that would be required by mitigation measure 6.13-2 have not been determined; this analysis assumed that the current land cover of the mitigation site(s) that would provide foraging habitat for Swainson's hawk was agricultural land harvested during July–August and providing low quality habitat. As mitigation for the project, it

was assumed that this land would be converted to high quality habitat with prey available from April through September. These assumptions represent the minimum acreage at an additional site that would need to be preserved, enhanced, and managed in perpetuity to comply with mitigation measure 6.13-2.

| Habitat Type Acrea  | ges Used i         | n Analyse       | Table 2-2<br>s of Effect |                 | inson's Ha         | wk Forag        | ing Habita         | ıt              |  |
|---|--------------------|-----------------|--------------------------|-----------------|--------------------|-----------------|--------------------|-----------------|--|
|   | Greenb             | riar Site       | Proposed                 | Reserves        | DEIR Mi            | tigation        | Total              |                 |  |
| Habitat   | Without<br>Project | With<br>Project | Without<br>Project       | With<br>Project | Without<br>Project | With<br>Project | Without<br>Project | With<br>Project |  |
| Alfalfa   | -                  | -               | -                        | 59.6            |                    | 49              | -                  | 108.9           |  |
| Grassland <sup>1</sup>  | -                  | 26.5            | -                        | -               | -                  | -               | -                  | 26.5            |  |
| Idle  | 62.5               | -               | -                        | -               | -                  | -               | 62.5               | -               |  |
| Ruderal   | 9.2                | -               | -                        | -               | -                  | -               | 9.2                | -               |  |
| Pasture   | 33.8               | -               | -                        | -               | -                  | -               | 33.8               | -               |  |
| Upland component of marsh                                     | -                  | -               | -                        | 59.5            | -                  | -               | -                  | 59.5            |  |
| Field crop – Moderate quality,<br>harvested September–October | 203.7              | -               | 28.4                     | -               | -                  | -               | 232                | -               |  |
| Field crop – Low quality,<br>harvested July–August            | 30.4               | -               | -                        | -               | 49                 | -               | 79.4               | -               |  |

The EDAW model of Swainson's hawk foraging habitat uses the same current and assumed future conditions as were used for the NBHCP. The range of habitat quality, however, was divided into four categories, rather than three. These ratings changed seasonally for cropland, and a relative quantitative value was assigned to each category so that the total quantity of food resources potentially available could be estimated. The following text describes EDAW's methodology for calculating this estimate.

For each month during April–September, each crop and other land cover type providing foraging habitat was assigned to one of four quality ratings: high, high-moderate, moderate, or low. These ratings are given in Table 2-3. Crops and the other land cover types that provide foraging habitat were assigned these ratings on the basis of prey abundance; the accessibility of prey to the hawk; and on the frequency of harvest, flood irrigation, and other activities that create valuable foraging opportunities for Swainson's hawks, as indicated by the existing literature (Estep 1989, Estep and Teresa 1992). The frequency of harvest, flood irrigation and other activities was considered in rating habitats because of the importance of these activities for hawk foraging. For example, in the radio telemetry study conducted by Estep (1989), approximately half of all Swainson's hawk foraging was associated with harvest, flood irrigation, and other agricultural activities.

Alfalfa combines a high frequency of mowing and irrigation with low vegetation that leave prey accessible to hawks. For these reasons, this land cover type was rated "high" quality.

Grassland, ruderal, idle cropland, upland components of marsh, and fallowed rice also have low vegetation that leaves prey accessible, and can have prey abundance comparable (or even greater than) alfalfa. However these land cover types lack the frequent cultivation and irrigation activities that provide valuable foraging opportunities, and therefore were rated "high-moderate."

Row crops with relatively dense vegetation that limits prey accessibility but still allows some foraging throughout the field (e.g., tomato, beets) were rated "moderate."

Dense, tall crops (e.g., corn, wheat) that restrict foraging to field margins were considered "low" quality foraging habitat. Because of its proximity to development, the proposed grassland along Lone Tree Canal also was considered to provide low quality foraging habitat.

| Table 2-3<br>Habitat Quality and Harvest Months for Swainson's Hawk Foraging Habitats in the Natomas Basin <sup>1</sup> |                   |                        |                 |                      |  |  |  |  |  |  |
|---|-------------------|------------------------|-----------------|----------------------|--|--|--|--|--|--|
| Habitat   | Harvest Month(s)  | Growing Season Quality | Harvest Quality | Post-Harvest Quality |  |  |  |  |  |  |
| Alfalfa   | April-Sept        | High                   | High            | High                 |  |  |  |  |  |  |
| $Grassland^2$   | -                 | High-Moderate          | -               | -                    |  |  |  |  |  |  |
| Idle  | -                 | High-Moderate          | -               | -                    |  |  |  |  |  |  |
| Fallowed Rice   | -                 | High-Moderate          | -               | -                    |  |  |  |  |  |  |
| Tomato  | July-August       | Moderate               | High            | Low                  |  |  |  |  |  |  |
| Sugar beet  | September-October | Moderate               | High            | Low                  |  |  |  |  |  |  |
| Beans   | October           | Moderate               | High            | Low                  |  |  |  |  |  |  |
| Squash, pumpkin   | October           | Moderate               | High            | Low                  |  |  |  |  |  |  |
| Upland Marsh  | -                 | Moderate               | -               | -                    |  |  |  |  |  |  |
| Pasture   | -                 | Moderate               | -               | -                    |  |  |  |  |  |  |
| Ruderal   | -                 | Moderate               | -               | -                    |  |  |  |  |  |  |
| Wheat   | June              | Low                    | High            | Low                  |  |  |  |  |  |  |
| Unspecified crop  | July-Aug          | Low                    | High            | Low                  |  |  |  |  |  |  |
| Safflower   | August            | Low                    | High            | Low                  |  |  |  |  |  |  |
| Onions and garlic   | August            | Low                    | High            | Low                  |  |  |  |  |  |  |
| Corn  | September         | Low                    | High            | Low                  |  |  |  |  |  |  |

#### Notes

The harvest of crops makes the relatively high density of prey in cropland much more accessible, and this brief period of high accessibility and high abundance is followed by continued accessibility but rapidly declining abundance. Therefore, crops providing low and moderate quality habitat during the growing season were considered to provide high quality habitat for a two weeks at harvest, and then subsequently their habitat quality was reduced to low. Harvest times were considered to be the same as in the NBHCP analysis (CH2M HILL 2003) and these are listed in Table 2-3. For crops harvested during a two-month period, half of the acreage was assumed to be harvested each month, and for that half of the acreage, the growing season and harvest quality ratings were averaged for that month.

To calculate an estimate of food resources provided by foraging habitats, the value of each habitat type was expressed relative to high quality habitat, which was assigned a value of "1." These values are an interpretation of the relevant existing scientific literature that includes studies of the use of foraging habitat and relative prey abundance in different crop and other cover types (Estep 1989, Estep and Teresa 1992). Because in low quality habitat, the tall and dense vegetation restricts foraging to field margins, low quality habitats were assigned a value of "0.1." (However, because harvest makes prey available, the value of these lands is raised to "1" for a two-week interval during the harvest period.) Because the vegetation height and density of moderate quality crops allows some access to prey throughout the field, these crops were assigned a value of "0.3." (During harvest, moderate

<sup>&</sup>lt;sup>1</sup> - Data based on CH2M Hill 2003, except for growing season quality of grassland, idle and fallowed rice, as described in methods section.

<sup>2 -</sup> Grassland in proposed reserve along Lone Tree Canal was considered to be low quality habitat because of surrounding development.

quality crops were assigned a "1" rating for a two-week interval, and their rating was subsequently reduced to "0.1".) Because high-moderate quality foraging habitat has accessible and relatively abundant prey, but not the frequent harvest, flood irrigation, and other activities of high quality habitat, it was assigned a value of "0.5".

Multiplying the acreage in each habitat quality category by these relative values, and then summing the products, provides an estimate of the total forage available to Swainson's hawks in the Natomas Basin. The units of this estimate are the equivalent acreage of high quality foraging habitat. These estimates, though rough approximations, provide an explicit, consistent basis for analyzing changes in the quantity of food potentially available to Swainson's hawk in the Natomas Basin. Estimates were calculated for the Greenbriar, proposed reserve, and mitigation sites with and without the proposed project and DEIR mitigation.

In addition to these analyses, other effects on habitat quality for Swainson's hawk and giant garter snake also were considered. As in the NBHCP, effects on habitat within 1 mile of recently documented Swainson's hawk nests (i.e., nests documented in the last 5 years) were considered. For giant garter snake, effects were also considered for upland land cover types that could provide habitat and that were adjacent to canals.

#### 2.3.5 Connectivity of Habitat in the Natomas Basin

The Greenbriar project could affect the connectivity of habitat by eliminating or creating waterways, affecting the use of waterways by covered species, or by altering the length, width, or habitat attributes of existing corridors of natural vegetation. In assessing these effects, several assumptions were made including the following.

- ▶ All of the Greenbriar site would be developed, except for a 250-foot wide corridor along Lone Tree Canal.
- ▶ All waterways in the developed portion of the Greenbriar site would be eliminated.
- ▶ In the absence of avoidance and minimization measures, all waterways and uplands within 800 feet of the Greenbriar, Spangler, or Natomas 130 sites could potentially be affected by the project. (Ecologically significant effects caused by developed land uses were considered to not extend beyond an 800-foot wide zone adjacent to developed land cover and highways, and the basis for selecting this width is further described in Section 2.2.2 *Zones with Human-Wildlife Conflicts*.)
- ▶ At the proposed Spangler and Natomas 130 reserves, waterways would remain except where rice was converted to upland land cover, and land cover would be changed as described in the Draft Conceptual Restoration Plan prepared by Wildlands, Inc. (2005) and subsequent revisions by the project applicant.

Interpretations of effects on connectivity were based on general ecological literature regarding wildlife use of corridors, recent reviews of the ecology of covered species, and consultations with species experts. Along canals, potential changes in physical conditions (e.g., flow regime, culvert dimensions), vegetation structure and extent, human disturbance, and predation were all evaluated as factors potentially altering connectivity.

#### 2.3.6 CONNECTIVITY OF TNBC RESERVES

The connectivity of TNBC reserves can be altered by altering upland corridors or waterways between existing reserves. Upland corridors are affected by narrowing their width, altering the habitat attributes of the land in them, or by altering their length. The assessment of these potential effects was based on the same assumptions and conducted in the same manner as previously described for Connectivity of Habitat in the Natomas Basin, except that only effects on corridors between existing reserves were considered rather than effects on all lands. (Corridors were considered to not pass through urban land.) We assumed that the most ecologically important upland corridors include the shortest paths between reserves.

Waterways are also important corridors connecting TNBC reserves. Thus, altering the location or habitat value of waterways could affect the connectivity of existing reserves. This effect was evaluated by identifying all waterways within 800 feet of the Greenbriar site, and determining if they were part of the shortest path along waterways between reserves, in a corridor between reserves with multiple waterways, or otherwise could be important for species movement between reserves (e.g., species use of the waterway has been documented). We also considered the recent documentation of habitat conditions along canals by Eric Hansen (Jones & Stokes 2005, Eric Hansen, unpublished data). Our analysis of waterways connecting TNBC reserves was based on analysis of GIS data for waterways in the Natomas Basin, and on boundaries of existing TNBC reserves, MAP, City of Sacramento, and Sutter County permit areas, and of the Greenbriar, Spangler, and Natomas 130 sites, and on species distribution data and consultation with knowledgeable individuals. For this analysis, ecologically significant effects of developed land uses and roads were not considered to extend in general beyond an 800-foot zone of adjacent land; the basis for selecting this width is further described in the section describing the evaluation of zones with human-wildlife conflicts.

#### 2.3.7 Habitat Value Of Existing TNBC Reserves

Changes in adjacent land cover can affect existing TNBC reserves by altering foraging habitat accessible from a reserve or by altering the habitat values of reserve lands through development or preservation of adjacent lands. Thus, we performed three analyses to evaluate effects on the habitat value of existing TNBC reserves. These analyses are described below.

- The effects of the project on foraging habitat were evaluated based on changes in land cover because of the project within 800 feet and 1 mile of existing reserves. Most effects of developed land uses and roads were considered to not extend beyond an 800-foot wide zone of adjacent land. (The basis for selecting this width is described in the section describing the evaluation of zones with human-wildlife conflicts.) Furthermore, as summarized in Section 4 of this document (*Potential Effects of the Greenbriar Project on Covered Species*), the territories and home ranges of some covered (and many other) species residing at the reserves are unlikely to extend more than 800 feet from reserve boundaries. However, Swainson's hawk and other raptors have much larger home ranges and territories; for these species, land within 1 mile of reserves was considered to include the most important habitat for individuals nesting on reserves. (This premise is comparable to that underlying the analysis of Swainson's hawk habitat in the Natomas Basin presented in *Natomas Basin Conservation Plan Impacts to Proposed Covered Species* [CH2M HILL 2003] and included in Appendix K of the NBHCP).
- ► The effects of additional development on habitat values of TNBC reserves were evaluated by calculating the acreage of existing TNBC reserves within 800 feet of additional developed land cover that would result from the project. This 800-foot criterion is the desired distance of reserves from urban land (described on page IV-16 of the NBHCP) and also includes the area that would experience ecologically significant effects caused by adjacent developed land uses and roads.
- ► The proximity of the proposed reserves to existing reserves was examined to determine if any were adjacent to existing reserves, and if they expanded the area, increased the habitat variety or reduced the perimeter-to area ratio of the reserve.

#### 2.3.8 WATER AVAILABILITY AT TNBC RESERVES

The project could alter water availability at TNBC reserves if it were to eliminate sections of canals that are required for water deliveries to TNBC reserves, contribute to the elimination of other canals by affecting demand for water deliveries and increase the land ownership of TNBC and its corresponding water use and ownership of stock in Natomas Mutual.

It was assumed that all canals in developed portions of the Greenbriar site would be eliminated, and that consequently, sections of canal off-site but directly connected to canal segments on the Greenbriar site could be

abandoned. The connection of each of these eliminated or potentially abandoned canal segments to TNBC reserves was evaluated, and the effect on water availability to reserves was assessed.

In addition, Natomas Mutual and RD 1000 were contacted regarding waterways that could be eliminated because of the project. Elimination of canals or drains by these water agencies or due to a development project, however, would likely require mitigation under either Section 7 or Section 10 of the Endangered Species Act, and therefore their effects would likely be mitigated even if their elimination occurred separately from the project.

The project's effect on TNBC stock ownership in Natomas Mutual also was considered. Natomas Mutual is a privately held water company comprised of landowner stockholders. As TNBC acquires mitigation lands in the Natomas Basin, it increases its shares in Natomas Mutual. This increased ownership could result in TNBC changing operations and maintenance practices to support the goals and objectives of the NBHCP. The project would increase TNBC ownership and thus its influence on the operations of Natomas Mutual. The magnitude of this increase in ownership and its likely effects were assessed.

#### 2.3.9 OPPORTUNITIES TO ESTABLISH ADDITIONAL TNBC RESERVES

The Greenbriar project could affect opportunities to establish additional TNBC reserves by reducing the acreage of land available for satisfying the mitigation requirements of the development permitted through the NBHCP, or by expanding existing reserves so that more interconnected reserves can be established that exceed the 400-acre minimum desired size. These potential effects were evaluated by estimating the acreage potentially available for NBHCP mitigation with and without the project, and by examining the connectivity of the proposed Spangler and Natomas 130 reserves to existing TNBC reserves.

The acreage potentially available for NBHCP mitigation without the project was estimated by subtracting the following areas from the Natomas Basin's total acreage of land suitable for preservation followed by restoration or enhancement: MAP, City of Sacramento, and Sutter County permit areas for urban development, the County-owned airport buffer, and levee slopes around the perimeter of the plan area. Land cover considered unsuitable for restoration or enhancement included existing developed land cover outside of permit areas, and other, ruderal and rural residential land cover.

The acreage potentially available for NBHCP mitigation after development of the project was estimated by subtracting the following areas from the acreage potentially available without the project: the proposed Spangler and Natomas reserves and the developed portion of the Greenbriar site (that otherwise would be suitable for preservation). The fragmentation by the project of a block of land that otherwise was potentially suitable for preservation also was considered.

The location of the proposed reserves was examined to determine if these lands expanded existing TNBC reserves, could contribute to the expansion of TNBC reserves in the future or could be expanded into a reserve that was greater than 400 acres in size, or if they were isolated from TNBC reserves by developed lands or other barriers.

#### 2.4 BASIS FOR INTERPRETATIONS OF EFFECTS ON COVERED SPECIES

For each covered species, we evaluated:

- ► construction-related effects on individuals using the Greenbriar site or adjacent lands,
- ▶ change in habitat quantity, and
- ► change in habitat quality.

For this evaluation, the available information on the ecology and distribution of each covered species was compiled, reviewed, and summarized. Interpretations of construction-related effects on individuals were based on the analysis of the likely alterations of survival and reproduction of individuals using the Greenbriar site or

adjacent lands. Interpretations of effects on habitat availability were based on the analysis of alterations to habitat acreage that was described previously.

Interpretations of change in habitat quality were based on the analyses of land cover acreages and connectivity of habitat in the Natomas Basin, and of the acreage in zones with human activity-wildlife conflicts. We also considered changes in the acreage of preserved lands, and in the acreage of high quality habitat.

For each covered species, the interpretations of effects on habitat acreage and quality (and of construction-related effects and human-wildlife conflicts) were used to evaluate the project's overall effect on the viability of the population using the Natomas Basin. A population's viability (i.e., its likelihood of long-term persistence) is strongly influenced by population size, population demography, and environmental variability (which in turn has a strong influence on reproduction and mortality). In the Natomas Basin, fluctuations in the acreage of crop types and changes in agricultural practices cause substantial environmental variability affecting the populations that rely on agricultural habitats. By reducing the quantity or quality of habitat, urban development can reduce population size and adversely affect demography.

### 2.5 BASIS FOR INTERPRETATIONS OF EFFECTS ON NBHCP CONSERVATION STRATEGY

The previously described analyses of effects on population and habitat attributes, and on covered species, were used to evaluate the potential effect of the Greenbriar project on the effectiveness of the NBHCP conservation strategy. This strategy is described in Section IV.C of the NBHCP. This section describes six key components of the NBHCP's conservation strategy for effectively mitigating 17,500 acres of urban development. These components are:

- ▶ basis for 0.5 to 1 mitigation ratio (Section IV.C.1.a),
- ▶ preparation of site specific management plans (Section IV.C.1.b),
- ▶ buffers within the reserve lands (Section IV.C.1.c),
- ► connectivity (Section IV.C.1.d),
- ▶ foraging habitat (Section IV.C.1.e), and
- ▶ 2,500-acre/400-acre minimum habitat block size requirements (Section IV.C.1.f).

Potential effects of the Greenbriar project on each of these components was assessed individually (using the results of the analyses described in Section 2.3 *Methodology for Analyzing Alterations of Populations and Habitats*); these effects were then synthesized into an overall effect of the Greenbriar project on the effectiveness of the NBHCP's conservation strategy.

## 2.6 BASIS FOR INTERPRETATIONS OF EFFECTS ON HCP GOALS AND OBJECTIVES

The NBHCP's goals and objectives represent the desired outcomes from implementation of the NBHCP's conservation strategy. Nine of the NBHCP's goals and objectives could be affected by the Greenbriar project. Table 2-4 lists these goals and objectives; it also identifies the population and habitat attributes potentially affected by the project that could affect attainment of the NBHCP's goals and objectives. This effects analysis evaluated the effects of the Greenbriar project on each of these nine goals and objectives of the NBHCP. Interpretations of the project's overall effect on the attainment of a goal or objective were based primarily on the sum of these anticipated effects. Substantial effects (beneficial or adverse) could alter the viability of a covered species or interfere with attainment of a goal or objective. Effects that would reduce the viability of a covered species, preclude attainment of a goal or objective, or otherwise result in a change to the NBHCP's conservation strategy were considered significant effects that would conflict with the NBHCP.

| Table 2-4<br>Relationships Between Applicable NBHCP Goals and Objectives and Attributes Potentially Affected by the Greenbriar Project <sup>1</sup>  |                                |  |  |   |   |  |  |  |
|--|--------------------------------|--|--|---|---|--|--|--|
|  | Species and Habitat Attributes |  |  |   |   |  |  |  |
| NBHCP Goals and Objectives   |                                | Zones with human-wildlife<br>conflicts | Acreage of habitat in<br>Natomas Basin | Connectivity of habitat in<br>Natomas Basin | Connectivity of existing<br>TNBC reserves | Habitat value of existing<br>TNBC reserves | Water availability at TNBC<br>reserves | Opportunities to establish<br>additional TNBC reserves |
| Overall Goal 1. Establish and manage in perpetuity a biologically sound and interconnected habitat reserve system that mitigates impacts on Covered Species resulting from Covered Activities and provides habitat for existing, and new viable populations of Covered Species. (NBHCP page I-15)  | -                              | -                                      | X                                      | X   | X   | X  | X                                      | X  |
| Overall Goal 3. Preserve open space and habitat that may also benefit local, non-listed and transitory wildlife species not identified within the NBHCP. (NBHCP page 1-16)   | -                              | -                                      | X                                      | X   | X   | X  | X                                      | X  |
| <b>Overall Goal 4.</b> Ensure that direct impacts of Authorized Development upon Covered Species are avoided or minimized to the maximum extent practicable. (NBHCP, page 1-16)  | X                              | -                                      | -                                      | -   | -   | -  | -                                      | -  |
| Overall Objective 1. Minimize conflicts between wildlife and human activities, including conflicts resulting from airplane traffic, roads and automobile traffic, predation by domestic pets, and harassment by people. (NBHCP, page I-16)   | X                              | X                                      | -                                      | -   | -   | -  | -                                      | -  |
| Overall Objective 3. Ensure connectivity between TNBC reserves to minimize habitat fragmentation and species isolation. Connections between reserves will generally take the form of common property boundaries between reserves, waterways (primarily irrigation and drainage channels) passing between reserves, and/or an interlinking network of water supply channels or canals. (NBHCP, page I-16) |                                |  |  | X   | X   | X  | X                                      |  |

| Table 2-4   |   |  |  |   |   |  |  |  |
|---|---|--|--|---|---|--|--|--|
| Relationships Between Applicable NBHCP Goals and Objectives and Attributes Potentially Affected by the Greenbriar Project <sup>1</sup>  |   |  |  |   |   |  |  |  |
|   | Species and Habitat Attributes  |  |  |   |   |  |  |  |
| NBHCP Goals and Objectives  | Survival and reproduction<br>of individuals using Project<br>Site or adjacent lands | Zones with human-wildlife<br>conflicts | Acreage of habitat in<br>Natomas Basin | Connectivity of habitat in<br>Natomas Basin | Connectivity of existing<br>TNBC reserves | Habitat value of existing<br>TNBC reserves | Water availability at TNBC<br>reserves | Opportunities to establish<br>additional TNBC reserves |
| Wetland Species/Habitat Goal/Objective 1. Acquire, enhance and create a mosaic of wetland habitats with adjacent uplands and connecting corridors to provide breeding, wintering, foraging, and cover areas for wetland species in the Plan Area. (NBHCP, page I-17)  |   |  |  | X   | X   | X  | X                                      | X  |
| Wetland Species/Habitat Goal/Objective 2. Provide habitat to maintain, attract and sustain viable populations of the Covered Species. The habitat areas should be configured to encompass natural species migration areas, minimize species isolation, and prevent future habitat fragmentation. (NBHCP, page I-17)   | -   | X                                      | X                                      | X   | X   | X  | X                                      | X  |
| <b>Upland Species/Habitat Goal/Objective 1.</b> Acquire, enhance and create a mosaic of upland habitat types for breeding, foraging, and cover for species dependent on upland habitats. (NBHCP, page 1-17)   | -   | -                                      | X                                      | -   | -   | X  | -                                      | X  |
| Upland Species/Habitat Goal/Objective 2. Ensure reserve land connectivity with travel corridors for upland-dependent species. The habitat areas should encompass grasslands, agricultural croplands, riparian habitats, and shelter and nesting habitat areas (fence rows, clusters of shrubs and small trees), as well as wetland areas to provide a year-round source of water for upland species. The upland areas should be configured to enhance natural species migration, minimize species isolation, and prevent future habitat fragmentation. (NBHCP, page I-17) | -   | -                                      | -                                      | X   | X   | X  | -                                      | X  |

Note:

<sup>1</sup> An "X" indicates that alteration of that species or habitat attribute could directly affect attainment of that goal or objective.

# 3 GREENBRIAR PROJECT'S ALTERATION OF POPULATION AND HABITAT ATTRIBUTES

### 3.1 CONSTRUCTION-RELATED EFFECTS ON SURVIVAL AND REPRODUCTION

Based on CNDDB, surveys of the Greenbriar site, and other data on the distribution of species in the Natomas Basin, species covered by the NBHCP that likely use the Greenbriar site include Swainson's hawk, burrowing owl, loggerhead shrike and giant garter snake. For these species, construction at the Greenbriar site could affect the survival and/or reproduction of individuals by killing, injuring or disturbing individuals, or by eliminating habitat that those individuals depend on for food or shelter. These potential effects are summarized below and described in detail in the sections addressing potential effects for each covered species.

Nesting Swainson's hawks could be affected by the project's construction activities. Though no Swainson's hawk nests have been documented on the Greenbriar, Spangler or Natomas 130 sites, five nests have been recently documented within one mile of the Greenbriar site, 12 nests within one mile of the proposed Natomas 130 reserve (where marsh habitat would be constructed), and 59 nests in the Natomas Basin (Jones & Stokes 2005). Swainson's hawks at any of these nest sites might have their reproduction and survival affected to some degree by construction of the project, and those at the nest sites within one mile could have reduced nesting success or abandon their nest. To avoid and minimize these potential effects, the project includes the same measures that were included in the NBHCP to avoid and minimize construction-related effects on Swainson's hawk. An evaluation of the applicability of NBHCP measures and their inclusion in the Greenbriar project and its mitigation is presented in Appendix A. (These measures are also comparable to those incorporated into the MAP HCP [which has been superseded by the 2003 NBHCP].)

Burrowing owls nesting on or near and foraging on the Greenbriar site could be affected by the project's construction activities. A burrowing owl has been observed on the Greenbriar site. Other burrowing owls could be residing on adjacent land, and any residing within about a mile of the Greenbriar site also could be foraging on the Greenbriar site. Construction of the project could cause nest abandonment or trap or injure owls in their burrows. To avoid and minimize these potential effects, the DEIR mitigation includes the same measures that were included in the NBHCP to avoid and minimize construction-related effects on burrowing owls. An evaluation of the applicability of NBHCP measures and their inclusion in the Greenbriar project and its mitigation is presented in Appendix A. (These measures are also comparable to those incorporated into the MAP HCP [which has been superseded by the 2003 NBHCP].)

Loggerhead shrikes nesting on or near (i.e., within a quarter-mile) and foraging on the Greenbriar site could be affected by the project's construction activities. Shrikes were observed on the Greenbriar site during March 2005 surveys. Because shrikes are distributed throughout the Natomas Basin and suitable habitat is present, shrikes also could be present at the proposed Natomas 130 reserve (where marsh habitat will be constructed). Construction of the project could cause nest abandonment. To avoid and minimize this potential effect, the project includes the same measures that were included in the NBHCP to avoid and minimize construction-related effects on loggerhead shrike. An evaluation of the applicability of NBHCP measures and their inclusion in the Greenbriar project or the DEIR mitigation is presented in Appendix A. (These measures are also comparable to those incorporated into the MAP HCP [which has been superseded by the 2003 NBHCP].)

Giant garter snakes foraging or residing on the Greenbriar site could be affected by the project's construction activities. Giant garter snakes have been observed along Lone Tree Canal, which provides high quality habitat for this species; the other canals on and bordering the Greenbriar site, and the uplands adjacent to these canals, also provide habitat for giant garter snake. The proposed reserve sites also contain or are bordered by giant garter snake habitat. Because giant garter snakes in the Natomas Basin travel widely (i.e., several miles or further)

during their daily and seasonal movements, the Lone Tree Canal is an important movement corridor for this species, and the Greenbriar site contains suitable habitat, giant garter snakes could be killed or injured during construction activities.

The construction activities associated with the Greenbriar project would be comparable to those covered by the NBHCP, as are the species and habitats affected by these activities. Therefore, the applicable measures from the NBHCP would be appropriate for avoiding and minimizing this project's construction-related effects, and the project includes the same measures that were included in the NBHCP to avoid and minimize construction-related effects on giant garter snake. The DEIR (EDAW 2005) also proposes additional measures to avoid and minimize construction-related effects on giant garter snake including exclusion fencing erected prior to the onset of the dormant season preceding construction, routine monitoring of giant garter snakes stranded on the interior (i.e., construction side) of the fence, and documentation and reporting of mortality with the provision to modify avoidance and minimization measures to prevent future moralities due to similar causes.

### 3.2 ZONES WITH HUMAN-WILDLIFE CONFLICTS

As described in the methodology, areas within 800 feet of the MAP, City of Sacramento, or Sutter County permit areas, or major highways, were considered to be areas with high levels of potential human-wildlife conflicts. The Greenbriar project would reduce the total area, and the area of most land cover types, in these zones, and would include measures to reduce effects on adjacent habitats, but it would increase the area of rice and managed marsh within 800 feet of urban development or major highways. Overall, the project with the DEIR mitigation would not significantly increase human-wildlife conflicts in the Natomas Basin.

#### 3.2.1 Future Conditions under the NBHCP

Under the future conditions resulting from implementation of the NBHCP, a portion of the Greenbriar site would be adjacent to urban development or major highways, and thus potentially experiencing high levels of human-wildlife conflicts. Urban development would be adjacent to the Greenbriar site along its eastern and western sides and part of its southern side (Exhibit 1). Lone Tree Canal and Lone Tree Road would be between the Greenbriar site and urban development to the west. Highway 99 would separate the site from the urban development to the east. Along the site's southern side, Interstate 5 would be between the site and both urban development and the agricultural or natural vegetation remaining to the southwest. Along the site's northern boundary, Elkhorn Boulevard would be a six land road between the Greenbriar site and agricultural or natural land cover to the north. The expansion of Elkhorn Boulevard was authorized by the MAP HCP, and although in this analysis it was not considered urban development or a major highway that would generate high levels of human-wildlife conflicts, it would increase levels of human-wildlife conflicts.

Under the future conditions resulting from implementation of the NBHCP, the proposed Spangler reserve would be bordered to the north by development in Sutter County's permit area. A portion of the Natomas 130 parcel would be within 800 feet of urban development in the City of Sacramento's permit area, but would be separated from it by Fisherman's Lake.

### 3.2.2 POTENTIAL EFFECTS OF GREENBRIAR PROJECT UNDER FUTURE CONDITION

Development of the Greenbriar project would reduce the area of habitat in zones with potentially high levels of human-wildlife conflicts. This counter-intuitive result would occur because the project would develop portions of the Greenbriar site that would otherwise be in such zones, and would create smaller new zones with potentially high levels of human-wildlife conflicts. Under the future condition resulting from the NBHCP, about 230 acres of the Greenbriar site would be within 800 feet of urban development or major highways. Development of the Greenbriar site would eliminate most of this acreage and would create a new, but smaller, zone with potentially high levels of human-wildlife conflicts north of the Greenbriar site (about 62 acres in size), because this

undeveloped land would be within 800 feet of urban land after development of the project. The net change would be a reduction of 137 acres in the extent of areas with high levels of human-wildlife conflicts.

Though land to the north would be adjacent to development on the Greenbriar site, a six-lane road (Elkhorn Boulevard) would be between this land and residential development on the Greenbriar site. The road would partially isolate the Greenbriar site from land to the north, and thus limit human-wildlife conflicts resulting from the Greenbriar Project.

Nonetheless, the project would increase the area of rice and managed marsh that is within 800 feet of urban development or a major highway, and thus increase the area of giant garter snake, northwestern pond turtle and white-faced ibis habitat in zones with potentially high levels of human-wildlife conflicts. In the 2001 land cover map, the area within 800 feet of the northern border of the Greenbriar site was primarily in rice (53 of 62 acres). This acreage was greater than the 47 acres of rice on the Greenbriar site that were within 800 feet of the MAP or City of Sacramento permit areas. Thus, based on 2001 land cover for the Greenbriar site, the acreage of rice in areas with high levels of human-wildlife conflicts would increase as a result of developing the Greenbriar site. In addition, up to about 14.2 acres of managed marsh could be created at the proposed Natomas 130 reserve within 800 feet of the City of Sacramento's permit area for urban development, and at the proposed Spangler reserve about 37 acres of the created marsh could be within 800 feet of the Sutter County's permit area. At the proposed reserves, on-site buffers and reserve management (e.g., limiting access) would reduce human-wildlife conflicts, and the proposed Natomas 130 reserve is separated from urban development in the City of Sacramento by Fisherman's Lake, which also would limit human-wildlife conflicts.

Compared to the total area of land in the Natomas Basin that is within 800 feet of a major highway or of the MAP, City of Sacramento, or Sutter County permit areas, these changes are relatively small. There is approximately 2,790 acres of land outside of the three permit areas but within 800 feet of such areas or of a major highway. Thus, the Greenbriar project would reduce the area of these zones by about 5%. Similarly, there are roughly 1,420 acres of rice and managed marsh in these zones, and the Greenbriar project would increase this area by 4% (52 acres).

Without mitigation, the Greenbriar project also could increase human-wildlife conflicts along Lone Tree Canal. Under the future condition resulting from the NBHCP, a 1.1 mile section of the Lone Tree Canal would be within 800 feet of urban development; these urban land uses and highways would be adjacent to one bank of the canal except at road crossings. Development of the project would place urban land uses within 200 feet of the other bank of Lone Tree Canal as well. The Lone Tree Canal is an important corridor for animal movement, particularly for giant garter snake. The project's potential effects on this canal, and measures to reduce those effects, are discussed in detail in Section 3.4 *Connectivity of Habitat in the Natomas Basin*.

The project and its mitigation would also implement measures to reduce human-wildlife conflicts. The project includes all of the applicable measures incorporated into the NBHCP to avoid and minimize human-wildlife conflicts. An evaluation of the applicability of NBHCP measures and their inclusion in the Greenbriar project or the DEIR mitigation is presented in Appendix A. To further reduce human-wildlife conflicts along Lone Tree Canal, the project also would implement a comprehensive set of measures including fencing and a barrier. These measures are described in more detail under Section 3.4 *Connectivity of Habitats in the Natomas Basin* and would be further developed during the HCP process.

Overall, the Greenbriar project, with the DEIR mitigation, would not cause a significant increase in human-wildlife conflicts in the Natomas Basin. This is in part because much of the Greenbriar site is, or under NBHCP and MAP permit conditions would be, bordered by urban development, highways, and major roads under the future condition, and in part because of the measures incorporated into the project and the DEIR mitigation.

#### 3.3 HABITAT ACREAGE IN THE NATOMAS BASIN

The project would reduce the acreage of habitat available in the Natomas Basin for several species covered by the NBHCP. These losses would result from changes in land cover at the Greenbriar and proposed reserve sites.

#### 3.3.1 Change in Habitat Acreage at the Greenbrian Site

The Greenbriar project would alter the Greenbriar and proposed reserve sites. Most of the Greenbriar site would be converted to urban land cover (Exhibit 2, Table 3-1). But, a 30.6 acre area along the western edge, bordering the Lone Tree Canal, would be conserved. This area would be preserved, restored as tule marsh (approximately 2.7 acres) or native grassland, and added to the TNBC reserve system. (The existing, disturbed patch of riparian land cover [at the southern end of this conserved area] would probably recover and persist.)

| Table 3-1<br>Land Cover Acreages of Greenbriar Project |                              |       |                  |  |       |                  |       |       |                  |
|--|------------------------------|-------|------------------|--|-------|------------------|-------|-------|------------------|
| Land Cayer Times                                       | Greenbriar Site <sup>1</sup> |       |                  | Proposed Spangler & Natomas<br>130 Reserves <sup>2</sup> |       |                  | Total |       |                  |
| Land Cover Types                                       | 2001                         | 2005  | Post-<br>Project | 2001   | 2005  | Post-<br>Project | 2001  | 20053 | Post-<br>Project |
| Alfalfa  | -                            | -     | -                | -  | -     | 59.6             |       |       | 59.6             |
| Canals   | 15.0                         | 15.0  | -                | 7.6  | 7.6   | 6.2              | 22.6  | 22.6  | 6.2              |
| Grassland  | -                            | -     | 26.5             | -  | -     | -                | -     | -     | 26.5             |
| Idle   | 62.5                         | 115.1 | -                | -  | 28.4  | -                | 62.5  | 143.5 | -                |
| Non-rice crops   | 234.1                        | 381.0 | -                | 28.4   | -     | -                | 262.6 | 381.0 | -                |
| Pasture  | 33.8                         | -     | -                | -  | -     | -                | 33.8  | -     | -                |
| Ponds & seasonally wet areas                           | -                            | 1.7   | 2.7              | -  | -     | 198.2            | -     | 1.7   | 200.9            |
| Rice   | 160.0                        | -     | -                | 228  | 228   | 0                | 395.4 | 228   | 0                |
| Riparian   | 1.4                          | 1.4   | 1.4              | 1.6  | 1.6   | 1.6              | 3.0   | 3.0   | 3.0              |
| Roads and Highways                                     | 17.5                         | 17.5  | -                | -  | -     | -                | 17.5  | 17.5  | -                |
| Ruderal  | 9.2                          | 2.0   | -                | -  | -     | -                | 9.2   | 2.0   | 0                |
| Rural Residential                                      | 43.3                         | 43.3  | -                | -  | -     | -                | 43.3  | 43.3  | -                |
| Tree Groves  | -                            | -     | -                | 0.2  | 0.2   | 0.2              | 0.2   | 0.2   | 0.2              |
| Urban  | -                            | -     | 546.4            | -  | -     | -                | -     | -     | 546.4            |
| Total  | 577                          | 577   | 577              | 265.8  | 265.8 | 265.8            | 842.8 | 842.9 | 842.9            |

#### Note:

If the Greenbriar site were to remain predominantly in agricultural land cover, a variety of crops probably would be cultivated on it and portions of the site would be idle in many years. Land cover in 2001 and 2005 indicates the range of habitat values the Greenbriar site could provide over the long-term, and thus that would be lost by the site's development. In 2001, the site contained idle, pasture, ruderal, canal, rice, riparian, non-rice crops, and rural residential land cover (Table 3-1). In 2005, pasture and rice were no longer present and the area of idle and non-rice cropland had expanded.

The Greenbriar site included the 30.6 acre area along Lone Tree Canal that would become a preserve and 546.4 acres that would be developed. Lone Tree Canal was considered immediately adjacent to but outside of the project site.

Reserve acreages do not include the additional preservation and enhancement of upland habitats required by mitigation measure 6.13-2 of the DEIR because location, acreage, and current land cover of this land has not been determined.

<sup>&</sup>lt;sup>3</sup> These 2005 acreages differ from those in the DEIR because they were based on a GIS analysis comparable to that performed for 2001 (as described in the methods) and the DEIR acreages were based on a different analysis that included a field survey of the site.

Estimates of habitat loss depend on whether they are based on 2001 or 2005 land cover. For some species (e.g., giant garter snake), estimates of habitat loss would be greater if based on 2001 land cover than if based on 2005 land cover. For other species (e.g., Swainson's hawk), estimates of habitat loss would be greater if based on 2005 land cover. For evaluating how the project would alter the future condition of the Natomas Basin, changes from 2001 land cover were used because 2001 land cover was the baseline for the NBHCP's estimates of future habitat conditions.

Although different analyses were conducted for this effects analysis and for the DEIR, both considered 2001 and 2005 conditions. To evaluate the proposed project's effects on the effectiveness of the NBHCP, this effects analysis performed an extensive analysis of the project's potential effects on the future condition of the Natomas Basin. This analysis used the 2001 land cover data that represents baseline conditions of the NBHCP, and also considered 2001–2004 changes in land cover, and 2005 conditions. To comply with CEQA requirements and to assure that the proposed project does not compromise the effectiveness of the NBHCP, the impact analysis in the DEIR evaluated conditions documented in 2005 when the Notice of Preparation (NOP) was released, and provides mitigation designed to reduce impacts to less than significant under both 2005 conditions (for CEQA purposes) and 2001 conditions (to assure that the project does not compromise the effectiveness of the NBHCP).

#### 3.3.2 Change in Habitat Acreage at Proposed Reserve Sites

Land cover would also be altered at the proposed reserve sites (Table 3-1). Approximately 45 acres of the Spangler site would be converted to upland foraging habitat (assumed to be alfalfa), 184 acres would be converted to marsh that would include upland components, and about 6 acres would be canal. At the Natomas 130 site, about 14 acres that were in non-rice crops in 2001, and are currently idle, would be converted to marsh, about 2 acres would remain in riparian habitat, and the remaining 14 acres at this site would be managed as foraging habitat for Swainson's hawk. The location and existing land cover of the mitigation site(s) providing at least an additional 49 acres of Swainson's hawk foraging habitat (to fulfill mitigation measure 6.13-2 of the DEIR) have not been specified, and thus the effects of these land cover changes are not included in Tables 3-1, 3-2 and 3-3. However, this mitigation needs to provide high quality habitat for Swainson's hawk, and so land would probably be converted from non-rice crops to alfalfa (or otherwise be managed to provide high quality foraging habitat).

#### 3.3.3 OVERALL CHANGE IN HABITAT ACREAGE

Together, these changes at the Greenbriar and proposed reserve sites, but not including additional DEIR mitigation for Swainson's hawk, would reduce the acreage of several natural or agricultural land cover types that provide habitat for covered species, and would increase the acreage of alfalfa, grassland, and of ponds or seasonally wet areas (Table 3-2).

Based on 2001 land cover, these changes represent a reduction in habitat acreage for most species that use non-rice cropland and other upland land cover, a net gain of habitat for two plant species that grow in wetlands and along canals, and a net loss for species using both canal and rice land cover (Table 3-3, which does not include additional DEIR mitigation for Swainson's hawk). (No change in the acreage of vernal pool or riparian habitats would result from the project.) Except for burrowing owl, the covered species that forage in non-rice crops and other upland land cover (Swainson's hawk, loggerhead shrike, tricolored blackbird, Aleutian Canada goose, and bank swallow) would lose from about 14 to 684 acres of habitat. Because the acreage of created marsh habitats would be much greater than the acreage of lost canal habitats, potential habitat for Sanford arrowhead and delta tule pea (which occur in marsh or canal habitats) would increase by 184 acres.

The acreage of habitat would decrease for white-faced ibis, giant garter snake, and northwestern pond turtle by 144–204 acres, because the loss of rice and canal habitats would be greater than the acreage of marsh created from non-habitat (Table 3-3).

| Table 3-2 Change in Land Cover Acreage Because of Natomas Basin HCP and Greenbriar Project |                         |                                      |   |                            |  |  |
|--|-------------------------|--------------------------------------|---|----------------------------|--|--|
|  | Natomas                 | Future Condition                     | Future Condition Resulting from NBHCP Plus Project <sup>1, 2, 3</sup> |                            |  |  |
| Land Cover   | Basin 2001 <sup>1</sup> | Resulting from NBHCP <sup>1, 2</sup> | 2001 Greenbriar Land Cover  | 2005 Greenbriar Land Cover |  |  |
| Airport  | 1,532                   | 1,492                                | 1,492   | 1,492                      |  |  |
|  |                         |                                      | (0)   | (0)                        |  |  |
| Alfalfa  | 368                     | 368                                  | 427   | 427                        |  |  |
|  |                         |                                      | (60)  | (60)                       |  |  |
| Canals   | 1,753                   | 1,162                                | 1,146   | 1,146                      |  |  |
|  |                         |                                      | (-16)   | (-16)                      |  |  |
| Grassland  | 882                     | 284                                  | 311   | 311                        |  |  |
|  |                         |                                      | (27)  | (27)                       |  |  |
| Highway or Major   | 1,353                   | 770                                  | 753   | 753                        |  |  |
| Road   |                         |                                      | (-18)   | (-18)                      |  |  |
| Idle   | 1,449                   | 422                                  | 360   | 307                        |  |  |
|  |                         |                                      | (-63)   | (-115)                     |  |  |
| Non-rice Crops   | 16,395                  | 9,533                                | 9,271   | 9,152                      |  |  |
|  |                         |                                      | (-263)  | (-381)                     |  |  |
| Oak Grove  | 94                      | 77                                   | 77  | 77                         |  |  |
|  |                         |                                      | (0)   | (0)                        |  |  |
| Orchard  | 178                     | 165                                  | 165   | 165                        |  |  |
|  |                         |                                      | (0)   | (0)                        |  |  |
| Other  | 460                     | 314                                  | 314   | 314                        |  |  |
|  |                         |                                      | (0)   | (0)                        |  |  |
| Pasture  | 660                     | 494                                  | 460   | 494                        |  |  |
|  |                         |                                      | (-34)   | (0)                        |  |  |
| Ponds & Seasonally   | 93                      | 2,259                                | 2,460   | 2,458                      |  |  |
| Wet Areas  |                         |                                      | (201)   | (199)                      |  |  |
| Rice   | 22,129                  | 11,643                               | 11,255  | 11,415                     |  |  |
|  |                         |                                      | (-388)  | (-228)                     |  |  |
| Riparian   | 115                     | 91                                   | 91  | 91                         |  |  |
|  |                         |                                      | (0)   | (0)                        |  |  |
| Ruderal  | 1,882                   | 370                                  | 361   | 368                        |  |  |
|  |                         |                                      | (-9)  | (-2)                       |  |  |
| Rural Residential  | 369                     | 287                                  | 244   | 244                        |  |  |
|  |                         |                                      | (-43)   | (-43)                      |  |  |
| Tree Grove   | 102                     | 44                                   | 44  | 44                         |  |  |
|  |                         |                                      | (0)   | (0)                        |  |  |
| Urban  | 3,725                   | 23,763                               | 24,309  | 24,309                     |  |  |
|  |                         |                                      | (546)   | (546)                      |  |  |
| Total  | 53,538                  | 53,538                               | 53,538  | 53,538                     |  |  |

#### Notes:

<sup>&</sup>lt;sup>1</sup> Acreage along Class II-IV canals included in acres of canals, thus reducing acreages in other categories from those given in NBHCP.

<sup>&</sup>lt;sup>2</sup> Acreages include changes in land cover occurring at proposed Spangler and Natomas 130 reserves.

 $<sup>^{\</sup>rm 3}$  Change in acreage from future condition of NBHCP is in parentheses.

Changes resulting from the preservation and enhancement of upland habitat required by Mitigation Measure 6.13-2 are not included in these acreages.

| Table 3-3  |                         |                                      |                            |   |  |  |
|--|-------------------------|--------------------------------------|----------------------------|---|--|--|
| Change in Habitat Acreage Because of Natomas Basin HCP and Greenbriar Project  Natomas  Future Condition  Future Condition Resulting from NBHCP Plus Project <sup>1, 2, 3, 3</sup> |                         |                                      |                            |   |  |  |
| Species  | Basin 2001 <sup>1</sup> | Resulting from NBHCP <sup>1, 2</sup> | 2001 Greenbriar Land Cover | 2005 Greenbriar Land Cover <sup>5</sup> |  |  |
| Giant garter snake   | 23,975                  | 15,064                               | 14,860                     | 15,019                                  |  |  |
| •  |                         |                                      | (-204)                     | (-45)                                   |  |  |
| Swainson's hawk  | 311                     | 211                                  | 211                        | 211                                     |  |  |
| (Nesting)  |                         |                                      | (0)                        | (0)                                     |  |  |
| Swainson's hawk  | 21,636                  | 12,018                               | 11,796                     | 11,638                                  |  |  |
| (Foraging) <sup>6</sup>  |                         |                                      | (-222)                     | (-380)                                  |  |  |
| Burrowing owl <sup>6</sup>   | 6,994                   | 3,647                                | 3,673                      | 3,631                                   |  |  |
|  |                         |                                      | (24)                       | (-16)                                   |  |  |
| Loggerhead shrike  | 24,339                  | 15,555                               | 15,415                     | 15,254                                  |  |  |
|  |                         |                                      | (-141)                     | (-301)                                  |  |  |
| Tricolored blackbird   | 40,434                  | 22,322                               | 21,724                     | 21,799                                  |  |  |
| (foraging)   |                         |                                      | (-598)                     | (-523)                                  |  |  |
| Aleutian Canada goose  | 39,184                  | 21,670                               | 20,986                     | 21,061                                  |  |  |
|  |                         |                                      | (-684)                     | (-609)                                  |  |  |
| White-faced ibis   | 24,343                  | 15,432                               | 15,228                     | 15,446                                  |  |  |
|  |                         |                                      | (-144)                     | (-14)                                   |  |  |
| Bank swallow   | 42,395                  | 25,834                               | 25,420                     | 25,494                                  |  |  |
|  |                         |                                      | (-414)                     | (-340)                                  |  |  |
| Valley elderberry  | 115                     | 91                                   | 91                         | 91                                      |  |  |
| longhorn beetle  |                         |                                      | (0)                        | (0)                                     |  |  |
| Northwestern pond  | 24,090                  | 15,155                               | 14,951                     | 15,110                                  |  |  |
| turtle   |                         |                                      | (-204)                     | (-45)                                   |  |  |
| Sanford's arrowhead  | 1,846                   | 3,421                                | 3,605                      | 3,604                                   |  |  |
|  |                         |                                      | (184)                      | (183)                                   |  |  |
| Delta tule pea   | 1,846                   | 3,421                                | 3,605                      | 3,604                                   |  |  |
| -  |                         |                                      | (184)                      | (183)                                   |  |  |

#### Notes

### 3.4 HABITAT QUALITY IN THE NATOMAS BASIN

Besides these changes in habitat acreage, changes in the quality of the remaining habitat also would occur. In part, changes in habitat quality result from changes in the acreage of land cover types providing lower or higher habitat quality. For example, the project would increase ruderal land cover that provides habitat for Swainson's hawk, burrowing owl, and loggerhead shrike, but this habitat is of lesser quality than that provided by other land cover types, including types whose acreage was reduced by the project (e.g., idle cropland). Similarly, marshland

Acreage along Class II-IV canals were included in acres of canals, thus reducing acreages in other land cover categories from those given in NBHCP as baseline conditions; this altered habitat estimates as well.

Acreages include changes in land cover occurring at proposed Spangler and Natomas 130 reserves, and assume that land in MAP, City of Sacramento, and Sutter County permit areas would not provide habitat under future conditions.

<sup>&</sup>lt;sup>3</sup> Change in acreage from future condition because of NBHCP is in parentheses.

<sup>&</sup>lt;sup>4</sup> Changes resulting from the preservation and enhancement of additional upland habitat to satisfy Mitigation Measure 6.13-2 are not included in this table's acreages because the acreage, location, and current land cover of this land has not been specified.

<sup>&</sup>lt;sup>5</sup> 2005 habitat acreages differ from those in the DEIR because different methodologies were used; this effects analysis relied on a GIS analysis comparable to analyses of 2001 land cover, whereas the DEIR used by GIS analyses and field surveys by biologists .to estimate habitat acreages.

For these species future condition acreages also include upland components of created marshes.

created by the project would provide higher quality habitat for some species (e.g., northwestern pond turtle and white-faced ibis) than the canal habitats eliminated by the project.

### 3.4.1 HABITAT QUALITY ADJACENT TO THE GREENBRIAR SITE

Habitat quality would be reduced on land adjacent to development at the Greenbriar site. Roads, urban, and exurban development detrimentally affect the provision of wildlife habitat and other ecosystem functions on adjacent lands. These effects are caused by a wide variety of mechanisms that include alteration of hydrology, water quality, disturbance regimes, and vegetation structure, and the introduction of non-native species, collisions with vehicles, noise disturbance, and harassment by humans, and predation by cats, dogs, and wildlife associated with human land uses. The distance that effects on wildlife habitat extend from developed land varies with the mechanism causing the effect, the species affected, and attributes of the development and its surrounding landscape, but distances may range from less than 10 to over 1,000 feet (De Snoo and de Wit 1998, Forman and Alexander 1998, Paul and Meyer 2001, ELI 2003, Miller et al. 2003, Allan 2004). The most likely causes of effects on adjacent habitats because of the project are:

- ▶ Decreased runoff to and lower water levels in Lone Tree Canal,
- ► Spread of non-native invasive species,
- ► Harm and harassment by humans, cats, and dogs,
- ▶ Dumping of trash,
- ▶ Increased levels of noise and nighttime light, and
- ► Loss of upland vegetation adjacent to canals.

Several of these effects on wildlife habitat could extend hundreds of feet from the site. Although the mechanisms by which development affects habitat are well understood, a moderate level of uncertainty exists regarding the magnitude and location of the effects resulting from specific development projects (including the Greenbriar project). The degradation of habitat on adjacent lands is also assessed in the sections of this report that address zones with high levels of human-wildlife conflicts and those addressing effects on covered species.

In addition, the habitat quality of adjacent agricultural lands would be altered by changes in crop types or the cessation of agriculture. Land cover on adjacent land north of the Greenbriar site could possibly change because of conflicts between rice cultivation and the residential development created by the project. Aerial application of pesticides and herbicides probably is not feasible immediately adjacent to residential development (C. Aubry, pers. comm.), which could cause part, or all, of the adjacent parcel to be removed from rice cultivation. The North Natomas Community Plan has reduced these conflicts through a 350-foot wide buffer of open space along roads separating developed and agricultural land uses (EDAW 2005). Similarly, the Metro Air Park includes a 250-foot wide buffer along its northern and eastern borders in which developed land uses are restricted to open space, warehouses, or parking areas (USFWS 2001). The Greenbriar project would not contain an open space buffer along its borders between its development and adjacent land uses, and the only buffer would be Elkhorn Boulevard, which would be a six lane road. The project would include notification of all prospective residents and tenants within 500 feet of existing agricultural uses describing the types of agricultural operations that could occur in proximity to their homes or businesses (DEIR mitigation measure 6.11-3). Nonetheless, agricultural-residential conflicts could occur.

The extent of potential conflicts is not known. If all agricultural use of land within 350 feet of the project's residential development were to cease, roughly 23 acres of rice would become idle land. This would increase the project's effects on giant garter snake, and on other species associated with rice but not idle land, and would decrease the project's effects on Swainson's hawk and other species associated with idle land but not rice. However, other scenarios are equally plausible, and it would be speculative to quantify the habitat that could be affected, and base mitigation on that estimate.

In addition to these local effects, development also degrades wildlife habitat through landscape-scale effects on the distribution of habitat. These effects are described in sections of this report addressing effects on connectivity, the habitat value of existing reserves, and on covered species.

#### 3.4.2 HABITAT QUALITY AT PROPOSED RESERVES

Habitat quality would be increased through preservation and management of at least 345 acres at the Spangler, Natomas 130, Greenbriar, and DEIR mitigation sites. Habitat quality would increase at these sites because:

- 1. Habitat would be preserved in perpetuity;
- 2. Habitat would be monitored and actively managed for the benefit of covered species;
- 3. Habitat would not be subject to continuous disturbance caused by farming or canal maintenance activities; and
- 4. Habitat would be relatively free of human intrusion (USFWS 2003).

In addition to the increase in habitat quality resulting from preservation, habitat quality would be increased at the proposed reserves as a result of habitat enhancement and conversion to land cover types that provide higher quality habitat.

As part of the proposed project, at the Spangler site, 184 acres of rice at the Spangler site and 14 acres of upland at the Natomas 130 site would be converted to marsh that provides higher quality habitat, and would be managed to increase habitat quality for covered species, particularly giant garter snake. Managed marsh provides substantially greater habitat values for giant garter snakes than does rice for several reasons. These reasons include:

- ► Giant garter snakes primarily use the margins of rice fields, whereas they use the full extent of managed marshes. These marshes are designed to provide open water, foraging habitat, dense cover, basking sites, and refugia in close proximity throughout the marsh. (For example, an acre of managed marsh provides several times the edge habitat than does a rice field.)
- ▶ Marshes provide habitat throughout the active period of the snake. Rice fields do not provide habitat during early and mid-spring, and are typically drained before the end of the snake's active period. Thus, for a portion of their active period, giant garter snakes must rely entirely on non-rice habitats. In the Natomas Basin, these habitats are canals and managed marsh. In contrast, managed marshes provide habitat year-round.
- ▶ Rice is fallowed periodically, and thus does not provide habitat in all years; in contrast, a managed marsh does provide habitat in all years.

The quality of existing upland habitats also would be enhanced at the proposed reserves and the DEIR mitigation site(s). Upland habitat at the proposed Spangler and Natomas 130 reserves would be enhanced, and additional mitigation land (at least 49 acres) would be enhanced through conversion to alfalfa (or would be otherwise managed to provide high quality foraging habitat for Swainson's hawk).

However, some uncertainty exists regarding the magnitude of habitat enhancement that would result from the project. For example, marsh creation would be used to replace habitat values lost at the Greenbriar site because marsh has greater habitat value than rice. (The general basis for this scenario is repeatedly outlined in the NBHCP, EIR, and BO.) And, for the reasons given previously, this difference in habitat value is inferred to be substantial. But, studies have not yet been conducted that document this difference in habitat value between managed marsh and rice. Furthermore, most marshes created by TNBC are only several years old, and the habitat attributes of created marsh changes rapidly during their first few years. Therefore, the long-term results of marsh creation and management have not yet been determined. Currently, it is known that giant garter snakes are using created marshes to some extent, our understanding of giant garter snake's ecology supports arguments that marsh

provides substantially higher quality habitat than rice (and higher quality than canals), and preserved lands are more likely to continue to provide habitat than unpreserved lands.

The effects of changes in the quality of habitat provided by enhanced and preserved land, are further described in the sections of this report that address potential effects on each covered species.

#### 3.4.3 Habitat Quality for Swainson's Hawk Foraging

The effects of the Greenbriar project on the quality of Swainson's hawk foraging habitat was evaluated through three analyses: acres of foraging habitat in low, moderate and high quality categories; total acres of foraging habitat available per month; and total foraging habitat available each month expressed as an equivalent acreage of high quality foraging habitat. The first two analyses (acres by habitat quality category and monthly availability) were conducted as in the NBHCP, and the third was developed for this evaluation of the Greenbriar project. All three methods are described in detail in the methods section. The acres of habitat types at the Greenbriar, proposed reserve and DEIR mitigation sites with and without the project that were used in these analyses of effects on Swainson's hawk foraging habitat are shown in Table 2-2.

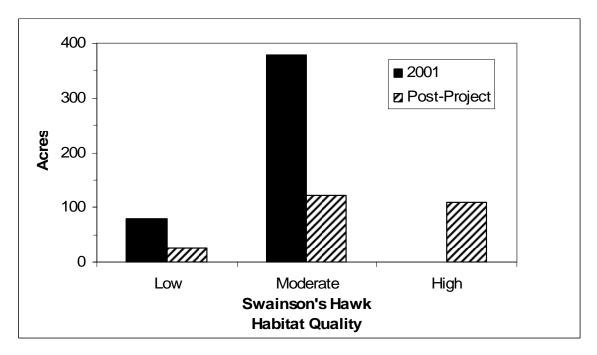
The project would result in a net loss of habitat acreage but an increased percentage of the remaining habitat would be in the high quality category (Exhibit 3a). This increase in high quality habitat would result from enhancement of habitat at the Spangler, Natomas 130, and the DEIR mitigation sites. Upland habitat at the proposed Natomas 130 reserve would be enhanced, and high quality foraging habitat would be created at the proposed Spangler reserve and to satisfy the DEIR mitigation at least 49 acres of land would be enhanced and managed to provide high quality foraging habitat for Swainson's hawk.

Based on the analysis approach in the NBHCP, the project would result in greater availability of foraging habitat during April—September, despite causing a net loss in overall acreage of habitat (Exhibit 3b). (However, this approach assumes that row and field crops are not available to foraging hawks except at harvest, and thus underestimates the acreage of foraging habitat available, particularly during April—May, which is prior to the harvest of row and field crops in the Natomas Basin.)

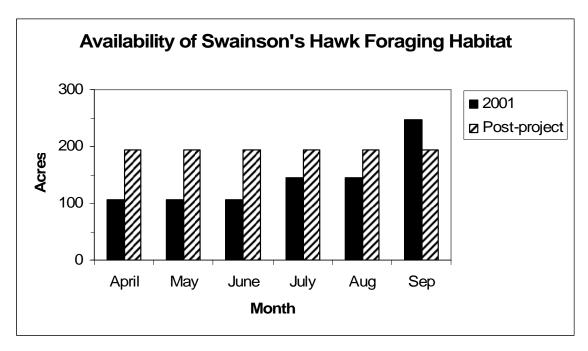
Based on EDAW's evaluation approach, total foraging resources would be comparable with and without the project. At the Greenbriar, proposed reserve, and DEIR mitigation sites, during April–June, slightly greater foraging resources would be available with the project (the equivalent of 129 acres of high quality foraging habitat with versus 122 acres without the project), while during July–September there would be less (129 versus 140 acres in July–August and 162 acres in September) (Exhibit 4). (Throughout the Natomas Basin, during July–September, more foraging resources are available because that is when most crops are harvested [CH2M HILL 2003].)

#### 3.5 CONNECTIVITY OF HABITAT IN THE NATOMAS BASIN

The Greenbriar project would cause adverse and beneficial effects on connectivity of habitats in the Natomas Basin. By developing the Greenbriar site, it would fragment habitats for loggerhead shrike, burrowing owl, Swainson's hawk, and the other covered bird species, which would adversely affect connectivity. It also could cause detrimental effects on connectivity because of human disturbance and predation on giant garter snake and northwestern pond turtle using habitat along Lone Tree Canal. However, the project and the DEIR mitigation include measures to reduce human disturbance and predation effects resulting from the project, and to create and enhance habitat along Lone Tree Canal, which would beneficially affect connectivity of canal and marsh habitats. In addition, the proposed reserves would increase connectivity of habitats for giant garter snake and northwestern pond turtle. Further, the project would ensure the long-term conservation of a corridor along a segment of Lone Tree canal. This canal is important for maintaining connectivity of canal habitats between the southern and northern Natomas Basin, but a corridor along the canal has not yet been preserved.



A) Total acres of high, moderate, and low quality habitat at the project and mitigation sites; quality assessed as in CH2M Hill 2003.

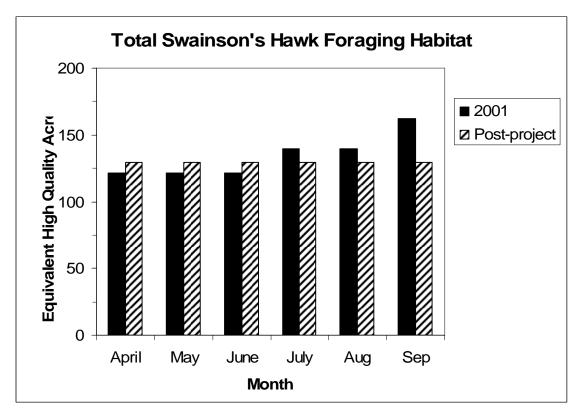


B) Acres of foraging habitat available by month; availability of prey assessed as in CH2M Hill 2003.

Notes: Estimates are based on approach used by CH2M Hill to support the NBHCP. Sources: Wildlands 2005, DWR 1993, and CH2M Hill 2001

Quality and Availability of Swainson's Hawk Foraging Habitat at the Project and Mitigation Sites

Exhibit 3



Low, moderate, high-moderate, and high quality habitats were combined in an estimate of the acreage of high quality habitat providing equivalent foraging resources, as described in the methods section.

Sources: Wildlands 2005, DWR 1993, and CH2M Hill 2001

#### **Total Swainson's Hawk Foraging Habitat**

Exhibit 4

Overall, the project (with the mitigation included as part of the project design and with the DEIR mitigation) is unlikely to significantly reduce connectivity of habitat for covered bird species. Depending on the location, land cover, and management of the mitigation land providing foraging habitat for Swainson's hawk, the project could cause small, but significant, effects (adverse or beneficial) on connectivity of habitat for covered bird species.

The following sections provide a detailed description of the Greenbriar project's effects on connectivity at the regional and local levels, and along Lone Tree Canal. This section also evaluates the effect of the Greenbriar project on the implementation of the connectivity measures in the NBHCP's conservation strategy.

### 3.5.1 OVERVIEW OF EXISTING AND FUTURE CONDITIONS

In 2001 and currently, the proposed Greenbriar site provides agricultural and canal habitats, as do some adjacent lands. However, because the Greenbriar site is bordered to the south and east by Interstate 5 and State Route 99, respectively, habitats for less mobile animals, or those highly sensitive to human disturbance, are at least partially isolated from similar habitats to the east or south. Birds, including covered species, can fly over these highways. The Greenbriar site's canal habitats are connected to similar habitats to the south by a culvert under Interstate 5 through which Lone Tree Canal flows, and the site's canal habitats are also connected to habitats north of the site by Lone Tree Canal and a culvert in the northeastern corner of the site. These culverts may limit animal movement from the southern to central Natomas Basin across the site. Nonetheless, Lone Tree Canal currently

provides a movement corridor and habitat for giant garter snake. In recent years, flows in the canal have not been optimal for giant garter snake, although the Metro Air Park HCP provides assurances that at least some water will be present in this drainage canal in the future (see pages 70-71 in Thomas Reid Associates 2001). The other canals within and along the southern and eastern borders of the Greenbriar site also have recently provided (or still provide) some habitat for giant garter snake, and they may also serve as a movement corridor. Lone Tree Canal is the primary remaining corridor for movement of giant garter snakes between the southern and central portions of the Natomas Basin (C. Aubry, pers. comm.; E. Hansen, pers. comm.). Loss of this corridor could isolate the southern portion of the Natomas Basin, dividing the current giant garter snake population into two smaller populations, which would substantially reduce the likelihood of giant garter snakes persisting in the Natomas Basin.

Under the future condition (i.e., assuming development as permitted under the NBHCP), the Greenbriar site would occupy much of one of two remaining corridors connecting the southern and central Natomas Basin. Except for these two corridors, the Sacramento International Airport, Metro Air Park and City of Sacramento would separate the southern and central Basin (Exhibit 1). A western corridor, between the airport and the Sacramento River, would be 0.4–1.6 miles wide. This western corridor may not contain sufficient canal, rice and wetland habitats to provide for connectivity of populations of giant garter snake, western pond turtle and other wetland and aquatic species between the southern and central portions of the Natomas Basin. To the east, another corridor would pass between the Metro Air Park and the City of Sacramento. At Interstate 5, this corridor would be about 0.4 miles wide and at the northern end of the Greenbriar site it would be almost a mile wide. In this eastern corridor, the Lone Tree Canal, which passes under Interstate 5, would be an important waterway, and possibly the only waterway, connecting habitats in the southern and central Natomas basin (Jones & Stokes 2005; C. Aubry, pers. comm.; E. Hansen, pers. comm.); this canal has a north-south orientation along the western edge of this corridor.

Under the future condition, the proposed Spangler and Natomas 130 reserves would be outside of but adjacent to permit areas where development has been authorized. The northern border of the proposed Spangler reserve would be immediately adjacent to development in the Sutter County permit area. The eastern border of the proposed Natomas 130 reserve would be across Fisherman's Lake from development in the City of Sacramento's permit area.

## 3.5.2 CONNECTIVITY OF AQUATIC, WETLAND, AND RICE HABITATS WITHIN THE NATOMAS BASIN

Within the Natomas Basin, aquatic, wetland, and rice habitats are connected by a series of irrigation and drainage canals. Most of these waterways are suitable for use and movement of a variety of animals, including giant garter snake and western pond turtle, and thus provide movement corridors for these animals between wetland and rice habitats.

In the Natomas Basin, irrigation water is provided by Natomas Central Mutual Water Company (Natomas Mutual), a private water company. Natomas Mutual diverts water from five locations along the Sacramento River and the Natomas Cross Canal, and distributes this water throughout the Basin through a series of canals and pump stations.

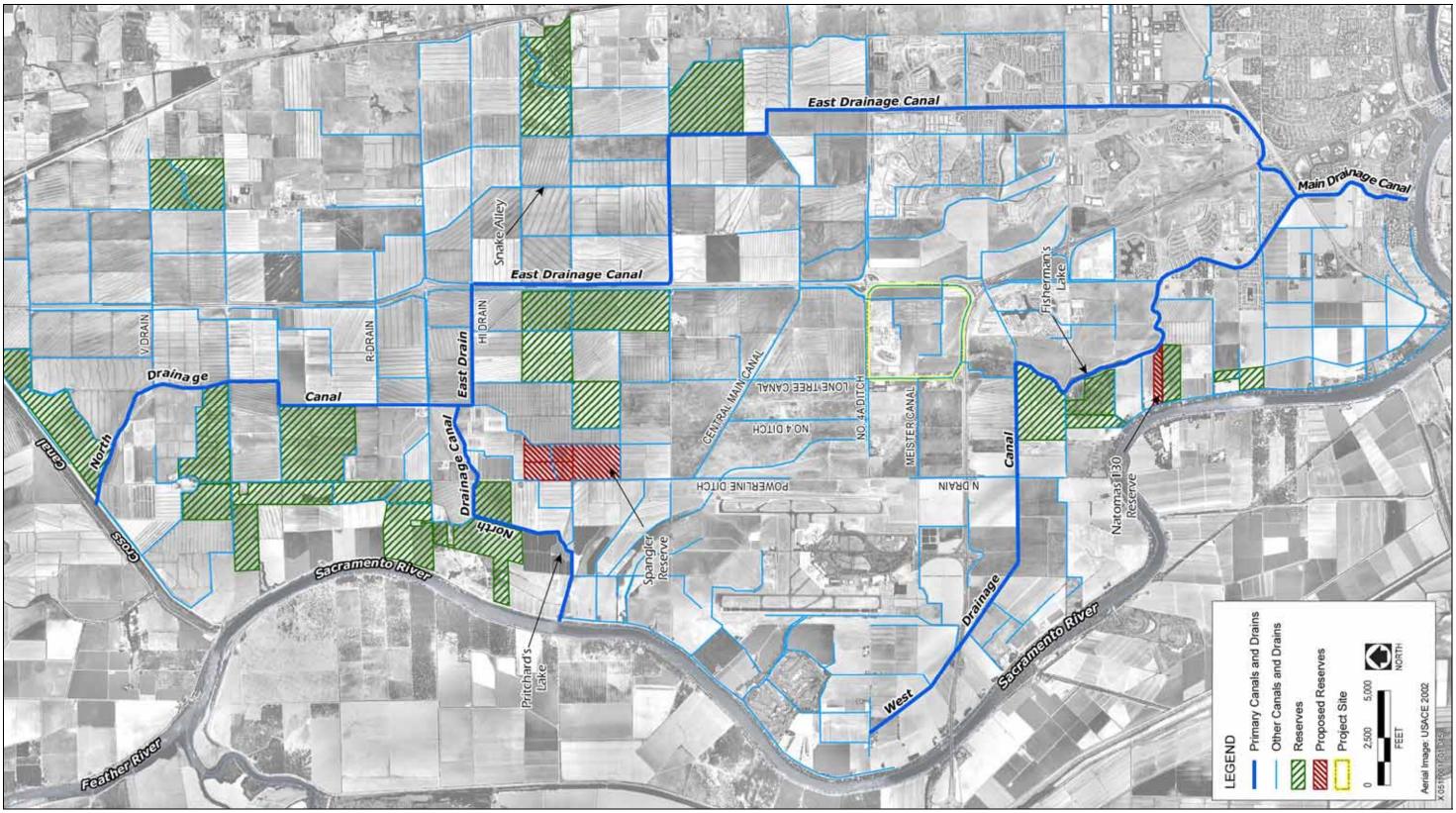
Drainage and flood control is provided by Reclamation District (RD) 1000, a public agency. RD 1000 operates the primary drainage canals within the Natomas Basin and is responsible for conveying and pumping nonurban stormwater runoff from the Basin. Runoff from agricultural lands within the Natomas Basin flows into numerous local drainage ditches that ultimately flow into the primary RD 1000 canals. RD 1000's primary system of interior drains includes the following:

- ► The East Drainage Canal conveys drainage water from the northern and eastern Natomas Basin to its confluence with the Main Drainage Canal northwest of the Interstate 80 (I-80)/Interstate 5 (I-5) interchange. At its closest point the East Drainage Canal is approximately 1.8 miles east of the Greenbriar site.
- ► The West Drainage Canal conveys drainage water from the western Natomas Basin northwest of Sacramento International Airport to its confluence with the Main Drainage Canal. Fisherman's Lake, a natural slough, is a portion of the West Drainage Canal. The West Drainage Canal is approximately 3,000 feet (0.6 mile) south of the Greenbriar site at its closest point across I-5, just before the drainage canal turns south toward Fisherman's Lake.
- ► The Main Drainage Canal conveys the combined flows of the East and West Drainage Canals from their confluence northwest of the I-80/I-5 interchange through South Natomas west of I-80. Drainage water from the Main Drainage Canal is pumped into the Sacramento River approximately 5 land miles to the south (downstream) of the Greenbriar site.
- ► The North Drainage Canal is an interior canal that conveys drainage water from the Sutter County portion of the Natomas Basin northward, where it is pumped into the Natomas Cross Canal.
- ► The Cross Canal conveys drainage water from central portions of Sutter County westward to the Sacramento River. The Cross Canal connects with the Sacramento River approximately 7.1 miles north of the Greenbriar site.
- ► The Natomas East Main Drainage Canal conveys drainage water from Dry Creek, Arcade Creek, and a large portion of the Natomas area north of the confluence with Dry Creek. The Natomas East Main Drainage Canal is also referred to as Steelhead Creek. The Natomas East Main Drainage Canal outfalls to the Sacramento River at the northern edge of Discovery Park and near the confluence of the Sacramento River and American River approximately 5.2 miles south of the Greenbriar site.

These primary drainage canals are significant corridors of aquatic habitat to which the entire drainage network is connected. Exhibit 5 graphically depicts this primary drainage system.

Although the canal network hydrologically connects aquatic and wetland habitats throughout the Natomas Basin, roads impede or block the movement of many animals through aquatic or wetland habitats. Even for animals that could attempt crossing a road surface, such as turtles and snakes, major roads are effectively impassable (Forman et al. 2003, Dodd et al. 2004, Aresco 2005). For major roads, passage is restricted to the culverts through which the canal waters flow. Culverts are themselves obstacles to animal movement; although a wide variety of animals will move through culverts, for most species, the frequency of these movements is low (Yanes 1995, Rodriguez et al. 1996, Clevenger et al. 2001, Forman et al. 2003, Ng et al. 2004). In general, the use of culverts decreases with their length and with the presence of fencing or debris pits (Yanes 1995, Rodriguez et al. 1996, Clevenger et al. 2001, Forman et al. 2003, Ng et al. 2004). Nonetheless, regular animal crossings (including by other species of garter snake) have been documented through even long culverts that are comparable to those under I-5 (see Forman et al. 2003, Ng et al. 2004, Dodd et al. 2004). Conversely, the use of culverts increases with presence of adjacent habitat or cover, roadside fencing that "funnels" animals towards culverts, and with increased visibility through the culvert (Yanes 1995, Rodriguez et al. 1996, Clevenger et al. 2001, Forman et al. 2003, Ng et al. 2004).

Within the Natomas Basin, Interstate 5 (I-5) and State Route 99 (SR 99) are major barriers to animal movement that are crossed by only a few long culverts. Thus, habitat south of I-5 (i.e., in the southern Natomas Basin), such as at Fisherman's Lake, is partially isolated from habitat north of I-5. Similarly, habitats west of SR 99 (i.e., in the northwestern Natomas Basin), such as at Pritchard Lake, are partially isolated from habitat east of SR 99 (i.e., in the northwestern Natomas basin), such as Snake Alley.



Source: CH2M Hill, EDAW 2005

Canals and Drains of Natomas Basin

In 2001 and presently, habitats east and west of SR 99 are linked by culverts on the V Drain, R Drain, H1 Drain, and Central Main Canal; each of these canals in turn connects to a series of drains and ditches.

In 2001, aquatic habitats north and south of I-5 were linked through culverts by the West Drainage Canal, the N Drain (parallel to Powerline Road), and the Lone Tree Canal. The West Drainage Canal passes north under I-5 to the west of the airport. The N Drain and Lone Tree Canal pass north under I-5 to the west and east of MAP where each is connected to a series of ditches, drains, and canals (including Meister Canal) throughout the northwestern portion of the Basin, and to the culverts under SR 99 to the northeastern portion of the Basin. After it passes under Interstate 5, the N Drain, via Powerline Ditch, also connects giant garter snake habitats south of I-5 to those in the northwestern portion of the Basin.

However, as the development authorized by the MAP HCP and the NBHCP has occurred, and will occur, the system of canals connected to the culverts under I-5 has been changing and will continue to change. Except for the West Drainage Canal, all corridors connecting giant garter snake habitats in the southern Natomas Basin to habitats north of I-5 pass through or drain the MAP, and thus they all will be altered under the future condition of the Natomas Basin permitted by the NBHCP. Development authorized by the MAP HCP and NBHCP will eliminate the Powerline Ditch, No. 4 and 4a ditches, and Meister Canal, eliminate water sources to the Airport East Ditch, and replace the open Central Main Canal with an underground pipe. It also will affect habitat along Lone Tree Canal by reducing the area of land draining into Lone Tree Canal, placing urban development along one side of the canal, and widening Elkhorn Boulevard to six lanes (Thomas Reid Associates 2001, USFWS 2002). (The widening of Elkhorn will not increase the length of the culvert, which is already 115 feet long, but it will increase its diameter from 2.5 feet to 4 feet.

Thus, under the future condition permitted by the NBHCP, giant garter snake habitat south of Interstate 5 would be largely isolated from habitat north of Interstate 5. Two possible corridors would remain: the West Drainage Canal and Lone Tree Canal. Both corridors could connect important habitats in the southern Natomas Basin (such as Fisherman's Lake which is along the West Drainage Canal) with those in the northwestern and northeastern portions of the Basin. Along both of these potential corridors, there will be obstacles to giant garter snake movement. Both waterways will pass under Interstate 5 through long culverts (over 300 feet long). The West Drainage Canal currently has limited connection to other waterways north of Interstate 5; in the future, it will probably remain isolated because zones of canals and drainage ditches that are currently not suitable habitat for giant garter snake will likely continue to separate it from habitats north and east of the airport. Lone Tree Canal will pass through a culvert under Elkhorn Boulevard (115 feet long). Development of the Metro Air Park will also affect water flow within Lone Tree Canal, however, the MAP HCP includes provisions under changed circumstances (pages 70-71 in Thomas Reid Associates 2001) that address these effects if water levels are less than 12 inches.

Even if snake movement along these north-south corridors were a rare event, this movement would be very important. It would allow genetic interchange between the Basin's northern and southern subpopulations of giant garter snake, and it would allow giant garter snakes to reestablish in the southern Natomas Basin if that smaller subpopulation were to become extirpated (e.g., due to environmental fluctuations or demographic stochasticity).

Thus, although the relative importance for connectivity of the Lone Tree Canal was not described in the NBHCP, the opportunity for giant garter snakes to move along Lone Tree Canal will be important for the viability of the giant garter snake population in the Natomas Basin.

Under the future condition permitted by the NBHCP at the Greenbriar site, water in Lone Tree Canal would flow south under Elkhorn Boulevard through a 4-foot diameter culvert 115 feet long. It would then flow in a waterway 12 feet wide at the bottom and about 6 feet deep. Along this waterway, set back 25 feet from its western bank will be a low wall 3 feet high, on the other side of which will be Lone Tree Road and commercial and industrial development. Along the eastern bank will be agricultural, ruderal, or natural vegetation. This vegetation would extend for nearly a mile and if cultivated it would include waterways that irrigate and drain the area. At the

southern end of the Greenbriar site, water from the Metro Air Park would enter the canal, and together these waters would flow into three 8-foot by 5-foot box culverts and two 6.5-foot diameter pipes, and pass under Interstate 5.

For this section of Lone Tree Canal between the Interstate 5 and Elkhorn Boulevard culverts, the Greenbriar project would alter these future conditions. The following description of conditions under the future condition with the Greenbriar project is based on the description of the Greenbriar project in the DEIR, BA, the draft conceptual mitigation plan for the project and mitigation measure 6.13-1 of the DEIR. Water would still flow through a 4-foot diameter culvert 115 feet long under Elkhorn Boulevard; there would still be a low wall and development along the western shore, and water would still enter from the Metro Air Park and then flow under Interstate 5 through three 8-foot by 5-foot box culverts and two 6.5-foot diameter pipes. However, near the center of this section of Lone Tree Canal, there would be an additional road crossing (100 feet wide with a 50-foot span that would be 7 feet in height) where Meister Way would cross the canal and an additional road crossing where residential Street 3 would cross the canal (a 53-foot wide crossing). (These crossings would be designed to minimize obstacles to giant garter snake movement [as described in mitigation measure 6.13-1 of the DEIR].) Also, along the eastern bank would be strip (a bench) of tules and other emergent vegetation. This strip of marsh and open water would be relatively narrow; grassland would be on its far side, and within 250 feet of the water flowing in the canal would be a barrier wall and fence separating the corridor along the canal from residential development to the east. There would also be fencing and a wall along Meister Way where it crossed the corridor of managed vegetation along Lone Tree Canal.

This corridor of vegetation along the eastern bank, and the associated structures, would be developed, preserved, maintained, monitored, and adaptively managed by TNBC or another 503(C)(1) organization. This management would be funded by an endowment sufficient for this purpose provided along with the fee title to TNBC (or another 503(C)(1) organization if necessary) which will be established through the process of developing an HCP for the project.

Flows within the canal would also be maintained. The MAP and Greenbriar projects would reduce the area draining into Lone Tree Canal. However, the MAP HCP contains assurances that sufficient water will be maintained in Lone Tree Canal to provide aquatic habitat (as described on pages 70-71 in Thomas Reid Associates 2001), and the Greenbriar project provides an additional assurance that suitable aquatic habitat will be maintained (as described in mitigation measure 6.13-1 of the DEIR).

## 3.5.3 POTENTIAL CONSEQUENCES OF THE GREENBRIAR PROJECT FOR FUTURE CONNECTIVITY

Development of the Greenbriar site, and the creation, enhancement and preservation of habitat at the proposed reserves, could affect the connectivity of habitats at local and regional scales. At a local scale, both development and habitat enhancement/restoration alter the spatial distribution of habitat. Development reduces connectivity and the quantity of habitat accessible to individuals on nearby lands, increases the distance individuals must travel to meet their needs for food and shelter, and increases the risks individuals are exposed to during these movements. Conversely, the enhancement and creation of habitat can increase connectivity, by creating larger areas of contiguous habitat, increasing the food and shelter provided by habitat, or by facilitating movement of individuals. The preservation and active management for habitat values also can maintain connectivity.

#### POTENTIAL EFFECTS ON CONNECTIVITY AT A LOCAL SCALE

Development of the Greenbriar site would adversely affect connectivity of some habitats at a local scale. At this scale, development of the Greenbriar site would reduce the quantity and contiguity of habitat available to individuals of some species using this site and adjacent lands. These individuals would lose part or all of the habitat in their home ranges or territories, and the remaining habitat could be split into separate pieces (i.e., fragments) that would be isolated by development, or require increased risk and energetic cost to access. This

fragmentation of habitat would occur along the northern and southern borders of the Greenbriar site where lands would not be developed under the future condition resulting from the NBHCP, and it would occur along the western border for those species still able to use the remaining corridor of land as habitat. Habitat fragmentation attributable to the Greenbriar project could affect all covered species, except those associated with vernal pools. For example, both burrowing owl and loggerhead shrike currently use the Greenbriar site; after development of the project, patches of habitat for these species would be smaller in size and separated by greater widths of non-habitat.

Conversely, the connectivity of habitats at a local scale would be increased by the creation, enhancement, and preservation of habitat at the proposed Spangler and Natomas 130 reserves, and at the unidentified DEIR mitigation site(s) providing the Swainson's hawk foraging habitat. For example, the marsh created at the Natomas 130 site would be in close proximity to similar habitats at Fisherman's Lake, and the adjoining TNBC Cummings Reserve (Exhibit 5). Based on the evaluation contained in this effects analysis, on balance, the proposed project would not adversely affect habitat connectivity within the Natomas Basin.

#### POTENTIAL EFFECTS ON CONNECTIVITY AT A REGIONAL SCALE

At a regional scale, development can create barriers that isolate areas of otherwise suitable habitat or can subdivide a population into two smaller, and thus less viable, populations. Conversely, habitat creation and enhancement as a result of a conservation strategy associated with development can reduce or eliminate barriers, and can increase connectivity at a regional scale.

In the absence of effective mitigation, development at the Greenbriar site could adversely affect habitat connectivity at a basin-wide scale. Land use at the Greenbriar site could affect connectivity of the southern and central Basin, because it occupies one of the two corridors of habitat that would remain under the future condition resulting from the NBHCP.

The Greenbriar project would convert this site to urban land cover except for a 250-foot wide zone that would remain along the Lone Tree Canal and patches of ruderal habitat east of the Greenbriar site (Exhibit 2). In addition, this remaining habitat along Lone Tree Canal would be crossed by Meister Way and Street 3, which would be new roads that connect the developed Greenbriar site to Lone Tree Road. This development would reduce connectivity of the southern and central Natomas Basin for some species.

If connectivity of habitats were reduced at the Greenbriar site, relatively few species would be adversely affected. First, most species in the Natomas Basin are abundant, widely distributed and highly mobile. (The species observed during monitoring for TNBC support this characterization [Jones & Stokes 2005].) This is largely a consequence of the Natomas Basin being primarily an agricultural (and developed) landscape that is frequently disturbed. Second, Interstate 5 (which is along the entire southern border of the site), and adjacent development to the east and west, already reduces use of the site as a movement corridor by terrestrial animals that are less mobile or are highly sensitive to human disturbance.

The species most likely to be adversely affected at a regional scale by a reduction in connectivity across the Greenbriar site are species dependant on the aquatic or wetland habitat in and immediately adjacent to canals. This is because under the future condition resulting from the NBHCP, there will be few corridors (or perhaps only this one) along canals between the southern and central Natomas Basin, none of which is likely to provide for relatively high levels of movement and dispersal. In particular, in the absence of comprehensive and effective avoidance, minimization, and mitigation measures to offset its effects, development at the Greenbriar site could cause substantial adverse effects on habitat connectivity for the giant garter snake.

At a regional scale, the mitigation for the Greenbriar project also could improve connectivity of wetland and rice habitats in the northern Natomas Basin through its enhancement of habitat at the proposed Spangler reserve, and in the southern Natomas Basin through its creation of marsh habitat at the proposed Natomas 130 reserve. These

sites are connected to the regional system of waterways; thus, the restoration, enhancement and preservation of habitat at these sites could facilitate the movement of covered species along these waterways. This effect, while less important than effects at the Greenbriar site, could still be significant.

The potential effects on connectivity of giant garter snake habitat are further evaluated in the following section.

#### POTENTIAL EFFECTS ON CONNECTIVITY OF GIANT GARTER SNAKE HABITAT AT THE GREENBRIAR SITE

The effects analysis for the connectivity of giant garter snake habitats are based on several assumptions including:

- 1. Giant garter snakes currently use Lone Tree Canal at the Greenbriar site and are likely to continue to do so under the future condition resulting from the NBHCP;
- 2. Occasionally snakes cross through the culverts under Interstate 5;
- 3. The frequency of crossings under Interstate 5 is affected by the extent that snakes use the adjacent sections of Lone Tree Canal;
- 4. The level of snake use is affected by the habitat features provided by Lone Tree Canal and immediately adjacent land (i.e., movement along the canal is not independent of habitat availability and condition along the canal); and
- 5. Mitigation for other projects affecting Lone Tree Canal south of Interstate 5 and north of Elkhorn Boulevard would sustain giant garter snake habitat along those segments of Lone Tree Canal.

In the absence of effective mitigation to maintain or improve connectivity, the Greenbriar project could substantially affect the use of Lone Tree Canal (and of the entire Greenbriar site) by giant garter snakes. The project would:

- eliminate canals and natural vegetation within the Greenbriar site,
- create additional road crossings of Lone Tree Canal at Meister Way and Street 3,
- ► create residential development within 250 feet of Lone Tree Canal, and
- reduce the acreage draining into Lone Tree Canal (potentially reducing flow in the canal).

In the absence of mitigation, these changes could affect giant garter snake use of Lone Tree Canal. Developing agricultural land at the Greenbriar site would directly eliminate habitat that provides prey, cover, basking sites, and refugia. Additional obstacles, increased predation, and increased human activities all could degrade the quality of remaining habitat, increase mortality and reduce snake use of this segment of Lone Tree Canal.

To offset the effects resulting from these changes and to retain giant garter snake habitats and the movement corridor along Lone Tree Canal, the project would have to:

- Assure that water would be provided in the canal to maintain adequate aquatic habitat,
- ▶ Minimize effects on giant garter snake movement at the crossings of Meister Road and Street 3,
- ► Maintain vegetation and conditions along the canal and in adjacent uplands to meet requirements for giant garter snake use and movement, and
- ▶ Reduce the effects of human disturbance, mortality from vehicle collisions, and predation by the cats, dogs, and wildlife associated with developed land uses.

Thus, measures would need to include:

- ▶ Providing some water to the canal in perpetuity or otherwise ensuring that adequate aquatic habitat would be maintained.
- ▶ Restricting adjacent land uses to allow only those compatible with provision of snake habitat, barriers to human and animal use of the site.
- ▶ Designing the Meister Road and Street 3 crossings to minimize impediments to snake movement (e.g., maximize cross-sectional area of and visibility across the canal crossing),
- ► Incorporating barriers that prevent giant garter snake access to developed areas and visually screening developed areas, and
- ▶ Funding site maintenance and management of habitat along the canal and on adjacent land.

The Greenbriar project with applicant-proposed and DEIR mitigation, includes such a set of measures. Measures in the DEIR include:

- a. To ensure that the project does not diminish habitat connectivity for giant garter snake between the southwest and northwest zones identified in the NBHCP, approximately 30.6 acres along Lone Tree Canal shall be protected and managed as giant garter snake habitat. This on-site habitat preservation shall protect an approximately 250-foot wide corridor of giant garter snake habitat that includes the canal and approximately 200 feet of adjacent uplands. Uplands within the linear open space/buffer area shall be managed as perennial grassland as described below. Additional aquatic habitat for giant garter snake shall be created along the east bank of Lone Tree Canal by construction and maintenance of a 2.7 acre tule bench. The habitat shall be managed in perpetuity as high-quality habitat for giant garter snake. Compliance and biological effectiveness monitoring shall be performed and annual monitoring reports prepared within six months of completion of monitoring for any given year. This monitoring, reporting, and adaptive management shall be performed as described in Section IV of the NBHCP.
- b. To ensure that the project does not diminish giant garter snake movement along Lone Tree Canal, all new road crossings of Lone Tree Canal shall be designed to minimize obstacles to giant garter snake movement. The use of culverts under new road crossings on Lone Tree Canal shall be prohibited unless it can be demonstrated that the culverts will not diminish the potential for giant garter snake movement through the section of Lone Tree Canal protected by the setback fence and conservation easement.
- c. Upland giant garter snake habitat within the Lone Tree Canal linear open space/buffer area shall be created and managed to provide cover, basking areas, and refugia during the winter dormant period. Hibernaculae would be constructed at regular intervals by embedding concrete or coarse rock in the bank or in a berm along the Lone Tree Canal corridor to provide additional winter refugia. Upland habitat with the linear open space/buffer areas shall be converted to native perennial grassland and managed, in perpetuity, as perennial grassland habitat.
- d. Aquatic habitat shall be maintained throughout the giant garter snake active season in Lone Tree Canal, in perpetuity. This is the legal responsibility and obligation of Metro Air Park property owners (MAP). The MAP HCP includes provisions for maintaining water in the canal such that the basic habitat requirements of the giant garter snake are met. The MAP HCP also provides a road map, through "Changed Circumstances", to address procedures to follow if water is not being maintained in the canal to meet these requirements. As described in the MAP HCP, the MAP is legally obligated to assure these requirements are met, and financial and procedural mechanisms are included in the MAP HCP to enforce this. It is, therefore, assumed that MAP will provide water to Lone Tree Canal, as required by the MAP HCP and ITP, in perpetuity. It is also assumed that USFWS will use all reasonable means available to it, to enforce this MAP HCP requirement. If

water is not provided to Lone Tree Canal by the MAP to meet the habitat requirements of giant garter snake, as required by the MAP HCP, and USFWS exhausts its enforcement responsibilities, the project applicant shall assume the responsibility of providing suitable giant garter snake aquatic habitat throughout the section of Lone Tree Canal protected by the fence and conservation easement. However, as stated herein, the project applicant shall only assume this responsibility if it has been sufficiently demonstrated to the City that USFWS has exhausted all reasonable means to compel MAP to comply with the relevant conditions of the MAP ITP. Specific requirements related to ensuring suitable aquatic habitat in Lone Tree Canal is present, in perpetuity, throughout the giant garter snake active season shall be developed through consultation with DFG and USFWS, and included in the new or amended HCP for Greenbriar, and may include mechanisms, such as installation of a well, to assure water is provided in the canal to meet habitat requirements.

- e. A barrier shall be installed between the giant garter snake habitat linear open space/buffer area and the adjacent Greenbriar development to ensure that giant garter snakes do not enter the development area, and to prohibit humans and pets from entering the giant garter snake habitat. The design of this barrier shall be subject to USFWS and CDFG review and approval. The entire length of the barrier, which shall be bordered by yards rather than roadways, shall be maintained on the preserve side by a nonprofit land trust to ensure that vegetation or debris does not accumulate near the barrier and provide opportunities for wildlife and pets to climb over the barrier. On the development side, Covenants, Codes and Restrictions (CCRs) shall prohibit accumulation of vegetation or debris adjacent to the barrier. Chain link fencing shall be placed at both ends of the corridor, with locked gates permitting entry only by RD 1000 and NMWD for channel maintenance, and by the preserve manager for habitat monitoring and maintenance purposes.
- f. Specific requirements associated with the barrier shall be developed through consultation with USFWS and DFG, and may include the following and/or other specifications that DFG and USFWS consider to be equally or more effective:
  - Adequate height and below-ground depth to prevent snakes or burrowing mammals from providing a through-route for snakes by establishing burrows from one side to the other crossing;
  - ► Constructed using extruded concrete or block construction extending a minimum of 36-inches above ground level;
  - ► Maintenance to repair the barrier and to prevent the establishment of vegetation or collection of debris that could provide snakes with a climbing surface allowing them to breech the barrier;
  - A cap or lip extending at least two-inches beyond the barrier's vertical edge to prevent snakes from gaining access along the barrier's top edge; and
  - ▶ Signage to discourage humans and their pets from entering the area.
- g. The Lone Tree Canal linear open space/buffer area shall be protected in perpetuity under a conservation easement and managed to sustain the value of this area for giant garter snake habitat connectivity. Compliance and biological effectiveness monitoring shall be performed and annual monitoring reports prepared. This monitoring, reporting, and adaptive management shall be performed as described in Section IV of the NBHCP or following procedures developed in formal consultation with USFWS and DFG and contained in an ESA Incidental Take Permit for the Greenbriar project.

#### **Assessment of Required Width and Other Setback Attributes**

To date, several recommendations have been made regarding the required width of a setback to conserve canal habitat for giant garter snake use and movement. These previous recommendations include:

- ▶ In the avoidance and minimization measures of a biological opinion for a programmatic consultation with the U.S. Army Corps of Engineers, a measure was included to avoid construction activities within 200 feet from the banks of giant garter snake aquatic habitat (USFWS 1997). The basis given for this distance was that most giant garter snake use of uplands was within 200 feet of aquatic habitat. This same biological opinion also included a requirement that replacement habitat must be located at least 200 feet from roadways "to reduce vehicular mortality" (USFWS 1997).
- ► The NBHCP includes a requirement (for which there may be exceptions) that reserves be at least 800 feet from existing or planned urban lands, because intensively developed land is "significantly incompatible with the objectives and purposes of the reserve system" and that urban lands are likely to cause significant adverse effects on reserve viability or on covered species occupying the reserve (City of Sacramento et al. 2003, page IV-16). The NBHCP does not include an explanation of why these effects would no longer be significant with urban land at a distance of 800 feet.
- ► The NBHCP includes a requirement that reserves contain a buffer (typically of natural or ruderal vegetation) 30–75 feet in width to minimize the effects of incompatible land uses. These effects are referred to as "population mortality effects"; the relationship of these effects to the width of the buffer is not described.
- ▶ Planning documents for North Natomas have included setbacks ranging from 200 to 250 feet in width between urban development and adjacent agricultural areas (Padre Associates 2005). Initially, these setbacks were intended to reduce conflicts between agriculture and development; later, open space and habitat benefits were added to their purpose.
- The Fisherman's Lake Buffer Zone Study (Padre Associates 2005) includes a species account for giant garter snake, a review of the USFWS, Natomas Community Plan, and NBHCP setbacks and buffers described above, and a brief evaluation of the effectiveness of the 250- and 800-foot wide buffers that were under consideration at Fisherman's Lake. This evaluation concludes that "For GGS, all scenarios from the City Boundary and the RD 1000 ROW Boundary alternatives would provide adequate protection of 200 feet from the edge of the channel banks per USFWS guidelines." Relationships between setback width and particular effects on giant garter snake were not evaluated in this study.

Although the documents with these recommendations did not include analyses to support their recommended setback or buffer widths, our understanding of the ecology of giant garter snake, and of the effects of development on adjacent habitats is sufficient to evaluate the width of habitat required in canal setbacks, the benefits of different buffer widths, and the need for active management and for other measures in setbacks in addition to buffers.

Without a setback that includes sufficient habitat for giant garter snake use and movement, a buffer to prevent adjacent development from degrading this habitat, other measures (such as barriers) incorporated into the setback, and active management of the setback, giant garter snakes might not use and move along Lone Tree Canal.

Determining the required width and constituents of setbacks are subject to several factors. First, increasing land values are a factor in the purchase of the needed setback areas. Second, the level of scientific understanding can adequately determine the need for setbacks, but is generally not adequate for determining the required width for the setbacks (or even a relatively wide range of widths, in many cases) (ELI 2003). In general, wider setbacks reduce adverse effects of adjacent development, but some types of effects diminish only gradually with increased setback width (such as increased predation), and some adverse effects are largely unaltered across a wide range of setback widths (such as the introduction and spread of invasive plants). Consequently, unless setbacks are actively managed and include additional measures (such as barriers) only very wide setbacks (over a thousand feet wide) can preclude most adverse effects.

Although such wide buffers would sustain habitat functions, they are often impracticable, and generally would be a more inefficient use of conservation. Narrower but actively managed setbacks with barriers are also expensive and provide relatively little habitat. They are, however, justified if the conserved habitat is irreplaceable or

otherwise of very high value. Assuming that giant garter snakes would use Lone Tree Canal under the future condition permitted by the NBHCP, and occasionally cross under I-5, Lone Tree Canal provides high value habitat that merits conservation even at a relatively high cost.

Along Lone Tree Canal, the purpose of the setback is to conserve giant garter snake use of, and movement along, the canal to facilitate the occasional movement of individuals through the culverts under I-5. In general, a moderate level of uncertainty exists of the attributes necessary for wildlife use of corridors (ELI 2003). Important factors affecting animal use of a corridor include the corridor's suitability as habitat, the feasibility of passing through the corridor and the level of effort and of risk involved in doing so. If a corridor does not meet a species' habitat requirements for residence or foraging, it may not be used for daily or seasonal movement, or for dispersal, and hence would not connect habitat patches (Noss et al. 1996, Rosenberg et al. 1997; Brinson et al. 2002).

Therefore, a setback along Lone Tree Canal should include sufficient habitat to support giant garter snake use of the canal for foraging and residence. This habitat would need to include the canal itself and adjacent uplands.

In general, even species associated with wetlands, streams and waterways may require and regularly use wide zones of adjacent uplands as habitat. For this reason, to provide habitat that meets year-round requirements, setbacks of several hundred feet or more have been recommended for many wetland- and riparian-associated animals (Semlitsch and Bodie 2003).

The width of uplands used by giant garter snakes varies considerably. Giant garter snakes primarily use canals, canal banks, immediately adjacent uplands, and the edges of rice fields. Giant garter snakes generally do not use non-rice agricultural crops (Wylie and Casazza 2000). Many summer basking and refuge areas used by this snake are immediately adjacent to canals and other aquatic habitats, and may even be located in the upper canal banks (Eric Hansen, pers. comm.).

Giant garter snakes, however, also use uplands hundreds of feet from waterways or wetlands. They have been observed hibernating as far as 820 feet from water, and any land within this distance could be important for snake survival in some cases (Hansen 1988). (Hibernaculae [i.e., hibernation sites] this distant from water, however, are most often found in areas with high winter floods.) Giant garter snakes also seek refuge in upland burrows during hot summer weather (Hansen and Brode 1993), and have been documented up to 164 feet from aquatic habitat during this time (Wylie et al. 1997). Use of sites at greater distances from wetlands is associated with landscapes where suitable close sites are not available. This is not generally the case in the agricultural landscape of the Natomas Basin because canal banks often provide refuges and hibernaculae, and the agricultural lands themselves are at slightly lower elevations than canal banks, generally have less cover and fewer refugia than canal banks, and may be flooded or tilled during winter.

The width required to provide cover, forage, refugia, and basking sites along Lone Tree Canal could be quite narrow. Many canals provide cover, foraging habitat, and refugia; and, giant garter snakes regularly use narrow corridors of habitat along canals crossing agricultural landscapes. Although giant garter snake use of, and movement along, a canal might require little more than habitat along the canal and its banks, habitat on adjacent land would likely increase giant garter snake use of, and movement along, a canal.

In addition to habitat, a setback also must contain a sufficient buffer to preclude degradation of canal habitats by human activities. Different types of effects on canal habitats could diminish substantially over short distances, gradually over relatively large distances, or the magnitude of effects could be largely unrelated to setback width. For example, alteration of local microclimates, drift of herbicides and pesticides applied on adjacent lands, and sediment and pollutants in runoff from adjacent land all typically diminish substantially across a distance of 50–100 feet (de Snoo and de Wit 1998, Wenger 1999, Forman et al. 2003).

In contrast, the effects of human disturbance diminish gradually with increasing distance. In this context, human disturbance is any human activity that changes the contemporaneous behavior or physiology or one or more animals (Nisbet 2000). Human activities could interrupt the foraging or reproductive activities of animals and

cause them to flee or avoid an area. This may expose these animals to increased risk of mortality, or reduce their reproductive success. In essence, animals perceive humans as potential predators and respond accordingly (Frid and Dill 2002). This perceived predation risk diminishes with distance, but it is affected by other factors. The sensitivity to human disturbance varies among animal species (Cooke 1980, Blumstein et al. 2003), across sites (Blumstein et al. 2003, Rodgers et al. 1997), on trails versus off trails (Miller et al. 2001), with barriers visible to animals (Ikuta and Blumstein 2003) the number of humans (Beale and Monaghan 2004), the type of activity (Holmes et al. 1993, Rodgers and Smith 1995, Rodgers and Smith 1997, Miller et al. 2001), and the visibility of humans to animals (Richardson and Miller 1997, Phillips et al. 2001). Also, to some extent, some animals habituate to human activities (Cooke 1980, Nisbet 2000).

Giant garter snakes are highly sensitive to such human disturbance, and will abandon otherwise suitable habitat as a result of increased human activity such as fishing (Eric Hansen, pers. comm.). Human visits to areas occupied by snakes could result in lowered snake abundance even when the visits are brief in duration and no more than one person, once per day (Eric Hansen, pers. comm.). Human activities can also degrade giant garter snake habitats by trampling vegetation, compacting soils, destabilizing banks, and crushing burrows.

Human use of habitats along Lone Tree Canal would diminish with increasing distance from development. However, human access from Elkhorn Boulevard, Lone Tree Road, Meister Way, and Street 3 would allow dumping, trampling of vegetation and refugia, and harassment of snakes to occur almost independent of buffer width. This human access would probably reduce giant garter snake use of this section of Lone Tree Canal. Maintained fences, however, would probably reduce human access to levels that would not reduce snake use of the canal or degrade habitat quality by trampling vegetation and damaging banks.

Similarly, domestic and feral cats and dogs associated with residential development can range widely (hundreds of feet), and harass or prey upon a wide variety of small animals (Crooks and Soule 1999, Hayes et al. 1999, Risbey et al. 2000, Odell and Knight 2001, Lepczyk et al. 2003). Therefore, although it has not been studied, such harassment and predation of giant garter snakes should be considered likely until evidence indicates otherwise. In addition to causing mortality, this predation and harassment could reduce giant garter snake use of the canal. A wide variety of fences have been used to exclude cats and other animals from conserved areas, and many have been found to be effective with regular maintenance (Long and Robley 2004, Moseby and Read 2005).

Some effects are unrelated to buffer width. For example, the effects of road crossings and other structures within setbacks are not mitigated by increasing buffer width. Roads frequently are located across riparian areas, canals, and conserved corridors. These crossings can provide human access across buffers and setbacks, alter physical processes, cause mortality of animals from collisions with vehicles, and create obstacles to animal movement.

At the Greenbriar site, existing culverts on Lone Tree Canal reduce animal movement and the project would also add an additional road crossing at Meister Way and at an additional residential street (Street 3). The canal would not pass under Meister Way through a culvert but rather the roadway would span the canal leaving a 50-foot wide by 7-foot high space for the canal to flow through. At Street 3, the crossing would be 53 feet wide, and although flow under the crossing could be accommodated by two 42-inch culverts, mitigation measure 6.13-1 of the DEIR prohibits placing Lone Tree Canal in culverts at new road crossings (unless it is demonstrated that the culverts would not reduce the potential for giant garter snake movement). Thus, this crossing also would likely be an open span. The effect of these crossings would not be directly related to setback width, but the flow of water through this section of canal, and the enhancement and management of vegetation near the crossings, would likely affect giant garter snake use.

Collisions with vehicles may be an important source of mortality for giant garter snake (Leidy 1992; E. Hansen pers. comm.). Numerous studies have documented mortality of snakes along roads (Rosen and Lowe 1994, Bonnet et al. 1999), negative correlations of reptile or amphibian abundance with road density or traffic levels (Marchand and Litvaitis 2004; Pellet et al. 2004), and the potential for roads to affect population persistence (Marchand and Litvaitis 2004; Gibbs and Shriver 2002). Increasing setback width would not reduce this effect along roads that cross the

setback. Therefore, barriers to prevent snakes from entering roads (and adjacent developed areas) should be incorporated into setbacks. The effectiveness of such barriers has been demonstrated for other species where culverts also exist to allow passage under the road (Guyot and Clobert 1988; Dodd et al. 2005; Aresco 2005).

Buffers can reduce the effects of altered hydrology where they include a considerable portion of the watershed, or where the alteration involves increased overland flow. The effects of water diversions, however, are not reduced by setbacks.

Because of the existence of effects that do not diminish with setback width (or that diminish gradually), additional measures are necessary to buffer canal habitats from adjacent land uses. These additional measures include barriers to human and pet access, visual barriers to shield nearby human activities from sight, provision of supplemental water, and active management of the buffer.

Where barriers are added to buffers, and conserved habitat and buffers are actively managed, the width required for an adequate setback (i.e., conserved habitat plus buffer) can be determined with more precision, because many types of adverse effects can be substantially reduced and some aspects of habitat structure can be maintained by human action.

For giant garter snake setbacks, the buffer must be of sufficient width to include barriers to human and pet access into the buffer, a barrier to prevent snake access to developed areas and roads, and a barrier that shields human activities in developed areas from the vision of snakes. It also should be of sufficient width to include an access road and additional habitat features that are necessary or beneficial for giant garter snake use of the protected corridor.

Because canals, unlike riparian areas, have stable boundaries, the habitat, barrier, and road components of a managed setback can be located in a zone immediately adjacent to the base of the canal bank. The width of this zone would vary primarily with the width desired for incorporating additional habitat components, because the road, fence, and other barrier features would require relatively standard widths.

A setback that consisted of a canal and a buffer of 25–50 feet from the base of each canal bank might be sufficiently wide to include a corridor of canal habitat for giant garter snake use and movement, and an access road and necessary barriers. But, it would not allow additional giant garter snake habitat to be incorporated.

Although giant garter snake uses narrow corridors within agricultural landscapes, additional habitat along canals may be necessary or beneficial in more intensively developed landscapes, particularly if such corridors are lengthy or include impediments to movement, as at the Greenbriar site. In an agricultural landscape, in addition to canal habitat, snakes have access to some cover basking sites, refugia, and foraging habitat on adjacent land, and the presence of these adjacent habitat features could influence snake use of canals. This adjacent habitat also could help protect them from predators, floodwaters, and canal maintenance and other human activities. In particular, because maintenance of vegetation along canals and fluctuations in water levels could temporarily degrade canal habitat along a conserved corridor, additional adjacent habitat may enhance use of the corridor by providing more stable conditions. (This may be important at the Greenbriar site because RD 1000 has an easement for access and maintenance of the Lone Tree Canal.)

Wider setbacks would provide the opportunity to incorporate such additional habitat, provide greater flexibility for future management, and would likely result in more effective conservation of conserved corridors along canals. Setbacks with buffers outside of the canal banks that are 100 feet or more in width probably should be sufficient to incorporate habitat components such as channels parallel to the canal and with an adjacent strip of marsh vegetation. To incorporate large water features or wide tracts of managed marsh, buffers would need to be several hundred feet wide. However, creating such extensive habitat immediately adjacent to development may not be desirable. A notable exception might be the inclusion of storm water retention basins; including these structures within canal setbacks may result in wider buffers that more effectively isolate canal habitat from development, while also making more land available for development. It is not known if storm water detention basins and associated structures can be designed to provide suitable habitat for giant garter snake.

In summary, canal habitats actively used by giant garter snake for movement along a canal may be relatively narrow (i.e., less than 50 feet from the canal banks). But, to sustain giant garter snake use of this habitat, a buffer is required to reduce adverse effects from adjacent development and allow additional habitat to be created along the canal as necessary, and to provide some flexibility for future management. To reduce adverse effects, buffers must either be very wide (hundreds to thousands of feet in width), or incorporate barriers to prevent human and pet access and to prevent giant garter snakes from entering developed areas, and must be accessible and actively managed. These components probably add 25–50 feet to the required buffer. Habitat components that may be necessary for giant garter snake use of a canal corridor through a developed landscape probably require at least an additional 50–100 feet, and some types of additional habitat features (e.g., large water bodies) may require a buffer with a width of several hundred feet. Therefore, the total width of setbacks should be at least the width of the canal and its banks, plus an additional 125–200 feet.

The setback proposed by the Greenbriar project is consistent with this width. With the DEIR mitigation it would contain fencing, barrier, habitat enhancement, and management measures, habitat would be enhanced, and the effects of adjacent land uses on this habitat would be minimized. (The specific design of fencing/barriers along Lone Tree Canal, the location of the access road, and the details of habitat enhancement and management measures would be developed in consultation with DFG and USFWS during the development of an HCP for the project.)

#### OVERALL EFFECT ON CONNECTIVITY OF GIANT GARTER SNAKE HABITATS

The DEIR mitigation would likely offset the Greenbriar project's effects on giant garter snake movement along Lone Tree Canal, and are in addition to, and do not conflict with, the measures incorporated into the MAP HCP. (For example, a smaller setback and a barrier also exist on the Metro Air Park side of Lone Tree Canal.)

In addition, because existing conditions do not provide high value habitat for giant garter snake along the entire length of Lone Tree Canal and are not optimal for movement of the snake along the canal, opportunities also exist to enhance connectivity. Management of the canal and adjacent uplands for giant garter snake would result in an improvement over current conditions, and over the future condition resulting from the NBHCP. The project and the mitigation proposed in the DEIR include measures to enhance habitat along the canal (e.g., the creation of marsh habitat along the eastern bank of the canal).

In conclusion, for giant garter snake, significant adverse effects on connectivity between habitats in the southern and central Natomas Basin would be unlikely, and would not cause adverse effects on the implementation of the NBHCP giant garter snake conservation measures.

#### 3.6 CONNECTIVITY OF EXISTING TNBC RESERVES

In the absence of effective avoidance, minimization, and mitigation, the Greenbriar project could adversely affect connectivity of TNBC reserves in the Natomas Basin. As described in the preceding section, in the absence of mitigation measures proposed in the DEIR connectivity of habitats in the southern and central portions of the Natomas Basin could be reduced by the Greenbriar development, and this reduction would be substantial for species that would not pass through the corridor remaining along Lone Tree Canal.

For species not passing through the remaining corridor along Lone Tree Canal, the connectivity of TNBC reserves would be reduced. The travel distances between reserves in the southern and central Natomas Basin, with and without passing through a corridor between the Metro Air Park and the City, indicate this change in reserve connectivity. For example, passing through the Greenbriar site, the distance between the nearest reserve in the southern Basin (the Rosa property) and the nearest reserve in the central Basin (the Tufts property) is about 4 miles across uplands and 4.2 miles along canals (Exhibit 5). If development of the Greenbriar site prevented a species from passing between the Air Park and the City, these distances would become 6.7 and 8.7 miles via uplands and canals, respectively. (These distances assume that an individual that cannot pass between the Air Park and the City also can not pass between the Air Park and the Airport.) Similarly, crossing the Greenbriar site, the shortest distance between

existing reserves in the southern and central Basin (i.e., the Rosa and Ayala properties) is about 3.8 miles across uplands and 5.2 miles along canals. If development of the project prevented movement through a corridor between the Air Park and City, then these distances would increase to 9.4 and 11.2 miles via uplands and canals, respectively. Though these examples involved the southern reserves closest to the central Natomas Basin, the change in connectivity would be comparable at other reserves in the southern Natomas Basin.

However, as described in the preceding section that addressed effects on habitat connectivity, the Greenbriar project (with the mitigation proposed in the DEIR) would include a set of measures to reduce effects on connectivity; in addition, canal and adjacent upland habitats would be enhanced along Lone Tree Canal. Therefore, significant adverse effects on the connectivity of existing TNBC reserves would be unlikely.

The project's proposed off-site reserve lands also could cause some positive effects on connectivity. This would be due primarily to the enhancement of habitat on the Spangler site, which could increase connectivity among the nearby reserves to the east and northwest (the Atkinson/Ruby and Sills reserves, respectively). The preservation of additional land to provide Swainson's hawk foraging habitat (as required by mitigation measure 6.13-2 of the DEIR) also could increase connectivity of existing TNBC reserves. The location of these lands, however, has not been determined, and thus this potential benefit cannot be described in any detail.

#### 3.7 HABITAT VALUE OF EXISTING TNBC RESERVES

The Greenbriar project would cause adverse and beneficial effects on the habitat value of existing TNBC reserves. The adverse effects would result from reducing the acreage of foraging habitat most accessible to (i.e., within 1 mile of) an existing TNBC reserve. The beneficial effects would result from preserving, creating and enhancing habitat adjacent to or near existing TNBC reserves.

#### 3.7.1 EFFECTS OF DEVELOPMENT AT GREENBRIAR SITE

No existing TNBC reserves are within 800 feet of the Greenbriar site and only one reserve (the Rosa property) is within a mile (Exhibit 5). Development at the Greenbriar site would detrimentally affect the quantity and connectivity of foraging habitat for raptors nesting at or near this reserve, and also would similarly affect the Souza and Natomas Farms reserves that are within one and a quarter miles of the site.

The foraging habitat available to raptors nesting at these existing reserves would be detrimentally affected by development at the Greenbriar site. Of the land within a mile of TNBC's Rosa property, about 31% is in the Metro Air Park or City of Sacramento permit areas; the Greenbriar site accounts for an additional 6%. Thus, habitat value for raptors nesting at this reserve would be reduced under the future condition of the Natomas Basin, and development of the Greenbriar site would further reduce habitat value for raptors. Development of the Greenbriar site also would detrimentally affect the value of TNBC's Souza and Natomas Farms reserves for nesting raptors, though to a lesser degree than at the Rosa property because these reserves are further from the Greenbriar site (Exhibit 5).

The DEIR requires additional mitigation to offset these effects. For Swainson's hawk foraging habitat lost, mitigation measure 6.13-2 of the DEIR requires preservation of habitat that provides equal or greater habitat values than the habitat lost at the Greenbriar site. To provide equal or greater foraging habitat values, this mitigation measure would require enhancement and preservation of at least 49 acres of to provide high quality habitat within one mile of an existing TNBC reserve (or of the Swainson's hawk zone along the Sacramento River). This DEIR mitigation is in addition to the project's proposed reserves. The habitat provided by this mitigation measure would likely offset the project's effect on Swainson's hawks and other raptors residing at or near existing reserves, though the reserves benefiting from habitat enhancements may differ from those adversely affected by the loss of foraging habitat on the Greenbriar site.

Though it is possible that the project could detrimentally affect foraging habitat available to giant garter snakes at the Rosa, Souza and Natomas Farms reserves, this effect was considered insignificant. Because canals connect these reserves to habitat suitable for giant garter snake on the Greenbriar site, and because the site is within 1–2 miles of these reserves (Exhibit 5), development of the Greenbriar site could reduce the quantity of suitable habitat available to giant garter snakes foraging or residing at these reserves. While not discountable, this effect may be negligible because the culvert at Interstate 5 may restrict snake movement along the canal such that snakes residing south of Interstate 5 rarely forage north of Interstate 5. Furthermore, loss of habitat within 1–2 miles of these reserves would be partially, or perhaps even fully, offset by the creation of 14 acres of marsh habitat at the Natomas 130 parcel that is also connected to these reserves by canals, and is at a distance from the reserves comparable to that of the Greenbriar site.

#### 3.7.2 EFFECTS OF PROPOSED RESERVES

The restoration of marsh at the proposed reserves would cause both adverse and beneficial effects on the habitat value of existing reserves. The acreage of Swainson's hawk foraging habitat would be reduced at the Natomas 130 parcel. Restoration at this proposed reserve would reduce the acreage of Swainson's hawk habitat because 14 acres of fallow agricultural land (which was non-rice crop in 2001) would be converted to marsh, which would provide only smaller areas of moderate quality foraging habitat, while only 14 acres would be enhanced for Swainson's hawk foraging on the remainder of the site. However, the enhanced foraging habitat would be of high quality which would provide resources sufficient to offset the lost habitat acreage.

The proposed reserves could increase habitat available to giant garter snakes at existing TNBC reserves in the Central Basin (i.e., the Tufts, Sills, Ruby, and Atkinson reserves) because one of these reserves (the Spangler property) could be accessible to snakes using those reserves. These existing reserves are all within two miles of the proposed Spangler reserve where marsh would be created and rice will be managed to enhance its habitat value for giant garter snake (Exhibit 5).

The project's proposed reserves would contribute to the size and connectivity of existing TNBC reserves. The North Natomas 130 parcel is immediately north of the TNBC Cummings reserve (Exhibit 5) and would increase the size of that reserve; the Spangler parcel is located between the Tufts and Atkinson reserves and is also connected to them via canals and drains (Exhibit 5); thus, it would increase their connectivity. The preservation of additional land to provide Swainson's hawk foraging habitat (as required by mitigation measure 6.13-2 of the DEIR) also could increase connectivity of existing TNBC reserves. By increasing the size and connectivity of existing reserves, and by increasing the area of preserved land in the vicinity of existing reserves, the project would beneficially affect the habitat value of existing reserves.

#### 3.7.3 OVERALL EFFECT ON HABITAT VALUE OF TNBC RESERVES

Overall, the Greenbriar project would not adversely affect the habitat quality of the existing TNBC reserve system, and could cause a beneficial effect by preserving, creating, and enhancing habitat on adjacent or nearby lands that would benefit wildlife residing at or using existing TNBC reserves. However, it could cause small adverse effects on the foraging habitat available to Swainson's hawks nesting at or near reserves in the southern Natomas Basin, and though its mitigation would provide foraging habitat for hawks nesting at TNBC reserves, these may not be the same reserves that would experience a loss of foraging habitat. Thus, individual reserves may experience small adverse or beneficial effects due to the Greenbriar project.

#### 3.8 WATER AVAILABILITY AT TNBC RESERVES

The Greenbriar project would eliminate several canals on the Greenbriar site, and would convert this site from predominantly agricultural to urban land cover. These changes, however, would not be anticipated to alter water availability to TNBC reserves or cause additional canals to be eliminated outside of the Greenbriar site (Dave Fischer, Natomas Central Mutual Water Company, pers. comm.).

The project would alter drainage of the Greenbriar site, and eliminate delivery of irrigation water by canals. These changes would affect water levels in canals and drains connected to the site. Because no TNBC reserves are adjacent to the Greenbriar site, these alterations are not anticipated to alter water availability at TNBC reserves.

The additional reserve lands associated with the Greenbriar project are in the Natomas Basin and thus would increase the portion of the Natomas Central Mutual Water Company held by shareholders concerned with the habitat values of the canal system and with the availability of water at TNBC reserves. In fact, TNBC has already requested changes to operations and maintenance practices (J. Roberts, pers. comm.). In the future, this may contribute to attainment of NBHCP goals and objectives, but is not anticipated to alter any specific operations by the water company in the near future.

#### 3.9 OPPORTUNITIES TO ESTABLISH ADDITIONAL TNBC RESERVES

The Greenbriar project would cause both beneficial and adverse effects on opportunities to establish additional TNBC reserves. The adverse effects would result from reducing the acreage of land available to provide the mitigation required by the NBHCP. The beneficial effects would result from increasing the total acreage of reserves in the Natomas Basin, and thus increasing opportunities to establish larger reserves.

#### 3.9.1 EFFECTS ON AVAILABILITY OF LAND FOR NBHCP RESERVE ESTABLISHMENT

Mitigation for the NBHCP consists of 8,750 acres of managed marsh, rice, and uplands. Based on the acreage of the Metro Air Park, City of Sacramento, and Sutter County permit areas for urban development, and of existing development outside of those areas, the Natomas Basin contains substantially more than 8,750 acres of land potentially suitable as and potentially available for mitigation. Of the Natomas Basin's 53,537 acres, about 26,376 are outside of permit areas and in land cover types suitable for preservation. However, at least 5,205 acres of these lands are unavailable for preservation as NBHCP mitigation (e.g., lands in suitable land cover that are owned by the Sacramento International Airport). Thus, there are about 21,171 acres of land that are both potentially suitable as mitigation and potentially available.

Although the acreage of potentially suitable and available land could be over twice the acreage required by the NBHCP for preservation, the NBHCP, nonetheless, requires that a substantial portion of suitable land in the Natomas Basin be preserved. Thus, numerous factors affecting the suitability of land for preservation could complicate establishment of an interconnected reserve system of this size, and may increase its cost or compromise the habitat quality of reserves. These factors include existing easements, infrastructure and buildings, availability of land for purchase, adjacent land uses and proximity to urban development, connectivity to other reserves, availability of water, suitability of soils for the establishment of managed marsh, and parcel size relative to the desired size of reserves.

The Greenbriar project would reduce the acreage available for preservation as mitigation for development permitted by the NBHCP and affect the feasibility of preserving land adjacent to the Greenbriar, proposed reserve and mitigation sites. Because of the Greenbriar project, 815 acres would become unavailable or unsuitable for preservation. These lands include: 546 acres developed at the Greenbriar site, 265.8 acres at the proposed Natomas 130 and Spangler reserves, 30.6 acres at the proposed reserve along Lone Tree Canal, and at least 49 acres of Swainson's hawk foraging habitat required by mitigation measure 6.13-2 of the DEIR at mitigation site(s) still to be determined. Of this land, 76 acres are already in land cover types that are unsuitable for preservation and subsequent restoration or enhancement (e.g., rural residential land). Thus, overall, the Greenbriar project reduces the acreage of land potentially suitable and available for preservation by 815 acres, from 21,171 to 20,356 acres, a reduction of about 4%. Even with this reduction, the remaining acreage of land potentially suitable and available for preservation (20,356 acres) would be more than twice the 8,750 acres the NBHCP requires for the reserve system.

## 3.9.2 EFFECTS OF GREENBRIAR SITE DEVELOPMENT ON TNBC RESERVE ESTABLISHMENT

Though the NBHCP did not identify the Greenbriar site as a potential reserve, the NBHCP also did not identify a complete set of potential reserve sites; therefore, most land outside of areas permitted for urban development, including the Greenbriar site, could be considered a potential reserve site. Development of the Greenbriar site would reduce options for establishing a reserve over 400 acres in size that included parcels adjacent to the Greenbriar site, and would eliminate any opportunity for a reserve that included the Greenbriar site. Consequently, this eliminates the option of preserving the entire corridor between the Metro Air Park and Sacramento City permit areas.

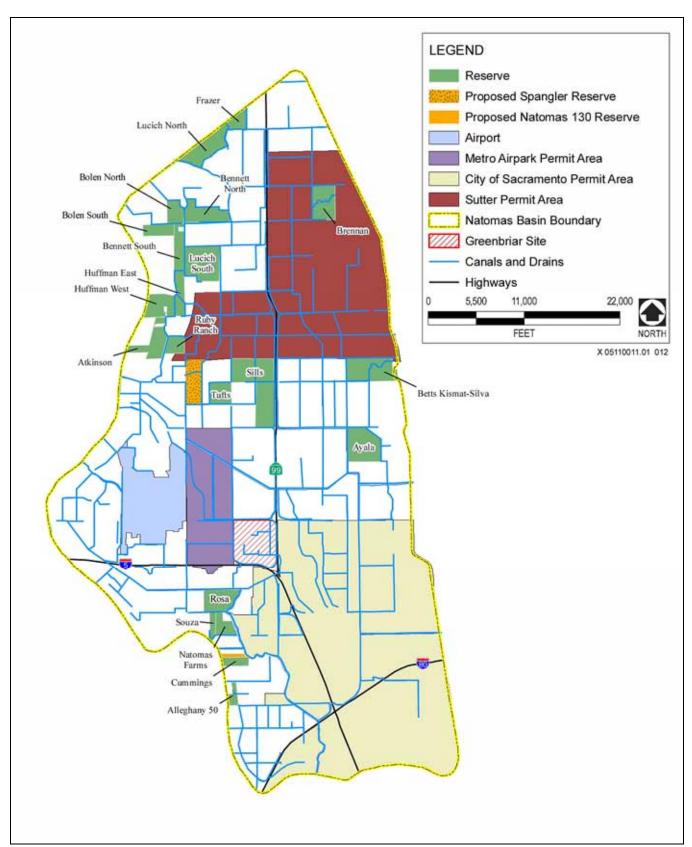
The Greenbriar site has, or could be enhanced to provide, conservation values that would merit preservation, but it also has several major limitations on the habitat values that it could provide. Much of the Greenbriar site provides habitat for covered species, and the site could be managed to provide various combinations of marsh, rice, upland, and canal habitats. It also occupies a corridor between the southern and central Natomas Basin that is important for the movement and dispersal of individuals, particularly for giant garter snake. A portion of the site, however, is in land cover types that are unsuitable for preservation and subsequent restoration or enhancement (e.g., rural residential land). Other portions of the site are immediately adjacent to major highways, or under the future condition of the Basin would be adjacent to urban development, and these areas would potentially experience high levels of human-wildlife conflicts. Nearly half of the site is either unsuitable for preservation and restoration or would be within 800 feet of a major highway or urban development. Highways and urban development would also reduce the connectivity of habitats on the Greenbriar site with habitats that would remain to the north and to the south. Despite these limitations, preserving the Greenbriar site could contribute more to sustaining the viability of the Basin's giant garter snake population and to attaining the goals and objectives of the NBHCP than would many other sites, because the Greenbriar site provides the opportunity to preserve and enhance the connectivity of canal habitats between the southern and central Natomas Basin.

Though it would develop most of the site, the project would preserve the most important portion of the site for giant garter snake and for connectivity between the southern and central Natomas Basin. It would preserve 30.6 acres immediately adjacent to Lone Tree Canal that would establish a 250-foot wide conserved corridor. This reserve would include barriers to reduce effects of adjacent development, measures to assure water flow, restoration and enhancement of habitat, and funding for TNBC to actively manage the site. Thus, the project would contribute to the conservation of a narrow, but ecologically important, corridor along this canal adjacent to the Metro Air Park.

#### 3.9.3 EFFECTS OF PROPOSED RESERVES ON NBHCP RESERVE ESTABLISHMENT

The Greenbriar project's reserves also could contribute to the size and connectivity of future reserves. By preserving additional land adjacent to TNBC reserves, the project creates additional opportunities to create reserves of a given size and to create larger reserves (which would tend to have greater habitat values per acre than smaller reserves). For example, the Spangler reserve potentially could be joined to the Tufts reserve through future land acquisitions, as it would be only about a quarter-mile from the Tufts reserve (Exhibit 6); in this case, preservation of the intervening parcel would result in a larger reserve than would have resulted without the Greenbriar project's preservation of the Spangler property.

Overall, the Greenbriar project would not substantially reduce opportunities for establishing additional reserves for the NBHCP because sufficient suitable land is available to provide reserves both for the NBHCP and for the Greenbriar project, the project would preserve the most ecologically important portion of the Greenbriar site, and the project's reserves would increase opportunities to establish larger reserves.



Source: Wildlands 2005

#### **Location of TNBC Reserves**

# 4 POTENTIAL EFFECTS OF THE GREENBRIAR PROJECT ON COVERED SPECIES

# 4.1 GIANT GARTER SNAKE

# 4.1.1 SPECIES ECOLOGY

#### HABITAT ASSOCIATIONS/REQUIREMENTS

# **Habitat Type**

Giant garter snakes (*Thamnophis gigas*) typically inhabit sloughs, marshes, and drainage canals characterized by slow flowing or standing water, permanent summer water, mud bottoms, earthen banks, and an abundance of preferred forage species.

During their active season (May through October), mature giant garter snakes typically spend the majority of their time in canals and sloughs (Wylie and Casazza 2000). During late spring and summer, rice fields also provide foraging habitat for this species (Brode and Hansen 1992). Use of rice, however, is concentrated around the perimeter of the fields (Wylie and Casazza 2000; E. Hansen, pers. comm.). (Rice may, however, be an important source of prey and may export prey with drain waters into connected canals.) Giant garter snakes avoid areas of dense riparian overstory, and use burrows, crevices, undercut banks and large rocks to hide from predators. Winter hibernaculae include small burrows and soil crevices above prevailing flood elevations; these are typically located near aquatic habitat and in grassland or ruderal vegetation. (In the Natomas Basin, most canal banks have small burrows and crevices, and thus the banks of canals that are dewatered in winter can provide hibernaculae.)

Managed marsh also provides habitat for giant garter snake. In contrast to rice, managed marsh provides habitat year-round, and habitat elements (such as dense cover, basking sites, and refugia) to meet all of the giant garter snakes daily and seasonal needs. Managed marshes in the Natomas Basin have been designed to provide these habitat elements throughout the marsh, as opposed to the limited availability of the same elements in rice, which contributes to the use of rice primarily around the perimeter of rice fields.

The USFWS (1997) has determined that essential habitat components consist of the following:

- Adequate water during the snake's active period (early spring through mid-fall) to provide a prey base and cover;
- ► Emergent, herbaceous wetland vegetation, such as cattail and bulrushes, for escape cover and foraging habitat;
- ▶ Upland habitat for basking, cover, and retreat sites; and
- ► Higher elevation uplands for cover and refuge from flood waters.

Land cover types designated as giant garter snake habitat in the NBHCP include canals, ponds and seasonally wet areas and rice. Managed marsh also provides habitat. Small fish are the primary prey of this species; they will also take amphibians when available.

# **Home Range Size and Movement**

Based on radio-telemetry studies by Wylie and Casazza (2000), the size of giant garter snake home ranges were between 32 and 215 acres (median = 86 acres) at Elverta and Fisherman's Lake sites. For comparison, home

ranges were between 5 and 213 acres (median = 39.5 acres) at Gilsizer Slough in Sutter County, and 22 and 2,070 acres (median = 128 acres) at the Colusa National Wildlife Refuge. Most giant garter snake activity within these home ranges is concentrated along canals, sloughs, and the edge of aquatic habitats (Wylie and Casazza 2000; Wylie et al. 2000; Wylie et al. 2003).

Giant garter snakes rely on canals and ditches as movement corridors. These corridors provide important habitat, are used during daily movements within a home range, and are necessary for giant garter snake dispersal and the resulting exchange of individuals and alleles between subpopulations. Unvegetated canals may be used as dispersal corridors, but snakes typically do not remain in exposed canals because of increased vulnerability to predators. Giant garter snakes have been reported traveling over one mile, and may move as much as two miles in a day (Hansen and Brode 1992).

The USFWS has previously considered 200 feet as the width of upland vegetation providing habitat along the borders of aquatic habitat for giant garter snake (USFWS 1997). However, the width of uplands used by giant garter snakes varies considerably. Many summer basking and refuge areas used by this snake are immediately adjacent to canals and other aquatic habitats, and may even be located in the upper canal banks (Eric Hansen, pers. comm.). Giant garter snakes have also been observed hibernating as far as 820 feet (250 m) from water, however, and any land within this distance may be important for snake survival in some cases (Hansen 1988). (Hibernaculae this distant from water, however, are most often found in areas with high winter floods.) Giant garter snakes also seek refuge in upland burrows during hot summer weather (Hansen and Brode 1993), and have been documented up to 164 feet from aquatic habitat during this time (Wylie et al. 1997).

# **Mechanisms of Habitat Degradation**

#### Increased Predation

Known predators of giant garter snake include raccoons, skunks, opossums, foxes, hawks, egrets, herons, and bitterns (USFWS 1999a). All of the mammalian predators in this list increase in proximity to residential areas as a result of supplemental food sources and reduced coyote abundance (Crooks and Soule 1999). Domestic dogs may also prey on giant garter snakes, and cats may prey on juveniles. Although predation of giant garter snake by cats and dogs has not been studied scientifically, the effects of cats and dogs on small animals has been documented in a variety of ecosystems, and based on current understanding, cat and dog predation on giant garter snake is highly likely.

## Disturbance from Human Activity

Giant garter snakes are highly sensitive to human disturbance, and will abandon otherwise suitable habitat as a result of increased human activity such as fishing (Eric Hansen, pers. comm.). Human visits to areas occupied by snakes may result in lowered snake abundance even when the visits are brief in duration and no more than one person, once per day (Eric Hansen, pers. comm.). Human activities can also degrade giant garter snake habitats by trampling vegetation, compacting soils, destabilizing banks, and crushing burrows, and can cause vehicle collisions with snakes.

# Habitat Fragmentation

In a dynamic habitat such as the Natomas Basin, giant garter snakes frequently move in response to changing conditions in their rice, marsh, canal, and ditch habitats, especially during the dry summer months (Wylie and Casazza 2000). Connectivity between these areas is thus extremely important for snake survival and reproduction, as well as the genetic interchange and patch-recolonization ability necessary for the viability of the overall Basin population. Any loss or degradation of snake movement corridors may thus cause effects that far outreach the area of the directly impacted corridors.

# Operation and Maintenance of Waterways

Water channels lose their habitat value for giant garter snakes when cleaned of aquatic vegetation, during low/no flow periods or when high water releases eliminate or alter basking sites, refugia, foraging areas or juvenile microhabitat (USFWS 1999a). In the Natomas Basin, canal and drain maintenance, and irrigation practices, involve periodic clearing of vegetation along waterways, and short-term, seasonal and inter-annual changes in flow in waterways. A recent habitat assessment of canals and drains throughout the Natomas Basin indicates that operation and management practices are reducing habitat quality along a substantial portion of these waterways (Jones & Stokes 2005). Water diversions may also reduce the abundance of the snakes' aquatic prey. Water diversions or changes in land use within the area served by a canal or drain watershed may alter flows or even cause a canal or drain to be abandoned.

# Water Quality

Aquatic communities may be greatly affected by surrounding land use. Urban areas can exert different and in some cases stronger effects than agricultural lands (Bury 1972, Moore and Palmer 2005). Residential developments typically result in increased runoff of hydrocarbons and of chemicals used for lawns and gardens, and increased stormwater volume (and associated increases in flow depths and velocities) because of high coverage of impervious surfaces.

#### DISTRIBUTION

#### Information on CNDDB Occurrences

The 2002 CNDDB records cited in the NBHCP listed 168 giant garter snake occurrences in California, 38 of which occurred in the Natomas Basin. As of 2005, there are 171 known occurrences in California, of which 170 are considered extant. At this time, CNDDB lists 42 occurrences in the Natomas Basin, of which 42 are considered extant.

# Other Information on Distribution and Abundance in Natomas Basin

A USGS-BRD study conducted from 1998 to 1999 recorded 277 individual giant garter snakes in the Natomas Basin (Wylie and Casazza 2000). Surveys conducted in 2004 for the Natomas Basin Conservancy recorded 152 snake observations, at least 86 of which were verified individuals (Natomas Basin Conservancy 2004). At the western edge of the Greenbriar site, sampling conducted during 1998 and 1999 detected at least five giant garter snakes in Lone Tree Canal; based on these results, giant garter snake population density for the canal was estimated at 2.4 snakes per 1,000 feet of canal length (95% confidence interval = 2–3.7) (Wylie et al. 2000). The density of snakes recorded at the Greenbriar site and elsewhere along canals and in rice lands of the Natomas Basin has a couple of important implications for this analysis. First, any alteration of even an acre of these land cover types is likely to affect at least one giant garter snake. Second, canals can provide moderate or high quality habitat, and thus arguments based on the premise that canals in general provide marginal habitat may be inaccurate.

Monitoring data collected in 2004 for The Natomas Basin Conservancy (Jones & Stokes 2005) recorded smaller snake sizes on average (corresponding to younger snakes with lower reproductive outputs) than in previous years. When combined with data from previous years, this suggests a declining trend in snake size, which would correspond to an on-going decline in population viability unless coupled with a rapidly increasing population size (which is not indicated by the monitoring data). However, changes in sampling techniques and sampling locations make the interpretation of these data problematic.

# 4.1.2 PROJECT EFFECTS ON SPECIES

#### LONG-TERM EFFECTS ON HABITAT

# **Effect on Quantity of Habitat**

Changes in habitat acreages are summarized in Table 4-1. At the Greenbriar site, there would be a loss of an estimated 172 acres of GGS habitat from conditions at the time of the NBHCP (2001). At the proposed reserves, approximately 45 acres of snake habitat would be converted to non-habitat and 14 acres of snake habitat would be created from non-habitat. Thus, the project as a whole would yield a net loss of 204 acres of snake habitat.

| Table 4-1<br>Change in Acreage of Giant Garter Snake Habitat at Project Sites and in the Natomas Basin |           |            |                    |          |        |                         |  |  |  |
|--|-----------|------------|--------------------|----------|--------|-------------------------|--|--|--|
| Land Cover Type  | Future    | Chang      | je at Each Project | Site     | Total  | <b>Future Condition</b> |  |  |  |
| Providing Habitat  | Condition | Greenbriar | Natomas 130        | Spangler | Change | with Project            |  |  |  |
| Canals   | 1,162     | -15.0      | 0.0                | -1.4     | -16.4  | 1,146                   |  |  |  |
| Ponds & seasonally wet areas   | 2,259     | 2.7        | 14.2               | 184      | 200.9  | 2,460                   |  |  |  |
| Rice   | 11,643    | -160.0     | -                  | -228     | -388   | 11,255                  |  |  |  |
| Total  | 15,064    | -172.4     | 14.2               | -45.4    | -203.5 | 14,860                  |  |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

# **Effects on Quality of Habitat**

# Areas Adjacent to Developed Land or Highways

As discussed above in *Mechanisms of Habitat Degradation*, without mitigation, snakes traveling through the Lone Tree Canal or using other canal and rice habitats near the proposed development would likely be adversely affected by the project's residential development through increased predation, disturbance, and degradation of aquatic habitat. (The adjacent Metro Air Park development does not include residential development.) Development of the Greenbriar site also would reduce the acreage of land draining into Lone Tree Canal, and thus would likely lead to reduced flows in the canal. In the absence of measures to offset these alterations, the quality of giant garter snake habitat along Lone Tree Canal would likely be reduced.

The project does, however, include measures to reduce these effects, and the DEIR mitigation includes additional measures. These measures are described in the following section (*Effects on Connectivity*).

The project also could create conflicts with continued cultivation of rice on the property north of the Greenbriar site. Aerial application of pesticide and herbicide probably is not feasible immediately adjacent to residential development (C. Aubry, pers. comm.), which could affect the viability of rice cultivation on the adjacent parcel. This issue is discussed further under *Habitat Quality in the Natomas Basin* in Chapter 3 of this report.

## Alteration of Habitat Quality at Proposed Reserve Sites

At the proposed Spangler and Natomas 130 reserves, in addition to the 14 acres of marsh habitat creation (from non-habitat), 190 acres of giant garter snake habitat would be enhanced by creating marsh from rice (i.e., 184 acres of marsh and 6 acres of associated canals). This change in land cover and management should considerably increase habitat quality for giant garter snake, because marsh provides higher quality habitat for giant garter snake than rice. The reasons that marsh provides higher quality habitat than rice include:

- ► Giant garter snakes use the full extent of managed marshes, whereas they primarily use the margins of rice fields:
- Marshes provide habitat throughout the active period of the snake, whereas rice fields do not provide habitat during early and mid-spring, and are typically drained before the end of the snake's active period; and
- ▶ Marsh provides habitat in all years, whereas rice is fallowed periodically.

Though some uncertainty exists regarding the magnitude of benefits resulting from these enhancements, it is likely that they offset the habitat values that would be lost by development at the Greenbriar site. The preservation and management of this 204 acres of habitat for giant garter snake also provides benefits (such as reduced human disturbance) in addition to the benefits resulting from the conversion of rice to managed marsh.

# Effects on Connectivity

The Greenbriar project's potential effects on connectivity of giant garter snake habitat are described in detail in Section 3.5 Connectivity of Habitat in the Natomas Basin.

#### Effects of Construction-Related Activities

During the construction at the Greenbriar and proposed reserve sites, giant garter snakes could be killed or injured by vehicle strikes (Leidy 1992), crushed beneath heavy machinery, entombed in or excavated from their winter retreats (Wylie and Casazza 2000). The Greenbriar DEIR and Natomas Basin HCP include measures to avoid and minimize direct loss of giant garter snakes through construction. For the Greenbriar project, these measures include:

- a. To ensure that the project does not diminish habitat connectivity for giant garter snake between the southwest and northwest zones identified in the NBHCP, approximately 30.6 acres along Lone Tree Canal shall be protected and managed as giant garter snake habitat. This on-site habitat preservation shall protect an approximately 250-foot wide corridor of giant garter snake habitat that includes the canal and approximately 200 feet of adjacent uplands. Uplands within the linear open space/buffer area shall be managed as perennial grassland as described below. Additional aquatic habitat for giant garter snake shall be created along the east bank of Lone Tree Canal by construction and maintenance of a 2.7 acre tule bench. The habitat shall be managed in perpetuity as high-quality habitat for giant garter snake. Compliance and biological effectiveness monitoring shall be performed and annual monitoring reports prepared within six months of completion of monitoring for any given year. This monitoring, reporting, and adaptive management shall be performed as described in Section IV of the NBHCP.
- b. To ensure that the project does not diminish giant garter snake movement along Lone Tree Canal, all new road crossings of Lone Tree Canal shall be designed to minimize obstacles to giant garter snake movement. The use of culverts under new road crossings on Lone Tree Canal shall be prohibited unless it can be demonstrated that the culverts will not diminish the potential for giant garter snake movement through the section of Lone Tree Canal protected by the setback fence and conservation easement.
- c. Upland giant garter snake habitat within the Lone Tree Canal linear open space/buffer area shall be created and managed to provide cover, basking areas, and refugia during the winter dormant period. Hibernaculae would be constructed at regular intervals by embedding concrete or coarse rock in the bank or in a berm along the Lone Tree Canal corridor to provide additional winter refugia. Upland habitat with the linear open space/buffer areas shall be converted to native perennial grassland and managed, in perpetuity, as perennial grassland habitat.
- d. Aquatic habitat shall be maintained throughout the giant garter snake active season in Lone Tree Canal, in perpetuity. This is the legal responsibility and obligation of Metro Air Park property owners (MAP). The

MAP HCP includes provisions for maintaining water in the canal such that the basic habitat requirements of the giant garter snake are met. The MAP HCP also provides a road map, through "Changed Circumstances", to address procedures to follow if water is not being maintained in the canal to meet these requirements. As described in the MAP HCP, the MAP is legally obligated to assure these requirements are met, and financial and procedural mechanisms are included in the MAP HCP to enforce this. It is, therefore, assumed that MAP will provide water to Lone Tree Canal, as required by the MAP HCP and ITP, in perpetuity. It is also assumed that USFWS will use all reasonable means available to it, to enforce this MAP HCP requirement. If water is not provided to Lone Tree Canal by the MAP to meet the habitat requirements of giant garter snake, as required by the MAP HCP, and USFWS exhausts its enforcement responsibilities, the project applicant shall assume the responsibility of providing suitable giant garter snake aquatic habitat throughout the section of Lone Tree Canal protected by the fence and conservation easement. However, as stated herein, the project applicant shall only assume this responsibility if it has been sufficiently demonstrated to the City that USFWS has exhausted all reasonable means to compel MAP to comply with the relevant conditions of the MAP ITP. Specific requirements related to ensuring suitable aquatic habitat in Lone Tree Canal is present, in perpetuity, throughout the giant garter snake active season shall be developed through consultation with DFG and USFWS, and included in the new or amended HCP for Greenbriar, and may include mechanisms, such as installation of a well, to assure water is provided in the canal to meet habitat requirements.

- e. A barrier shall be installed between the giant garter snake habitat linear open space/buffer area and the adjacent Greenbriar development to ensure that giant garter snakes do not enter the development area, and to prohibit humans and pets from entering the giant garter snake habitat. The design of this barrier shall be subject to USFWS and CDFG review and approval. The entire length of the barrier, which shall be bordered by yards rather than roadways, shall be maintained on the preserve side by a nonprofit land trust to ensure that vegetation or debris does not accumulate near the barrier and provide opportunities for wildlife and pets to climb over the barrier. On the development side, Covenants, Codes and Restrictions (CCRs) shall prohibit accumulation of vegetation or debris adjacent to the barrier. Chain link fencing shall be placed at both ends of the corridor, with locked gates permitting entry only by RD 1000 and NMWD for channel maintenance, and by the preserve manager for habitat monitoring and maintenance purposes.
- f. Specific requirements associated with the barrier shall be developed through consultation with USFWS and DFG, and may include the following and/or other specifications that DFG and USFWS consider to be equally or more effective:
  - Adequate height and below-ground depth to prevent snakes or burrowing mammals from providing a through-route for snakes by establishing burrows from one side to the other crossing;
  - ► Constructed using extruded concrete or block construction extending a minimum of 36-inches above ground level;
  - ► Maintenance to repair the barrier and to prevent the establishment of vegetation or collection of debris that could provide snakes with a climbing surface allowing them to breech the barrier;
  - A cap or lip extending at least two-inches beyond the barrier's vertical edge to prevent snakes from gaining access along the barrier's top edge; and
  - ► Signage to discourage humans and their pets from entering the area.
- g. The Lone Tree Canal linear open space/buffer area shall be protected in perpetuity under a conservation easement and managed to sustain the value of this area for giant garter snake habitat connectivity. Compliance and biological effectiveness monitoring shall be performed and annual monitoring reports prepared. This monitoring, reporting, and adaptive management shall be performed as described in Section IV of the NBHCP or following procedures developed in formal consultation with USFWS and DFG and contained in an ESA Incidental Take Permit for the Greenbriar project.

In combination, these measures would minimize injury and mortality to giant garter snakes as a direct result of construction-related activities.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

As discussed above in *Mechanisms of Habitat Degradation*, without mitigation, giant garter snakes would likely experience increased predation near the proposed residential development because of the increased abundance of domestic dogs and cats, as well as human-associated raccoons, skunks and opossums. Domestic cats have been recorded between 98–590 feet from homes, unattended domestic dogs between 590–1,083 feet from homes (Odell and Knight 2001), and increased abundance of native predators may extend farther. As this distance is well beyond the proposed 250-foot wide corridor between the proposed residential development and the Lone Tree Canal, the project would likely result in increased predation of snakes using the canal. The increased human population in the area would also increase the potential for human activity near the canal, which may lead to site avoidance or abandonment by snakes (Eric Hansen, pers. comm.). Increased human activity along the canal could result in increased canal maintenance including further clearing of vegetation. Snake mortality because of vehicle strikes (Leidy 1992) may also increase on existing roads because of the increased traffic associated with the project.

The project does, however, include measures to reduce these effects, and the DEIR mitigation includes additional measures. These measures are described in the preceding section (*Effects on Connectivity*).

## **OVERALL EFFECT ON POPULATION VIABILITY**

The project would cause both adverse and beneficial effects on the giant garter snake population of the Natomas Basin. Beneficial effects would include preserving, creating, and enhancing habitat at the reserve sites, preserving a corridor along Lone Tree Canal, and contributing to the connectivity of habitat and existing TNBC reserves adjacent to or near the proposed reserves. Adverse effects would include a reduction in the total acreage of habitat, and possibly degradation of habitat near the Greenbriar site and reduced connectivity along Lone Tree Canal due to increased human disturbance and predation. The DEIR mitigation, however, would reduce adverse effects and ensure that connectivity of giant garter snake habitat was conserved along Lone Tree Canal.

Overall, the project would not adversely affect giant garter snake, and its overall effect on population viability could be beneficial. The loss of habitat acreage would probably be offset by the increased habitat quality resulting from the preservation of habitat, and conversion of rice to marsh.

The proposed creation of 14 acres of marsh from non-rice crops, conversion of 184 acres of rice to marsh, and preservation of an additional 6.2 acres along associated canals would likely offset the loss of 388 acres of rice and 16 acres of canal habitat. The basis of this interpretation is the greater habitat value of managed marsh relative to rice and the general benefits of habitat preservation.

Managed marsh provides substantially greater habitat values for giant garter snakes than rice for several reasons. These reasons include:

- ► Giant garter snakes primarily use the margins of rice fields, whereas they use the full extent of managed marshes. These marshes are designed to provide open water, foraging habitat, dense cover, basking sites, and refugia in close proximity throughout the marsh. (For example, an acre of managed marsh provides several times the edge habitat than does a rice field.)
- ▶ Marshes provide habitat throughout the active period of the snake. Rice fields do not provide habitat during early and mid-spring, and are typically drained before the end of the snake's active period. Thus, for a portion of their active period, giant garter snakes must rely entirely on non-rice habitats. In the Natomas Basin, these habitats are canals and managed marsh. In contrast, managed marshes provide habitat year-round.

▶ Rice is fallowed periodically, and thus does not provide habitat in all years; in contrast, a managed marsh does provide habitat in all years.

Preservation of habitat has benefits in addition to those of habitat enhancement. In the Natomas Basin, a particularly important benefit of habitat preservation is that it ensures that the habitat will continue to exist, and it buffers total habitat availability from year to year fluctuations. For giant garter snake, privately owned habitat in the Natomas Basin is primarily rice and associated canals, and there are no assurances that rice cultivation will continue on any particular site. Furthermore, agricultural markets will cause the total acreage of rice, and consequently of giant garter snake habitat, to fluctuate substantially from year to year. Such environmental fluctuations strongly influence populations and reduce their viability. In contrast, preserved lands will provide habitat on a much more consistent basis, and thus reduce the magnitude of fluctuations in habitat availability.

Both habitat enhancement and preservation also can contribute to population viability by reducing anthropogenic causes of mortality. Preservation reduces human disturbance, and minimizes activities that could harm or kill snakes. Habitat enhancement also reduces or eliminates agricultural activities that can harm or kill snakes. In addition, the preservation and enhancement of habitat typically results in larger blocks of higher quality habitat, and this should reduce long distance movements by snakes, which would also reduce the risk of mortality associated with those movements. (Dispersal and other long distance movements are dangerous for snakes, particularly where road crossings are involved [Bonnet et al. 1999, Rosen and Lowe 1994].)

For these reasons, an acre of managed marsh may provide habitat values comparable to or substantially greater than two acres of rice. The project would reduce rice acreage by 388 acres (and canal acreage by 16 acres) and would increase the acreage of preserved, managed marsh by 201 acres. Thus, it is likely that the project would not reduce habitat values for giant garter snake, and thus would not reduce the viability of the giant garter snake population due to a reduction in habitat values.

The project is also unlikely to reduce the viability of the giant garter snake population due to adverse effects on connectivity. The project (with the DEIR mitigation) would conserve connectivity and habitat for giant garter snake along Lone Tree Canal, which is an important waterway connecting the southern and central Natomas Basin, and proposed reserves would contribute to connectivity of habitats and reserves in the southern and central Basin.

# 4.2 NORTHWESTERN POND TURTLE

# 4.2.1 SPECIES ECOLOGY

## HABITAT ASSOCIATIONS/REQUIREMENTS

## **Habitat Type**

Northwestern pond turtles (*Clemmys marmorata marmorata*) are most commonly found in permanent or nearly permanent wetlands, ponds, slow-moving streams and irrigation ditches (Zeiner et al. 1988). Adjacent upland areas are also used for basking and egg-laying. Land cover types designated as pond turtle habitat in the NBHCP include canals, ponds and seasonally wet areas, rice and riparian. Special habitat features that improve turtle abundance, survival and reproductive success are rocks, logs, open mud banks, emergent aquatic vegetation and streamside vegetation. These features provide the turtles with basking sites and cover from predators (Stebbins 1972). Although pond turtles feed primarily on aquatic invertebrates (USFWS 1992), they also feed on plants, small fish and carrion.

# **Home Range Size and Movement**

Upland areas adjacent to aquatic habitat are essential for reproduction, and eggs may be laid as far as 1,319 feet (0.25 mi) from water (Hays et al. 1999). Hatchling and adult turtles may winter in upland sites, and turtles may move more than one mile overland in response to desiccation of local water bodies or other forms of habitat loss or degradation.

# **Mechanisms of Habitat Degradation**

## Increased Predation

Hayes et al. (1999) documented predation on pond turtles by domestic dogs; unattended dogs have been recorded between 590–1,083 feet (180–330 m) from homes (Odell and Knight 2001). These distances indicate the project would likely result in increased predation of any pond turtles using Lone Tree Canal for movement between habitat areas to the north and south of the property. Populations of native pond turtle predators such as raccoons and opossums also typically increase in proximity to residential areas as a result of supplemental food sources and reduced coyote abundance (Crooks and Soule 1999).

## Disturbance from Human Activity

Pond turtle observations have been known to decline in areas with increased human activity (Eric Hansen, pers. comm.). Human visits to areas occupied by turtles may result in lowered turtle abundance even when the visits are brief in duration and no more than one person, once per day (Eric Hansen, pers. comm.).

# Habitat Fragmentation

Although pond turtles may travel less frequently than giant garter snakes, turtles occupying dynamic habitats such as the Natomas Basin may need to travel in response to changing conditions in their aquatic habitats, especially during the dry summer months. Connectivity between these areas may thus be important for turtle survival and reproduction, as well as the genetic interchange and patch-recolonization ability that may be necessary for the viability of the overall Basin population. Any loss or degradation of turtle movement corridors may thus yield effects that outreach the area of the directly impacted corridors.

# Operation and Maintenance of Waterways

Water channels lose their habitat value for pond turtles when cleaned of aquatic vegetation, during low/no flow periods and when high water releases eliminate or alter basking sites, refugia, foraging areas or hatchling microhabitat (Holland 1991a; USFWS 1999). Water diversions or changes in land use within the area served by a canal or drain watershed may alter flows or even cause a canal or drain to be abandoned.

#### Water Quality

Aquatic communities may be greatly affected by surrounding land use. Urban areas can exert different and in some cases stronger effects than agricultural lands (Bury 1972; Moore and Palmer 2005). Residential developments typically result in increased traffic and fuel runoff, runoff of chemicals used for lawns and gardens, and increased stormwater volume and currents because of high coverage of impervious surfaces. Increased exposure to contaminants has been implicated in pond turtle population declines (Bury 1972; Holland 1991).

#### DISTRIBUTION

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 117 known occurrences in California, of which 116 were considered extant. At that time, CNDDB did not list northwestern pond turtle occurrences in the Natomas Basin. As of 2005, there are 232 known occurrences in California, of which 231 are considered extant. At this time, CNDDB does not list northwestern pond turtle occurrences within one mile of the Natomas Basin.

## Other Information on Distribution and Abundance in Natomas Basin

Surveys conducted in 2004 for the Natomas Basin Conservancy documented six northwestern pond turtle occurrences in the Natomas Basin. Two of these occurrences were just over one mile from the Greenbriar site, one was less than a mile from the proposed Natomas 130 reserve, and another was just over a mile from the proposed Spangler reserve. Many Natomas Basin canals are considered suitable habitat for this species, and high quality habitat exists near the Greenbriar and Natomas 130 sites, at Fisherman's Lake.

# 4.2.2 Project Effects on Species

## **LONG-TERM EFFECTS ON HABITAT**

### **Effect on Quantity of Habitat**

Effects on the acreage of pond turtle habitat are summarized in Table 4-2. The proposed development at the Greenbriar site would result in the loss of an estimated 172 acres of pond turtle habitat from conditions at the time of the NBHCP (2001), and an additional 45 acres of rice habitat would be converted to upland at the Spangler site. Although the canal and marsh on the Greenbriar site were determined by the DEIR biologist to be of marginal quality and unlikely to support pond turtles, we have included these acres in our analysis for consistency with the broad habitat categories in the GIS analysis and NBHCP, and also because turtles may occasionally use the site as a movement corridor between higher quality habitats to the north and south of the site. At the proposed reserves, approximately 14 acres of pond turtle habitat would be created from non-habitat. Thus, the project as a whole would yield a net loss of 204 acres of turtle habitat.

| Table 4-2<br>Change in Acreage of Northwestern Pond Turtle Habitat at Project Sites and in the Natomas Basin |           |            |                             |          |                  |              |  |  |
|--|-----------|------------|-----------------------------|----------|------------------|--------------|--|--|
| Land Cover Type<br>Providing Habitat   | Future    | Chanç      | Change at Each Project Site | Total    | Future Condition |              |  |  |
|  | Condition | Greenbriar | Natomas 130                 | Spangler | Change           | with Project |  |  |
| Canals   | 1,162     | -15.0      | 0.0                         | -1.4     | -16.4            | 1,146        |  |  |
| Ponds & seasonally wet areas   | 2,259     | 2.7        | 14.2                        | 184      | 200.9            | 2,460        |  |  |
| Rice   | 11,643    | -160.0     | -                           | -228     | -388.0           | 11,255       |  |  |
| Riparian   | 91        | 0.0        | 0.0                         | -        | 0                | 91           |  |  |
| Total  | 15,155    | -172.4     | 14.2                        | -45.4    | -203.5           | 14,951       |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

## **Effects on Quality of Habitat**

# Areas Adjacent to Developed Land or Highways

As discussed above in *Mechanisms of Habitat Degradation*, turtles traveling through the Lone Tree Canal or inhabiting other canals and wetlands downstream from the proposed development would likely be adversely affected by residential development through increased predation, disturbance, and degradation of aquatic habitat. (The adjacent Metro Air Park development does not include residential development.) Development of the Greenbriar site also would reduce the acreage of land draining into Lone Tree Canal, and thus could lead to reduced flows in the canal. In the absence of measures to offset this alteration, the quality of pond turtle habitat along Lone Tree Canal could be reduced by this loss of water. However, both the MAP HCP (see pages 70-71 in Thomas Reid Associates 2001) and the DEIR (mitigation measure 6.13-1) contain measures to assure the maintenance of aquatic habitat in Lone Tree Canal.

As described under *Connectivity of Habitats in the Natomas Basin* (in Section 3 of this report), the project and mitigation proposed in the DEIR for the Greenbriar project include measures that would substantially reduce the effects of development at the Greenbriar site on adjacent pond turtle habitat.

# Alteration of Habitat Quality at Proposed Reserve Sites

In addition to 14 acres of managed marsh that would be created from upland at the Natomas 130 reserve and the 2.7 acres of marsh that would be created along Lone Tree Canal, rice would be converted to marsh at the Spangler reserve enhancing 190 acres of habitat (184 acres of marsh and 6 acres of associated canals). This created and enhanced habitat would be preserved and managed for its habitat values.

These changes should considerably increase habitat quality for pond turtle, primarily because marsh provides much higher quality habitat for pond turtle than rice, management would include reduce adult mortality caused by human disturbance, and nesting and overwintering habitat would be created. Though a moderate level of uncertainty exists regarding the magnitude of benefits resulting from these enhancements, it is likely that they offset the habitat values that would be lost by development at the Greenbriar site.

## Effects on Connectivity

The importance of habitat connectivity for this species is discussed in *Mechanisms of Habitat Degradation*, above. In the absence of effective mitigation, the project would reduce connectivity of pond turtle habitat by altering adjacent uplands, reducing water flows in the canal, and increasing predation and human disturbance. However, as described under *Connectivity of Habitats in the Natomas Basin* (in Section 3 of this report), the project and mitigation proposed in the DEIR for the Greenbriar project include measures that would substantially reduce these effects. These measures include creation, enhancement and preservation of habitat (including tule bench along Lone Tree Canal) in the 30.6 acre reserve along Lone Tree Canal, a barrier/fencing to reduce predation and human disturbance effects, an additional assurance that aquatic habitat would be maintained in Lone Tree Canal, and funding to maintain and operate this conserved area. These measures would substantially reduce project's effects on connectivity.

# **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Construction-related activities associated with the project could affect this species, though the Greenbriar site currently provides only marginally suitable habitat. Also, construction-related degradation of water quality in Lone Tree Canal could affect turtles downstream. In addition, pond turtles could be harmed during restoration activities at the proposed Natomas 130 reserve, by crushing under equipment or entombment in their winter burrows. Measures to avoid and minimize take of northwestern pond turtles and giant garter snakes, described in the Greenbriar project DEIR and Natomas Basin HCP, would reduce any direct construction-related effects on

this species. These measures where listed in Section 4.1 *Giant Garter Snake* under *Effects of Construction-related Activities*.

## **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

As discussed above in *Mechanisms of Habitat Degradation*, in the absence of avoidance and minimization northwestern pond turtles would likely experience increased predation near the proposed residential development because of the increased abundance of domestic dogs and cats, as well as human-associated raccoons, skunks and opossums. The increased human population in the area would also increase the potential for human activity near the canal, which may lead to site avoidance by turtles (Eric Hansen, pers. comm.). Mortality because of vehicle strikes may also increase on existing roads because of the increased traffic that the project would produce.

However, as described under *Connectivity of Habitats in the Natomas Basin* (in Section 3 of this report), the project and the DEIR mitigation include measures that would substantially reduce these effects.

## **OVERALL EFFECT ON POPULATION VIABILITY**

The project would cause both adverse and beneficial effects on the northwestern pond turtle population in the Natomas Basin. Beneficial effects would include preserving, creating, and enhancing habitat at the reserve sites, preserving a corridor along Lone Tree Canal, and contributing to the connectivity of habitat and existing TNBC reserves adjacent to or near the proposed reserves. Adverse effects would include a reduction in the total acreage of habitat, and possibly degradation of habitat near the Greenbriar site and reduced connectivity along Lone Tree Canal due to increased human disturbance and predation. The DEIR mitigation would reduce these adverse effects and ensure that connectivity of pond turtle habitat was maintained along Lone Tree Canal.

Overall, the project would not adversely affect pond turtle. The loss of habitat acreage would be more than offset by the increased habitat quality resulting from the preservation of habitat, conversion of rice to marsh, and management of rice to enhance habitats. The project would have a beneficial effect on pond turtle habitat largely because the created marsh would provide much higher quality habitat for pond turtle than rice (USFWS 2003). Also, the project (with the DEIR mitigation) would conserve connectivity and habitat for pond turtle along Lone Tree Canal and near proposed reserves in the southern and central Basin. These beneficial effects on habitat and connectivity may be sufficient to increase the viability of the Natomas Basin's northwestern pond turtle population.

# 4.3 SWAINSON'S HAWK

## 4.3.1 Species Ecology

## HABITAT ASSOCIATIONS/REQUIREMENTS

## **Habitat Type**

Swainson's hawks (*Buteo swainsoni*) are most commonly found in grasslands, low shrublands, and agricultural habitats that include large trees for nesting. Land cover types designated as Swainson's hawk nesting habitat in the NBHCP include oak groves, tree groves, and riparian. These habitats are suitable for nesting only where adjacent to adequate foraging habitat. Land cover types designated as Swainson's hawk foraging habitat in the NBHCP include alfalfa, grassland, idle, non-rice crops, pasture, and ruderal. Swainson's hawks will also nest in these foraging habitats if large trees are available; however, isolated trees may be less suitable for nesting than trees in groves or riparian areas.

Prey abundance and accessibility (for capture) are the most important features determining the suitability of hawk foraging habitat. In addition, agricultural operations (e.g., mowing, flood irrigation) have a substantial influence

on the accessibility of prey and thus create important foraging opportunities for Swainson's hawk (Estep 1989). Crops which are tall and dense enough to preclude the capture of prey (e.g., corn) do not provide suitable habitat except around field margins, but prey in these habitats are accessible during and immediately following harvest. Other crops (e.g., tomato, sugar beet) are tall and dense enough to inhibit but not to prevent the capture of prey during the growing season, and also provide valuable foraging opportunities during their harvest. Alfalfa, idle crop land, and most ruderal land and grassland have low and or open vegetation that doesn't impede prey capture, but prey abundance varies among these habitats and so does the frequency of agricultural operations (which are absent from ruderal land and grassland). Based on these considerations, we have divided crops and other foraging habitats into four categories of quality (i.e., low, moderate, high-moderate, and high) (Table 2-3). The basis for this classification is described in detail in the methods section (Section 2) under *Habitat Quality*.

## **Home Range Size and Movement**

Although the most important foraging habitat for Swainson's hawks lies within a one-mile radius of each nest (City of Sacramento et al. 2003), Swainson's hawks have been recorded foraging up to 18.6 miles from nest sites (Estep 1989). Any habitat within this foraging distance may provide food at some time in the breeding season that is necessary for reproductive success. In a dynamic agricultural environment such as the Natomas Basin, the area required for hawk foraging depends on the time of season, crop cycle, crop type, and discing/harvest schedule, as these factors affect the abundance and availability of prey (City of Sacramento et al. 2003). Swainson's hawk foraging ranges during the breeding season have been estimated at approximately 1,000-7,000 acres (Bechard 1982, Estep 1989, Johnsgard 1990).

# **Mechanisms of Habitat Degradation**

# Reduction of Prey Base

The order of habitat suitability for Swainson's hawks listed above was determined by the abundance and availability of prey. Conversion of higher-suitability habitats to lower-suitability habitats would be accompanied by a reduction in prey base that may reduce nest survival or the fat reserves required by hawks for their fall migration to Central Mexico (Swainson's Hawk Technical Advisory Committee 2001), without any change in overall habitat acreage.

Changes in the hawks' rodent prey base may also result from impacts of residential development to adjacent mammalian predator communities. Crooks and Soule (1999) quantified the impacts of domestic cats on rodents and other small animals. They estimated that the average domestic cat population in moderately sized fragments (~50 acres of upland habitat bordered by 100 residences) returns about 840 rodents, 525 birds, and 595 lizards to residences each year. Assuming that cats do not bring back all prey that they kill, actual impacts to hawk prey numbers are probably even greater. Crooks and Soule (1999) also documented increased extirpations of songbird species in habitat fragments with higher densities of cats, raccoons and opossums, all of which often increase in proximity to residential development. Although rodents are the primary prey of breeding Swainson's hawks in the Natomas Basin, songbirds also contribute to their diets.

Several studies indicate that the abundance of bird species is lower near residential development. Compared to undeveloped areas at least 2,297 feet from development, Odell and Knight (2001) demonstrated lower densities of the hawks' secondary songbird prey within 1,083 feet of sparse residential development (less than 0.4 dwelling units/acre); impacts of higher density development are expected to be greater. Similarly, Blair (1996) reported 1/3 fewer bird species in lands adjacent to residential development, when compared to habitat preserves in the same area. Increased predation on the hawks' rodent prey is likely to extend between 98–590 feet from homes because of domestic cats, 590–1,083 feet from homes because of domestic dogs, and farther because of increased populations of small wild predators such as opossums and foxes (Odell and Knight 2001).

## Habitat Fragmentation and Reduced Patch Size

The contiguity of foraging habitat and its placement near nest sites may also affect hawk foraging (and subsequently breeding) success. Longer foraging flights carry higher energetic costs than foraging closer to nests, and reduce the amount of time adults are present to defend nests from predators. Similarly, there may be a threshold of required habitat area near each nest, related to the foraging ranges discussed above, such that habitat loss beyond this threshold would result in a greater impact to nest survival than habitat loss from a larger area. The diversity and abundance of Swainson's hawk prey have also been reported to decline in fragmented habitat (Crooks et al. 2001; Helzer and Jelinski 1999; Hinsley et al. 1995).

#### Increased Predation

Corvids (crows, magpies) and great horned owls are the most common predators of Swainson's hawk eggs and nestlings (England et al. 1997). Corvid populations typically increase near human settlement because of the supplemental food source of human refuse and additional perches provided by urban trees, street lights, and other infrastructure (Steenhof et al. 1993; Marzluff et al. 2001). This increase in predator abundance may result in increased nest predation near residential development.

#### Nest Disturbance

Swainson's hawk responses to nest disturbance vary with each nesting pair and the timing, regularity, and nature of the disturbance. Although some researchers have described disturbed nest sites that successfully fledge young (Estep 1989; England et al. 1995), others have recorded nest abandonment in response to human activity, especially during nest building and incubation (Bent 1937; Stahlecker 1975). In addition to nest abandonment, significant disturbances near hawk nests may interfere with parental care and feeding of young in a way that reduces nest success.

## **DISTRIBUTION**

# **Information on CNDDB Occurrences**

When information was compiled for the NBHCP in 2001, there were 892 known occurrences in California, of which 882 were considered extant. The NBHCP did not list CNDDB occurrences for the Natomas Basin, but local surveys (described below) provided extensive data. As of 2005, there are 1,380 known Swainson's hawk occurrences in California, of which 1,350 are considered extant. At this time, 35 occurrences are known in the Natomas Basin, of which 34 are considered extant. Sixteen additional occurrences are known within one mile of the Basin, all of which are considered extant. Of these occurrences, two are within one mile of the Greenbriar site and eight are within one mile of the proposed reserve sites. All ten of these occurrences are considered extant.

#### Other Information on Distribution and Abundance in Natomas Basin

Estep (2001) indicates that nesting sites and foraging activity occur throughout the Basin, depending on the availability of suitable nest trees in proximity to upland foraging areas. The most recent survey of the Natomas Basin at the time the Habitat Conservation Plan was prepared located 62 breeding sites in or immediately adjacent to the Basin (Swainson's Hawk Technical Advisory Committee 2001). Hawks nesting at the 35 sites adjacent to the Basin were located along the Sacramento River and may have depended on the Basin's foraging habitat for their survival and reproduction. The NBHCP asserts that the Swainson's hawk population supported by the Natomas Basin is "important to the continued viability" of the species, which has been estimated by the California Department of Fish and Game to have declined by 94% from historical conditions in the state (Bloom 1980, California Department of Fish and Game 1989).

The most recent survey published by the Natomas Basin Conservancy mapped 89 nest sites in or adjacent to the Basin in 2004, of which 59 were active in that year. Each of these nests was within the 18.6 mile recorded

foraging distance from the project and proposed reserve sites and may be affected by changes in land cover at those sites. The Natomas Basin Conservancy has mapped five nests within one mile of the Greenbriar site, two of which were active in 2004, and 12 nests within one mile of the proposed Natomas 130 reserve, six of which were active in 2004. No Swainson's hawk nests have been mapped within one mile of the proposed Spangler reserve.

The most recent monitoring report prepared for The Natomas Basin Conservancy (Jones & Stokes 2005) also contains information on population trends in the Natomas Basin. In 2004, the number of successful nests increased by five, but the downward trend in number of young per successful nest has continued, resulting in reproduction relatively similar to previous years (1999–2003).

# 4.3.2 Project Effects on Species

## **LONG-TERM EFFECTS ON HABITAT**

# **Effect on Quantity of Habitat**

The project would not change the acreage of Swainson's hawk nesting habitat at the Greenbriar or proposed reserve sites from current (2005) conditions or conditions at the time of the NBHCP (2001), but would preserve two acres of nesting habitat.

The project's effects on foraging habitat are summarized in Table 4-3. The project would reduce the acreage of Swainson's hawk foraging habitat in the Natomas Basin from conditions at the time of the NBHCP (2001). The proposed development at the Greenbriar site would reduce foraging habitat by an estimated 313 acres from conditions in 2001. At the proposed Spangler and Natomas 130 reserves, foraging habitat would increase by 91 acres. Thus, the project as a whole would yield a net loss of 222 acres of Swainson's hawk foraging habitat.

| Table 4-3 Change in Acreage of Swainson's Hawk Foraging Habitat at Project Sites and in the Natomas Basin |           |            |                    |          |                |                  |  |  |
|---|-----------|------------|--------------------|----------|----------------|------------------|--|--|
| Land Cover Type<br>Providing Habitat  | Future    | Chanç      | ge at Each Project | Site     | - Total Change | Future Condition |  |  |
|   | Condition | Greenbriar | Natomas 130        | Spangler | Total Change   | with Project     |  |  |
| Alfalfa   | 368       | -          | 14.2               | 45.4     | 59.6           | 428              |  |  |
| Grassland   | 284       | 26.5       | -                  | -        | 26.5           | 311              |  |  |
| Idle  | 422       | -62.5      | -                  | -        | -62.5          | 360              |  |  |
| Non-rice crops  | 9,533     | -234.1     | -28.4              | -        | -262.5         | 9,271            |  |  |
| Pasture   | 494       | -33.8      | -                  | -        | -33.8          | 460              |  |  |
| Ruderal   | 370       | -9.2       | -                  | -        | -9.2           | 361              |  |  |
| Upland marsh components   | 547       | -          | 4.3                | 55.2     | 59.5           | 607              |  |  |
| Total   | 12,018    | -313.1     | -9.9               | 100.6    | -222.4         | 11,796           |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

#### **Effects on Quality of Habitat**

## Areas Adjacent to Developed Land or Highways

Although the expanded urban area that would be created by the Greenbriar project would result in a net reduction of areas within 800 feet or one mile of urban development or highways, the project would expand a gradient of urban influence into the previously unaffected area to the north of the property and could increase the urban

influence on the agricultural land to the southwest. The impacts to Swainson's hawk prey in this area that could occur as a result of proximity to development are discussed under *Mechanisms of Habitat Degradation*, above. However, the existing roads that border the site, would function as partial barriers that limit the extent of urban influences on adjacent agricultural lands.

The current land use immediately to the north of the Greenbriar site is rice and as such does not support Swainson's hawk habitat except when fallowed. However, the creation of hawk habitat at the Greenbriar site between 2001 and 2005 attests to the potential for the area to the north to become hawk habitat in the future. The recent creation of habitat at the Greenbriar site resulted from the conversion of the rice acreage to non-rice crops and fallow agriculture. The current land use to the southwest of the property is idle cropland, which supports Swainson's hawk habitat.

# Altered Habitat Quality at Proposed Reserve and Mitigation Sites

The project with the DEIR mitigation would enhance and preserve at least 190 acres of foraging habitat (26.5 acres of grassland along Lone Tree Canal, 59.7 acres of alfalfa [or other high quality foraging habitat] and 59.5 acres of upland marsh components at Spangler and Natomas 130, and at least an additional 49 acres of high quality foraging habitat required by the *DEIR* mitigation). Habitat at the unspecified DEIR mitigation site(s) and at the proposed Spangler and Natomas 130 reserves would be actively managed with the primary goal of providing high quality foraging habitat.

Conservation of the corridor along Lone Tree canal may improve its value as foraging habitat because it would be converted to perennial grassland that might have higher habitat value than the corridor's current or recent agricultural land cover. This corridor, however, would be a relatively narrow band of potential habitat surrounded by urban development, and this setting might limit its use by Swainson's hawk. Consequently, this proposed corridor was considered to provide only low quality foraging habitat.

Habitat quality for Swainson's hawks would increase in the remaining upland habitat at the proposed Natomas 130 reserve because it would be managed to provide high quality Swainson's hawk habitat.

The proposed Spangler property does not currently function as Swainson's hawk habitat except when fallowed. One hundred eighty four acres of this proposed reserve would be restored to marsh (with upland components providing foraging habitat) and the remainder (45 acres) would be converted to upland managed to provide high quality foraging habitat for Swainson's hawk. Although the Spangler property is within the 18.6 mile maximum foraging distance from all known nests in the Basin, its distance from the Greenbriar site would limit its benefit as foraging habitat for hawks affected by the project regardless of the reserve's management.

Mitigation measure 6.13-2 of the DEIR requires the enhancement and preservation of at least 49 acres to provide high quality foraging habitat that would prevent a net loss of foraging habitat values. This mitigation is in addition to the proposed reserves.

The effect of the Greenbriar project with the DEIR mitigation on the quality of Swainson's hawk foraging habitat was evaluated through three analyses:

- 1. acres of foraging habitat in low, moderate and high quality categories;
- 2. total acres of foraging habitat available per month; and
- 3. total foraging habitat available each month expressed as an equivalent acreage of high quality foraging habitat.

The first two analyses (acres by habitat quality category and monthly availability) were conducted as in the NBHCP, and the third was developed for this effects analysis. All three methods are described in detail in the methods section. The acres of habitat types at the Greenbriar, proposed reserve and DEIR mitigation sites with and without the project that were used in these analyses are shown in Table 2-2, and are also tabulated in tables 3-1 and 4-3.

Though the project would result in a net loss of habitat acreage, an increased percentage of the remaining habitat would be in the high quality category (Exhibit 3a). This increase in high quality habitat would result from the creation and enhancement of habitat at the Spangler, Natomas 130, and the DEIR mitigation sites. Upland habitat at the proposed Natomas 130 reserve would be enhanced, 45 acres of high quality foraging habitat would be created at the Spangler site and to provide DEIR mitigation at least 49 acres of land would be enhanced and managed to provide high quality foraging habitat for Swainson's hawk.

Based on the analysis approach in the NBHCP, the project also would result in greater availability of foraging habitat during April–September, despite causing a net loss in overall acreage of habitat (Exhibit 3). (However, this approach assumes that row and field crops are not available to foraging hawks except at harvest, and thus underestimates the acreage of foraging habitat available, particularly during April–May, which is prior to the harvest of row and field crops in the Natomas Basin.)

Based on EDAW's analysis approach, total foraging resources would be comparable with and without the project. At the Greenbriar, proposed reserve, and DEIR mitigation sites, during April–June, slightly greater foraging resources would be available with the project (the equivalent of 129 acres of high quality foraging habitat with versus 122 acres without the project), while during July–September there would be less (129 versus 140 acres in July–August and 162 acres in September) (Exhibit 4). (Throughout the Natomas Basin, during July–September, more foraging resources are available because that is when most crops are harvested [CH2M HILL 2003].)

## Effects on Connectivity

With the exception of the 250-foot wide proposed conservation easement along Lone Tree Canal, the Greenbriar site would become urban land cover, which would reduce upland connectivity between the Swainson's hawk nests south of the site and foraging habitat north of the Greenbriar site. This connectivity will already be reduced by development of the Metro Air Park, which would leave the Greenbriar site as the last north-south habitat corridor in the Basin east of the mile-wide corridor along the Sacramento River. Although nesting hawks have the ability to fly past a developed Greenbriar site to northern foraging areas, they may be less likely to use foraging habitat beyond this 546-acre urban area because of the energetic cost and additional time away from the nest required by the flight. (Long foraging flights are more likely to follow lines of contiguous habitat, as hawks may scan for prey along the entire flight.)

For Swainson's hawk, the consequences of this potential habitat fragmentation depend on the distribution of foraging and nesting habitat under the future condition of the Natomas Basin resulting from the NBHCP. Currently, there is relatively little foraging habitat north and east of the Greenbriar site, and this habitat is already fragmented. There also is very little potential nesting habitat north and east of the Greenbriar site. (Both foraging habitat and nesting habitat are concentrated to the south and west of the Greenbriar site.) Thus, changes in land cover at the Greenbriar site are unlikely to cause substantial alterations of movement of Swainson's hawks across the Greenbriar site. However, the distribution of Swainson's hawk habitat in the Natomas Basin could change, and under the future condition of the Natomas Basin there would be non-urban land both north of the Greenbriar site in the central Natomas Basin and to the south of the Greenbriar site in the southern Natomas Basin. Thus, the potential for effects on connectivity of Swainson's hawk habitat can not be discounted.

The potential effects of habitat fragmentation and reduced upland connectivity on Swainson's hawk prey are discussed under *Mechanisms of Habitat Degradation*, above.

## **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Construction at the Greenbriar site and habitat management at the proposed reserve sites has the potential to displace and/or disturb nesting Swainson's hawks. Nest disturbance from the operation of heavy construction equipment and continued activity near nest sites could cause nest abandonment or interfere with the incubation and feeding of young in a way that reduces nesting success.

The DEIR for the Greenbriar project and the Natomas Basin HCP both include measures to avoid and minimize construction-related effects on Swainson's hawks. In the DEIR, these measures include:

- ▶ Pre-construction surveys shall be conducted for Swainson's hawk and other raptors no more than 14 days and no less than 7 days prior to the beginning of any construction activity between March 15 and August 15. The survey area shall include all potential nesting sites located within ½ mile of the project and mitigation-sites
- ▶ Should nesting be discovered within the survey area, a qualified biologist shall notify DFG and no new disturbance shall occur within 1/2 mile of the nest until the nest is no longer active or appropriate avoidance measures are approved by DFG to ensure that the nest is adequately protected. Potential mitigation measures may include visual screening and timing restrictions for construction activity. Monitoring (funded by the project applicants) of active nests by a DFG-approved raptor biologist shall be required to determine if project construction is disturbing Swainson's hawks at the nest site. Exact implementation of this measure shall be based on specific information at the project site.

These measures should adequately reduce the impacts to Swainson's hawks that may result specifically from construction-related activities. Any construction-related displacement of hawks from foraging habitat is akin to habitat loss, as discussed above.

## **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

The proposed development is located within a ½ mile of one Swainson's hawk nest active in 2005. Although this nest tree was cut down (without authorization) during the breeding season, the pair attempted to renest in another nearby tree and may return in future years. This breeding pair would be close enough to the Greenbriar site that human disturbance from the residential development proposed at the Greenbriar site may cause nest abandonment (Bent 1937; Stahlecker 1975) or interfere with incubation and feeding of young in a way that reduces reproductive success. Predation of eggs and young chicks by crows and other corvids may also increase as a result of increased human refuse and infrastructure at the Greenbriar site (Steenhof et al. 1993; Marzluff et al. 2001). Mortality because of vehicle strikes may also increase on existing roads because of the increased traffic associated with the project. Human-wildlife conflicts are unlikely to occur at the proposed reserves.

## **OVERALL EFFECT ON POPULATION VIABILITY**

The project would cause both adverse and beneficial effects on the Swainson's hawk population nesting and foraging in the Natomas Basin. Adverse effects would include a reduction in the total acreage of foraging habitat, fragmentation, and possibly degradation of habitat near the Greenbriar site, and a reduction in habitat available to hawks nesting at reserves near the Greenbriar site. Beneficial effects would include increasing the acreage of high quality habitat, preserving high quality habitat within a mile of TNBC reserves (or of the Swainson's Hawk zone along the Sacramento River), and possibly contributing to the connectivity of foraging habitat adjacent to the mitigation site(s) required by mitigation measure 6.13-2.

Overall, based on the USFWS interpretation of effects on Swainson's hawk due to the NBHCP (USFWS 2003), the Greenbriar project would not be expected to adversely affect the viability of the Swainson's hawk population in the Natomas Basin. Because the availability of foraging habitat during April-July is considered to limit the abundance and reproductive success of Swainson's hawk in the Natomas Basin (CH2M HILL 2003; USFWS 2003), and the project would not reduce the acreage of habitat available during these months, the project would not be expected to reduce the number of hawks nesting in the Natomas Basin or their reproductive success.

# 4.4 BURROWING OWL

# 4.4.1 SPECIES ECOLOGY

#### HABITAT ASSOCIATIONS/REQUIREMENTS

## **Habitat Type**

Burrowing owls (*Athene cunicularia hypugea*) typically inhabit grasslands, savannahs and other open habitats with low-lying vegetation. Land cover types designated as burrowing owl habitat in the NBHCP include alfalfa, grassland and pasture. Owls are also known to nest and forage in idle agricultural fields, ruderal fields and the edges of cultivated fields, although these areas provide lower quality habitat than native grasslands. The NBHCP also describes canals as potential nesting habitat for burrowing owls, although it does not include canals in the habitat table for this species. Levees and upper banks of canals and ditches provide burrowing owl nesting habitat when canal maintenance activities are limited, water levels remain below nesting burrows and the area remains relatively undisturbed. Small mammal populations (particularly California ground squirrels) are the most important feature in burrowing owl habitat, as these mammals provide both food and nesting burrows for the owls. When natural burrows are scarce, burrowing owls will also nest in artificial structures such as culverts. They often nest in elevated areas such as berms and levees, where they may scan adjacent lands for predators and prey. Burrowing owls feed primarily on large insects and rodents, and will also feed opportunistically on birds, reptiles and amphibians (NatureServe 2005).

# **Home Range Size and Movement**

Although the more northern burrowing owl populations migrate seasonally, burrowing owls are year-round residents of the Natomas Basin. The owls often form loose colonies, with nest burrows 46–2,952 feet apart (Ross 1974; Gleason 1978). Surprisingly few data are available on home range size for this species. Published estimates vary from 0.05–1.86 square miles (Haug and Oliphant 1990).

#### **Mechanisms of Habitat Degradation**

#### Increased Predation

Ground- and burrow-nesting birds such as burrowing owls are particularly vulnerable to predation by domestic dogs and cats. Many wild predators of burrowing owls also increase near human habitation. In proximity to residential development, dominant carnivores such as coyotes are typically replaced by foxes, opossums, skunks, and other small predators that feed on burrowing owls (Sheffield 1997; Wellicome 1997b; Crooks and Soule 1999). Avian predators such as great-horned owls and crows may also increase in proximity to residential development, in response to introduced nesting trees, increased food supplies and increased hunting perches such as street lights and other infrastructure (Steenhof et al. 1993; Marzluff et al. 2001). This increase in predator abundance would likely result in increased predation of burrowing owl nests and adults near residential development.

## Reduction of Prey Base

Changes in the owls' prey base may result from residential development affecting adjacent mammalian predator communities. Rodents and insects are the primary prey of burrowing owls; songbirds also contribute to their diets (NatureServe 2005). Crooks and Soule (1999) quantified the effects of domestic cats on small animals. They estimated that the average domestic cat population in moderately sized fragments (~50 acres of upland habitat bordered by 100 residences) returns about 840 rodents, 525 birds and 595 lizards to residences each year. Assuming that cats do not bring back all prey that they kill, actual effects on prey numbers are probably even greater. Crooks and Soule (1999) documented increased extirpations of songbird species in habitat fragments with

higher densities of cats, raccoons and opossums, all of which often increase in proximity to residential development.

Compared to undeveloped areas at least 2,296 feet from development, Odell and Knight (2001) demonstrated lower densities of the owls' secondary songbird prey within 1,083 feet of sparse residential development (about 0.4 houses per acre); impacts of higher density development are expected to be greater. Similarly, Blair (1996) reported 1/3 fewer bird species in lands adjacent to residential development, when compared to habitat preserves in the same area.

# Habitat Fragmentation and Reduced Patch Size

Habitat fragmentation has been implicated as a major cause of population decline in grassland birds in general, and is likely to specifically impact burrowing owls. Helzer and Jelinski (1999) found both overall avian species richness and the presence of several common grassland species to increase with the size of habitat patches (especially when >124 acres) and decrease with the perimeter-area ratio of these patches, which reflects the proportion of habitat influenced by edge effects.

In fragments 5–250 acres in size, Crooks et al. (2001) found fragment size to be the most important factor determining extinction and colonization of songbirds. No fragments up to 247 acres in size were large enough to support the full complement of native bird species with 95% probability over a 100-year period. Burrowing owls forage in larger habitat patches than the smaller birds studied by Crooks et al. (2001), and are likely to be similarly affected by fragmentation. Hinsley et al. (1995) also demonstrated the instability of bird populations in habitat fragments.

#### Nest Disturbance

Although burrowing owls are tolerant of human activity outside of the breeding season, they have been shown to abandon nests if disturbed during incubation. In addition to nest abandonment, significant disturbances near owl nests may interfere with parental care and feeding of young in a way that reduces nest success.

#### **DISTRIBUTION**

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 370 known occurrences in California, of which 300 were considered extant. At that time, three occurrences were known from the Natomas Basin, all of which were considered extant. As of 2005, there are 709 known occurrences in California, of which 671 are considered extant. At this time, seven occurrences are known in the Natomas Basin, of which six are considered extant. Of these occurrences, one is within a mile of the Greenbriar site, and none are within a mile of the proposed reserve sites.

#### Other Information on Distribution and Abundance in Natomas Basin

No systematic surveys have been conducted to determine burrowing owl distribution or abundance across the Natomas Basin. A burrowing owl was incidentally observed in a culvert on the southwestern portion of the Greenbriar site during the March 17, 2005 site visit. A number of owl pellets and whitewash were also observed, indicating extended use of the site by at least one owl for roosting and foraging over a period of time, and possible nesting. During biological effectiveness monitoring for the NBHCP, burrowing owls were observed in the eastern Basin south of Elverta Road and in the central Basin along Highway 99 (approximately 1.3 miles north of the Greenbriar site) (Jones & Stokes 2005). Burrowing owls have also been incidentally observed east of the Greenbriar site along Elkhorn Blvd. and west of the Greenbriar site on the Metro Air Park and Sacramento International Airport.

# 4.4.2 PROJECT EFFECTS ON SPECIES

#### LONG-TERM EFFECTS ON HABITAT

# **Effect on Quantity of Habitat**

The project's effects on foraging habitat for burrowing owl are summarized in Table 4-4. The project would reduce the acreage of burrowing owl habitat in the Natomas Basin from conditions at the time of the NBHCP (2001). The proposed development at the Greenbriar site would reduce habitat by an estimated 94 acres from conditions in 2001. At the proposed reserves, 118 acres of burrowing owl habitat would be created (assuming the Swainson's hawk foraging also provided burrowing owl habitat). Thus, the project as a whole would yield a net gain of 24 acres of burrowing owl habitat. Additional burrowing owl foraging habitat may be created by the enhancement and management of at least 49 acres of land to provide high quality foraging habitat for Swainson's hawk that is required by mitigation measure 6-13.2 of the DEIR.

| Table 4-4 Change in Acreage of Burrowing Owl Habitat at Project Sites and in the Natomas Basin |           |            |                    |          |                |                         |  |  |  |
|--|-----------|------------|--------------------|----------|----------------|-------------------------|--|--|--|
| Land Cover Type  | Future    | Chanç      | ge at Each Project | Site     | - Total Change | <b>Future Condition</b> |  |  |  |
| Providing Habitat  | Condition | Greenbriar | Natomas 130        | Spangler | - Total Change | with Project            |  |  |  |
| Alfalfa  | 368       | -          | 14.2               | 45.4     | 59.6           | 428                     |  |  |  |
| Canals   | 1,162     | -15.0      | 0.0                | -1.4     | -16.4          | 1,146                   |  |  |  |
| Grassland  | 284       | 26.5       | -                  | -        | 26.5           | 311                     |  |  |  |
| Idle   | 422       | -62.5      | -                  | -        | -62.5          | 360                     |  |  |  |
| Pasture  | 494       | -33.8      | -                  | -        | -33.8          | 460                     |  |  |  |
| Ruderal  | 370       | -9.2       | -                  | -        | -9.2           | 361                     |  |  |  |
| Upland marsh components  | 547       | -          | 4.3                | 55.2     | 59.5           | 607                     |  |  |  |
| Total  | 3,647     | -94.1      | 18.5               | 99.2     | 23.7           | 3,673                   |  |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

# **Effects on Quality of Habitat**

# Areas Adjacent to Developed Land or Highways

Although the expanded urban area that would be created at the Greenbriar site would result in a net reduction of areas within 800 feet or 1 mile of development, the project would expand a gradient of urban influence into the previously unaffected area to the north of the property and could increase the urban influence in the idle field to the southwest. The potential effects on burrowing owls and their prey in these areas are discussed under *Mechanisms of Habitat Degradation*, above. These adverse effects, however, would be limited by Interstate 5 along the Greenbriar site's southern border, and by Elkhorn Boulevard (which would be expanded to six lanes) that would serve as partial barriers between development on the Greenbriar site and adjacent agricultural lands.

The current land use immediately to the north of the Greenbriar site is rice and as such does not support burrowing owl habitat. However, the creation of burrowing owl habitat at the Greenbriar site between 2001 and 2005 attests to the potential for the area to the north to become burrowing owl habitat in the future. The habitat creation on the Greenbriar site resulted from the conversion of a portion of the rice acreage to fallow agriculture. The current land use to the southwest of the property is fallow agriculture, which supports burrowing owl habitat.

# Altered Habitat Quality at Proposed Reserve and Mitigation Sites

In addition to habitat lost due to development of the Greenbriar site, and created at the proposed reserves, the quality of burrowing owl habitat could be altered at the conserved corridor along Lone Tree Canal, the proposed Spangler and Natomas 130 reserves, and the mitigation site that would be required by mitigation measure 6.13-2 of the DEIR.

Conservation of the corridor along Lone Tree canal may improve its value as foraging habitat because it would be converted to perennial grassland that might have higher habitat value. This corridor, however, would be a relatively narrow band of potential habitat surrounded by urban development, and this setting might limit its use by burrowing owl.

At all of the proposed reserves, management practices would enhance habitat for burrowing owl. These enhancements include maintaining buffers in as natural a state as possible, controlling feral cats if necessary, and reducing human disturbance due to trespassers (City of Sacramento et al. 2003, John Roberts, TNBC, personal communication). Also, preservation of habitat, even without enhancement measures, provides some benefits, including that it precludes land use changes that would eliminate habitat, and should reduce or eliminate uses that could cause mortality of individuals.

In addition to habitat enhancement at the proposed reserves, mitigation measure 6.13-2 of the DEIR requires that at least 49 acres be enhanced to provide high quality foraging habitat. This mitigation could also benefit burrowing owls. This mitigation land will be managed to provide high quality foraging habitat for Swainson's hawk, but would also enhance foraging habitat for burrowing owl.

## Effects on Connectivity

With the exception of the 250-foot wide conservation easement proposed along Lone Tree Canal, the development at the Greenbriar site would eliminate the existing contiguity of upland habitats to the north and south of the site. This connectivity will already be substantially reduced by development at the Metro Air Park, which would leave the Greenbriar site as the last north-south corridor of habitat in the Basin east of the mile-wide corridor along the Sacramento River. Owl survival and reproduction are likely to be higher in larger, more contiguous habitat areas. Connectivity benefits owls by providing greater ease of locating mates, greater flexibility in year-round foraging opportunities, and safer passages for juvenile dispersal. The potential effects of reduced connectivity on upland birds in general are discussed under *Mechanisms of Habitat Degradation*, above.

The proposed reserves and mitigation site(s) could increase connectivity of burrowing owl habitat elsewhere in the Natomas Basin. If larger, more contiguous areas of habitat resulted from the creation of these reserves, this would benefit owl survival and reproduction. Other foraging habitat is available near the Natomas 130 site, and thus this proposed reserve would result in larger more continuous areas of habitat (Jones & Stokes 2005). The land cover surrounding the Spangler property is primarily rice (Jones & Stokes 2005)

## **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Earth-moving activities may trap or injure owls in their burrows, and disturbance near nests may cause nest abandonment. Both the Greenbriar DEIR and Natomas Basin HCP require comparable measures to avoid impacts to burrowing owls during construction. The DEIR measures include:

- a. No more than 30 days and no less than 14 day prior to project site grading, a qualified biologist shall conduct focused surveys for burrowing owls in areas of suitable habitat on and within 300 feet of the project site. Surveys shall be conducted in accordance with DFG protocol (DFG 1995).
- b. If no occupied burrows are found in the survey area, a letter report documenting survey methods and findings shall be submitted to DFG, and no further mitigation is necessary.

- c. If occupied burrows are found in the survey area, impacts shall be avoided by establishing a buffer of 165 feet during the non-breeding season (September 1 through January 31) or 300 feet during the breeding season (February 1 through August 31). The size of the buffer area may be adjusted if a qualified biologist and DFG determine it would not be likely to have adverse effects. No project activity shall commence within the buffer area until a qualified biologist confirms that the burrow is no longer occupied. If the burrow is occupied by a nesting pair, a minimum of 6.5 acres of foraging habitat contiguous to the burrow shall be preserved until the breeding season is over.
- d. If impacts to occupied burrows are unavoidable, on-site passive relocation techniques may be used if approved by DFG to encourage owls to move to alternative burrows outside of the impact area. However, no occupied burrows shall be disturbed during the nesting season unless a qualified biologist verifies through non-invasive methods that the burrow is no longer occupied. Foraging habitat for relocated pairs shall be provided in accordance with guidelines provided by DFG (1995). DFG guidelines recommend a minimum of 6.5 acres of foraging habitat per pair or unpaired resident bird, be acquired and permanently protected.
- e. If relocation of the owls is approved for the site by DFG, the developer shall hire a qualified biologist to prepare a plan for relocating the owls to a suitable site. The relocation plan must include: (a) the location of the nest and owls proposed for relocation; (b) the location of the proposed relocation-site; (c) the number of owls involved and the time of year when the relocation is proposed to take place; (d) the name and credentials of the biologist who will be retained to supervise the relocation; (e) the proposed method of capture and transport for the owls to the new site; (f) a description of the site preparations at the relocation-site (e.g., enhancement of existing burrows, creation of artificial burrows, one-time or long-term vegetation control, etc.); and (g) a description of efforts and funding support proposed to monitor the relocation. Relocation options may include passive relocation to another area of the site not subject to disturbance through one way doors on burrow openings, or construction of artificial burrows in accordance DFG guidelines.
- f. The project applicant shall implement Mitigation Measure 6.12-2 to mitigate for the loss of burrowing owl foraging habitat.

By following these measures, the potential for injury, entrapment, and nest abandonment would be reduced. However, nests may be abandoned because of loss of the surrounding foraging habitat during construction, and owl viability at relocation sites is not guaranteed.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

On the remaining habitat adjacent to the proposed development, human activity may cause owl nest abandonment or interfere with the incubation and feeding of young in a way that reduces reproductive success. Increased owl predation would also likely occur in proximity to the proposed development, as a result of the typical increase in human-associated owl predators discussed above under Mechanisms of Habitat Degradation. Increased predation by domestic cats is likely to extend between 98–540 feet from homes, predation by domestic dogs is likely to extend between 540–990 feet from homes, and increased predation by wild predators is likely to extend farther (Odell and Knight 2001). Mortality because of vehicle strikes may also increase on existing roads because of the increased traffic that would result from the project.

## **OVERALL EFFECT ON POPULATION VIABILITY**

The Greenbriar project with the DEIR mitigation would cause both adverse and beneficial effects on burrowing owl. Adverse effects would include loss of occupied habitat, and fragmentation and some degradation of habitat adjacent to development at the Greenbriar site. Beneficial effects would include a net increase in acreage of foraging habitat, and preservation and enhancement of at least 197 acres of habitat, and possibly increased connectivity of habitats in the vicinity of the mitigation lands. Overall, the project would likely result in a beneficial effect on burrowing owl. However, the project is unlikely to have a substantial effect on burrowing

owls using the Natomas Basin, and since the Basin accounts for a very small portion of the Central Valley's burrowing owl population and of the habitat it occupies (USFWS 2003), the project would not alter the viability of the burrowing owl population using the Natomas Basin.

# 4.5 LOGGERHEAD SHRIKE

# 4.5.1 SPECIES ECOLOGY

#### HABITAT ASSOCIATIONS/REQUIREMENTS

# **Habitat Type**

Loggerhead shrikes (*Lanius ludovicianus*) are most commonly found in grasslands, agricultural lands, open shrublands, and open woodlands (Bent 1950). Land cover types designated as shrike habitat in the NBHCP include alfalfa, grassland, non-rice crops, oak groves, orchard, pasture, ponds and seasonally wet areas, riparian, ruderal, rural residential, tree groves, and canals. Special habitat features that improve shrike abundance, survival, and reproductive success are hunting perches, low nesting trees and shrubs, thorny vegetation, and/or barbed wire on which to impale their prey. Shrikes select a variety of prey including insects, reptiles, mammals, and birds.

# **Home Range Size and Movement**

The mean territory size of breeding loggerhead shrikes in mainland California is 22 acres (Miller 1931). The range-wide maximum and minimum breeding territory sizes recorded are 1.7 and 44 acres (Yosef and Grubb 1994). Territory size varies with habitat quality, prey abundance and availability, and density of hunting perches (Kridelbaugh 1982, Yosef and Grubb 1992). Loggerhead shrikes have been observed foraging up to a quarter mile from active nests (Brooks 1988). Shrikes are year-round residents in California, and breeding pairs disband in autumn to defend separate, adjacent, winter territories (Miller 1951, Craig 1978). As food availability decreases in winter, seasonal home ranges may increase to 128 acres (Blumton et al. 1989). Juvenile shrikes move an average of 3.4 miles from their natal territories to their fall territories.

#### **Mechanisms of Habitat Degradation**

#### Increased Predation

Domestic cats are a common predator of loggerhead shrike adults, juveniles and nests (Luukkonen 1987, Novak 1989), and would increase in abundance following the proposed development. Crooks and Soule (1999) quantified the impacts of domestic cat predation on songbirds such as loggerhead shrikes, and estimated that the average domestic cat population in moderately sized fragments (~50 acres of upland habitat bordered by 100 residences) returns about 525 birds to human residences each year. Assuming that cats do not bring back all prey that they kill, actual impacts to birds are probably even greater.

Many wild mammalian predators of shrikes also increase near human habitation. In proximity to residential development, dominant, larger carnivores such as coyotes are typically replaced by foxes, opossums, skunks, and other small predators that feed on shrikes and other songbirds. Crooks and Soule (1999) have recorded increased avian extirpation rates in habitat fragments as a result of these predator increases.

Shrike nest predators such as crows also typically increase in proximity to residential development, in response to introduced nesting trees, increased food supplies, and increased hunting perches such as street lights and other infrastructure (Steenhof et al. 1993; Marzluff et al. 2001). Predation of loggerhead shrike nests is also more intense along roads, urban edges, and other linear habitats (DeGeus 1990), presumably because of the increased use of linear rights-of-way by crows and mammalian predators (Knight et al. 1995). Of loggerhead shrike nest failures, 40–90% have been attributed to predation in the various studies of this species (NatureServe). Shrike

mortality from vehicle collisions has also been significant in some areas (NatureServe), and may increase with increased traffic generated by the proposed residential development.

#### Nest Disturbance

Loggerhead shrikes will abandon nests if disturbed by humans during egg-laying or early in incubation. Shrikes are generally tolerant of human activity near nests later in the breeding season, however, and nest abandonment is not generally a significant factor in nest failure (Collister 1994).

# Habitat Fragmentation

Habitat fragmentation has been implicated as a major cause of population decline in grassland birds in general, and is likely to specifically affect loggerhead shrikes. Helzer and Jelinski (1999) found both overall avian species richness and the presence of several common grassland species to increase with the size of habitat patches (especially when >50 ha) and decrease with the perimeter-area ratio of these patches, which reflects the proportion of habitat influenced by edge effects. Hinsley et al. (1995) and Crooks et al. (2001) also demonstrated the instability of upland bird populations in habitat fragments.

#### DISTRIBUTION

## **Information on CNDDB Occurrences**

Although loggerhead shrikes are known to occur in open habitats throughout California (California Department of Fish and Game 1990), they have not been extensively surveyed and few occurrence data are available in the state. The CNDDB lists five occurrences for this species, all in southern California.

## Other Information on Distribution and Abundance in Natomas Basin

The Natomas Basin Conservancy lists 82 shrike occurrences throughout the Basin, and suitable nesting and foraging habitat is common throughout the area. Shrikes were observed on the Greenbriar site during March 2005 surveys.

## 4.5.2 Project Effects on Species

## LONG-TERM EFFECTS ON HABITAT

#### **Effect on Quantity of Habitat**

The project's effects on the acreage of shrike habitat are summarized in Table 4-5. The project would reduce the acreage of loggerhead shrike habitat in the Natomas Basin from conditions at the time of the NBHCP (2001). The proposed development at the Greenbriar site would reduce habitat by an estimated 369 acres from conditions in 2001. At the proposed Spangler reserve, shrike habitat would increase by 228 acres because habitat would be created (by converting rice to marsh and upland habitat). Thus, the project as a whole would yield a net loss of 141 acres of loggerhead shrike habitat.

# **Effects on Quality of Habitat**

# Areas Adjacent to Developed Land or Highways

Although the urban area that would be created by the Greenbriar project would result in a net reduction of areas within 800 feet or 1 mile of development, the project would expand a gradient of urban influence into the previously unaffected area to the north of the property and could increase the urban influence in the idle field to

the southwest. The potential affects on loggerhead shrikes in these areas are discussed under *Mechanisms of Habitat Degradation*, above.

| Table 4-5 Change in Acreage of Loggerhead Shrike Habitat at Project Sites and in the Natomas Basin |           |            |                    |          |                |                  |  |  |  |
|--|-----------|------------|--------------------|----------|----------------|------------------|--|--|--|
| Land Cover Type  | Future    | Chang      | je at Each Project | Site     | - Total Change | Future Condition |  |  |  |
| Providing Habitat  | Condition | Greenbriar | Natomas 130        | Spangler | - Total Change | with Project     |  |  |  |
| Alfalfa  | 368       | -          | 14.2               | 45.4     | 59.7           | 428              |  |  |  |
| Canals   | 1,162     | -15.0      | 0.0                | -1.4     | -16.4          | 1,146            |  |  |  |
| Grassland  | 284       | 26.5       | -                  | -        | 26.5           | 311              |  |  |  |
| Idle   | 422       | -62.5      | -                  | -        | -62.5          | 360              |  |  |  |
| Non-rice crops   | 9,533     | -234.1     | -28.4              | -        | -262.6         | 9,270            |  |  |  |
| Oak groves   | 77        | -          | -                  | -        | 0.0            | 77               |  |  |  |
| Orchards   | 165       | -          | -                  | -        | 0.0            | 165              |  |  |  |
| Pasture  | 494       | -33.8      | -                  | -        | -33.8          | 460              |  |  |  |
| Ponds & seasonally wet areas   | 2,259     | 2.7        | 14.2               | 184      | 200.9          | 2,460            |  |  |  |
| Riparian   | 91        | 0.0        | 0.0                | -        | 0.0            | 91               |  |  |  |
| Ruderal  | 370       | -9.22      | -                  | -        | -9.2           | 361              |  |  |  |
| Rural residential  | 287       | -43.319    | -                  | -        | -43.3          | 244              |  |  |  |
| Tree groves  | 44        | -          | 0.0                | -        | 0.0            | 44               |  |  |  |
| Total  | 15,555    | -368.8     | 0.0                | 228      | -140.8         | 15,415           |  |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

The current land use immediately to the north of the Greenbriar site is rice and as such does not support loggerhead shrike habitat. However, the creation of shrike habitat at the Greenbriar site between 2001 and 2005 attests to the potential for the area to the north to become impacted shrike habitat in the future. The habitat creation on the Greenbriar site resulted from the conversion of a portion of the rice acreage to fallow agriculture and non-rice crops. The current land use to the southwest of the property is fallow agriculture, which supports loggerhead shrike habitat.

Adverse effects on adjacent land, though probably not insignificant, would be limited by Interstate 5 along the Greenbriar site's southern border and by Elkhorn Boulevard (which would be expanded to six lanes) that would serve as partial barriers between development on the Greenbriar site and adjacent agricultural lands.

## Altered Habitat Quality at Proposed Reserve and Mitigation Sites

In addition to habitat loss due to development of the Greenbriar site and habitat creation from rice at the proposed Spangler reserve, the quality of loggerhead shrike habitat could be altered at the conserved corridor along Lone Tree Canal, the proposed Natomas 130 reserve, and the mitigation site(s) that would be required by mitigation measure 6.13-2 of the DEIR.

Conservation of the corridor along Lone Tree canal may improve its value as foraging habitat because it would be converted to perennial grassland that might have higher habitat value than the current and recent agricultural land cover. This corridor, however, would be a relatively narrow band of potential habitat surrounded by urban development, and this setting might limit its use by loggerhead shrike.

At the proposed Natomas 130 reserve, there would be little overall change in habitat quality. Habitat quality would decrease on the 14 acres of created marsh, because this land cover type provides lower quality shrike habitat than the agricultural cropland it would replace. Conversely, habitat quality would increase on the 14 acres managed to provide high quality foraging habitat for Swainson's hawk. At the Spangler site, 235 acres would be enhanced for loggerhead shrike by the conversion of rice to managed marsh and uplands. Loggerhead shrike habitat would also be enhanced at the on 49 acres at the *DEIR* mitigation site. Mitigation measure 6.13-2 of the DEIR requires the enhancement and preservation of at least 49 acres to provide high quality foraging habitat. This DEIR mitigation is in addition to the proposed reserves. Its management to provide high quality foraging habitat for Swainson's hawk would also increase habitat quality for loggerhead shrike.

Overall, the project would preserve and actively manage 345 acres of habitat (30.4 acres at the Natomas 130 site, 235.4 acres at the Spangler site, 30.6 acres at the Greenbriar site, and at least 49 acres at the mitigation site required by mitigation measure 6-13.2 of the DEIR). This preservation and management would provide additional benefits (such as reduced human disturbance).

## Effects on Connectivity

With the exception of the 250-foot wide proposed conservation easement along Lone Tree Canal, development at the Greenbriar site would eliminate the existing contiguity of upland habitats to the north and south of the site. This connectivity will already be substantially reduced by development at the Metro Air Park, which would leave the Greenbriar site as the last north-south habitat corridor in the Basin east of the mile wide corridor along the Sacramento River. Shrike survival and reproduction are likely to be higher in larger, more contiguous habitat areas. Connectivity benefits shrikes by providing greater ease of locating mates, greater flexibility in year-round foraging opportunities, and safer passages for juvenile dispersal and seasonal movements. The potential effects of reduced connectivity on upland birds in general are discussed under *Mechanisms of Habitat Degradation*, above.

Except for the proposed Spangler reserve, the proposed reserve and mitigation sites already provide shrike habitat, and thus their preservation and management are unlikely to significantly increase habitat connectivity. The creation of habitat at the proposed Spangler reserve could locally increase connectivity of shrike habitats.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Construction activities associated with the proposed development or the proposed habitat creation on proposed reserve sites could disturb or displace loggerhead shrikes and may cause nest abandonment. In the Greenbriar project DEIR and Natomas Basin HCP, preconstruction surveys for loggerhead shrikes would be conducted before construction. If shrikes are found, disturbance would be avoided during the nesting season to the maximum extent possible.

# **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

On the remaining habitat adjacent to the proposed development, human activity may cause shrike nest abandonment or interfere with the incubation and feeding of young in a way that reduces reproductive success. Increased shrike predation would also be likely to occur in proximity to the proposed development, as a result of the typical increase in human-associated predators discussed above under *Mechanisms of Habitat Degradation*. Human-wildlife conflicts are unlikely to occur at the proposed reserve sites.

# **OVERALL EFFECT ON POPULATION VIABILITY**

Overall, the Greenbriar project could cause a small adverse or beneficial effect on loggerhead shrike. Though it would enhance 298 acres of shrike habitat and preserve 345 acres of habitat, these beneficial effects might not fully offset the project's adverse effects on loggerhead shrike, which include a net loss of 141 acres of habitat, reduced habitat quality on 45 acres (14 acres at Natomas 130 and 30.6 acres along Lone Tree Canal),

fragmentation of habitat, a reduction of connectivity, and probably some increased mortality and habitat degradation adjacent to the Greenbriar site. However, the project's effects would be small relative to the quantity of habitat that would remain in the Natomas Basin (e.g., the project would cause the loss of approximately 1% of habitat that would be available under the future condition), and the Natomas Basin represents only a small portion of the habitat used by shrikes in the Central Valley (USFWS 2003). Thus, the project is unlikely to alter the viability of the loggerhead shrike population using the Natomas Basin.

# 4.6 TRICOLORED BLACKBIRD

# 4.6.1 SPECIES ECOLOGY

#### HABITAT ASSOCIATIONS/REQUIREMENTS

# **Habitat Type**

Tricolored blackbirds (*Agelaius tricolor*) nest in dense colonies that range from less than 25 individuals to over 80,000. As nesting and foraging habitat differ for this species, we analyzed these habitats separately. Common nesting substrates include tule and cattail marsh, blackberry, thistle, willow, nettle, and some grain crops (Beedy and Hayworth 1991). Because patches of dense nesting substrate do not necessarily correlate with the land cover types defined by the NBHCP, the NBHCP analyzed these patches separately as "tricolored blackbird nesting habitat." Special habitat features that improve nesting blackbird abundance, survival and reproductive success include dense nesting substrates and proximity to concentrated insect populations large enough to sustain the colony (Grinnell and Miller 1944, DeHaven 2000).

Tricolored blackbirds forage in grassland, pasture, silage, wetlands and flooded fields, rice, and other grain fields (Zeiner et al. 1990). Land cover types designated as tricolored blackbird foraging habitat in the NBHCP include alfalfa, grassland, non-rice crops, pasture, and rice. As they represent a transition between cropland and grassland habitats, idle and ruderal fields may also provide marginal foraging habitat. Tricolored blackbirds are primarily insectivorous, with grasshoppers, beetles, and weevils dominating their diet (Beedy and Hayworth 1991).

## **Home Range Size and Movement**

Breeding tricolored blackbirds concentrate foraging activity in proximity to nesting colonies, and may travel up to 4 miles from nest or roost sites to forage. The species is generally nomadic when not breeding, and may be found year-round throughout lowland California.

## **Mechanisms of Habitat Degradation**

#### Increased Predation

Abundance of blackbird predators such as domestic cats and foxes typically increases in proximity to residential development (Crooks and Soule 1999). Although increased predation near residential development would likely be much less for vigilant, mobile flocks of foraging blackbirds than for more stationary nesting birds such as loggerhead shrikes or burrowing owls, predation rates would be expected to increase for all small bird species near residential development.

#### Nest Disturbance

Nesting colonies of tricolored blackbirds are highly sensitive to disturbance, which may cause nest abandonment or interfere with the incubation and feeding of young in a way that reduces reproductive success (NBHCP 2001).

#### Water Diversion and Runoff

Water diversions may degrade wetland habitat for tricolored blackbirds nesting downstream from a diversion.

#### **DISTRIBUTION**

#### Information on CNDDB Occurrences

The NBHCP does not list state-wide or Basin-specific CNDDB occurrences of tricolored blackbirds, but notes 9 occurrences in Sutter County, 7 of which were extant in 2001. As of 2005, there are 408 known occurrences in California, of which 339 are considered extant. At this time, CNDDB does not list tricolored blackbird occurrences within one mile of the Natomas Basin.

## Other Information on Distribution and Abundance in Natomas Basin

At the time of the NBHCP in 2001, the Betts-Kismat-Silva reserve on the eastern edge of the Natomas Basin supported a tricolored blackbird colony of approximately 4,000 nesting birds (NBHCP 2001). At the time of the most recent TNBC monitoring report in 2004, the blackbirds did not nest at this site, although 125–300 birds were regularly seen in the area. Tricolored blackbirds similarly did not nest at this site in 2005 (unpublished data). Tricolored blackbirds are known to forage throughout the Basin (NBHCP), and have been observed foraging on the Metro Air Park site near the Greenbriar site (Thomas Reid Associates, 2000).

# 4.6.2 PROJECT EFFECTS ON SPECIES

## LONG-TERM EFFECTS ON HABITAT

# **Effect on Quantity of Habitat**

The Project's effects on the acreage of nesting habitat for tricolored blackbirds are summarized in Table 4-6. The Greenbriar and proposed reserve sites do not currently support tricolored blackbird nesting habitat. The proposed creation of 198 acres of marsh at the Natomas 130 and Spangler sites would provide potential nesting habitat in these managed marshes. However, at the Natomas 130 site, because of the extensive urban development nearby and variety of habitats surrounding the parcel, it is unclear whether the foraging habitat surrounding the created marsh would be adequate to sustain a nesting colony of blackbirds. This is not the case at the Spangler site where most of the marsh (184 of 198 acres) would be created.

| Table 4-6 Change in Acreage of Tricolored Blackbird Nesting Habitat at Project Sites and in the Natomas Basin |           |            |                    |          |                |                         |  |  |
|---|-----------|------------|--------------------|----------|----------------|-------------------------|--|--|
| Land Cover Type<br>Providing Habitat  | Future    | Chanç      | ge at Each Project | Site     | - Total Change | <b>Future Condition</b> |  |  |
|   | Condition | Greenbriar | Natomas 130        | Spangler | - Total Change | with Project            |  |  |
| Ponds & seasonally wet areas  | 2,259     | 2.7        | 14.2               | 184.0    | 200.9          | 2,460                   |  |  |
| Total   | 2,259     | 2.7        | 14.2               | 184.0    | 200.9          | 2,460                   |  |  |
|   |           |            |                    |          |                |                         |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

The Project's effects on the acreage foraging habitat for tricolored blackbirds are summarized in Table 4-7. The project would reduce the acreage of tricolored blackbird foraging habitat in the Natomas Basin. The proposed development at the Greenbriar site would eliminate an estimated 402 acres of habitat, based on 2001 land cover.

At the proposed Spangler and Natomas 130 reserves, 197 acres of foraging habitat would be eliminated (by conversion of rice and non-rice crop to marsh). Thus, the project as a whole would yield a net loss of 598 acres of tricolored blackbird foraging habitat.

| Table 4-7 Change in Acreage of Tricolored Blackbird Foraging Habitat at Project Sites and in the Natomas Basin |           |                             |             |          |                |                         |  |  |  |
|--|-----------|-----------------------------|-------------|----------|----------------|-------------------------|--|--|--|
| Land Cover Type  | Future    | Change at Each Project Site |             |          | - Total Change | <b>Future Condition</b> |  |  |  |
| Providing Habitat  | Condition | Greenbriar                  | Natomas 130 | Spangler | Total Change   | with Project            |  |  |  |
| Alfalfa  | 368       | -                           | 14.2        | 45.4     | 59.6           | 428                     |  |  |  |
| Grassland  | 284       | 26.5                        | -           | -        | 26.5           | 311                     |  |  |  |
| Non-rice crops   | 9,533     | -234.1                      | -28.4       | -        | -262.6         | 9,270                   |  |  |  |
| Pasture  | 494       | -33.8                       | -           | -        | -33.8          | 460                     |  |  |  |
| Rice   | 11,643    | -160.0                      | -           | -228     | -388.0         | 11,255                  |  |  |  |
| Total  | 22,322    | -401.5                      | -14.2       | -182.6   | -598.3         | 21,724                  |  |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

# **Effects on Quality of Habitat**

# Areas Adjacent to Developed Land or Highways

Although the urban area that would be created by the proposed Greenbriar development would result in a net reduction of areas within 800 feet or 1 mile of development, the project would expand a gradient of urban influence into the previously unaffected area to the north of the property and increase the urban influence in the idle field to the southwest. The potential effects in this area on tricolored blackbirds are discussed under *Mechanisms of Habitat Degradation*, above. These effects include increased predation of foraging tricolored blackbirds but not of nesting blackbirds. Tricolored blackbird nesting habitat does not currently exist in the vicinity of the Greenbriar site; therefore, the project would not result in nest disturbance unless new nests were established near the site.

The current land use to the north of the Greenbriar site is rice, which provides tricolored blackbird foraging habitat. The current land use to the southwest of the property is fallow agriculture, which does not support quality blackbird habitat. However, the conversion of rice to non-rice crops at the Greenbriar site between 2001 and 2005 attests to the potential for agricultural habitats to change; the area to the southwest may thus become blackbird foraging habitat in the future (and conversely, foraging habitat to the north could become less suitable).

Adverse effects on adjacent land, though probably not insignificant, would be limited by Interstate 5 along the Greenbriar site's southern border and by Elkhorn Boulevard (which would be expanded to six lanes) along the site's northern border, which would serve as partial barriers between development on the Greenbriar site and adjacent agricultural lands.

## Habitat Alteration at Proposed Reserve and Mitigation Sites

The project would preserve approximately 198 acres of nesting habitat (14 acres at the Natomas 130 site and 184 acres at the Spangler site). (The 2.7 acres of marsh created at the Greenbriar site was not considered suitable as nesting habitat because of its small size and surrounding urban development.) In addition to its other benefits, preservation should reduce the level of human disturbance, which could enhance the quality of nesting habitat.

The project with the DEIR mitigation would preserve at least 135 acres of foraging habitat: 14 acres at the Natomas 130 site, 45 acres at the Spangler site, 27 acres at the Greenbriar site, and at least an additional 49 acres required by mitigation measure 6-13.2 of the DEIR. (The Spangler site is within foraging distance of the TNBC Betts-Kismat-Silva reserve where tricolored blackbirds have nested.) At the Natomas 130, Spangler, and DEIR mitigation sites, management of 109 acres to provide high quality foraging habitat for Swainson's hawk would also enhance habitat values for tricolored blackbird; however, because the benefits of such management for tricolored blackbirds have not been documented, a moderate level of uncertainty exists regarding their magnitude. (The preservation of land along Lone Tree Canal and its conversion to grassland was not considered an enhancement of foraging habitat because this site would also be affected by the proposed development.)

# Effects on Connectivity

Because tricolored blackbirds are largely nomadic when not nesting, connectivity for this species is mostly pertinent to a 4-mile radius of foraging habitat surrounding nesting colonies. The Greenbriar site is at the edge of this radius from the TNBC Betts-Kismat-Silva reserve where tricolored blackbirds have nested, and thus development at the Greenbriar site would not affect connectivity of foraging habitat near this reserve (although it would reduce the habitat acreage within 4 miles of the reserve). The proposed Spangler reserve is similarly located along the edge of this radius and would preserve foraging habitat within 4 miles of the TNBC Betts-Kismat-Silva reserve (but would not affect connectivity). The proposed Natomas 130 reserve is located outside of this 4-mile radius. The land that would be preserved to provide Swainson's hawk foraging habitat also might increase connectivity of tricolored blackbird habitat depending on its location, but the location of this mitigation land has not yet been specified.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Construction-related activities are unlikely to affect tricolored blackbirds because they do not nest in the vicinity of the Greenbriar and proposed reserve sites. Potential effects would be limited to displacement of birds foraging or roosting on the sites during the initial phases of construction when fields are graded. This impact is largely akin to habitat loss, as the physical flight of the birds from these areas would not cause a significant effect.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

Because tricolored blackbirds do not currently nest in the vicinity of the proposed development or reserve sites, nest disturbance by humans would not be created by the project. Increased populations of human-associated predators may result in increased predation of foraging blackbirds near a developed Greenbriar site, as discussed in *Mechanisms of Habitat Degradation*, above.

#### **OVERALL EFFECT ON POPULATION VIABILITY**

There is a moderate level of uncertainty regarding the overall effect of the Greenbriar project on tricolored blackbird because of the limited current use of the Natomas Basin by tricolored blackbird, opposite effects on nesting and foraging habitat, and uncertainty regarding the benefits provided by foraging habitat enhancement. Recently, only a single colony of tricolored blackbirds has nested in the Natomas Basin (Jones & Stokes 200). However, substantial quantities of foraging habitat (over 21,000 acres, Table 3-3) and an increasing acreage of nesting habitat exist in the Basin, and thus tricolored blackbird use of the Basin could increase. The Greenbriar project would increase the quantity of nesting habitat in the Natomas Basin (by 198 acres), but would decrease the quantity of foraging habitat (by 598 acres). Although currently, nesting habitat is more limited than foraging habitat in the Natomas Basin, under the future condition much more nesting habitat will exist, and thus the additional nesting habitat that would be provided by the project may not affect the tricolored blackbird population more than the loss of foraging habitat that would also result. This loss of foraging habitat would be partially but not fully offset by the preservation of 135 acres of foraging habitat and enhancement of 109 of these 135 acres. However, the magnitude of the benefits provided by this enhancement is moderately uncertain. Because of these

uncertainties, overall, the project could cause a small adverse or beneficial effect on tricolored blackbird use of the Natomas Basin.

Because the project would only cause a small effect on tricolored blackbird use of the Natomas Basin, and because the Natomas Basin accounts for only a small portion of the habitat for and population of tricolored blackbird in the Central Valley, the Greenbriar project is unlikely to alter the viability of the tricolored blackbird population using the Natomas Basin.

# 4.7 WHITE-FACED IBIS

# 4.7.1 SPECIES ECOLOGY

#### HABITAT ASSOCIATIONS/REQUIREMENTS

# **Habitat Type**

White-faced ibis (*Plegadis chihi*) breed in wetlands with dense emergent vegetation such as cattails and rushes. They forage in shallow wetlands, irrigation ditches and a variety of irrigated crops and flooded agricultural fields (Ryder and Manry 1994, Cogswell 1977). Land cover types designated as ibis habitat in the NBHCP include alfalfa, canals, ponds and seasonally wet areas, and rice. White-faced ibis feed on aquatic and moist-soil invertebrates such as earthworms, larval insects, snails, and bivalves. Although white-faced ibis feed intensively in rice fields, rice seeds have not been noted in food samples and only trace, incidental amounts of vegetation have been recorded in ibis diets (Belknap 1957).

# **Home Range Size and Movement**

Nesting colonies have ranged in size from 1.3 acres to 600 acres (USFWS 1985e). Foraging distances from nesting sites vary widely and depend on the availability of food. Some colonies concentrate their foraging activity within 2–4 miles of their breeding sites (Bray 1986, Bray and Klebenow 1988), while others forage 25–30 miles from nest sites (Trost 1989). Some colony locations are used for nesting year after year, while others are used more sporadically depending on water conditions and the availability of food (Ryder 1967).

## **Mechanisms of Habitat Degradation**

## Water Quality and Water Diversion

White-faced ibis depend on healthy populations of aquatic invertebrate prey, which in turn may be greatly affected by surrounding land use. Urban areas can cause different and in some cases stronger effects than agricultural lands (Bury 1972, Moore and Palmer 2005). Residential developments typically result in increased runoff of hydrocarbons and of chemicals used for lawns and gardens, and increased stormwater volume (and associated increased depths and velocities) because of high coverage of impervious surfaces. Water diversions may also reduce the abundance of ibis prey. Decreased abundance of aquatic invertebrates has been shown to impact insectivorous birds in both observational field studies and controlled field experiments (Baxter et al. 2004, in press and in review).

## **DISTRIBUTION**

# **Information on CNDDB Occurrences**

When information was compiled for the NBHCP in 2001, there were seven known breeding colonies in California, all of which were considered extant. At that time, no colonies were known in the Natomas Basin, and the nearest known nesting occurrence was in Yolo County, north of Woodland. As of 2005, there are 15 known

occurrences in California, of which 13 are considered extant. At this time, CNDDB does not list white-faced ibis occurrences within one mile of the Natomas Basin.

#### Other Information on Distribution and Abundance in Natomas Basin

White-faced ibis are common winter foragers in the Natomas Basin (NBHCP), and 10,000 to 11,000 ibis have been estimated in the Sacramento Valley as a whole (Hickey and Shufford 1996, Thomas Reid Associates 2000).

# 4.7.2 Project Effects on Species

#### LONG-TERM EFFECTS ON HABITAT

# **Effect on Quantity of Habitat**

Neither the Greenbriar site nor the proposed reserves currently support potential nesting habitat for white-faced ibis. However, the proposed creation of 198 acres of marsh at the Natomas 130 and Spangler sites could provide nesting habitat. (The 2.7 acres of marsh proposed along Lone Tree Canal was not considered suitable nesting habitat because of its small size and the surrounding urban development.) Thus, the project could increase white-faced ibis nesting habitat in the Natomas Basin by up to 198 acres from conditions at the time of the NBHCP (2001).

The project's effects on the acreage of white-faced ibis foraging habitat are summarized in Table 4-8. The project would reduce the acreage of white-faced ibis foraging habitat in the Natomas Basin from conditions at the time of the NBHCP (2001). The proposed development at the Greenbriar site would reduce habitat by an estimated 172 acres from conditions in 2001. At the proposed Natomas 130 reserve, 28 acres of white-faced ibis habitat would be created from non-habitat (by converting 28 acres of non-rice crop to 14 acres of marsh and 14 acres of alfalfa). Thus, the project as a whole would yield a net loss of 144 acres of white-faced ibis habitat. (This total change does not include habitat at the mitigation site required by mitigation measure 6-13.2 of the DEIR for Swainson's hawk foraging habitat because the existing land cover type of that site is not known.)

| Table 4-8 Change in Acreage of White-faced Ibis Habitat at Project Sites and in the Natomas Basin |           |            |                         |                |                         |              |  |  |  |
|---|-----------|------------|-------------------------|----------------|-------------------------|--------------|--|--|--|
| Land Cover Type<br>Providing Habitat  | Future    | Chang      | ge at Each Project Site | - Total Change | <b>Future Condition</b> |              |  |  |  |
|   | Condition | Greenbriar | Natomas 130             | Spangler       | · Total Change          | with Project |  |  |  |
| Alfalfa   | 368       | -          | 14.2                    | 45.4           | 59.6                    | 428          |  |  |  |
| Canals  | 1,162     | -15.0      | 0.0                     | -1.4           | -16.4                   | 1,146        |  |  |  |
| Ponds & seasonally wet areas  | 2,259     | 2.7        | 14.2                    | 184            | 200.9                   | 2,460        |  |  |  |
| Rice  | 11,643    | -160.0     | -                       | -228           | -388.0                  | 11,255       |  |  |  |
| Total   | 15,432    | -172.4     | 28.4                    | 0              | -143.9                  | 15,288       |  |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

# **Effects on Quality of Habitat**

## Areas Adjacent to Developed Land or Highways

Potential impacts to white-faced ibis that forage near developed areas are discussed under *Mechanisms of Habitat Degradation*, above. They are primarily associated with canal and wetland habitats, but also forage in rice, and these habitats exist near the Greenbriar site.

# Habitat Alteration at Proposed Reserves and Mitigation Sites

A total of 316 acres of white-faced ibis habitat would be preserved. Of this preserved habitat, 190 acres (184 acres of rice and 6 acres of associated canals) would be enhanced by the conversion of rice to marsh at the proposed Spangler reserve. In addition, habitat values for white-faced ibis might be improved by habitat enhancement for Swainson's hawk at the proposed Natomas 130 and Spangler reserves (60 acres) and at the DEIR mitigation site (at least 49 acres to satisfy mitigation measure 6.13-2 of the DEIR).

# Effects on Connectivity

Habitat connectivity is of lesser importance to foraging ibis than to nesting or less mobile animals. Ibis survival is likely to be higher, however, in larger, more contiguous foraging habitat where prey is more abundant and the energetic costs of travel are decreased.

## **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Construction-related activities are unlikely to affect white-faced ibis because they do not nest in the vicinity of the Greenbriar and proposed reserve sites. Potential effects would be limited to displacement of birds foraging or roosting on the sites during the initial phases of construction when fields are graded. This would be largely akin to habitat loss, as the physical flight of the birds from these areas would not cause a significant effect.

## **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

Humans entering active colonies may cause partial or total desertion of the colony, particularly during nest-site selection, nest-building, and incubation (Ryder and Manry 1994). Because white-faced ibis do not currently nest in the Basin, the project is unlikely to affect human conflicts with this species. (Foraging ibis are less sensitive to disturbance than nesting birds.) Similarly, changes in predator communities associated with residential development would be unlikely to affect large ibis as much as smaller birds such as burrowing owls and loggerhead shrikes.

#### **OVERALL EFFECT ON POPULATION VIABILITY**

The Greenbriar project is not likely to affect the viability of the white-faced ibis population using the Natomas Basin. Currently, white-faced ibis uses the Natomas Basin only for winter foraging. The Greenbriar project would reduce the area of foraging habitat in the Natomas Basin (by 1%), and would at least partially offset this effect by preserving and enhancing 2% of foraging habitat in the Natomas Basin. The abundance of white-faced ibis, however, is not considered limited by the availability of winter foraging habitat, and the Greenbriar project would not substantially alter the quantity of winter foraging habitat in the Natomas Basin; thus, the project's effect on foraging habitat is not likely to alter the population viability of white-faced ibis. The project would also increase the acreage of nesting habitat by creating marsh, and this could lead to the establishment of a white-faced ibis nesting colony in the Natomas Basin. While not discounted, this effect was not considered likely.

# 4.8 ALEUTIAN CANADA GOOSE

# 4.8.1 SPECIES ECOLOGY

# HABITAT ASSOCIATIONS/REQUIREMENTS

# **Habitat Type**

Aleutian Canada geese (*Branta canadensis leucopareia*) winter in California's central valley. They forage primarily in pasture, corn, wheat, rice and other grain crops, wetlands, and grasslands, and typically prefer short

vegetation. Wintering geese roost in large ponds and lakes, flooded fields, and rice checks. Land cover types designated as Aleutian Canada goose habitat in the NBHCP include non-rice crops, pasture, and rice. While Aleutian Canada geese feed primarily on grasses and wetland sedges during their Alaskan summer, they forage primarily on seeds and agricultural grains while in California in fall and winter (NatureServe 2005).

# **Home Range Size and Movement**

Aleutian Canada geese nest in the western Aleutian Islands and migrate through coastal Oregon and northern California after the breeding season. Most wintering Aleutian Canada geese concentrate in the Modesto, Los Banos, and Colusa areas of California; the Natomas Basin may provide important foraging and roosting habitat during goose migration.

## **Mechanisms of Habitat Degradation**

Because Canada geese are particularly well-adapted to foraging in agricultural landscapes and may persist in small numbers in suburban parks, habitat loss is a greater issue for this species than habitat degradation. This species is similarly not dependent on animal prey populations or sensitive to the increases in small mammalian or corvid predators that typically occur near residential developments.

#### **DISTRIBUTION**

## Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 13 known occurrences in California, all of which were considered extant. At that time, no occurrences were known from the Natomas Basin. As of 2005, there are 10 known occurrences in California, all of which are considered extant. At this time, CNDDB does not list Aleutian Canada goose occurrences within one mile of the Natomas Basin.

## Other Information on Distribution and Abundance in Natomas Basin

Although Aleutian Canada geese have not been recorded in the Basin, its proximity to important wintering areas suggests that they are likely to forage and roost in the Basin during migration.

# 4.8.2 Project Effects on Species

## LONG-TERM EFFECTS ON HABITAT

## **Effect on Quantity of Habitat**

The project's effects on the acreage of Aleutian Canada goose habitat are summarized in Table 4-9. The project would reduce the acreage of Aleutian Canada goose habitat in the Natomas Basin from conditions at the time of the NBHCP (2001). The proposed development at the Greenbriar site would reduce habitat by an estimated 428 acres from conditions in 2001. At the proposed Spangler and Natomas 130 reserves, an additional 256 acres of goose habitat would be eliminated (by converting rice and non-rice crop to marsh). Thus, the project as a whole would yield a net loss of 684 acres of Aleutian Canada goose habitat.

| Table 4-9<br>Change in Acreage of Aleutian Canada Goose Habitat at Project Sites and in the Natomas Basin |   |   |  |   |   |  |  |  |  |
|---|---|---|--|---|---|--|--|--|--|
| Future  | Change at Each Project Site                   |   |  | Total Change  | Future Condition  |  |  |  |  |
| Condition   | Greenbriar                                    | Natomas 130   | Spangler   | - Total Change  | with Project  |  |  |  |  |
| 9,533   | -234.1  | -28.4   | -  | -262.6  | 9,270   |  |  |  |  |
| 494   | -33.8   | -   | -  | -33.8   | 460   |  |  |  |  |
| 11,643  | -160.0  | -   | -228   | -388.0  | 11,255  |  |  |  |  |
| 21,670  | -428.0  | -28.4   | -228   | -684.4  | 20,986  |  |  |  |  |
|   | Future<br>Condition<br>9,533<br>494<br>11,643 | Future Condition         Change Greenbriar           9,533         -234.1           494         -33.8           11,643         -160.0 | Future Condition         Change at Each Project Each Project Greenbriar           9,533         -234.1         -28.4           494         -33.8         -           11,643         -160.0         - | Future Condition         Change at Each Project Sites and Each Project Site           Greenbriar         Natomas 130         Spangler           9,533         -234.1         -28.4         -           494         -33.8         -         -           11,643         -160.0         -         -228 | Future Condition         Change at Each Project Sites and in the Nato           Greenbriar         Natomas 130         Spangler           9,533         -234.1         -28.4         -         -262.6           494         -33.8         -         -         -33.8           11,643         -160.0         -         -228         -388.0 |  |  |  |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

# **Effects on Quality of Habitat**

# Areas Adjacent Developed Land or Highways

As discussed above under Mechanisms of Habitat Degradation, the predominant impacts typically associated with areas adjacent to housing developments are unlikely to adversely affect Canada geese. This species is especially well-adapted to foraging in close proximity to humans.

# Habitat Alteration at Proposed Reserve and Mitigation Sites

Aleutian goose habitat probably would not be preserved or enhanced at the proposed reserve and DEIR mitigation sites. However, the 109 acres that would be actively managed to provide high quality foraging habitat for Swainson's hawk (at the proposed reserve and DEIR mitigation sties) might provide goose habitat values.

## Effects on Connectivity

Habitat connectivity is of lesser importance to foraging geese than to nesting or less mobile animals. Goose survival is likely to be higher, however, in larger, more contiguous foraging habitat where food is more abundant and the energetic costs of travel are decreased.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Construction-related activities are unlikely to affect Aleutian Canada geese because they do not nest in the vicinity of the Greenbriar and proposed reserve sites. Potential effects would be limited to displacement of birds foraging or roosting on the sites during the initial phases of construction when fields are graded. This effect is largely akin to temporary habitat loss.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

Because Aleutian Canada geese do not nest in the Basin, the project would not likely result in human conflicts with this species, other than the changes in habitat. Foraging geese are less sensitive to disturbance than nesting birds. Similarly, changes in predator communities associated with residential development would be unlikely to affect large geese as significantly as smaller birds such as burrowing owls and loggerhead shrikes.

## **OVERALL EFFECT ON POPULATION VIABILITY**

Currently, Aleutian Canada geese do not nest in the Natomas Basin, but do roost and forage in the Basin during seasonal migration to a limited extent. Although the Greenbriar Project would reduce the acreage of foraging

habitat in the Natomas Basin (by 3%), an effect on the population's viability is unlikely because the population's size is not considered to be limited by the quantity of foraging habitat available during migration and the Greenbriar project would not substantially alter the availability of this habitat, which is abundant in the Natomas Basin (approximately 21,000 acres).

## 4.9 BANK SWALLOW

## 4.9.1 SPECIES ECOLOGY

#### HABITAT ASSOCIATIONS/REQUIREMENTS

## **Habitat Type**

Bank swallows (*Riparia riparia*) nest in colonies in vertical banks, cliffs and bluffs that are typically along streams but occasionally near roads or gravel quarries. Nesting colonies may range in size from 10 to 1,500 pairs, and average 100–200 nesting pairs (NBHCP). Bank swallows forage in a variety of open habitats including wetlands, open water, grasslands, agricultural fields, shrublands, and open or riparian woodlands. Aquatic and flooded habitats provide the best foraging opportunities. Land cover types designated as bank swallow habitat in the NBHCP include alfalfa, canals, grassland, non-rice crops, pasture, ponds and seasonally wet areas, rice, and riparian. Swallows are almost exclusively insectivorous and catch their prey while flying.

## **Home Range Size and Movement**

Most breeding season foraging flights are within a kilometer (0.62 mile) of the nesting colony (Garrison 1999). Bank swallows are long-distance migrants and may use any available foraging habitat in the Basin during migration.

## **Mechanisms of Habitat Degradation**

### Bank Erosion and Water Diversion

The major contributors to bank swallow habitat degradation are flood and erosion control projects that apply riprap or reduce the slope of river banks and canals, rendering them unusable for nesting and reducing their habitat quality for roosting and foraging (Garrison et al. 1987, Small 1994). Diversion of water may affect bank swallows if it results in the dewatering of canals or reduction of aquatic habitat for larval insects.

#### Water Quality and Runoff

Aquatic communities may be greatly affected by surrounding land use. Urban areas can cause different and in some cases stronger effects than agricultural lands (Bury 1972, Moore and Palmer 2005). Residential developments typically result in increased runoff of hydrocarbons and of chemicals used for lawns and gardens, and increased stormwater volume (and associated increases in depths and velocities) because of high coverage of impervious surfaces. Decreased abundance of aquatic invertebrates has been shown to impact insectivorous birds in both observational field studies and controlled field experiments (Baxter et al. 2004, in press and in review).

#### Predation and Nest Disturbance

Although predation of most birds increases in proximity to human settlement, bank swallows are largely protected from human-associated predators because of the cliff locations of their nests. These aerial hunters are also largely protected from human-associated predators while foraging because they spend relatively very little time foraging from perches or among vegetation. Kestrels are the primary predators of this species while foraging; snakes are

most common while nesting. Bank swallows are typically tolerant of human activity near nesting colonies, if humans do not attempt to climb the nest banks (Garrison 1999).

#### **DISTRIBUTION**

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 171 known occurrences in California, of which 170 were considered extant. At that time, no nesting colonies were known in the Natomas Basin. As of 2005, there are 176 known occurrences in California, of which 171 are considered extant. At this time, CNDDB does not list bank swallow occurrences within one mile of the Natomas Basin.

#### Other Information on Distribution and Abundance in Natomas Basin

Although no nesting colonies are known in the Basin, the area provides potential foraging habitat for migrating swallows.

## 4.9.2 Project Effects on Species

## **LONG-TERM EFFECTS ON HABITAT**

## **Effect on Quantity of Habitat**

The project would not affect bank swallow nesting habitat, as bank swallow nesting colonies do not exist at the Greenbriar or proposed reserve sites, nor would nesting habitat be created, enhanced or preserved at the proposed reserves.

The project's effects on the acreage of bank swallow foraging habitat are summarized in Table 4-10. The project would reduce the acreage of bank swallow foraging habitat in the Natomas Basin from conditions at the time of the NBHCP (2001). The proposed development at the Greenbriar site would reduce habitat by an estimated 414 acres from conditions in 2001. At the proposed Natomas 130 and Spangler reserves, habitat acreages would be increased by about 20 acres. Thus, the project as a whole would yield a net loss of 394 acres of bank swallow habitat.

| Table 4-10 Change in Acreage of Bank Swallow Habitat at Project Sites and in the Natomas Basin |                     |                             |             |          |                |                  |  |
|--|---------------------|-----------------------------|-------------|----------|----------------|------------------|--|
| Land Cover Type  | Future<br>Condition | Change at Each Project Site |             |          | - Total Change | Future Condition |  |
| Providing Habitat  |                     | Greenbriar                  | Natomas 130 | Spangler | - Total Change | with Project     |  |
| Alfalfa  | 368                 | -                           | 14.2        | 45.4     | 59.6           | 428              |  |
| Canals   | 1,162               | -15.0                       | 0.0         | -1.4     | -16.4          | 1,146            |  |
| Grassland  | 284                 | 26.5                        | -           | -        | 26.5           | 311              |  |
| Non-rice crops   | 9,533               | -234.1                      | -28.4       | -        | -262.6         | 9,270            |  |
| Pasture  | 494                 | -33.8                       | -           | -        | -33.8          | 460              |  |
| Ponds & seasonally wet areas   | 2,259               | 2.7                         | 14.2        | 184.0    | 200.9          | 2,460            |  |
| Rice   | 11,643              | -160.0                      | -           | -228.0   | -388.0         | 11,255           |  |
| Riparian   | 91                  | 0.0                         | 0.0         | -        | 0.0            | 91               |  |
| Total  | 25,834              | -413.8                      | 0.0         | 20.2     | -393.6         | 25,420           |  |

Note: Acreages are based on 2001 land cover mapping used to evaluate future condition resulting from the NBHCP and future land cover proposed at project sites.

#### **Effects on Quality of Habitat**

## Areas Adjacent to Developed Land or Highways

As discussed above under Mechanisms of Habitat Degradation, the predominant effects typically associated with areas adjacent to housing developments are unlikely to negatively affect bank swallows. Effects on water quality and canal management, however, could potentially affect bank swallows.

## Habitat Alteration at Proposed Reserve and Mitigation Sites

At least 345 acres of bank swallow habitat would be preserved and enhanced at the proposed reserves and at the mitigation site required by mitigation measure 6.13-2 of the DEIR. At the Spangler site, rice habitat would be converted to marsh, preserved, and managed to provide habitat values, in particular for giant garter snake. At the Spangler site, rice would also be converted to upland habitat. This upland habitat, as well as upland habitat at the Natomas 130 and the DEIR mitigation site, would be managed to provide high quality foraging habitat for Swainson's hawk. At all of these sites, habitat values for bank swallow are likely to increase as a result of the proposed management. However, because the benefits of such management for bank swallows have not been documented, a moderate level of uncertainty exists regarding their magnitude.

## Effects on Connectivity

Because bank swallows do not nest in the Basin, connectivity is of less concern for this species than for less mobile species or species with limited foraging distances from breeding sites. Larger patches of more contiguous habitat are likely to be of greater value to migrating swallows, by providing more abundant food with the lower energetic cost of foraging in a contiguous area.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Construction-related activities are unlikely to affect bank swallows because they do not nest in the vicinity of the Greenbriar and proposed reserve sites. Potential effects would be limited to displacement of birds foraging or roosting on the sites during the initial phases of construction when fields are graded. This impact is largely akin to temporary habitat loss.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

Direct human-wildlife conflicts are unlikely to be of concern for bank swallows in the Natomas Basin. Habitat quantity and quality are the primary concerns for this species.

#### **OVERALL EFFECT ON POPULATION VIABILITY**

Although the Greenbriar project would affect land suitable for bank swallow foraging (eliminating 394 acres and preserving and enhancing 345 acres), none of these lands are near (i.e., within a mile) bank swallow nesting habitat. Currently, bank swallows are not nesting near the Natomas Basin. Near the Natomas Basin, most of the bank length of the Sacramento River is not suitable for bank swallow nesting, in part because of extensive riprap (USFWS 2003). Even if bank swallow colonies established along the Sacramento River in the future, the project and mitigation sites are not within a mile of the river, and thus would not provide important foraging habitat for colonies along the river. Although these lands may provide foraging habitat to migrating swallows, habitat availability during migration is not considered to limit the abundance of this population, and large areas of such habitat (over 25,000 acres) would remain in the future condition of the Natomas Basin with the Greenbriar project. Therefore, the Greenbriar project is unlikely to alter the viability of bank swallow populations using the Natomas Basin.

## 4.10 VALLEY ELDERBERRY LONGHORN BEETLE

## 4.10.1 SPECIES ECOLOGY

### HABITAT ASSOCIATIONS/REQUIREMENTS

## **Habitat Type**

Valley elderberry longhorn beetles (*Desmocerus californicus dimorphus*) are dependent on elderberry bushes, which primarily occur in riparian areas. Small elderberry patches are also found in some oak groves and rural residential areas (NBHCP). The NBHCP lists riparian as the only land cover type that provides habitat for this species.

## **Home Range Size and Movement**

Dispersal of valley elderberry longhorn beetles is extremely limited. Many adults live their entire lives on their original host plants and do not disperse at all. Dispersing individuals typically limit travel in their home drainages, limiting the ability of the species to colonize fragmented habitat (Collinge et al. 2001).

## **Mechanisms of Habitat Degradation**

Elderberry habitat is degraded by fragmentation, pesticide and herbicide use, exotic species invasion, and hydrological alteration such as flood management, channel maintenance, and increased water diversions for urban and agricultural development (USFWS 1984; Huxel 2000; Collinge et al. 2001).

#### **DISTRIBUTION**

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 168 known occurrences in California, all of which were considered extant. At that time, "several" occurrences were known along the southern and western edges of the Natomas Basin, along the American and Sacramento rivers. As of 2005, there are 190 known occurrences in California, all of which are considered extant. At this time, two occurrences are known in the Natomas Basin and six additional occurrences are known within a mile of the Basin. All eight of these occurrences are considered extant. CNDDB does not list valley elderberry longhorn beetle occurrences within one mile of the Greenbriar site; CNDDB lists one VELB occurrence within one mile of a proposed reserve.

#### Other Information on Distribution and Abundance in Natomas Basin

The TNBC Biological Effectiveness Monitoring report concurs with the CNDDB to list eight extant VELB occurrences in the Basin, none of which are within a mile of the Greenbriar site, and one of which is within a mile of a proposed reserve.

## 4.10.2 Project Effects on Species

#### **LONG-TERM EFFECTS ON HABITAT**

#### **Effect on Quantity of Habitat**

The project will not affect the quantity of elderberry habitat available to the beetle, as elderberry shrubs are not present in the vicinity of the Greenbriar or proposed reserve sites.

#### **Effects on Quality of Habitat**

## Areas Adjacent to Developed Land or Highways

As no elderberry shrubs exist in proximity to the Greenbriar site, the gradient of urban influence within 800 feet of the Greenbriar site will not affect the quality of VELB habitat.

#### Enhancement at Reserves

The planting of elderberry shrubs is not currently planned at the proposed reserves. However, an acre of riparian habitat exists on the Natomas 130 parcel and may be suitable for shrub planting in the future.

## Effects on Connectivity

Because of the beetle's limited dispersal capability, habitat connectivity is critical for the colonization of unoccupied shrubs and the maintenance of genetic diversity. However, because all of the Basin's known VELB occurrences are located in riparian habitat near the Sacramento River, the project would not affect connectivity for this species. The proposed Natomas 130 reserve is located along the Sacramento River and would contribute to the preservation of contiguous riparian habitat along the river corridor.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

Construction-related activities for the project are unlikely to affect this species because its habitat does not exist at the Greenbriar and Spangler sites and may not be present at the Natomas 130 site. To avoid and minimize any potential impacts at the Natomas 130 site, preconstruction surveys for elderberry shrubs would be conducted according to USFWS guidelines (USFWS 1999b). If elderberry shrubs are found, they would be preserved on site unless their preservation would significantly inhibit other habitat restoration objectives on site. Following USFWS guidelines, elderberry shrubs would be avoided during habitat construction with a 100-foot construction buffer. If avoidance is not possible, shrub loss would be mitigated by transplanting the shrubs during their dormant season and planting a specified number of seedlings.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

Human-wildlife conflicts for this species would not be affected by the project because elderberry habitat does not exist on site. Although VELB and elderberry shrubs are not known to be present on the proposed reserves, preservation of the Natomas 130 parcel may reduce human conflicts with habitat in the Sacramento River riparian corridor.

#### **OVERALL EFFECT ON POPULATION VIABILITY**

VELB is not known from the vicinity of the Greenbriar site or the proposed reserve sites. A small area of riparian vegetation, which is potentially suitable habitat for this species, exists at the Natomas 130, and would be preserved by the project. It is not known if elderberry bushes are present in this riparian vegetation, and the draft restoration plan does not include the planting of elderberry bushes. Thus, the preservation of this riparian vegetation would be a very small potential benefit to VELB that would not be sufficient to alter its population viability.

## 4.11 CALIFORNIA TIGER SALAMANDER

## 4.11.1 SPECIES ECOLOGY

### HABITAT ASSOCIATIONS/REQUIREMENTS

#### **Habitat Type**

California tiger salamanders (*Ambystoma californiense*) require two major habitat components: aquatic breeding sites and terrestrial aestivation or refuge sites. Tiger salamanders breed primarily in vernal pools and other ephemeral rainwater ponds (Loredo et al. 1996). They will occasionally breed in stockponds, reservoirs and small lakes, but fail to reproduce in water bodies that support predatory fish or bullfrogs (Stebbins 1972, Zeiner et al. 1988). The highest quality breeding habitat for tiger salamanders exists in large, contiguous vernal pool complexes in a grassland matrix with pools that last for more than 10 weeks (Jennings and Hayes 1994).

California tiger salamanders spend the majority of their lives in upland habitats within one mile (1.6 km) of aquatic breeding areas (Center for Biological Diversity 2001). These upland habitats are essential for salamander foraging, aestivation, migration, and dispersal. Upland habitats used by migrating salamanders include grassland, pasture, and open woodlands. The NBHCP lists ponds and seasonally wet areas as the only land cover type providing tiger salamander habitat because these upland habitats will only be used by salamanders when in close proximity to aquatic breeding areas. Tiger salamanders depend on burrows of small mammals such as California ground squirrels and Botta's pocket gopher for shelter during aestivation.

## **Home Range Size and Movement**

California tiger salamanders typically range within 2,200 feet (0.7 km) of breeding habitat during the breeding season (Trenham and Shaffer). During migration, however, they have been recorded as far as one mile (1.6 km) from aquatic habitats (Center for Biological Diversity 2001).

#### **Mechanisms of Habitat Degradation**

Tiger salamander habitat is frequently degraded by roads, buildings, and other barriers to migration (Shaffer and Fisher 1991; Shaffer and Stanley 1992; Barry and Shaffer 1994). Erosion because of grading for nearby developments can degrade breeding wetlands by increasing sedimentation. Tiger salamanders are also sensitive to pesticides, herbicides and fertilizers associated with suburban lawn care and agriculture. Burrowing mammal control programs and the introduction of predatory bullfrogs and nonnative fishes have also contributed to declines in tiger salamander populations (Jennings and Hayes 1994).

#### **DISTRIBUTION**

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 465 known occurrences in California, all of which were considered extant. At that time, no occurrences were known from the Natomas Basin. As of 2005, there are 793 known occurrences in California, of which 738 are considered extant. At this time, CNDDB does not list California tiger salamander occurrences within one mile of the Natomas Basin.

#### Other Information on Distribution and Abundance in Natomas Basin

California tiger salamanders have not been recorded in the Natomas Basin.

## 4.11.2 Project Effects on Species

#### LONG-TERM EFFECTS ON HABITAT

## **Effect on Quantity of Habitat**

The project would have no effect on the quantity of California tiger salamander habitat. Suitable breeding habitat does not exist in the maximum salamander dispersal distance from these sites. Restoration plans for the proposed reserves do not include the creation of tiger salamander habitat.

## **Effects on Quality of Habitat**

The project would have no effect on the quality of California tiger salamander habitat, as salamander habitat does not exist in the vicinity of the Greenbriar and proposed reserve sites.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

The project would have no effect on tiger salamanders during construction-related activities, as salamander habitat does not exist in the vicinity of the Greenbriar and proposed reserve sites.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

The project would have no effect on human-wildlife conflicts relating to tiger salamanders, because salamander habitat does not exist in the vicinity of the Greenbriar and proposed reserve sites.

#### **OVERALL EFFECT ON POPULATION VIABILITY**

California tiger salamander is not known from the vicinity of the Greenbriar site or the proposed reserve sites, or adjacent lands. Potentially suitable habitat for this species does not exist at or in the vicinity of the Greenbriar and proposed reserve sites. Therefore, the Greenbriar project would cause no effects on the population viability of California tiger salamander.

## 4.12 WESTERN SPADEFOOT TOAD

## 4.12.1 SPECIES ECOLOGY

## HABITAT ASSOCIATIONS/REQUIREMENTS

#### **Habitat Type**

Western spadefoot toads (*Scaphiopus hammondii*) breed in shallow, seasonal wetlands in a matrix of grassland, chaparral or woodland habitat, and are rarely found in creeks, drainages, and ponds. Grassland vernal pools provide optimal spadefoot habitat; the toads attach their eggs to rain pool vegetation and burrow underground after the pools become dry (Stebbins 1972). The NBHCP lists ponds and seasonally wet areas as the only land cover type that provides habitat for this species. Adults feed on insects, worms, and other invertebrates; tadpoles feed on invertebrates and algae.

## **Home Range Size and Movement**

During the breeding season, western spadefoot toads rarely travel more than several meters from breeding pools (Jennings and Hayes 1994). Outside of the breeding season, data are not available on the dispersal distances, movement patterns, or colonization abilities of this species (Jennings and Hayes 1994).

## **Mechanisms of Habitat Degradation**

The project would not degrade habitat for this species, as its habitat does not exist in the vicinity of the Greenbrian proposed reserve sites.

#### DISTRIBUTION

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 173 known occurrences in California, of which 172 were considered extant. At that time, no occurrences were known from the Natomas Basin. As of 2005, there are 308 known occurrences in California, of which 306 are considered extant. At this time, CNDDB does not list western spadefoot occurrences within one mile of the Natomas Basin.

#### Other Information on Distribution and Abundance in Natomas Basin

Western spadefoot toads have not been recorded in the Natomas Basin.

## 4.12.2 Project Effects on Species

## **LONG-TERM EFFECTS ON HABITAT**

#### **Effect on Quantity of Habitat**

The project would have no effect on the quantity of western spadefoot habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites. Restoration plans for the proposed reserves do not include the creation of western spadefoot habitat.

## **Effects on Quality of Habitat**

The project would have no effect on the quality of western spadefoot habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites. Restoration plans for the proposed reserves do not include the creation of western spadefoot habitat.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

The project would have no effect on spadefoot toads during construction-related activities, because spadefoot habitat does not exist in the vicinity of the Greenbriar or proposed reserve sites.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

The project would have no effect on human-wildlife conflicts relating to spadefoot toads, because spadefoot habitat does not exist in the vicinity of the Greenbriar and proposed reserve sites.

## **OVERALL EFFECT ON POPULATION VIABILITY**

Western spadefoot toad is not known from the vicinity of the Greenbriar site or the proposed reserve sites, or adjacent lands. Potentially suitable habitat for this species does not exist at or in the vicinity of the Greenbriar and proposed reserve sites. Therefore, the Greenbriar project would cause no effects on the population viability of western spadefoot toad.

## 4.13 VERNAL POOL FAIRY SHRIMP

## 4.13.1 Species Ecology

#### HABITAT ASSOCIATIONS/REQUIREMENTS

#### **Habitat Type**

Vernal pool fairy shrimp (*Branchinecta lynchi*) inhabit vernal pools (79% of observations) and other seasonal wetlands (Helm 1998). Although they may occur in larger, deeper pools, vernal pool fairy shrimp are typically found in pools less than 2,200 square feet and less than 2 inches deep (Helm 1998). The NBHCP lists ponds and seasonally wet areas as the only land cover type that provides habitat for this species.

## **Mechanisms of Dispersal**

Vernal pool fairy shrimp rely on wind and motile species such as birds, mammals, and amphibians for their dispersal. Shrimp eggs are transported in the stomachs of waterfowl and amphibians, and in small clumps of soil attached to mammalian hooves and hair, bird feet, and feathers. Dispersal distances have not been measured, but will likely equate with movement distances of the egg-transporting animals (Silveira 1998 cited in Bay Area O&M). As such, connectivity of upland and aquatic habitat between vernal pools will benefit shrimp dispersal by increasing the opportunities for egg transport by mammals and amphibians. Dispersal may continue between disconnected pools through avian transport.

## **Mechanisms of Habitat Degradation**

The project would not degrade habitat for this species, because its habitat does not exist in the vicinity of the Greenbriar or proposed reserve sites.

#### **DISTRIBUTION**

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 270 known occurrences in California, all of which were considered extant. At that time, no occurrences were known from the Natomas Basin. As of 2005, there are 366 known occurrences in California, all of which are considered extant. At this time, two occurrences are known in the Natomas Basin and eight additional occurrences are known within one mile of the Basin. All ten of these occurrences are considered extant, and are located near the eastern border of the Basin. At this time, CNDDB does not list vernal pool fairy shrimp occurrences within one mile of the Greenbriar or proposed reserve sites.

#### Other Information on Distribution and Abundance in Natomas Basin

Vernal pool fairy shrimp were not detected by Natomas Basin Conservancy surveys, and no additional information is available regarding their distribution in the Basin.

## 4.13.2 Project Effects on Species

#### **LONG-TERM EFFECTS ON HABITAT**

## **Effect on Quantity of Habitat**

The project would have no effect on the quantity of vernal pool fairy shrimp habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites. Restoration plans for the proposed reserves do not include the creation of vernal pool fairy shrimp habitat.

## **Effects on Quality of Habitat**

The project would have no effect on the quality of vernal pool fairy shrimp habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites. Restoration plans for the proposed reserves do not include the creation of vernal pool fairy shrimp habitat.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

The project would have no effect on vernal pool fairy shrimp during construction-related activities, because habitat for this species does not exist in the vicinity of the Greenbriar or proposed reserve sites.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

The project would have no effect on the quantity of vernal pool fairy shrimp habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites.

#### **OVERALL EFFECT ON POPULATION VIABILITY**

Vernal pool fairy shrimp is not known from the vicinity of the Greenbriar site or the proposed reserve sites, or adjacent lands. Potentially suitable habitat for this species does not exist at or in the vicinity of the Greenbriar and proposed reserve sites. Therefore, the Greenbriar project would cause no effects on the population viability of vernal pool fairy shrimp.

## 4.14 VERNAL POOL TADPOLE SHRIMP

#### 4.14.1 Species Ecology

#### HABITAT ASSOCIATIONS/REQUIREMENTS

#### **Habitat Type**

Vernal pool tadpole shrimp (*Lepidurus packardi*) are found primarily in vernal pools; they inhabit other seasonal wetlands to a limited extent. They occupy vernal pools with a variety of depths and water volumes, and with areas ranging from 20 square feet to over 3,750,000 square feet (Helm 1998). The NBHCP lists ponds and seasonally wet areas as the only land cover type that provides habitat for this species.

#### **Mechanisms of Dispersal**

Vernal pool tadpole shrimp rely on wind and motile species such as birds, mammals, and amphibians for their dispersal. Shrimp eggs are transported in the stomachs of waterfowl and amphibians, and in small clumps of vernal pool soil attached to mammalian hooves and hair, bird feet, and feathers. Dispersal distances have not been measured, but will likely equate with movement distances of the egg-transporting animals (Silveira 1998 cited in

Bay Area O&M). As such, connectivity of upland and aquatic habitat between vernal pools will benefit shrimp dispersal by increasing the opportunities for egg transport by mammals and amphibians. Dispersal may continue between disconnected pools through avian transport.

## **Mechanisms of Habitat Degradation**

The project would not degrade habitat for this species, because its habitat does not exist in the vicinity of the Greenbriar or proposed reserve sites.

#### **DISTRIBUTION**

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 154 known occurrences in California, of which 153 were considered extant. At that time, no occurrences were known from the Natomas Basin. As of 2005, there are 209 known occurrences in California, of which 208 are considered extant. At this time, one occurrence is known in the Natomas Basin and one additional occurrence is known within one mile of the Basin. Both of these occurrences are considered extant, and are located near the eastern border of the Basin. At this time, CNDDB does not list vernal pool tadpole shrimp occurrences within one mile of the Greenbriar or proposed reserve sites.

#### Other Information on Distribution and Abundance in Natomas Basin

Vernal pool tadpole shrimp were not detected by Natomas Basin Conservancy surveys, and no additional information is available regarding their distribution in the Basin.

## 4.14.2 Project Effects on Species

### **LONG-TERM EFFECTS ON HABITAT**

#### **Effect on Quantity of Habitat**

The project would have no effect on the quantity of vernal pool tadpole shrimp habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites. Restoration plans for the proposed reserves do not include the creation of vernal pool tadpole shrimp habitat.

#### **Effects on Quality of Habitat**

The project would have no effect on the quality of vernal pool tadpole shrimp habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites. Restoration plans for the proposed reserves do not include the creation of vernal pool tadpole shrimp habitat.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

The project would have no effect on vernal pool tadpole shrimp during construction-related activities, because habitat for this species does not exist in the vicinity of the Greenbriar and proposed reserve sites.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

The project would have no effect on human conflicts with vernal pool tadpole shrimp, because habitat for this species does not exist in the vicinity of the Greenbriar or proposed reserve sites.

#### **OVERALL EFFECT ON POPULATION VIABILITY**

Vernal pool tadpole shrimp is not known from the vicinity of the Greenbriar site or the proposed reserve sites, or adjacent lands. Potentially suitable habitat for this species does not exist at or in the vicinity of the Greenbriar and proposed reserve sites. Therefore, the Greenbriar project would cause no effects on the population viability of vernal pool tadpole shrimp.

## 4.15 MIDVALLEY FAIRY SHRIMP

## 4.15.1 SPECIES ECOLOGY

#### HABITAT ASSOCIATIONS/REQUIREMENTS

## **Habitat Type**

Midvalley fairy shrimp (*Branchinecta mesovallensis* n. sp.) appear to be vernal pool obligates, as 93% of observations have occurred in vernal pools and the remaining 7% have occurred in vernal swales (Helm 1998). This species is associated with the smallest (less than 2,200 square feet) and most ephemeral (average depth of 4 inches) vernal pools (Helm 1998). The NBHCP lists ponds and seasonally wet areas as the only land cover type that provides habitat for this species.

## **Mechanisms of Dispersal**

Midvalley fairy shrimp rely on wind and motile species such as birds, mammals, and amphibians for their dispersal. Shrimp eggs are transported in the stomachs of waterfowl and amphibians, and in small clumps of vernal pool soil attached to mammalian hooves and hair, bird feet, and feathers. Dispersal distances have not been measured, but will likely equate with movement distances of the egg-transporting animals (Silveira 1998 cited in Bay Area O&M). As such, connectivity of upland and aquatic habitat between vernal pools will benefit shrimp dispersal by increasing the opportunities for egg transport by mammals and amphibians. Dispersal may continue between disconnected pools through avian transport.

#### **Mechanisms of Habitat Degradation**

The project would not degrade habitat for this species, because its habitat does not exist in the vicinity of the Greenbriar or proposed reserve sites.

#### DISTRIBUTION

#### Information on CNDDB Occurrences

When information was compiled for the NBHCP in 2001, there were 14 known occurrences in California, all of which were considered extant. At that time, no occurrences were known from the Natomas Basin. As of 2005, there are 62 known occurrences in California, all of which are considered extant. At this time, CNDDB does not list midvalley fairy shrimp occurrences within one mile of the Natomas Basin.

#### Other Information on Distribution and Abundance in Natomas Basin

Midvalley fairy shrimp have not been recorded in the Natomas Basin.

## 4.15.2 Project Effects on Species

#### LONG-TERM EFFECTS ON HABITAT

## **Effect on Quantity of Habitat**

The project would have no effect on the quantity of midvalley fairy shrimp habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites. Restoration plans for the proposed reserves do not include the creation of midvalley fairy shrimp habitat.

## **Effects on Quality of Habitat**

The project would have no effect on the quality of midvalley fairy shrimp habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites. Restoration plans for the proposed reserves do not include the creation of midvalley fairy shrimp habitat.

#### **EFFECTS OF CONSTRUCTION-RELATED ACTIVITIES**

The project would have no effect on midvalley fairy shrimp during construction-related activities, because habitat for this species does not exist in the vicinity of the Greenbriar and proposed reserve sites.

#### **EFFECTS OF HUMAN-WILDLIFE CONFLICTS**

The project would have no effect on the quantity of midvalley fairy shrimp habitat, because habitat for this species does not currently exist in the vicinity of the Greenbriar or proposed reserve sites.

#### **OVERALL EFFECT ON POPULATION VIABILITY**

Midvalley fairy shrimp is not known from the vicinity of the Greenbriar site or the proposed reserve sites, or adjacent lands. Potentially suitable habitat for this species does not exist at or in the vicinity of the Greenbriar and proposed reserve sites. Therefore, the Greenbriar project would cause no effects on the population viability of midvalley fairy shrimp.

## 4.16 COVERED PLANT SPECIES

Of the seven plant species covered by the NBHCP (Table 4-11), the Greenbriar project would not affect the five vernal pool-associated species because these species are not known to occur in the vicinity of the Greenbriar or proposed reserve sites (or in the Natomas Basin), nor is suitable habitat present at or near these sites. These plant species are: Boggs Lake hedge-hyssop, Sacramento Orcutt grass, slender Orcutt grass, Colusa grass and legenere. The other two covered plant species (delta tule pea and Sanford's arrowhead) are not known to occur at the Greenbriar or the proposed reserve sites, or in the Natomas Basin (Table 4-1), but potentially suitable habitat for these species does occur at or near some of these sites, which have not been surveyed for these species. Therefore, the possibility that the project could affect these species cannot be discounted; thus, the DEIR mitigation includes a rare plant survey requirement and the applicable avoidance and minimization measures from the NBHCP for these species. The project also would eliminate approximately 16 acres of canal at the Greenbriar site and would create approximately 201 acres of marsh at the proposed reserves. Thus, overall, the project would increase the acreage of potentially suitable habitat for these species (i.e., marsh and canal habitats) in the Natomas Basin by about 184 acres (or about 4%). Nonetheless, because these species are not known to occur in the Natomas Basin, the project probably would not alter the viability of any of their populations.

| Table 4-11 Primary Habitats and Distribution of Plant Species Covered by the NBHCP |   |  |  |  |  |  |  |
|--|---|--|--|--|--|--|--|
| Species  | Growth form   | Primary Habitat(s)   | Distribution   |  |  |  |  |
| Delta tule pea (Lathyrus jepsonii var. jepsonii)                                   | Biennial-perennial,<br>herbaceous vine in the<br>pea family (Fabaceae)  | Riparian scrub, marsh<br>(primarily tidal, fresh or<br>brackish)   | Alameda, Contra Costa, Napa,<br>Sacramento, San Joaquin, and Solano<br>Counties; not known from the Natomas<br>Basin   |  |  |  |  |
| Sanford's arrowhead (Sagittaria sanfordii)   | Perennial, rhizomatous<br>aquatic with emergent<br>leaves, in the water-<br>plantain family<br>(Alismataceae) | Marsh and other shallow freshwater habitats  | Butte, Del Norte, Fresno, Kern, Merced,<br>Orange, Sacramento, Shasta, San<br>Joaquin, and Tehama Counties; not<br>known from the Natomas Basin                                  |  |  |  |  |
| Bogg's Lake hedge-<br>hyssop<br>(Gratiola heterosepala)                            | Small semi-aquatic<br>annual, up to 4 inches in<br>height, in the figwort<br>family<br>(Scrophulariaceae)     | Vernal pools and swallow lake margins  | Fresno, Lake, Lassen, Madera, Merced,<br>Modoc, Placer, Sacramento, San Joaquin<br>Shasta, Siskiyou, Solano, and Tehama<br>Counties; not known from the Natomas<br>Basin         |  |  |  |  |
| Sacramento Orcutt grass (Orcuttia viscida)   | Annual in the grass family (Poaceae)  | Vernal pools (generally larger, deeper pools)  | Sacramento County; not known from the Natomas Basin  |  |  |  |  |
| Slender Orcutt grass<br>(Orcuttia tenuis)  | Annual in the grass family (Poaceae)  | Vernal pools (generally larger, deeper pools)  | Butte, Lake, Lassen, Modoc, Plumas,<br>Sacramento, Shasta, Siskiyou, and<br>Tehama Counties; not known from the<br>Natomas Basin   |  |  |  |  |
| Colusa grass<br>(Neostapfia colusana)  | Annual in the grass family (Poaceae)  | Vernal pools (generally larger, deeper pools)  | Colusa, Merced, Solano, Stanislaus, and<br>Yolo Counties; not known from the<br>Natomas Basin or Sacramento County   |  |  |  |  |
| Legenere Annual, in the bellflower (Legenere limosa) family (Campanulaceae)        |   | Vernal pools and swales,<br>seasonal marshes, artificial<br>ponds, floodplains of<br>intermittent streams, and<br>other seasonally inundated<br>habitats | Lake, Napa, Placer, Sacramento, San<br>Joaquin, San Mateo, Santa Clara, Shasta,<br>Solano, Sonoma, Stanislaus, Tehama, and<br>Yuba Counties; not known from the<br>Natomas Basin |  |  |  |  |

# 5 POTENTIAL EFFECTS ON THE CONSERVATION STRATEGY OF THE NBHCP

Based on the analyses presented in sections 3 (Alteration of Population and Habitat Attributes by the Greenbriar Project) and 4 (Potential Effects of the Greenbriar Project on Covered Species), this section summarizes the effect of the Greenbriar project on the conservation strategy of the NBHCP that is described is section IV.C of the NBHCP. Overall, the Greenbriar project (with the DEIR mitigation) would not reduce the effectiveness of the NBHCP's conservation strategy because it would not alter the basis of this conservation strategy. In Section IV.C.1 (pages IV 5-15), the NBHCP describes the basis of the key components of the NBHCP's conservation strategy and how these components provide effective mitigation for 17,500 acres of urban development. These components are:

- ▶ Basis for 0.5 to 1 mitigation ratio (Section IV.C.1.a),
- ▶ Preparation of site specific management plans (Section IV.C.1.b),
- ▶ Buffers within the reserve lands (Section IV.C.1.c),
- ► Connectivity (Section IV.C.1.d),
- ► Foraging habitat (Section IV.C.1.e), and
- ▶ 2,500-acre/400-acre minimum habitat block size requirements (Section IV.C.1.f).

The effects of the Greenbriar project on each of these components is described in the following sections, and then these effects are synthesized, along with the effects on population viability of the covered species (see chapters 3 and 4) as the overall effect of the Greenbriar project on the effectiveness of the NBHCP's conservation strategy.

## 5.1 BASIS FOR 0.5 TO 1 MITIGATION RATIO

On pages IV-6 and IV-7, the NBHCP describes eight key considerations for determining that the 0.5 to 1 mitigation ratio mitigates the impacts of incidental take authorized under the NBHCP. These eight key considerations are summarized below.

- 1. Overall, reserves will provide greater habitat value than the agricultural land that will be converted to urban development. (This consideration overlaps with other considerations.)
- 2. Much of the land to be developed is either of limited value as habitat or serves as habitat to a limited number of species.
- 3. For several wetland and vernal pool-associated species, reserves will provide opportunities for reintroduction to the Basin.
- 4. Reserves would provide habitat for migratory bird species that have limited habitat in the Basin.
- 5. Reserves would be managed to minimize take related to agricultural and land management activities.
- 6. Reserves would provide permanent habitat for covered species.
- 7. Reserves would be monitored and adaptively managed.
- 8. Reserves would be consolidated into large blocks of habitat.

Because the Greenbriar project would not alter the habitat value of land authorized for development under the NBHCP, and would not adversely affect the habitat value of TNBC reserves established under the NBHCP, the project would not affect this basis for the 0.5:1 mitigation ratio for the 17,500 acres of urban development

authorized by the NBHCP. Similarly, the project would not adversely affect the monitoring and management of reserves, or opportunities to consolidate reserves into large blocks of habitat. (The project's effects on the habitat quality of existing reserves, water availability at TNBC reserves, and opportunities to establish additional TNBC reserves are evaluated in sections 3.7, 3.8, and 3.9, respectively.)

Although not explicitly stated in section IV of the NBHCP, the 0.5:1 mitigation ratio is related to other elements of the conservation strategy (e.g., maintenance of habitat connectivity). With the DEIR mitigation, the Greenbriar project would not adversely affect these other elements of the conservation strategy, and thus the project would not affect this basis of the 0.5:1 mitigation ratio.

The 0.5:1 mitigation ratio of the NBHCP is also related to the habitat values provided by other lands in the Natomas Basin (outside of reserves established through the NBHCP). With the DEIR mitigation, the Greenbriar project would not cause a net loss in habitat values for giant garter snake and Swainson's hawk in the Natomas Basin, and thus the project would not affect this basis of the 0.5:1 mitigation ratio.

In order to be compatible with the conservation strategy of the NBHCP, the Greenbriar project has had to propose a conservation strategy that differs in some regards from the NBHCP conservation strategy. These differences include a larger mitigation ratio, greater emphasis on measures to maintain connectivity, and more extensive restoration and enhancement of preserved land. The implementation of the Greenbriar conservation strategy will likely be more costly (on a per acre basis) than the NBHCP conservation strategy, and thus will likely require a greater endowment for NBHCP reserves.

## 5.2 PREPARATION OF SITE SPECIFIC MANAGEMENT PLANS

For each reserve, TNBC prepares and implements a site-specific management plan that addresses the specific resources and habitat values of each reserve site, and how these will be managed in support of the goals and objectives of the NBHCP.

The potential effects of the Greenbriar project that could affect reserve management include altering adjacent land uses, connectivity, water availability, or affecting opportunities to establish additional reserves. These effects are evaluated in sections 3.7, 3.6, 3.8, and 3.9, respectively. In brief, the project would not affect water availability, the proposed reserves and mitigation could change adjacent land uses of existing and future reserves but the effect would be beneficial, and with the DEIR mitigation it would not affect connectivity. Therefore, the Greenbriar project probably would not affect the management plans prepared for existing and future reserves with the exception of altering Swainson's hawk foraging habitat in the vicinity of the Greenbriar site and the proposed reserves, and of preserving and enhancing land that could be consolidated into current or future reserves, which could alter existing site-specific plans.

Also, where the proposed reserves could be consolidated into existing or future reserves, the site-specific management plans of these reserves would need to be revised. These revisions would reflect the beneficial effects of the increased in reserve size. This would occur, for example, at the Cummings reserve, which would probably be consolidated with the proposed Natomas 130 reserve that is immediately adjacent to it.

## 5.3 BUFFERS WITHIN RESERVE LANDS

Buffers are incorporated into reserves to minimize the effects of incompatible adjoining land uses. These buffers consist of a 30–70 foot wide strip of native or ruderal vegetation along the edge of the reserve. Development at the Greenbriar site would not alter the need for or effectiveness of reserve buffers at existing reserves because the Greenbriar site is not adjacent to an existing reserve. (Potential effects of the Greenbriar project on human-wildlife conflicts and reserve habitat values are evaluated in sections 3.2 and 3.7, respectively.) Also, because under the future condition of the Natomas Basin resulting from the NBHCP, the Greenbriar site would already be bordered by urban development, highways or major roads on all sides, development of the Greenbriar site could

cause only very limited effects on the effectiveness of buffers within future reserves, even if reserves were established on adjacent land to the north or southwest (i.e., adjacent land that would not be developed under the future condition of the Natomas Basin).

The proposed reserves could reduce the need for buffers at existing and future reserves. The proposed Natomas 130 reserve borders the existing Cummings reserve (Exhibit 5), and thus along their shared border, there would no longer be a need for a buffer from incompatible adjacent land uses. If in the future, reserves were established adjacent to the reserves proposed by this project, buffers would be unnecessary along their shared borders.

## 5.4 CONNECTIVITY

The conservation strategy of the NBHCP emphasizes the need for maintaining connectivity of reserves and the importance of existing canals and drains for providing that connectivity. But, the NBHCP would not preserve or enhance habitat along canals, although it does contemplate future needs to preserve habitat along canals in some instances. The NBHCP states (on page IV-8) that elimination of drains or canals would primarily be related to urban development, and thus would be unlikely to affect reserves. Nonetheless, the NBHCP acknowledges (on page IV-9) that once reserves are established and key connectivity corridors have been identified, changes in water delivery and drainage along these waterways could occur, and thus these changes must be considered by TNBC and measures taken to ensure connectivity. Suggested measures include MOAs, easements, or purchase of land.

Lone Tree Canal is a key connectivity corridor between existing reserves (Jones & Stokes 2005). The project's potential adverse effects on connectivity, and in particular on Lone Tree Canal, would be mitigated so that connectivity would not be reduced (and could be enhanced) along the adjacent section of Lone Tree Canal. This mitigation includes enhancing and preserving habitat within a 250-foot wide setback along the canal, installing a barrier/fencing to keep snakes out of adjacent development and to exclude humans and domestic/feral animals from the Lone Tree Canal corridor, providing an additional assurance for water flow in the canal, and creating habitat along the canal. (Both the potential effects and the mitigation that reduces or eliminates them are described in greater detail in Section 3.5 Connectivity of Habitat in the Natomas Basin and in Section 3.6 Connectivity of Existing TNBC Reserves.) This mitigation would ensure that connectivity would be maintained along this section of Lone Tree Canal, and is comparable to the measures contemplated in the NBHCP (on page IV-9) for ensuring connectivity.

The proposed reserves would likely have a beneficial effect on connectivity of TNBC reserves by enhancing and preserving habitat in between existing and future reserves. For example, the proposed Spangler reserve is located between the Ruby Ranch and Atkinson reserves to the west and the Tufts and Sills reserves to the east (Exhibit 5). Therefore, the enhancement and preservation of habitat at this site would likely enhance and preserve connectivity between these reserves.

#### 5.5 FORAGING HABITAT

As described on pages IV-11 through IV-13 of the NBHCP, the viability of populations of covered bird species, and in particular the Swainson's hawk, depends on foraging habitat both on TNBC reserves and on unpreserved agricultural lands in the Natomas Basin. Therefore, the NBHCP includes measures to be implemented if foraging habitat outside of the permit areas (i.e., the areas authorized for urban development under the NBHCP) is converted to urban land uses without adequate provisions to maintain foraging habitat values and the effectiveness of the operating conservation program is potentially compromised. These measures include modifying acquisition criteria, substituting impacted reserves with unaffected replacement sites, modifying the percentages of habitat types at TNBC reserves, and pursuing outside funding to acquire additional reserves.

The Greenbriar project, however, would include adequate provisions to maintain foraging habitat values, and thus would not compromise the effectiveness of the operating conservation program. The effects on habitat acreage

and quality in the Natomas Basin are evaluated in Sections 3.3 and 3.4, respectively. (In addition, effects on habitat values of existing reserves are evaluated in Section 3.7.) The project would reduce the acreage of foraging habitat but would increase habitat quality at the proposed reserves and at the DEIR mitigation site. As a result, for Swainson's hawk, total foraging resources available in the Natomas Basin would not be reduced by the project. For other bird species, foraging resources of the Natomas Basin either would not be reduced or the reduction would not be sufficient to alter the viability of the species' population in the Natomas Basin (as described for each species in Section 4 *Potential Effects of the Greenbriar Project on Covered Species*).

To evaluate the effects of habitat loss and enhancement on foraging resources for Swainson's hawk in the Natomas Basin, the approach used by CH2M HILL in evaluating the NBHCP was used in this effects analysis and a new model developed by EDAW was also used. The EDAW model expresses the habitat value of different habitats, on a monthly basis, in terms of the equivalent acreage of high quality foraging habitat. The basis and structure of this model, and the scenarios evaluated, are described in detail in Section 2.2 Methodology for Analyzing Alterations of Populations and Habitats. Based on CH2M HILL's approach, there was a net decrease in habitat acreage, but an increase in high quality habitat and an increase in available habitat during April-August. Based on the EDAW model, during April–June, the increase in foraging habitat value at the proposed reserves and mitigation sites would be slightly greater than the value of the lost foraging habitat (the equivalent of 129 acres of high quality habitat with the project versus 122 acres without the project). During July-September, the increase in foraging habitat value at the proposed reserves and mitigation sites would not fully offset the value of the foraging habitat lost at the Greenbriar site (129 versus 140 acres during July-August and 162 acres in September). However, during these months, foraging resources in the Natomas Basin increase due to harvesting of crops, and so the project's affect on foraging resources available during July-September is not likely to affect the viability of Swainson's hawk, nor the effectiveness of the conservation strategy of the NBHCP. The results of these analyses of foraging resources are presented in Section 3.4 Habitat Quality in the Natomas Basin, and are displayed in Exhibits 3 and 4.

## 5.6 MINIMUM HABITAT BLOCK SIZE REQUIREMENTS

A requirement of the NBHCP is that by the end of the 50-year period, one habitat block within the reserve system will be at least 2,500 acres in size and the balance of reserve lands shall be in habitat blocks of at least 400 acres in size. The NBHCP (on page IV-14) provides four bases for this size requirement. These bases are:

- 1. large blocks minimize the "perimeter effect",
- 2. large blocks promote biodiversity by allowing multiple species and niches to occupy the site,
- 3. the benefit to genetic diversity of dispersing interconnected reserves throughout the Natomas Basin, and
- 4. the 400-acre reserve size is considered the minimum size to allow persistence of covered species.

No aspect of the Greenbriar project would alter any of these bases for the minimum habitat block size requirements of the NBHCP. The project could however affect opportunities to establish additional TNBC reserves, and thus affect the ability to consolidate reserves into habitat blocks that satisfy the size requirements. The Greenbriar project's potential affect on opportunities to establish additional TNBC reserves was evaluated in Section 3.9. In brief, the project would adversely affect the preservation of large blocks of habitat at or adjacent to the Greenbriar site, but elsewhere it would enhance and preserve additional habitat (296 acres plus at least 49 acres of DEIR mitigation), increasing opportunities to establish additional reserves; The project also would reduce the quantity of land available to provide mitigation under the NBHCP, but the remaining acreage of land potentially suitable for preservation would substantially exceed the acreage required for the NBHCP's reserve system. Overall, the project would probably have a beneficial effect on the fulfillment of the requirement for minimum habitat block size.

Interestingly, the Greenbriar project does illustrate the need for smaller reserves in some instances to preserve connectivity. The Greenbriar project necessitates enhancement and preservation of land along a waterway to maintain connectivity for the giant garter snake. This land would be partially isolated by major roads and both

existing and proposed development, and would not become part of a larger habitat block in the future. In general, corridors along canals and drains near roads and development will be more difficult to incorporate into larger blocks of habitat because of the adverse effects of roads and development on reserves. Yet, it is in precisely these locations that preserving and managing corridors would be most beneficial or even necessary. Though it acknowledges that evidence may be discovered in support of smaller reserves, the NBHCP does not address the effects of preserving corridors on the attainment of its minimum habitat block size requirements.

Overall, the project would beneficially affect the establishment of large blocks of preserved habitat. It would enhance and preserve 296 acres of additional habitat, most of which would be adjacent to or near existing TNBC reserves; the DEIR mitigation would increase this benefit by requiring the preservation of at least an additional 49 acres of land. The project would adversely affect the preservation of large blocks of habitat by developing existing habitat at the Greenbriar site. However, under the future condition of the Natomas Basin, this land would be surrounded by major roads and urban development, and the project would preserve the most ecologically important portion of the site, which is the corridor of land along Lone Tree Canal.

## 5.7 EFFECTIVENESS OF THE CONSERVATION STRATEGY OF THE NBHCP

As described in the preceding sections, effects on the key components of the NBHCP's conservation strategy resulting from the Greenbriar project (with the DEIR mitigation) would be minor, and some of these effects would be beneficial. Therefore, the Greenbriar project would not reduce the effectiveness of the conservation strategy, and thus no changes in the conservation strategy would be necessitated by the project.

In large part, the project would avoid affecting the effectiveness of the conservation strategy because of its mitigation of effects on connectivity and foraging habitat. This mitigation of effects on connectivity (through substantial investment in wide setbacks, barriers, and habitat management in perpetuity) and foraging habitat (by increasing habitat values on mitigation lands sufficiently to replace habitat values lost on development sites) could serve as a general approach for future projects to avoid reducing the effectiveness of the conservation strategy of the NBHCP.

# 6 POTENTIAL EFFECTS OF THE GREENBRIAR PROJECT ON NBHCP GOALS AND OBJECTIVES

For each applicable goal and objective in the NBHCP, this section summarizes the effects of the Greenbriar project on attainment of that goal or objective. These effects were analyzed in the preceding sections of this report that addressed effects on covered species, habitat acreage, human-wildlife conflicts, connectivity, habitat values at TNBC reserves, water availability at TNBC reserves, and the opportunity to establish additional reserves.

Because the Greenbriar project would be located outside of the areas where urban development was authorized by the NBHCP, and thus would result in a net increase of land potentially developed in the NBHCP plan area, the project's avoidance, minimization and mitigation measures could be consistent with the measures of the NBHCP and yet the project could still detrimentally affect attainment of the NBHCP's goals and objectives, or otherwise reduce the likelihood of sustaining populations of covered species in the Natomas Basin.

For example, the 0.5 to 1 ratio of developed to conserved land in the NBHCP was not necessarily intended to apply to development outside the 17,500 acre permit area (as described on page IV-12 of the NBHCP), and was based, in part, on the interpretation that on average habitat quality was lower in the areas permitted for development than in the areas that would be preserved (City of Sacramento et al. 2003).

Similarly, the NBHCP conservation strategy was based in part on the assumption that most of the Natomas Basin in agricultural use at the time of the NBHCP's approval would remain in agricultural land uses that provide habitat for most covered species (e.g., as described on page IV-11 of the NBHCP). The retention of a substantial acreage of existing agricultural habitats limits the risks associated with relying on enhancement and restoration efforts to offset habitat losses. It also retains, largely unaltered, the canals and upland corridors that connect habitats; and it would leave reserves surrounded by agricultural lands that increase the benefits of reserves for covered species. Therefore, development outside of areas permitted by the NBHCP could eliminate higher quality habitats, reduce habitat connectivity, and detrimentally affect reserves to a much greater degree than the development permitted by the NBHCP. Such development also could create conflicts with the continued use of adjacent lands for agriculture.

These examples illustrate that both the types and magnitudes of effects caused by development outside of the areas permitted by the NBHCP can differ from those caused by comparable development inside of the areas permitted by the NBHCP; thus, mitigation comparable to that in the NBHCP may not adequately offset these effects. This situation was anticipated during the development of the NBHCP and is reflected in the text of the NBHCP, BO, Final EIR/EIS and the implementation agreement for the NBHCP (e.g., page IV-12 of the NBHCP).

Therefore, interpretations of the Greenbriar project's effects on the NBHCP were based primarily on the sum of the anticipated effects on the TNBC reserve system, and on the sum of anticipated effects on the viability of populations of covered species using the Natomas Basin. An overall negative effect on the existing reserve system was considered adverse to the attainment of the NBHCP's goals and objectives. Effects that would preclude attainment of a goal or objective, reduce the viability of a covered species or otherwise necessitate a change in the NBHCP's conservation strategy were considered substantial effects that would conflict with the NBHCP.

Overall, the Greenbriar project would not conflict with attainment of the goals and objectives of the NBHCP. Through most mechanisms by which a project could affect the NBHCP, the Greenbriar project causes adverse and beneficial effects on the goals and objectives of the NBHCP. However, many of these effects are small relative to the acreages of development authorized by the NBHCP and of habitats in the Basin. Also, most beneficial and adverse effects would be reduced by opposing effects, and the DEIR mitigation further reduces adverse effects. Consequently, the Greenbriar project would not cause an overall adverse effect on attainment of any of the goals or objectives of the NBHCP, and the project could provide an overall benefit towards the attainment of several goals. (For example, the project [with DEIR mitigation] would preserve 345 acres of land and this preserved land

would contribute to the connectivity and quality of habitat preserved through the NBHCP.) In the following sections of text, the project's effects are assessed for each potentially affected goal and objective of the NBHCP. These assessments, in turn, are based on the analyses presented in Chapter 3 Alteration of Population and Habitat Attributes by the Greenbriar Project and Chapter 4 Potential Effects of the Greenbriar Project on Covered Species.

## 6.1 OVERALL GOALS

## 6.1.1 OVERALL GOAL 1

Establish and manage in perpetuity a biologically sound and interconnected habitat reserve system that mitigates impacts on Covered Species resulting from Covered Activities and provides habitat for existing, and new viable populations of Covered Species. (NBHCP, p. I-15)

A project could potentially affect attainment of this goal by affecting the:

- ▶ acreage of habitat in the Natomas Basin,
- quality of habitat in the Natomas Basin,
- connectivity of habitat in the Natomas Basin,
- ► connectivity of TNBC reserves,
- habitat value of TNBC reserves,
- water availability at TNBC reserves, and opportunities to establish additional TNBC reserves.

The Greenbriar project would cause both adverse and beneficial effects on the attainment of this goal through all of these mechanisms, except for water availability at TNBC reserves (which the project would not affect). The project's beneficial effects would include increased habitat quality resulting from the preservation, creation, and enhancement of habitats, increased connectivity of existing TNBC reserves and of habitats, and increased opportunities to establish additional TNBC reserves. Without mitigation, the project's adverse effects would include a reduction in the acreage of upland and wetland habitats in the Natomas Basin, reduced foraging habitat values within a mile of an existing TNBC reserve, fragmented upland habitats in the vicinity of the Greenbriar site, degraded habitat quality of adjacent agricultural lands to the north and southwest, and possibly reduced connectivity along Lone Tree Canal (despite preserving and enhancing a corridor of habitat along the canal). A detailed assessment of these effects is provided in sections 3 Alteration of Population and Habitat Attributes by the Greenbriar Project and 4 Potential Effects of the Greenbriar Project on Covered Species.

The mitigation proposed in the DEIR would reduce the project's adverse effects by incorporating additional measures to ensure that connectivity along Lone Tree Canal is sustained (as described in Sections 3.5, 3.4, 4.1, and 4.2.), and to preserve and enhance an additional 49 acres of foraging habitat within a mile of existing TNBC reserves (as described in Sections 3.4, 3.7, and 4.3). This mitigation also would cause additional beneficial effects (as described in Sections 3.6, 3.7, and 3.8), because the preserved and enhanced foraging habitat would not only mitigate effects on foraging habitat and on TNBC reserves, but also could increase connectivity of habitat and of TNBC reserves. Similarly, by ensuring that connectivity along Lone Tree Canal would be maintained, the project (with its proposed mitigation) would conserve a portion of an important corridor connecting reserves and habitats of the southern and central Natomas Basin. (The connectivity of upland habitats, however, would still be reduced at the Greenbriar site.)

As described in Section 3.9, the project (with the DEIR mitigation) would have an overall beneficial effect on the establishment and management of reserves for the NBHCP. Because the acreage of land in the Natomas Basin that is potentially available and suitable for preservation substantially exceeds the 8,750 acres that will be preserved by the NBHCP, the project would not preclude the preservation of sufficient land to attain the NBHCP's goals and objectives. It would provide 345 acres of additional reserve lands, with much of this acreage adjacent to or near existing reserves, which would increase the connectivity of habitats and the resources available

to covered species using reserves established by the NBHCP; in addition, it would conserve an important corridor of canal habitat along Lone Tree Canal. The project also would increase opportunities to establish new reserves, particularly to create larger reserves by preserving additional land adjacent to existing TNBC and project's proposed reserves. (Sections 3.6–3.9 provide a detailed assessment of effects on the management and establishment of TNBC reserves.)

Although the project would cause a net reduction in the acreage of upland and wetland habitats, the preservation and enhancement of habitat by the project would adequately mitigate for its impacts on upland and wetland habitats for covered species. Effects on the acreage and quality of habitats are summarized below, and a detailed assessment of these effects is presented in Sections 3.3 and 3.4. (These effects are also evaluated separately for each covered species in Chapter 4 *Potential Effects of the Greenbrier Project on Covered Species.*)

For wetland land cover (i.e., rice, canal, and ponds and seasonally wet areas), the net reduction in acreage resulting from the project would be offset by an increase in the habitat quality by creating marsh habitat at the project's proposed reserves. Based on 2001 land cover mapping, the Greenbriar project would eliminate 388 acres of rice and 16 acres of canal habitats, but would increase the acreage of marsh by 201 acres, creating a net loss of 204 acres of these wetland land cover types and of the habitats they provide. An acre of marsh, however, provides a greater quantity and variety of habitat than does an acre of rice, and thus the additional habitat values provided by the created marsh offsets the habitat lost in the rice and canal land cover types. Managed marsh provides substantially greater habitat values for giant garter snakes than rice for several reasons. These reasons include:

- ► Giant garter snakes use the full extent of managed marshes, whereas they primarily use the margins of rice fields;
- Marshes provide habitat throughout the active period of the snake, whereas rice fields do not provide habitat during early and mid-spring, and are typically drained before the end of the snake's active period; and
- ▶ Marsh provides habitat in all years, whereas rice is fallowed periodically.

In addition, the project would preserve, and manage for its habitat values, 201 acres of marsh (i.e., about 1.0 acre for each acre lost) and approximately 6 acres of canal habitat. This preservation and management would increase the habitat value of these lands because:

- ► Habitat would be preserved in perpetuity;
- ► Habitat would be monitored and actively managed for the benefit of covered species;
- ▶ Habitat would not be subject to continuous disturbance caused by farming or canal maintenance activities; and
- ▶ Habitat would be relatively free of human intrusion (USFWS 2003).

Therefore, the loss of wetland habitats (i.e., those provided by land cover mapped as rice, canal, and ponds and seasonally wet areas) is more than offset by the creation of a comparable area of marsh (from rice and upland land cover), and the preservation and management of this marsh. These effects are described in detail in Sections 3.3—

3.4 and 4.1–4.2. As described in Section 3.5, the project with its mitigation would also conserve an important corridor of canal and adjacent upland habitat at the Greenbriar site.

For upland land cover (i.e., alfalfa, grassland, idle, non-rice crop, pasture, and ruderal), the net reduction in acreage resulting from the project also would be offset by an increase in the habitat quality of preserved and enhanced habitat. Based on 2001 land cover mapping, the Greenbriar project would cause a net reduction of 281 acres of upland land cover providing habitat for covered species, but would enhance the habitat value of 14 acres at the proposed Natomas 130 site and 45 acres at the Spangler site, and the DEIR mitigation for loss of Swainson's hawk would enhance at least an additional 49 acres; thus, a total of 109 acres of upland habitat would be enhanced. This habitat would be preserved, as would 27 acres of grassland along Lone Tree Canal and 60 acres of upland components within created marshes; thus, a total of 195 acres of upland habitat would be preserved. For

some covered species associated with uplands (including Swainson's hawk, burrowing owl, and loggerhead shrike) the additional habitat values provided by the preservation and enhancement of this upland habitat (i.e., 0.7 acres preserved for each acre lost and over half of this enhanced) would fully offset the habitat values of the upland acreage lost as a result of the project. For other covered species (including Aleutian Canada goose, tricolored blackbird, and bank swallow), the additional habitat values provided by the preservation and enhancement of this 195 acres of upland habitat would only partially offset the habitat values of the upland acreage lost as a result of the project. (The analysis of the foraging habitat value lost at the Greenbriar site and of the value gained at the proposed reserve and mitigation sites is summarized in Section 3.4 *Habitat Quality in the Natomas Basin.*) For example, based on the methods used by CH2M HILL, the upland habitats that would result from the project would provide a greater acreage of available foraging habitat during April–August, when Swainson's hawks are nesting in the Basin. Based on EDAW's model of habitat values, the enhancement of uplands by the project (with the DEIR mitigation) would provide foraging habitat values during the months of April–June that are slightly greater than the habitats that would be eliminated by the project (Exhibits 3b and 4). During July–August, the project's enhancement of habitat would not fully offset the lost habitat values, but during these months foraging habitat values increase in the Natomas Basin as a result of crop harvest.

On the basis of the project's establishment of reserves that provide habitat for covered species and mitigate the project's impacts to those covered species, implementing the proposed project (with the DEIR mitigation measures) would either not alter or would improve the connectivity of the NBHCP reserve system and provide habitat for viable populations of covered species. In addition, because the viability of covered species would either be unaltered or improved (e.g., giant garter snake, northwestern pond turtle), the project would not adversely affect attainment of this goal.

## 6.1.2 OVERALL GOAL 3

Preserve open space and habitat that may also benefit local, non-listed and transitory wildlife species not identified within the NBHCP. (NBHCP, page I-16)

A project could potentially affect attainment of this goal by affecting the:

- ► Acreage of habitat in the Natomas Basin,
- Quality of habitat in the Natomas Basin,
- ► Connectivity of habitat in the Natomas Basin,
- ► Connectivity of TNBC reserves,
- ▶ Habitat value of existing TNBC reserves,
- ▶ Water availability at TNBC reserves, and
- Opportunities to establish additional TNBC reserves.

The Greenbriar project would cause both beneficial and adverse effects on the attainment of this goal through most of these mechanisms. By preserving, enhancing, and creating habitat, the project would increase the quality of habitats, increase the connectivity of habitats and TNBC reserves, and create additional opportunities to establish additional TNBC reserves. By developing most of the Greenbriar site, the project would reduce the acreage of habitat in the Natomas Basin, and it would fragment, degrade, and reduce the connectivity of adjacent habitats, reduce the foraging habitat available at an existing TNBC reserve, and without the DEIR mitigation, it could reduce connectivity along Lone Tree Canal (despite preserving a corridor along it.)

The DEIR mitigation reduces the project's adverse effects by incorporating additional measures to ensure that connectivity along Lone Tree Canal is sustained (including additional requirements for fencing and barriers), and to preserve and enhance an additional 49 acres of upland foraging habitat within a mile of existing TNBC reserves. This additional foraging also could increase connectivity of habitat and of TNBC reserves. Similarly, by ensuring that connectivity along Lone Tree Canal would not be reduced, the project (with the DEIR mitigation)

would conserve a portion of an important corridor connecting reserves and habitats of the southern and central Natomas Basin. (The connectivity of upland habitats, however, would still be reduced at the Greenbriar site.)

As described in Sections 3.6–3.9, the project (with the DEIR mitigation) would have an overall beneficial effect on the establishment and management of reserves for the NBHCP. Because the acreage of land in the Natomas Basin that is potentially available and suitable for preservation substantially exceeds the 8,750 acres that will be preserved by the NBHCP, the project would not preclude the preservation of sufficient land to attain the NBHCP's goals and objectives. It would provide reserve lands adjacent to or near existing reserves, increasing the connectivity of habitats and the resources available to covered species using reserves established by the NBHCP; in addition, it would conserve a portion of an important corridor of canal habitat along Lone Tree Canal. The project also would increase opportunities to establish new reserves, particularly to create larger reserves by preserving additional land adjacent to existing TNBC and project's proposed reserves.

Because the project would cause both beneficial and adverse effects on the attainment of this goal, and because the project's adverse effects would not reduce the likelihood that the NBHCP would be able to preserve sufficient habitat for non-listed species to attain this goal, the Greenbriar project would not adversely affect the attainment of this goal.

## 6.1.3 OVERALL GOAL 4

Ensure that direct impacts of Authorized Development upon Covered Species are avoided or minimized to the maximum extent practicable. (NBHCP, page I-16)

A project could potentially affect attainment of this goal by causing construction-related effects on the survival or reproduction of individuals that are using the project or mitigation sites and adjacent lands.

Development of the Greenbriar site would likely affect giant garter snake, Swainson's hawk, burrowing owl, and loggerhead shrike, and could affect several other covered species including northwestern pond turtle, tricolored blackbird, white-faced ibis, Aleutian Canada goose, Sanford's arrowhead, and Delta tule pea. These potential effects (which are described in detail in Chapter 4) would be comparable to the construction-related effects that could be caused by development permitted by the NBHCP.

The avoidance and minimization measures incorporated into the project and into the DEIR mitigation would substantially reduce these effects. These measures include all of the applicable avoidance and minimization measures that were included in the NBHCP to avoid and minimize construction-related effects, which are a comprehensive set of effective measures for reducing these effects. (An assessment of the applicability of these measures is in Appendix A.) In addition, the DEIR mitigation would include several more stringent minimization measures. Therefore, with its proposed mitigation, the project would not adversely affect attainment of this goal because it would implement a comprehensive set of measures to avoid and minimize effects on covered species. The Greenbriar project also would not alter the effectiveness of any NBHCP conservation measures for avoiding and minimizing the effects of development authorized by the NBHCP (Appendix A).

## 6.2 OVERALL OBJECTIVES

#### 6.2.1 OVERALL OBJECTIVE 1

Minimize conflicts between wildlife and human activities, including conflicts resulting from airplane traffic, roads and automobile traffic, predation by domestic pets, and harassment by people. (NBHCP, page I-16)

A project could potentially affect attainment of this objective by causing construction-related effects on survival or reproduction of individuals using project sites and adjacent lands, or by altering the area, types of habitats, or level of conflicts in zones with high levels of human-wildlife conflicts.

Without the DEIR mitigation, the project would reduce the overall area in zones with high levels of human-wildlife conflicts, but it would increase the area of rice habitat and the level of conflicts within such zones, and it would cause construction-related effects in these zones. (Section 3.2 provides a detailed description of effects on zones with high levels of human-wildlife conflicts.) These human-wildlife conflicts and construction-related effects would be comparable to those resulting from the development authorized by the NBHCP.

The DEIR mitigation includes avoidance and minimization measures that would substantially reduce these effects. These measures include all of the applicable measures that were included in the NBHCP to avoid and minimize construction-related effects and to reduce human-wildlife conflicts. (An assessment of the applicability of these measures is included as Appendix A.) As described in Section 3.1, these measures represent a comprehensive set of effective measures for avoiding and minimizing the project's effects. In addition, the project also incorporates additional measures (e.g., fencing and barriers) to reduce human-wildlife conflicts along Lone Tree Canal.

Therefore, with the DEIR mitigation, the project would not adversely affect attainment of this objective because it would implement a comprehensive set of measures that would minimize human-wildlife conflicts. The Greenbriar project also would not alter the effectiveness of any NBHCP conservation measures for minimizing human-wildlife conflicts (Appendix A).

## 6.2.2 OVERALL OBJECTIVE 3

Ensure connectivity between TNBC reserves to minimize habitat fragmentation and species isolation. Connections between reserves will generally take the form of common property boundaries between reserves, waterways (primarily irrigation and drainage channels) passing between reserves, and/or an interlinking network of water supply channels or canals. (NBHCP, page I-16)

A project could potentially affect attainment of this goal by affecting:

- Connectivity of habitat in the Natomas Basin,
- ► Connectivity of TNBC reserves,
- ► Habitat value of TNBC reserves, and
- ▶ Water availability at TNBC reserves.

The Greenbriar project would cause beneficial and adverse effects on the attainment of this objective through most of these mechanisms. The main beneficial effect would be increased connectivity of habitats and TNBC reserves due to preservation, creation, and enhancement of habitat at the project's proposed reserves, two of which are adjacent to or near (i.e., within a half mile of) existing TNBC reserves. Adverse effects would include reducing the foraging habitat within a mile of a TNBC reserve, fragmenting and reducing the connectivity of upland habitats adjacent to the Greenbriar site, and possibly reducing the connectivity of wetland habitats and TNBC reserves because of effects on Lone Tree Canal (despite preserving a corridor along the canal). (Sections 3.4–3.7 provide detailed descriptions of these effects.)

The DEIR mitigation reduces the project's adverse effects by incorporating additional measures to ensure that connectivity along Lone Tree Canal is sustained, and to preserve and enhance foraging habitat within a mile of existing TNBC reserves. This mitigation also would cause additional beneficial effects because the preserved and enhanced foraging habitat would not only mitigate effects on TNBC reserves, but also could increase connectivity of habitat and of TNBC reserves. Similarly, by ensuring that connectivity along Lone Tree Canal will not be reduced, the project (with the DEIR mitigation) would conserve a portion of an important corridor connecting reserves and habitats of the southern and central Natomas Basin. (The connectivity of upland habitats, however, would still be reduced at the Greenbriar site.)

In the absence of an adverse effect on connectivity along Lone Tree Canal, the project would cause only small effects on the attainment of this objective, and most of these effects would be beneficial. Therefore, the project's overall effect on the attainment of this objective would not be adverse.

## 6.3 WETLAND SPECIES/HABITAT GOALS AND OBJECTIVES

## 6.3.1 WETLAND SPECIES/HABITAT GOAL/OBJECTIVE 1

Acquire, enhance and create a mosaic of wetland habitats with adjacent uplands and connecting corridors to provide breeding, wintering, foraging, and cover areas for wetland species in the Plan Area. (NBHCP, page I-17)

A project could potentially affect attainment of this goal by affecting:

- ► Acreage of habitat in the Natomas Basin,
- ▶ Quality of habitat in the Natomas Basin,
- ► Connectivity of habitat in the Natomas Basin,
- ► Connectivity of TNBC reserves,
- ► Habitat value of TNBC reserves,
- ▶ Water availability at TNBC reserves, and
- ▶ Opportunities to establish additional TNBC reserves.

The Greenbriar project with the DEIR mitigation would cause beneficial and adverse effects on the attainment of this goal/objective through several of these mechanisms. By acquiring, enhancing, and creating wetland habitats, the project would increase the area of preserved land in the Natomas Basin, which would increase the connectivity of habitats and create additional opportunities to create larger reserves. By developing most of the Greenbriar site, the project would reduce the acreage of wetland habitats in the Natomas Basin (by approximately 204 acres), and without the DEIR mitigation, could reduce the connectivity of wetland habitats because of effects on Lone Tree Canal, and could cause some degradation of wetland habitats on lands to the north and southwest of the Greenbriar site. With its proposed mitigation, however, the project would not adversely affect connectivity of habitats along Lone Tree Canal. (Section 3.5 provides an assessment and more detailed description of the anticipated effects on connectivity.) Therefore, the main adverse effect of the project on attainment of this goal would be due to the reduction of the acreage of wetland habitats.

This reduction in wetland acreage would not cause an effect on attainment of this goal/objective that would necessitate changes to the conservation strategy of the NBHCP. First, the effect would be offset by the enhancement of 204 acres of wetland habitats on the project's proposed reserves (which is described in Section 3.4). Second, as described in Section 3.3, only a small percentage of the Basin's wetland habitats would be lost (approximately 1%). Third, as described in Section 3.5, no reduction in the connectivity of wetland habitats or in opportunities to preserve, enhance, and acquire wetland habitats would result. Fourth, as described in Section 4, the population viability of covered species using these habitats would not be reduced.

Because the project would contribute directly to the attainment of this goal, and would not cause any adverse effects on the goal's attainment that would need to be offset by changes in the conservation strategy of the NBHCP, the project's overall effect on the attainment of this goal is not adverse.

## 6.3.2 WETLAND SPECIES/HABITAT GOAL/OBJECTIVE 2

Provide habitat to maintain, attract and sustain viable populations of the Covered Species. The habitat areas should be configured to encompass natural species migration areas, minimize species isolation, and prevent future habitat fragmentation. (NBHCP, page I-17)

A project could potentially affect attainment of this goal by affecting:

- ▶ Zones with human-wildlife conflicts,
- ▶ Acreage of habitat in the Natomas Basin,
- ▶ Quality of habitat in the Natomas Basin
- ► Connectivity of habitat in the Natomas Basin,
- ► Connectivity of TNBC reserves,
- ► Habitat value of TNBC reserves,
- ▶ Water availability at TNBC reserves, and
- ▶ Opportunities to establish additional TNBC reserves.

The Greenbriar project, with the DEIR mitigation, would cause beneficial and adverse effects on the attainment of this goal/objective through several of these mechanisms. Based on the analyses presented in Section 3 *Alteration of Habitat and Population Attributes by the Greenbriar Project*, the project (with the DEIR mitigation) would cause a net loss in the acreage of wetland habitats, improve the habitat quality of some wetlands, and could improve connectivity of habitat and TNBC reserves, and increase opportunities to establish additional TNBC reserves. Overall, the project would not adversely affect attainment of this goal.

The net loss of habitat acreage resulting from the project would be offset by the creation of marsh at the project's proposed reserves. Based on 2001 land cover mapping, the Greenbriar project would eliminate 388 acres of rice and 16 acres of canal habitats, but would increase the acreage of marsh by 201 acres, creating a net loss of 204 acres of these wetland land cover types and of the habitats they provide. An acre of marsh, however, provides a greater quantity and variety of habitat than does an acre of rice, and thus the additional habitat provided by the created marsh offsets the habitat lost in the rice and canal land cover types. In addition, the project would preserve, and manage for its habitat values, 201 acres of marsh (i.e., about 1.0 acre for each acre lost). This preservation and management would increase the habitat quality of these lands because:

- 1. Habitat would be preserved in perpetuity;
- 2. Habitat would be monitored and actively managed for the benefit of covered species;
- 3. Habitat would not be subject to continuous disturbance caused by farming or canal maintenance activities; and
- 4. Habitat would be relatively free of human intrusion (USFWS 2003).

Therefore, the loss of wetland (i.e., land cover mapped as rice, canal, and ponds and seasonally wet areas) is more than offset by the creation of a comparable area of marsh (from rice and upland land cover) and the preservation, and management of the created marsh. Because the project would increase the acreage of land preserved in the Natomas Basin, it would provide opportunities to increase the size and connectivity of TNBC reserves (which are described in Sections 3.6 and 3.9). The project with the DEIR mitigation would also conserve an important corridor of canal and adjacent upland habitat at the Greenbriar site (as described in Section 3.5).

Consequently, as described in Section 4 *Potential Effects of the Greenbriar Project on Covered Species*, the project would either benefit or be unlikely to alter the viability of covered species using wetland land cover (i.e., rice, canal, or ponds and seasonally wet areas). Because the project would not reduce the viability of covered species, and creates additional reserves that contribute to efforts to sustain viable populations and prevent fragmentation of habitat, the project does not adversely affect this goal/objective.

## 6.4 UPLAND SPECIES/HABITAT GOALS AND OBJECTIVES

## 6.4.1 UPLAND SPECIES/HABITAT GOAL/OBJECTIVE 1

Acquire, enhance and create a mosaic of upland habitat types for breeding, foraging, and cover for species dependent on upland habitats. (NBHCP, page I-17)

A project could potentially affect attainment of this goal by affecting:

- ▶ Acreage of habitat in the Natomas Basin,
- ▶ Quality of habitat in the Natomas Basin,
- ▶ Habitat value of existing TNBC reserves, and
- ▶ Opportunities to establish additional TNBC reserves.

For upland habitats, the Greenbriar project would affect the attainment of this goal through each of these mechanisms. The project's beneficial effects on the attainment of this goal/objective would include the preservation, creation and enhancement of habitats that increase habitat quality and contribute to the connectivity of existing TNBC reserves and of habitats, and increase opportunities to establish additional TNBC reserves. The project's adverse effects on the attainment of this goal/objective would include reduced acreage of upland habitats in the Natomas Basin, reduced foraging habitat within a mile of an existing TNBC reserve, fragmented and reduced connectivity of upland habitats in the vicinity of the Greenbriar site, and probably degraded quality of adjacent habitat to the north and southwest of the Greenbriar site. Sections 3 Alteration of Population and Habitat Attributes by the Greenbriar Project and 4 Potential Effects of the Greenbriar Project on Covered Species provide detailed assessments of these effects.

The DEIR mitigation reduces the project's adverse effects by incorporating a measure to preserve and enhance additional foraging habitat within a mile of existing TNBC reserve(s) that would be sufficient to offset the loss of habitat values due to the Greenbriar project. This mitigation also would cause additional beneficial effects because the preserved and enhanced foraging habitat would not only mitigate effects on TNBC reserves, but also could increase connectivity of habitat and of TNBC reserves.

The project would not cause effects on habitat acreage, quality, and connectivity sufficient to alter the likelihood of attaining this goal/objective. Under the future condition of the Natomas Basin resulting from the NBHCP, approximately 12,000 acres of upland habitats would remain in the Natomas Basin. To attain this goal/objective of the NBHCP, under the future condition of the NBHCP, 18% of this remaining upland habitat would need to be preserved and enhanced as part of the TNBC. The project would reduce the acreage of upland habitat in the Natomas Basin (under the future condition) by about 2.5%. To offset effects resulting from the reduction in upland acreage, the project would preserve and enhance much of another 1.7% of the upland habitats that would remain under the future condition. This land would be unavailable for the NBHCP. Thus, the Greenbriar project would reduce the upland habitat available for preservation through the NBHCP by several percent, which would not be sufficient to affect the attainment of this goal/objective.

In contrast, as described in Section 3.9, the land preserved by this project could increase opportunities to establish reserves. For example, the NBHCP has minimum size requirements for habitat blocks within the reserve system. At least two of the reserves resulting from this project (the proposed Natomas 130 and Spangler reserves) would be adjacent to or near (i.e., within a half mile or less of) existing reserves (Exhibit 5); these lands would provide opportunities additional to create larger reserves by preserving additional land connected to existing TNBC reserves and/or the project's proposed reserves. Therefore, the Greenbriar project could contribute directly to preserving, creating, and enhancing blocks of habitat of sufficient size for effective conservation of upland habitats by the NBHCP.

Overall, the project would not adversely (and could beneficially) affect this goal/objective. Because the acreage of upland habitat in the Natomas Basin that is potentially available and suitable for preservation is substantially more than the acreage of upland habitat that would be preserved and enhanced by the NBHCP, and the project would affect only a small percentage of this land, the project would not preclude the preservation of sufficient land to attain the NBHCP's goals and objectives. The project would, however, increase opportunities to establish new reserves, which would aid the attainment of this goal/objective.

## 6.4.2 UPLAND SPECIES/HABITAT GOAL/OBJECTIVE 2

Ensure reserve land connectivity with travel corridors for upland-dependent species. The habitat areas should encompass grasslands, agricultural croplands, riparian habitats, and shelter and nesting habitat areas (fence rows, clusters of shrubs and small trees), as well as wetland areas to provide a year-round source of water for upland species. The upland areas should be configured to enhance natural species migration, minimize species isolation, and prevent future habitat fragmentation. (NBHCP, page I-17)

A project could potentially affect attainment of this goal by affecting:

- ► Connectivity of habitat in the Natomas Basin,
- ► Connectivity of existing TNBC reserves,
- ► Habitat value of existing TNBC reserves, and
- ▶ Opportunities to establish additional TNBC reserves.

The Greenbriar project, with the DEIR mitigation, would affect the attainment of this goal/objective through each of these mechanisms. Beneficial effects would include the preservation, creation, and enhancement of upland habitats that contribute to the connectivity of existing TNBC reserves and of habitats, and increase opportunities to establish additional TNBC reserves. Adverse effects would include reduced foraging habitat within a mile of an existing TNBC reserve, and fragmented and reduced connectivity of upland habitats in the vicinity of the Greenbriar site. Sections 3.5–3.7 and 3.9 provide a detailed assessment of these effects.

The DEIR mitigation would reduce the project's adverse effects by incorporating a measure to preserve and enhance foraging habitat within a mile of existing TNBC reserves (or of the Swainson's hawk zone along the Sacramento River). This mitigation also would cause additional beneficial effects because the preservation and enhancement of at least an additional 49 acres of foraging habitat would not only mitigate effects on TNBC reserves, but also could increase connectivity of habitat and of TNBC reserves.

The project's proposed reserves at the Spangler and Natomas 130 sites would contribute to travel corridors connecting reserve lands. The proposed Natomas 130 site would contain upland and wetland habitats, and would be immediately adjacent to a TNBC reserve, Fisherman's Lake, and the Sacramento River (Exhibit 5). The proposed Spangler reserve would contain mainly wetland habitats, but upland habitats would be a component of the created marshes and reserve buffers, and this site is within a quarter mile of an existing reserve and would connect to habitat on buffer lands surrounding Sacramento International Airport to the south (Exhibit 5).

The proposed reserve on the Greenbriar site, along Lone Tree Canal, would contain grassland, marsh, and canal habitats managed to sustain connectivity of habitat for giant garter snake. This would also provide some benefit as a travel corridor for upland species; however, the partial isolation of the site by Elkhorn Boulevard to the north and Interstate 5 to the south would limit this benefit.

The project would, however, reduce connectivity of upland habitats adjacent to the Greenbriar site, and this could reduce dispersal and movement of upland species between reserves in the central and southern Natomas Basin. Under the future condition of the Natomas Basin resulting from the NBHCP, the Greenbriar site would be a corridor of upland habitat between the Metro Air Park and the City of Sacramento. At Interstate 5, this corridor would be about 0.4 miles wide and at the northern end of the Greenbriar site it would be almost a mile wide. The Greenbriar project would reduce this to a 250-foot wide and approximately one-mile long corridor of grassland, marsh, riparian, and canal habitats that would be preserved and managed as part of the TNBC reserve system. A moderate level of uncertainty exists regarding the attributes necessary for wildlife use of corridors, and this much narrower corridor surrounded by urban development may not be used, or may be used less frequently, by upland wildlife.

However, as described in Section 3.5, a reduction in connectivity of upland habitats at and adjacent to the Greenbriar site, would affect relatively few upland species. First, most upland species in the Natomas Basin are abundant, widely distributed and highly mobile. (The species observed during monitoring for TNBC support this characterization [Jones & Stokes 2005].) Second, Interstate 5 (which is along the entire southern border of the site), adjacent urban development, and in the future a six lane Elkhorn Boulevard along the site's northern border, limits use of the site by animals that are less mobile or are highly sensitive to human disturbance.

Based on the assessments presented in Section 4 Potential Effects of the Greenbriar Project on Covered Species, a reduction in connectivity of upland habitats at the Greenbriar site also would be unlikely to alter the viability of the populations of covered species using upland habitats in the Natomas Basin. Of the covered species, Swainson's hawk, burrowing owl, and loggerhead shrike all could be affected, because they probably use the Greenbriar site. These are highly mobile animals that could fly over or around the site, though they may not choose to do so, may do so less frequently, or doing so may expose them to additional risks. Development at the Greenbriar site would reduce and fragment upland habitats, and this could reduce the survival or reproduction of individuals using the site and adjacent lands. However, habitat would be enhanced and preserved along Lone Tree Canal and at the proposed reserves, and the DEIR mitigation would enhance and preserve additional upland habitat within a mile of existing TNBC reserves. This enhanced and preserved land would likely improve connectivity of upland habitats, and could increase the survival or reproduction of individuals using those sites. Also, burrowing owls and loggerhead shrikes using the Natomas Basin are part of large populations, a reduction of connectivity at the Greenbriar site would affect a very small portion of their range and numbers, and their loss of habitat would be mitigated by habitat preservation, creation, and enhancement at the proposed reserve and DEIR mitigation sites. Thus, the project is unlikely to alter the viability of populations of covered species using the Natomas Basin.

A moderate level of uncertainty exists regarding the overall effect of the Greenbriar project on this goal/objective. The proposed changes at the Greenbriar site would have an uncertain effect on the movement and dispersal of upland species; also there is some uncertainty regarding the project's contributions to connectivity elsewhere in the Basin because the location of the DEIR mitigation site has not been determined.

However, because the project would cause adverse and beneficial effects that are similar in nature and magnitude, and because it would affect only a small portion of the Basin's land area, the project would have only a small overall effect on the attainment of this goal/objective, whether it was beneficial or adverse. This effect would not alter the viability of any covered species using upland habitats, and would not necessitate any changes in the conservation strategy of the NBHCP.

## 7 CUMULATIVE EFFECTS

For the Greenbriar project, this section evaluates cumulative effects as defined by NEPA and ESA. In Section 7 of the Greenbriar DEIR, *Other CEQA-Required Analyses*, projects contributing to potential cumulative effects are described and the cumulative impacts of these projects, and the Greenbriar project, are analyzed. That analysis evaluates cumulative effects as defined by Section 15130 of the California Environmental Quality Act Guidelines (State CEQA Guidelines). Because that analysis addresses a range of resources and issues, it is broader and includes more detail on proposed projects than does the following analyses, which only address effects on species covered by the NBHCP.

## 7.1 ANALYSIS OF CUMULATIVE EFFECTS UNDER NEPA

NEPA defines cumulative impacts as those that result "from the incremental impact of the action when added to other past, present, and reasonably foreseeable future actions regardless of what agency (federal or nonfederal) or person undertakes such other actions" (40 CFR 1508.7).

## 7.1.1 CUMULATIVE CONTEXT

The Natomas Basin includes much of the American Basin, which is one of the nine major basins in the Central Valley. Basins are flat, low-lying areas adjacent to the natural levees that form along the major rivers. Theses basins fill with flood waters and over time they accumulate the fine sediments carried by these waters. Prior to urban development, the Natomas Basin would regularly become inundated by the winter river flows, and remain inundated for weeks to months during most years (Kelley 1989; Smith and Verrill 1996). The predominant vegetation was probably seasonal wetland with marsh growing at the lowest elevations, and riparian forest and scrub growing at higher elevations on alluvial soils near the Sacramento and American Rivers.

The City of Sacramento has developed over the past 150-plus years beginning in the late 1840s immediately following the discovery of gold. Over this time the City, and the Sacramento region, has shifted largely, though not entirely, from natural habitat to agriculture and urban development.

Reclamation of the Natomas Basin through a series of levees and drains was first attempted in the 1860s after the state created a Board of Swampland Commissioners. The Board's appointed engineer estimated that the construction of this system of levees and drains would cost only about \$38,000, which was far less than the \$1 per acre fee that had been established to fund such reclamation. This estimate was inaccurate and the project ran out of funds within a year, and inundation of the Natomas Basin continued. It was not until 1915 that a system of levees and drainage and irrigation canals was completed, and the Natomas Basin drained. At that time, virtually the entire basin was converted to agricultural land uses.

In the Natomas Basin, urbanization occurred much later than agricultural uses. In 1924, after almost the entire Natomas Basin had been converted to agricultural land uses, developed land uses were still almost nonexistent. There were few structures, and few roads, most of which were not paved (McClure 1925). By the 1960s, Sacramento International Airport, and major highways had been constructed, and some urban development had begun in the southern Basin, adjacent to Sacramento. Over the next 40 years, this urban development continued, primarily in the southern basin, and by 2001 approximately 21% of the Basin was occupied by developed land cover.

## 7.1.2 Projects Contributing to Cumulative Impacts

#### DEVELOPMENT AUTHORIZED BY THE NBHCP

The NBHCP authorized 17,500 acres of land in the Natomas Basin for development. About two-thirds of this land has yet to be developed. Once this land is developed it is projected to contain over 50,000 homes as well as a variety of other retail, commercial and industrial uses; to date, about 15,000 homes have been constructed (McCarthy and Lamb 2006). This development is occurring in three areas authorized by the NBHCP: North Natomas and Metro Air Park in Sacramento County, and the Measure M area of Sutter County. Authorized development includes projects sponsored by either private developers or public entities that occur within these permitted areas.

This development is described in more detail below, and the effects of this development have previously been analyzed in conjunction with the NBHCP (CH2M HILL 2002). Additional information on the effects caused by this development is also provided in Section 3.3 *Habitat Acreage in the Natomas Basin*, and Appendix B *Change in Natomas Basin Land Cover in 2001–2004*.

## **North Natomas Community Plan**

Development projects in the North Natomas community that have been approved but are yet to be fully built out have been identified and evaluated by the NNCP and the associated environmental review documents prepared in compliance primarily with CEQA.

The North Natomas community is bounded by Elkhorn Boulevard to the north, I-80 to the south, the Natomas East Main Drainage Canal to the east, and the West Main Drain Canal to the west, covering more than 9,000 acres in the northwest portion of the city that was predominantly in agricultural use prior to development. The NNCP provides a long-term vision for the development of the North Natomas community. The environmental consequences from implementation of the NNCP were addressed in the 1986 NNCP EIR (certified by the Sacramento City Council in May 1986) as well as the 1993 Supplement to the 1986 NNCP EIR. Development within the NNCP started to take off in 1999.

There are several development projects that have been approved in the North Natomas community. Some of these projects are fully built-out and occupied at this juncture, while others are still in development phases. These projects are generally located to the south and east of the project site and include: the Westborough project, Cambay West, Natomas Crossing, Natomas Town Center, Panhandle, and Natomas Creek. In 2000, there were approximately 2,002 people, occupying 740 housing units in North Natomas (SACOG 2001). Currently, there are about 15,000 homes (McCarthy and Lamb 2006). At buildout (year 2016), the NNCP estimates a population of 66,495 in the North Natomas community occupying 33,257 housing units on approximately 9,038 acres, and 72,016 employees. Buildout has been rapid since approval of the NNCP and NBHCP, and this trend is expected to continue as a result of high demand for developed uses near downtown Sacramento.

#### **Metro Air Park**

In addition to development anticipated within the North Natomas community, the Metro Air Park is a newly developing project located adjacent to the Sacramento International Airport and along the westerly edge of the Greenbriar site. The Metro Air Park totals 1,983 acres and has been approved for development of approximately 20 million square feet of commercial and industrial development, and off-site infrastructure. This off-site infrastructure includes the widening of Elkhorn Boulevard along the northern border of the Greenbriar site. The project is located in an area that has historically been dominated by agricultural uses. Construction of the Metro Air Park began in September 2003.

Development within the Metro Air Park (authorized by the MAP HCP and NBHCP) will eliminate several canals connecting habitats north and south of Interstate 5, and connecting habitats from the Sacramento International Airport to Highway 99. It will eliminate the Powerline Ditch, No. 4 and 4a ditches, and Meister Canal. It also will eliminate water sources to the Airport East Ditch, and replace the open Central Main Canal with an underground pipe, and will affect habitat along Lone Tree Canal by reducing the area of land draining into Lone Tree Canal and placing urban development along one side of the canal (Thomas Reid Associates 2001, USFWS 2002).

#### Measure M

In 2004, Sutter County voters passed Measure M, an advisory measure intended to provide the Board of Supervisors with an indication of how the citizens of Sutter County feel about the types and level of development in the 7,500-acre area of the South Sutter County Industrial / Commercial Reserve. The southern boundary of the Measure M area forms the Sutter/Sacramento county line, approximately 4 miles north of Greenbriar. The vote did not approve any specific development proposals, but did provide guidance on how development may be viewed in the future. Measure M included potential development for the South Sutter area of the following uses:

- ► At least 3,600 acres for commercial/industrial development;
- ► At least 1,000 acres for schools, parks, other public uses, and retail; and
- ▶ No more than 2,900 acres for residential development, with a population cap of 39,000.

Applications for the Measure M area have not been submitted to Sutter County, as of December 2005, so the specifics of development proposals are not known beyond the parameters outlined above.

#### OTHER PROPOSED PROJECTS CONTRIBUTING TO CUMULATIVE EFFECTS

Several other projects are being planned in the Natomas Basin outside of that areas permitted for development by the NBHCP. These projects are described below.

#### Sacramento International Airport Development Plan

The Airport Development Plan will include the major improvements that are needed over a 20-year planning period. These improvements are safety, security, and capacity enhancement projects that will enable the Sacramento County Airport System to meet customer service goals at increased levels of activity in passengers, air cargo, and aircraft operations.

The plan is still under development; but, the Sacramento International Airport Master Plan Study (PB Aviation 2004) contains a recommended Airport Development Plan that illustrates the type, location, and scale of projects under consideration. Most projects would be within the existing Airport Operations Area (AOA) Outside of the APA, potential projects include roughly 400 acres of development (parking and commercial development) on adjacent land along Interstate 5, and roughly 500 acres of development (aviation-related and commercial development) on adjacent land to the north of the AOA.

The recommended Airport Development Plan also would eliminate several waterways, including:

- ▶ 4.4 miles of the drainage ditch north of Elverta Road,
- ▶ 2.0 miles of the drainage ditch west of Power Line Road,
- ▶ 1.0 miles of the canal adjacent to the access road west of Power Line Road, and
- ▶ 0.5 miles of the drainage ditch along Bayou Road.

Together with the elimination of canals permitted by the MAP HCP, the elimination of these waterways could further reduce connectivity of habitats within the Natomas Basin. However, the effect on connectivity would be addressed during environmental review of development projects at the airport, and avoidance, minimization, and mitigation measures would likely reduce the effect on connectivity to an insignificant level.

## Sacramento Area Flood Control Levee Upgrade Project

To assess the risk of levee failure and to identify potential remedies, SAFCA commissioned the Natomas Levee Evaluation Study in 2005. This study indicated that the risk of flooding at the 100-year level was greater than previously assumed (SAFCA 2006). A variety of remedies were proposed for identified problems. Most of these remedies involve levee improvement and bank protection techniques, including construction of cutoff walls within existing levees, and placement of toe rock and revegetation of banks at locations along existing levees that pose erosion problems. These remedies would cause an estimated 8 acres of permanent habitat loss for species covered by the NBHCP (EDAW 2005).

As a potential remedy, the study also assessed constructing a secondary levee along the upper 5 miles of the east levee of the Sacramento River. This levee would be set back about 1,000 feet from the existing levee. Under this alternative the existing levee would continue to confine the river; the new levee would ensure safe containment of a 200-year flood if the existing levee were to fail. The construction of this levee would directly affect roughly 133 acres of habitat for species covered by the NBHCP. (This estimate assumes a 175-foot wide footprint and is based on additional information in SAFCA 2006, EDAW 2005.) The levee also would bisect several canals and existing TNBC reserves. The overall affect of this potential remedy on covered species also would depend on the future condition of the land between the secondary levee and the Sacramento River, and the future habitat quality of the levee slopes. The design of the secondary levee alternative has not yet been developed to this level of detail.

## Natomas Mutual Water Company American Basin Fish Screen and Habitat Improvement Project (ABFSHIP)

The Natomas Mutual Water Company (Natomas Mutual) annually diverts nearly 100,000 acre feet of water from the Sacramento River and the Natomas Cross Canal and distributes that water throughout the Natomas Basin. Natomas Mutual is currently planning and designing two new diversions to replace its existing five diversions. These pumps would be located along the Sacramento River near Sankey Road and between Elverta Road and Elkhorn Road, respectively. These new diversions would retain the same pumping capacity of the existing diversions (630 cfs), plus an additional 14 cfs to accommodate the Bolen Ranch, which would then eliminate its existing, independent diversion. The new pumps, however, would be variable frequency drive pumps that would facilitate the management of water levels throughout the canal system. Other changes to the current infrastructure would include:

- ► Construction of a new highline canal between the proposed Sankey Diversion along the landside of the Natomas Cross Canal south Levee to the existing Northern Pumping Plant;
- Relocation and extension of the existing Vestal Drain adjacent to the new highline canal between RD 1000's Pumping Plant No. 4 and the new Sankey Diversion site;
- Decommissioning and removal of the existing Verona Diversion Dam and Lift Pumps;
- ► Additional capacity for the internal re-lift pumps at RD 1000 Pumping Plant No. 3 in place of the removed Riverside Pumping Plant;
- ► Re-grading the Riverside Main Highline Canal from RD 1000 pumping Plant No. 3 to the existing Riverside Pumping Plant;
- Upgrading of two control structures, the County Line Check and Lift Pump and the Elkhorn Check and Lift Pumps;
- ► Removing the five pumping plants (two along the Natomas Cross Canal and three along the Sacramento River);

- ▶ Re-grading the North Drainage Canal from the V Drain to Highway 99 in order to improve conveyance; and,
- ► Re-grading the Elkhorn Main Highline Canal between the existing Prichard Pumping Plant and the existing Elkhorn Pumping Plant.

The design and environmental review of these infrastructure improvements have not been completed, and thus it would be speculative and possibly misleading to assess the effects on covered species based on current information. However, many of these improvements are also being considered as part of the Sacramento River Water Reliability Study, for which we have used available information to make a rough estimate of their effects. This estimate is provided in the section below that describes the Sacramento River Water Reliability Study.

## Sacramento River Water Reliability Study

The Sacramento River Water Reliability Study (SRWRS) was initiated in 2002 by the Bureau of Reclamation, Placer County Water Agency (PCWA), Sacramento Suburban Water District (SSWD), City of Roseville (Roseville), and City of Sacramento (Sacramento). Its goal is to develop a water supply plan that is consistent with the Water Forum Agreement (The Water Forum 2000). It would fulfill this goal by provide additional water supply to PCWA for planned urban growth, to SSWD for groundwater stabilization, to Roseville for planned urban growth and a local conjunctive use program, and to Sacramento for water supply reliability and wheeling services with neighboring water purveyors to meet their water supply demands and to reduce their reliance on groundwater. It also would increase the interconnectivity and source redundancy to the water supply system to maximize long-term water supply reliability.

An initial alternatives report has been prepared for this study (USBR 2005) that developed four alternatives. These alternatives are:

- ► SRWS Elverta Diversion Alternative. This alternative consists of a diversion on the Sacramento River with an associated pump station and water treatment plant, and treated water pipelines to water distribution systems of the SRWRS partners. Water pipelines would extend from the Sacramento River across the Natomas Basin along or adjacent to Elverta Road, and from Elverta Road south to the City of Sacramento. Their total length would be approximately 9 miles.
- ▶ Joint SRWS-ABFSHIP Elverta Diversion Alternative. This alternative consists of a consolidated diversion on the Sacramento River and associated facilities to accommodate the needs of the SRWRS partners and the NMWC from the Elkhorn Diversion planned under the ABFSHIP. Water pipelines would extend from the Sacramento River across the Natomas Basin along or adjacent to Elverta Road, and from Elverta Road south to the City of Sacramento. Their total length would be approximately 9 miles.
- ARPS-Elverta Diversion Alternative. This alternative consists of facility expansions by PCWA in Placer County, increased use of groundwater by Roseville, and construction of a diversion on the Sacramento River and of associated treatment and transmission facilities by Sacramento. (Under this alternative, NMWC would construct and operate its planned Elkhorn Diversion independent of the SRWRS, or continue to divert from its existing diversion.) Water pipelines would extend from the Sacramento River along or adjacent to Elverta Road for approximately 5 miles, and from Elverta Road south to the City of Sacramento. Their total length would be approximately 6.5 miles.
- ► ARPS-Joint Sacramento-ABFSHIP Elverta Diversion Alternative. This alternative would include the same facilities as the ARPS-Elverta Alternative plus additional diversion capacity and facilities at the diversion if the ABFSHIP lead agencies select the Sankey/Elkhorn Diversions alternative for the ABFSHIP. Water pipelines would extend from the Sacramento River along or adjacent to Elverta Road for approximately 5 miles, and from Elverta Road south to the City of Sacramento. Their total length would be approximately 6.5 miles.

The effects of these alternatives have been assessed qualitatively relative to each other, but have not yet been quantified. Similarly, specific designs for these pipelines have not been developed and the likely mitigation is not known. Therefore, their potential effects on existing canals, Jacob's slough are not known.

However, a rough estimate of the acreage of affected habitat can be made. Assuming a 100-foot wide corridor of habitat would be permanently eliminated along these pipelines, and that the water treatment plant and associated facilities would eliminate 100 acres of habitat, these alternatives would eliminate from 179 to 209 acres of habitat for covered species. This, however, is probably an overestimate, because the corridor of permanently eliminated habitat would probably be much less than 100 feet wide, particularly if pipelines follow existing roads, which may be the case for most of their length.

## **Downtown Sacramento-North Natomas-Airport Light Rail Line**

Since the early 1990s, the Sacramento Regional Transit District has been considering a light rail line that would connect downtown Sacramento, North Natomas, and the Sacramento International Airport (SACOG 2000). The route proposed for this rail line would pass through areas permitted for development in North Natomas, cross the Greenbriar site, the Metro Air Park, and then run along Interstate 5, and enter the Sacramento International Airport. This project would affect only a small area of habitat for covered species because most of this route is within existing development, areas permitted for development by the NBHCP, or the likely footprint of other proposed projects.

Assuming a 100-foot wide corridor of habitat was lost along this route, the project would eliminate roughly 21 acres outside of areas permitted for development by the NBHCP. About half of this acreage (10 acres) would be on the Greenbriar site, and a portion of the remainder may be within areas considered for development under the recommended Airport Development Plan for Sacramento International Airport (PB Aviation 2004).

Because this rail line has not been designed nor has any environmental review been performed, it is not known what the effects on canals and connectivity would be. Based on the general location of the proposed route, however, these effects appear to be limited. At the Greenbriar site, the rail line would cross Lone Tree Canal on the Meister Way Road crossing proposed by the Greenbriar project. On the north side of Interstate 5 between MAP and Sacramento International Airport, the only canal is adjacent to the off ramp from the interstate, and this canal is currently unsuitable as habitat for giant garter snake.

#### West Lakeside

An application for development within the Joint Vision area is on file for the West Lakeside project. No other applications for the Joint Vision area have been filed and its future development potential is in its early consideration stage by the City and County. As such, development of the Joint Vision is considered separately in this analysis. The West Lakeside project is a proposal located approximately 0.25 mile south of the project site adjacent to the eastern border of West Main Drain Canal. This project would develop 133 acres resulting in 524 residential units, a 10-acre elementary school, and approximately 33 acres of open space land uses (e.g., parks and detention basins). Thus, this project could eliminate up to 133 acres of habitat for species covered by the NBHCP. These effects could include habitat along canals that subsequently drain in to the West Drainage Canal.

## FUTURE POTENTIAL CUMULATIVE PROJECT: CITY/COUNTY JOINT VISION

#### **Joint Vision**

The Joint Vision Plan is a collaborative effort between the City and County of Sacramento to develop a vision for the 10,000-acre area of the County between the northern city limits and Sutter County. Concepts for development have been considered and include a mixture of residential densities, an industrial park (in addition to Metro Air Park), and open spaces throughout, including most extensively in the northern extent separating development from the Sutter County boundary. In fact, a large amount of open space is anticipated to be dedicated (for habitat

preservation and farmland retention) in this area. To date, no land use plans have been adopted, and all considerations to date have been conceptual.

The ultimate development scenario that will be proposed for the Joint Vision area is not known and likely will not be known within the time that this analysis and development are being considered. However, because the development potential of the area is large and it is being actively studied, the Greenbriar EIR and this analysis includes disclosure of the plan to the extent it can be known. It is considered as future potential cumulative development, and because this is a speculative development proposal at this time, it is considered separately and less extensively than the cumulative development that is currently planned and proposed (i.e., specific development proposals have been submitted). The Joint Vision plan will be the subject of extensive CEQA review and consideration by the City and County, neighboring jurisdictions, regulatory agencies including DFG and USFWS, local service providers and the Sacramento County Local Agency Formation Commission (LAFCO), and its likely implementation is best described as unknown.

#### CUMULATIVE EFFECTS OF PROPOSED AND POTENTIAL PROJECTS

Because the extent of habitat prior to conversion to agriculture is unknown, and the location and design of proposed projects has not been fully determined, the total percentage reduction in habitat acreage for covered species cannot be calculated. But, the percentage of the Natomas Basin that has been converted to developed land uses provides a rough approximation of the percentage of habitat for covered species that has been lost.

In 2001, 21% (11,243 acres) of the Basin was in developed uses. By 2004, developed land cover had increased to 24% (12,849 acres). Under the future condition permitted by the NBHCP, 50% (26,769 acres) of the Natomas Basin would be developed or otherwise unsuitable for providing habitat for covered species (e.g., canals and open space inside urban areas). Estimated changes in habitat acreage from 2001 to this future condition are provided by CH2M HILL (2002) and in Section 3.3 *Habitat Acreage in the Natomas Basin*.

In addition to the development permitted by the NBHCP, other projects proposed in the Natomas Basin (and described in the section *Other Proposed Projects Contributing to Cumulative Effects*) would increase the extent of developed land cover in the Natomas Basin (Table 7-1). These projects would likely increase developed land cover from 50% (26,769 acres) of the Natomas Basin (under the NBHCP) to 51.8–52.1% (27,733–27,893 acres) of the Natomas Basin. With the Greenbriar project, this change would increase to 52.9–53.2% (28,322–28,482 acres).

Concurrent with this change in developed land cover, would be an increase in the area preserved and managed for covered species. Assuming that the mitigation ratio for the proposed projects would be between 0.5 and 3 acres preserved for each acre developed, the extent of preserved habitat would increase from 16% (8,566 acres) of the Natomas Basin under the NBHCP to 17.5–24.2% (9,369–12,956 acres) with mitigation land from the additional proposed projects (not including the Greenbriar project). With the additional proposed projects and the Greenbriar project, the portion of the Natomas Basin preserved as habitat for covered species would be 18.3–25.0% (9,797–13,385 acres).

Because design, and even the location, of some proposed projects has not been determined, and the quantity, location, and type of mitigation land (e.g., agricultural land, managed marsh) are not known, detailed assessments of their effects on habitat for each covered species would be somewhat speculative, and possibly misleading.

It is important to note that proposed projects would be required to comply with the federal Endangered Species Act and the California Endangered Species Act. Both of these acts require that impacts to endangered species are minimized and fully mitigated. This minimization and mitigation would lessen the impacts of the proposed projects on biological resources, to the extent that they are not considerable. These projects, therefore, would not be expected to contribute substantially to a cumulatively significant impact on these biological resources.

| Project   | Acres <sup>3</sup> | Notes  |
|---|--------------------|--|
| Sacramento International Airport<br>Development Plan  | 900                | Based on recommended Airport Development Plan in<br>the Sacramento International Airport Master Plan;<br>does not include drainage and stormwater projects<br>outside of development areas.  |
| Sacramento Area Flood Control Levee<br>Upgrade Project  | 8–133              | Based on project description in SAFCA 2006, supplemental information in EDAW 2005, and an assumed 175-foot wide footprint for the secondary levee considered as an alternative in this project.  |
| Natomas Mutual Company American Basin<br>Fish Screen and Habitat Improvement<br>Project (ABFSHIP) | _                  | Most components of this project were included in the acreages estimated for the Sacramento River Water Reliability Study.  |
| Sacramento River Water Reliability Study  | 179–209            | Based on USBR 2005, and an assumption of a 100-<br>foot wide corridor of permanent habitat loss along<br>pipelines, and 100 acres of habitat loss due to facilities<br>at diversions.  |
| Downtown Sacramento-North Natomas-<br>Airport Light Rail Line                                     | 21                 | Based on SACOG 2000, and an assumed 100-foot wide corridor of permanent habitat loss along sections of the route outside of areas permitted for development by the NBHCP or under consideration for development by Sacramento International Airport. |
| West Lakeside   | 133                | Acreage is the proposed project footprint.   |
| Subtotal  | 1,241–1,396        |  |
| Greenbriar  | 546                | This is the acreage of the Greenbriar site minus the 30.6 acre preserve proposed along Lone Tree Canal   |
| Total   | 1,794–1,949        |  |

Similarly, the Greenbriar project also must minimize and fully mitigate impacts to biological resources to comply with the federal Endangered Species Act and California Endangered Species Act. Because this minimization and mitigation would lessen the Greenbriar project's impacts on biological resources, to the extent that they are not considerable, the Greenbriar project would not contribute substantially to a cumulatively significant impact on these biological resources.

In addition to the development authorized by the NBHCP and additional proposed projects, the development in the Joint Vision area represents a potential proposed project. Development within the Joint Vision area could result in the conversion of several thousand acres of open space land that provides various levels of habitat for Swainson's hawk, giant garter snake, and other species that are currently covered by the NBHCP. It would create a landscape in which it would be more difficult to maintain connectivity among TNBC reserves and to sustain the habitat quality of TNBC reserves. It also would create the need to preserve most other privately owned agricultural land in the Natomas Basin as mitigation for species covered by the NBHCP.

It is very likely, and expected, that any development within this area would require a new habitat conservation plan, consistent with the federal Endangered Species Act and the California Endangered Species Act. As stated above, compliance with these laws requires that impacts to endangered species are minimized and fully mitigated.

<sup>&</sup>lt;sup>2</sup> - Proposed projects do not include the Joint Vision, which was considered a potential proposed project.

<sup>&</sup>lt;sup>3</sup> – Permanent loss of agricultural and natural vegetation based on estimates of project footprints.

However, it must be recognized that this level of additional development would be expected to have residual environmental impacts to the various species in the area.

While the extent of potential mitigation for development within this area is not currently known, there is the potential that mitigating all of the effects of the Joint Vision on populations of covered species in the Natomas Basin may not be feasible, and some other means of mitigation could be proposed for consideration. For example, sufficient land may not be available in the Natomas Basin to preserve and enhance as mitigation for the effects of developing the Joint Vision, and out of basin mitigation could be proposed for consideration. However, this possibility is entirely speculative and cannot be evaluated until development of the Joint Vision area is actually proposed. To date, and as described above, there are no formal proposals for development of the Joint Vision area, and there are no proposals to consider for mitigation of species under the ESA or CESA.

#### 7.2 CUMULATIVE EFFECTS UNDER ESA

For the purposes of Federal Endangered Species Act compliance, cumulative effects include the effects of future state, tribal, or private actions that are reasonably certain to occur in the action area considered in this biological opinion (USFWS and NMFS 1998). Future Federal actions that are unrelated to the proposed action are not considered because they require separate consultation pursuant to Section 7 of the Endangered Species Act. In addition, once the Section 7 consultation for a Section 10(a)(1)(B) permit has been completed, non-Federal proposals for development within that Section 10(a)(1)(B) planning area are considered part of the environmental baseline for future consultations. Therefore, for this analysis of cumulative effects, as defined for the Endangered Species Act, development projects within those portions of the Natomas Basin that were authorized for development by the NBHCP are considered part of the environmental baseline. The other currently planned and proposed projects described in the cumulative effects analysis in the Greenbriar DEIR and in the NEPA cumulative effects analysis (presented in the preceding section) will require Federal actions and therefore are also not considered in this ESA cumulative effects analysis. (For example, these potential future projects would require a permit to fill wetlands under Section 404 of the Clean Water Act.)

An undetermined number of future State or private actions could occur in the Natomas Basin without a 404 permit to fill wetlands or an ITP through Section 10 of the ESA. Future state or private actions that could potentially affect species covered by the NBHCP include actions that affect:

- ▶ herbicide or pesticide applications,
- vegetation management along canals or drains,
- ▶ agricultural practices (including crop types cultivated, and fallowing or abandonment of land),
- discharge of contaminants into waterways,
- presence of humans along waterways or on agricultural lands,
- ► canal flow regimes, or
- ► traffic levels on local roads.

All of these activities can degrade habitat or cause the injury or death of covered species. Changes in these activities can be caused by state and private actions on agricultural lands. Such changes regularly occur, for example, in response to market conditions and new technologies. For example, the recent increase in water prices in the Natomas Basin is likely to result in changes in crop acreages in the Natomas Basin. Also, in anticipation of development, rice may be fallowed (although land use changes during 2001-2004 do not indicate this has occurred during that time period [Appendix B]). However, attempting to predict the changes in agricultural practices that are likely to occur in the Natomas Basin over long periods of time, and their consequences for species covered by the NBHCP, would be speculation.

Similarly, numerous state and private actions in developed areas also could affect covered species through the same set of mechanisms (herbicide or pesticide applications, vegetation management along canals or drains, etc.), and not all of these actions would involve a federal action and future consultation under Section 7 of the ESA.

Yet, attempting to predict the changes in activities in developed areas that are likely to occur in the Natomas Basin, and their consequences for species covered by the NBHCP, also would be speculation. We are not aware of any state or private actions (for which there is no related federal actions) that are reasonably certain to occur in developed areas of the Natomas Basin and whose effects will significantly affect covered species.

#### 8 REFERENCES

- Allan, J. D. 2004. Landscapes and riverscapes: the influence of land use on stream ecosystems. *Annual Review of Ecology and Systematics* 35:257-284.
- Aresco, Matthew, J. 2005. Mitigation Measures to Reduce Highway Mortality of Turtles and Other Herpetofauna at a North Florida Lake. In *Journal of Wildlife Management* 69(2)549–560.
- Aubry, Craig. U.S. Fish and Wildlife Service, Sacramento, CA. November 4, 2005 email correspondence with Amanda Olekszulin regarding Greenbriar project.
- Barry, S. J., and H. B. Shaffer. 1994. The status of the California tiger salamander (*Ambystoma californiense*) at Lagunita: a 50-year update. *Journal of Herpetology* 28:159–164.
- Baxter, C.V., K.D. Fausch, M. Murakami and P.L. Chapman. 2004. Non-native stream fish invasion restructures stream and riparian forest food webs by interrupting reciprocal prey subsidies. *Ecology* 85: 2656-2663.
- Baxter, C.V., K.D. Fausch and W. C. Saunders. In press. Tangled webs: Reciprocal flows of invertebrate prey link streams and riparian zones. *Freshwater Biology*.
- Baxter, C.V., K.D. Fausch, M. Murakami and P.L. Chapman. In review. Invaders disrupt cross-habitat subsidies to native consumers: an experimental-comparative study in stream salmonids. *Ecology*.
- Beale, Colin M. and Pat Monaghan. 2004. Human disturbance: people as predation-free predators? In *Journal of Applied Ecology* 41:335–343.
- Bechard, M. J. 1982. Effect of vegetative cover on foraging site selection by Swainson's Hawk. *Condor* 84: 153–159.
- Beedy, E. C., and W. J. Hamilton III. 1999. Tricolored Blackbird (*Agelaius tricolor*). In *The Birds of North America*, No. 423 (A. Poole and F. Gill, eds.). *The Birds of North America*, Inc., Philadelphia, PA.
- Beedy, E. C. and A. Hayworth. 1991. Breeding status, distribution and habitat association of tricolored blackbirds (*Agelaius tricolor*), 1850-1989. (JSA 88-187). Prepared by Jones and Stokes Associates, Inc., Sacramento, CA for the U. S. Fish and Wildlife Service, Sacramento, CA. Cited in Natomas Basin Habitat Conservation Plan.
- Belknap, H. W. 1957. Observations on the White-faced Ibis (*Plegadis chihi*) in Louisiana. M.S. thesis, Louisiana State University, Baton Rouge. Cited in Ryder, R. A., and D. E. Manry. 1994. White-faced Ibis (*Plegadis chihi*). In *The Birds of North America*, No. 130 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Bent, A. C. 1937. Life histories of North American birds of prey, Part 1. Bulletin of the United States National Museum 167. Cited in England, A. S., M. J. Bechard, and C. S. Houston. 1997. Swainson's Hawk (*Buteo swainsoni*). In *The Birds of North America*, No. 265 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, PA, and the American Ornithologists' Union, Washington, D.C.
- Berryman Ecological. 2005. Greenbriar Farms section 7 biological assessment. Prepared for North Natomas 575 Investors LLC, Sacramento, CA. Prepared by Berryman Ecological, Meadow Vista, CA.
- Blair, R. B. 1996. Land use and avian species along an urban gradient. *Ecological Applications* 6:506-519.

- Bloom, P. H. 1980. The status of the Swainson's Hawk in California, 1979. Wildlife Management Branch, Nongame Wildlife Investigation, Job II–8.0. California Department of Fish and Game, Sacramento, CA. Cited in *Natomas Basin Habitat Conservation Plan*.
- Blumstein, Daniel T., Laura L. Anthony, Robert Harcourt, and Geoff Ross. 2003. Testing a key assumption of wildlife buffer zones: is flight initiation distance a species-specific trait? In *Biological Conservation* 110:97–100.
- Blumton, A. K. 1989. Factors affecting Loggerhead Shrike mortality in Virginia. M.S. thesis, Virginia Polytechnic Institution and State University, Blacksburg, VA. Cited in Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In *The Birds of North America*, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Bonnet, Xavier, Guy Naulleau, and Richard Shine. 1999. The dangers of leaving home: dispersal and mortality in snakes. In *Biological Conservation* 89: 39–50.
- Bray, M. P. 1986. Feeding ecology of White-faced Ibises in the Lahontan Valley, Nevada. P-R Report, Federal Aid Project. W-53-R, Study I, Jobs 02, Nevada Department of Wildlife, Reno, NV. Cited in Ryder, R. A., and D. E. Manry. 1994. White-faced Ibis (*Plegadis chihi*). In *The Birds of North America*, No. 130 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Bray, M. P., D. A. Klebenow. 1988. Feeding ecology of White-faced Ibises in a Great Basin valley, USA. Colonial Waterbirds 11: 24–31. Cited in Ryder, R. A., and D. E. Manry. 1994. White-faced Ibis (*Plegadis chihi*). In The Birds of North America, No. 130 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Brinson, M. M., L. J. MacDonnell, D. J. Austen, R. L. Beschta, T. A.Dillaha, D. L. Donahue, S. V. Gregory, J. W. Harvey, M. C. Molles, E. I. Rogers, and J. A. Stanford. 2002. Riparian areas: functions and strategies for management. Washington, D.C.: Committee on Riparian Zone Functioning, National Research Council.
- Brode, J. and G. Hansen. 1992. Status and Future Management of the Giant Garter Snake (*Thamnophis gigas*) within the Southern American Basin, Sacramento and Sutter Counties, California. California Department of Fish and Game, Inland Fisheries Division, Endangered Species Project. Sacramento, CA. Cited in Natomas Basin Habitat Conservation Plan.
- Brooks, B. L. 1988. The breeding distribution, population dynamics, and habitat availability of an upper midwest Loggerhead Shrike population. M.S. thesis, University of Wisconsin, Madison, WI. Cited in Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In The Birds of North America, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Bury, R. B. 1972. The effects of diesel fuel on a stream fauna. California Fish and Game 58:291–295. Cited in U.S. Fish and Wildlife Service. 1999a. Draft recovery plan for the giant garter snake (*Thamnophis gigas*). Portland, OR.
- California Department of Fish and Game. 1988. Five-year status report: Swainson's Hawk. California Department of Fish and Game, Wildlife Management Division, Nongame Bird and Mammal Section, Sacramento, CA. Cited in Natomas Basin Habitat Conservation Plan.
- ———. 2005. Change in Area of Winter-Flooded and Dry Rice in the Northern Central Valley of California Determined by Satellite Imagery. In *California Fish and Game* 91(3):207–215.

- Center for Biological Diversity. 2001. California Endangered Species Act listing petition for the California tiger salamander. <a href="http://www.sw-center.org/swsbd/search.html">http://www.sw-center.org/swsbd/search.html</a>>
- CH2M Hill. 2003. Natomas Basin Habitat Conservation Plan impacts to covered species. Prepared for City of Sacramento and Sutter County. Prepared by CH2M Hill, Sacramento, CA.
- City of Sacramento, Sutter County, and Natomas Basin Conservancy. 2003. Final Natomas Basin Habitat Conservation Plan. Prepared for U.S. Fish and Wildlife Service and California Department of Fish and Game.
- Clevenger, Anthony P., Bryan Chruszcz, and Kari Gunson. 2001. Drainage culverts as habitat linkages and factors affecting passage by mammals. In *Journal of Applied Ecology* 38:1340–1349.
- CNDDB (California Natural Diversity Database). 2005. California Department of Fish and Game, Natural Heritage Division. Sacramento, CA.
- Cogswell, H. L. 1977. Water birds of California. University of California Press, Berkeley. Cited in Ryder, R. A., and D. E. Manry. 1994. White-faced Ibis (*Plegadis chihi*). In The Birds of North America, No. 130 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Collinge, S. K., M. Holyoak, C. B. Barr, and J. T. Marty. 2001. Riparian habitat fragmentation and population persistence of the threatened valley elderberry longhorn beetle in Central California. Biological Conservation 100:103-113.
- Collister, D. M. 1994. Breeding ecology and habitat preservation of the Loggerhead Shrike in southeastern Alberta. M.S. thesis, University of Calgary, Calgary, AB. Cited in Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In The Birds of North America, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Cooke, A. S. 1980. Observations on How Close Certain Passerine Species Will Tolerate an Approaching Human in Rural and Suburban Areas. In *Biological Conservation* 18:85–88.
- Craig, R. B. 1978. An analysis of the predatory behavior of the Loggerhead Shrike. Auk 95: 221–234. Cited in Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In The Birds of North America, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Crooks, K. R., and M. E. Soulé. 1999. Mesopredator release and avifaunal extinctions in a fragmented system. Nature 400:563-566.
- Crooks, K. R., A. V. Suarez, D. T. Bolger and M. E. Soule. 2001. Extinction and colonization of birds on habitat islands. Conservation Biology 15:159-172.
- DeHaven, R. L. 2000. Breeding tricolored blackbirds in the Central Valley, California: a quarter-century perspective. U. S. Fish and Wildlife Service. Cited in Natomas Basin Habitat Conservation Plan.
- DeGeus, D. W. 1990. Productivity and habitat preferences of Loggerhead Shrikes inhabiting roadsides in a midwestern agroenvironment. M.S. thesis, Iowa State University, Ames, IA. Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In The Birds of North America, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.

- DeSnoo, G. R. and P. J. de Wit. 1998. Buffer zones for reducing pesticide drift to ditches and risks to aquatic organisms. Ecotoxicology and Environmental Safety 41:112–118.
- Dodd, Jr., C. Kenneth, William J. Barichivich, and Lora L. Smith. 2004. Effectiveness of a barrier wall and culverts in reducing wildlife mortality on a heavily traveled highway in Florida. In *Biological Conservation* 118:619–631.
- EDAW. 2005. Natomas Levee Evaluation Project: evaluation of potential effects on terrestrial biological resources and cultural resources. January 19, 2005. Memo prepared by EDAW, Sacramento, CA. Prepared for SAFCA, Sacramento, CA.
- ———. 2006. Greenbriar Development Project Sacramento, California: Administrative Draft Environmental Impact Report. Prepared for: Environmental Planning Services, City of Sacramento, Sacramento, CA. Prepared by EDAW, Sacramento, CA.
- Environmental Law Institute [ELI]. 2003. Conservation Thresholds for Land Use Planners. Washington, DC.
- England, A. S., M. J. Bechard, and C. S. Houston. 1997. Swainson's Hawk (*Buteo swainsoni*). In The Birds of North America, No. 265 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, PA, and the American Ornithologists' Union, Washington, D.C.
- England, A. S., J. A. Estep, W. R. Holt. 1995. Nest-site selection and reproductive performance of urban-nesting Swainson's Hawks in the Central Valley of California. *Journal of Raptor Research* 29: 179–186.
- Estep, J. A. 1989. Biology, movements and habitat relationships of the Swainson's hawk in the Central Valley of California, 1986-87. California Department of Fish and Game, Nongame Bird and Mammal Section Report. Cited in Natomas Basin Habitat Conservation Plan.
- ———. 2003. Nesting Swainson's Hawks (Buteo swainsoni) in the Natomas Basin Habitat Conservation Plan Area, 2003 Annual Survey Results. Prepared for The Natomas Basin Conservancy. Sacramento, CA.
- Estep, J. A. and S. Teresa. 1992. Regional Conservation planning for the Swainson's hawk (Buteo swainsonii) in the Central Valley of California. Pages 775-789 in D. R. McCullough and R. H. Barrett (eds.). Wildlife 2001: populations. Elsevier Applied Science, New York, NY.
- Fisher, David. Office manager, Natomas Mutual Water Company, Natomas, CA. September 27, 2005 telephone conversation with John Hunter, EDAW regarding effect of Greenbriar project on water supply, delivery, and availability.
- Forman, R. T. T. and L. E. Alexander. 1998. Roads and their ecological effects. *Annual Review of Ecology and Systematics* 29:207-231.
- Forman, R. T. T., D. Sperling, J. A. Bissonette, A. P. Clevenger, C. D. Cutshall, V. H. dale, L. Fahrig, R. France, C. R. Goldman, K. Heanue, J. A. Jones, F. J. Swanson, T. Turrentine, and T. C. Winter. 2003. Road ecology: science and solutions. Island Press, Covelo, CA.
- Frid, Alejandro and Lawrence Dill. 2002. Human-caused Disturbance Stimuli as a Form of Predation Risk. In *Conservation Ecology* 6(1):11. Available <a href="http://www.consecol.org/vol6/iss1/art11">http://www.consecol.org/vol6/iss1/art11</a>.
- Garrison, B. A. 1999. Bank Swallow (*Riparia riparia*). In The Birds of North America, No. 414 (A. Poole and F. Gill, eds.). *The Birds of North America*, Inc., Philadelphia, PA.
- Garrison, B. A., J. M. Humphrey, S. A. Laymon. 1987. Bank Swallow distribution and nesting ecology on the Sacramento River, California. Western Birds 18: 71–76. Cited in Garrison, B. A. 1999. Bank Swallow

- (*Riparia riparia*). In *The Birds of North America*, No. 414 (A. Poole and F. Gill, eds.). *The Birds of North America*, Inc., Philadelphia, PA.
- Gibbs, James P. and Gegory Shriver. 2002 (December). Estimating the Effects of Road Mortality on Turtle Populations. In *Conservation Biology* 16(6):1647–1652.
- Gill, Jennifer A., Ken Norris, and William J. Sutherland. 2001. Why behavioral responses may not reflect the population consequences of human disturbance. In *Biological Conservation* 97:265–268.
- Gleason, R. S. 1978. Aspects of the breeding biology of Burrowing Owls in southeastern Idaho. M.S. thesis, University of Idaho, Moscow, ID. Cited in Haug, E. A., B. A. Millsap, and M. S. Martell. 1993. Burrowing Owl (*Speotyto cunicularia*). In *The Birds of North America*, No. 61 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Grinnell, J. and A. H. Miller. 1944. The distribution of the birds of California. *Pacific Coast Avifauna* No. 27. Cited in *Natomas Basin Habitat Conservation Plan*.
- Guyot, Ghislaine and Jean Clobert. 1997. Conservation Measures for a Population of Hermann's Tortoise (*Testudo hermanni*) in Southern France Bisected by a Major Highway. In *Biological Conservation* 79:251–256.
- Hansen, Eric. Private consultant, Natomas, CA. October 20, 2005 written comments on a preliminary draft of the biology section for the Greenbriar project DEIR provided to Leo Edson, EDAW.
- Hansen, G. E. 1988. Review of the status of the giant garter snake (*Thamnophis couchi gigas*) and its supporting habitat during 1986–1987. Final report for California Department of Fish and Game, Contract C-2060. Cited in U.S. Fish and Wildlife Service. 1999a. Draft Recovery Plan for the Giant Garter Snake (*Thamnophis gigas*). Portland, OR.
- ———. 1998. Cherokee Canal Sediment Removal Project Post-construction Giant Garter Snake (Thamnophis gigas) Surveys. Final report for California Department of Water Resources, Contract No. B-81535. Unpublished. 9 pp.
- Hansen, G. E. and J. M. Brode. 1980. Status of the Giant Garter Snake (Thamnophis couchii gigas) (Fitch). *Inland Fisheries Endangered Species Special Publication* 80(5):1–14. California Department of Fish and Game. Sacramento, CA.
- ———. 1993. Results of relocating canal habitat of the giant garter snake (*Thamnophis gigas*) during widening of State Route 99/70 in Sacramento and Sutter counties, California. Final report for Caltrans Interagency Agreement 03E325 (FG7550) (FY 87/88-91-92). Cited in U.S. Fish and Wildlife Service. 1999a. Draft recovery plan for the giant garter snake (*Thamnophis gigas*). Portland, OR.
- Haug, E. A., B. A. Millsap, and M. S. Martell. 1993. Burrowing Owl (*Speotyto cunicularia*). In *The Birds of North America*, No. 61 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Haug, E. A. and L. W. Oliphant. 1990. Movements, activity patterns, and habitat use of burrowing owls in Saskatchewan. Journal of Wildlife Management 54:27-35. Cited in Haug, E. A., B. A. Millsap, and M. S. Martell. 1993. Burrowing Owl (*Speotyto cunicularia*). In *The Birds of North America*, No. 61 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.

- Hayes, D. W., K. R. McAllister, S. A. Richardson, and D. W. Stinson. 1999. Washington state recovery plan for the western pond turtle. Olympia, WA: Washington Department of Fish and Wildlife.
- Helm, B. 1998. The biogeography of eight large branchiopods endemic to California. Pages 124–139 in C. W. Witham, E. Bauder, D. Belk, W. Ferren, and R. Ornduff (eds.), Ecology, conservation, and management of vernal pool ecosystems proceedings from a 1996 conference. Sacramento, CA: California Native Plant Society. Cited in *Natomas Basin Habitat Conservation Plan*.
- Helzer C. J. and D. E. Jelinski. 1999. The relative importance of patch area and perimeter-area ratio to grassland breeding birds. *Ecological Applications* 9:1448-1458
- Hinsley, S. A., P. E. Bellamy and I. Newton. 1995. Bird species turnover and stochastic extinction in woodland fragments. *Ecography* 18:41-50.
- Holland, D. C. 1991. Status and reproductive dynamics of a population of western pond turtles (*Clemmys marmorata*) in Klickitat County, Washington in 1990. Unpublished report. Olympia, WA: Washington Department of Wildlife.
- Holmes, Tamara L., Richard L. Knight, Libby Stegall, and Gerald R. Craig. 1993. Responses of Wintering Grassland Raptors to Human Disturbance. In *Widl. Soc. Bull.* 21:461–468.
- Huxel, G. R. 2000. The effect of the Argentine ant on the threatened valley elderberry longhorn beetle. *Biological Invasions* 2:81–85.
- Ikuta, Laurie A. and Daniel T. Blumstein. 2003. Do fences protect birds from human disturbance? In *Biological Conservation* 112:447–452.
- Jaeger, Jochen A. G. and Lenore Fahrig. 2004 (December). Effects of Road Fencing on Population Persistence. In *Conservation Biology* 18(6):1651–1657.
- Jennings, M. R., and M. Hayes. 1994. Amphibian and reptile species of special concern in California.

  Sacramento. California Department of Fish and Game, Inland Fisheries Division. Rancho Cordova, CA.

  Cited in *Natomas Basin Habitat Conservation Plan*.
- Johnsgard, P. A. 1990. Hawks, eagles, and falcons of North America. Smithsonian Institution Press, Washington, D.C. Cited in *Natomas Basin Habitat Conservation Plan*.
- Jones & Stokes. 2005. Biological effectiveness monitoring for the Natomas Basin Habitat Conservation Plan Area 2004 annual survey results (agency version). Prepared for The Natomas Basin Conservancy, Sacramento, CA. Prepared by Jones & Stokes, Sacramento, CA.
- Kelley, R. 1989. Battling the inland sea: floods, public policy, and the Sacramento Valley. University of California Press, Berkeley, CA.
- Knight, R. L., H. A. L. Knight and R. J. Camp. 1995. Common ravens and number and type of linear rights-of-way. *Biological Conservation* 74:65-67.
- Kridelbaugh, A. L. 1982. An ecological study of Loggerhead Shrikes in central Missouri. M.S. thesis, University of Missouri, Columbia. Cited in Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In *The Birds of North America*, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.

- Leidy, G. R. 1992. Ecology, status and management of the giant garter snake (*Thamnophis gigas*). Prepared for Sutter Bay Associates and the North Natomas Landowners Association, Inc.
- Lepczyk, Christopher A., Angela G. Mertig, and Jianguo Liu. 2003. Landowners and cat presation across rural-to-urban landscapes. In *Biological Conservation* 115: 191–201.
- Loredo, I., D. Van Vuren, and M. L. Morrison. 1996. Habitat use and migration behavior of the California tiger salamander. Journal of Herpetology 30:282–285.
- Luukkonen, D. R. 1987. Status and breeding ecology of the Loggerhead Shrike in Virginia. M.S. thesis, Virginia Polytechnic Institution and State University, Blacksburg, VA. Cited in Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In The Birds of North America, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Marchand, Michael N. and John A. Litvaitis. 2004 (June). Effects of Habitat Features and Landscape Composition on the Population Structure of a Common Aquatic Turtle in a Region Undergoing Rapid Development. In Conservation Biology 18(3):758–767.
- Marzluff, J. M., R. Bowman, and R. Donnelly, editors. 2001. Avian ecology and conservation in an urbanizing world. Kluwer Academic Publishers, New York.
- Mcarthy, M. and C. Lamb. 2006. New Natomas levee angst: Army Corps of Engineers declaration adds heft to reports of risky protection. May 26. Sacramento Business Journal 23(11):1.
- McClure, W. F. 1925. Sacramento flood control project revised plans. Submitted to The Reclamation Board. California State Printing Office, Sacramento, CA.
- Miller, A. H. 1931. Systematic revision and natural history of the American shrikes (*Lanius*). University of California Publishing, Zoology 38: 11–242. Cited in Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In The Birds of North America, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Miller, A. H. 1951. A comparison of the avifaunas of Santa Cruz and Santa Rosa islands, California. Condor 53: 117–123. Cited in Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In *The Birds of North America*, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Miller, J. R., J. A. Wiens, N. T. Hobbs, and D. M. Theobald. 2003. Effects of human settlement on bird communities in lowland riparian areas of Colorado (USA). *Ecological Applications* 13:1041–1059.
- Miller, Scott G., Richard L. Knight, and Clinton K. Miller. 2001. Wildlife responses to pedestrians and dogs. In *Wildlife Society Bulletin* 29(1):124–132.
- Moore, A. A. and M. A. Palmer. 2005. Invertebrate biodiversity in agricultural and urban headwater streams: implications for conservation and management. *Ecological Applications* 15:1169-1177.
- Moseby, K. E. and J. L. Read. 2006. The efficacy of feral cat, fox and rabbit exclusion fence designs for threatened species protection. In *Biological Conservation* 127:429-437.
- Natomas Basin Conservancy. 2004. Biological effectiveness monitoring for the Natomas Basin Habitat Conservation Plan Area 2004 annual survey results (agency version).

- NatureServe. 2005. NatureServe Explorer: An online encyclopedia of life. Version 4.5. NatureServe, Arlington, Virginia. Available <a href="http://www.natureserve.org/explorer">http://www.natureserve.org/explorer</a>>.
- Nisbet, Ian C. T. Date unavailable. Commentary: Disturbance, Habituation, and Management of Waterbird Colonies. In *Waterbirds* 23(2):312–332.
- Noss, R. F., H. B. Quigley, H. G. Hornocker, T. Merrill, and P. C. Paquet. 1996. Conservation biology and carnivore conservation in the Rocky Mountains. Conservation Biology 10:949–963.
- Novak, P. G. 1989. Breeding ecology and status of the Loggerhead Shrike in New York state. M.S. thesis, Cornell University, Ithaca, NY. Yosef, R. 1996. Cited in Loggerhead Shrike (*Lanius ludovicianus*). In The Birds of North America, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Ng, Sandra J., Jim W. Dole, Raymond M. Sauvajot, Seth P. D. Riley, and Thomas J. Valone. 2004. Use of highway undercrossings by wildlife in southern California. In *Biological Conservation* 115:499–507.
- Odell, E. A., and R. L. Knight. 2001. Songbird and medium sized mammal communities associated with exurban development in Pitkin County Colorado. *Conservation Biology*. 15:1143-1150.
- Padre Associates. 2005. Fisherman's Lake buffer zone study. January 15, 2005 version. Padre Associates, Sacramento, CA.
- Paul, Michael J. and Judy L. Meyer. 2001. Streams in the Urban Landscape. Annual Review of Ecology and Systematics 32:333–365.
- PB Aviation. 2004. Sacramento International Airport master plan study. Prepared by Parsons Brinkerhoff Aviation, Sacramento, CA. Prepared for Sacramento County Airport System, Sacramento, CA.
- Pellet, Jerome, Antoine Guisan, and Nicolas Perrin. 2004 (December). A Concentric Analysis of the Impact of Urbanization on the Threatened European Tree Frog in an Agricultural Landscape. In *Conservation Biology* 18(6):1599–1606.
- Phillips, Gregory E., William Alldredge, and William W. Andree. 2001. Mitigating Disturbance of Migrating Mule Deer Caused by Cyclists and Pedestrians at a Highway Underpass Near Vail, Colorado. Available <a href="http://repositories.cdlib.org/jmie/roadeco/Philips2001a">http://repositories.cdlib.org/jmie/roadeco/Philips2001a</a>>. Davis, CA. John Muir Institute of the Environment, Road Ecology Center, University of California, Davis.
- Richardson, Cary T. and Clinton K. Miller. 1997. Recommendations for protecting raptors from human disturbance: a review. In *Wildlife Society Bulletin* 25(3)634–638.
- Risbey, Danielle A., Michael C. Calver, Jeff Short, J. Stuart Bradley, and Ian W. Wright. 2000. The impact of cats and foxes on the small vertebrate fauna of Heirisson Prong, Western Australia. II. A field experiment. In *Wildlife Research* 27: 223–235.
- Roberts, John. Executive director. The Natomas Basin Conservancy, Natomas, CA. October 24, 2005 email correspondence with John Hunter, EDAW, regarding questions about current TNBC preserve management.
- Rodgers, Jr., James A. and Henry T. Smith. 1995 (February). Set-Back Distances to Protect Nesting Bird Colonies form Human Disturbance in Florida. In *Conservation Biology* 9(1)89–99.
- ——. 1997. Buffer zone distances to protect foraging and loafing waterbirds from human disturbance in Florida. In *Wildlife Society Bulletin* 25(1)139–145.

- Rodriguez, Alejandro, Giulia Crema, and Miguel Delibes. 1996. Use of non-wildlife passages across a high speed railway by terrestrial vertebrates. In *Journal of Applied Ecology* 33:1527–1540.
- Rosen, Philip C. and Charles H. Lowe. 1994. Highway Mortality of Snakes in the Sonoran Desert of Southern Arizona. In Biological Conservation 68:143–148.
- Rosenberg, D., B. Noon, and E. Meslow. 1997. Biological corridors: form, function, and efficacy. Bioscience 47:677–687.
- Ross, P. V. 1974. Ecology and behavior of a dense colony of Burrowing Owls in the Texas Panhandle. M.S. thesis, West Texas State University, Canyon, TX. Cited in Haug, E. A., B. A. Millsap, and M. S. Martell. 1993. Burrowing Owl (*Speotyto cunicularia*). In The Birds of North America, No. 61 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Ryder, R. A. 1967. Distribution, migration and mortality of the White-faced Ibis (*Plegadis chihi*) in North America. Bird-Banding 38: 257–277. Cited in Ryder, R. A., and D. E. Manry. 1994. White-faced Ibis (*Plegadis chihi*). In The Birds of North America, No. 130 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Ryder, R. A., and D. E. Manry. 1994. White-faced Ibis (*Plegadis chihi*). In The Birds of North America, No. 130 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- SACOG (Sacramento Area Council of Governments). 2000. Sacramento International Airport Transit Access Study. Sacramento Area Council of Governments, Sacramento, CA.
- Semlitsch, R. D. and J. R. Bodie. 2003. Biological criteria for buffer zones around wetlands and riparian habitats for amphibians and reptiles. *Conservation Biology* 17:1219–1228.
- Shaffer, H. B. and R. Fisher. 1991. Final report to the California Department of Fish and Game: California tiger salamander surveys, 1990. Contract (FG9422). Rancho Cordova, CA: California Department of Fish and Game, Inland Fisheries Division.
- Shaffer, H. B., and S. Stanley. 1992. Final report to California Department of Fish and Game: California tiger salamander surveys, 1991. Contract (FG9422). Rancho Cordova, CA: California Department of Fish and Game, Inland Fisheries Division.
- Sheffield, S.R. 1997. Current status, distribution, and conservation of the burrowing owl in Midwestern North America. Pp. 399-407 in J.R. Duncan, D.H. Johnson, and T.H. Niccolls, (eds.). Biology and conservation of owls of the Northern Hemisphere. U.S.D.A. Forest Service, GTR NC-190. North Central Forest Experiment Station, St. Paul, MN. Cited in Haug, E. A., B. A. Millsap, and M. S. Martell. 1993. Cited in Burrowing Owl (*Speotyto cunicularia*). In The Birds of North America, No. 61 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Silveria, J. G. 1998. Avian uses of vernal pools and implications for conservation practice. Pages 92–106 in C. W. Witham, E. Bauder, D. Belk, W. Ferren, and R. Ornduff (eds.), Ecology, conservation, and management of vernal pool ecosystems proceedings from a 1996 conference. Sacramento, CA: California Native Plant Society.
- Small, A. 1994. California birds: their status and distribution. Ibis Publishing Company, Vista, CA. Cited in Natomas Basin Habitat Conservation Plan.

- Smith, D. W. and W. L. Verrill. 1996. Vernal pool-soil-landform relationships in the Central Valley, California. Pages 15–23 in C. W. Witham, E. T. Bauder, D. Belk, W. R. Ferren, and R. Ornduff (eds.) Ecology, conservation, and management of vernal pool ecosystems: proceedings from a 1996 conference. California Native Plant Society, Sacramento, CA.
- Stahlecker, D. W. 1975. Impacts of a 230 kV transmission line on Great Plains wildlife. M.S. thesis, Colorado State University, Fort Collins, CO. Cited in Connelly, J. W., S. T. Knick, M. A. Schroeder, and S. J. Stiver. 2004. Conservation assessment of Greater Sage-Grouse and sagebrush habitats. Western Association of Fish and Wildlife Agencies. Unpublished Report. Cheyenne, Wyoming, USA.
- Stebbins, R. C. 1972. California amphibians and reptiles. Berkeley, CA: University of California Press. Cited in Natomas Basin Habitat Conservation Plan.
- Steen, David A. and James P. Gibbs. 2004. Effects of Roads on the Structures of Freshwater Turtle Populations. In *Conservation Biology* 18(4):1143–1148.
- Steenhof, K., M. N. Kochert AND J. A. Roppe. 1993. Nesting by raptors and common ravens on electrical transmission line towers. Journal of Wildlife Management 57:271-281.
- Swainson's Hawk Technical Advisory Committee (SHTAC). 2001. Nesting Swainson's hawks (*Buteo swainsoni*) in the Natomas Basin Habitat Conservation Plan Area, 2001 annual survey results. Prepared for the Natomas Basin Conservancy. September, 2001. Cited in Natomas Basin Habitat Conservation Plan.
- Thelander, C. G. (ed). 1994. *Life on the Edge: A Guide to California's Endangered Natural Resources: Wildlife*. BioSystems Books. Santa Cruz, CA.
- The Natomas Basin Conservancy [TNBC]. 2006. Draft briefing paper on the NBHCP fee. The Natomas Basin Conservancy, Sacramento, CA.
- The Water Forum. 2000. Water forum agreement. The Water Forum, Sacramento, CA. Available at: http://www.waterforum.org/AGREE.HTM
- Thomas Reid Associates. 2000. Draft habitat conservation plan for the Metro Air Park project in the Natomas Basin, Sacramento County, California. Prepared for Metro Air Park Property Owners Association. Prepared by Thomas Reid Associates, Palo Alto, CA. November 2000. Cited in Natomas Basin Habitat Conservation Plan.
- Thomas Reid Associates. 2001. Habitat conservation plan for the Metro Air Park project in the Natomas Basin, Sacramento County, California. Prepared for Metro Air Park Property Owners Association. Prepared by Thomas Reid Associates, Palo Alto, CA.
- Trenham, P. C. and H. B. Schaffer. In review. Upland spatial distribution and habitat use in a declining amphibian. Section of Evolution and Ecology and Center for Population Biology, UC Davis.
- Trost, C. H.1989. White-faced Ibis, *Plegadis chihi*. Pp. 57–58 in Rare, sensitive, and threatened species of the Greater Yellowstone Ecosystem (T. W. Clark, A. H. Harvey, R. D. Dorn, D. L. Genter, and C. Groves, eds.). Northern Rockies Conservation Cooperative, Jackson, WY. Cited in Ryder, R. A., and D. E. Manry. 1994. White-faced Ibis (*Plegadis chihi*). In The Birds of North America, No. 130 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- USBR (U.S. Bureau of Reclamation). 2005. Sacramento River water reliability study: initial alternatives report, final version. U.S. Bureau of Reclamation, Sacramento, CA.

- U.S. Fish and Wildlife Service. 1984. Recovery plan for the valley elderberry longhorn beetle. Portland, OR. —. 1992. 90-Day finding and commencement of status reviews for a petition to list the western pond turtle and California red-legged frog. Federal Register 57(193):45761-45762. —. 1996. Mitigation guidelines for the valley elderberry longhorn beetle. Sacramento, CA. —. 1997. Programmatic Formal Consultation for U.S. Army Corps of Engineers 404 Permitted Projects with Relatively Small Effects on the Giant Garter Snake within Butte, Colusa, Glenn, Fresno, Merced, Sacramento, San Joaquin, Solano, Stanislaus, Sutter and Yolo Counties, California. Letter to Art Champ, U.S. Army Corps of Engineers, from Joe Medlin, Field Supervisor, U.S. Fish and Wildlife Service, Sacramento Fish and Wildlife Office, Sacramento, CA. —. 1999a. Draft recovery plan for the giant garter snake (*Thamnophis gigas*). Portland, OR. —. 1999b. Conservation guidelines for the valley elderberry longhorn beetle. Updated July 9, 1999. —. 2001. Final environmental impact statement for the Metro Air Park habitat conservation plan. U.S. Fish and Wildlife Service, Sacramento, CA. —. 2002. Intraservice biological opinion and conference opinion on issuance of a Section 10(a)(1)(B) incidental take permit to the Metro Air Park Property Owners Association for urban development in the Natomas Basin, California. U. S. Fish and Wildlife Service, Sacramento Fish and Wildlife Office, Sacramento, CA. —. 2003. Intra-service biological opinion on issuance of a section 10(a)(1)(B) incidental take permit to the City
- USFWS and NMFS. 1998. Endangered species consultation handbook: procedures for conducting consultation and conference activities under Section 7 of the Endangered Species Act.

Counties, California. U.S. Fish and Wildlife Service, Sacramento, CA.

of Sacramento and Sutter County for urban development in the Natomas Basin, Sacramento and Sutter

- Wellicome, T.I., G.L. Holroyd, K. Scalise, and E.R. Wiltse. 1997. The effects of predator exclusion and food supplementation on burrowing owl population change in Saskatchewan. Pp. 487-497 in J.R. Duncan, D.H. Johnson, and T.H. Niccolls, (eds.). Biology and conservation of owls of the Northern Hemisphere. U.S.D.A. Forest Service, GTR NC-190. North Central Forest Experiment Station, St.Paul, MN. Cited in Haug, E. A., B. A. Millsap, and M. S. Martell. 1993. Burrowing Owl (*Speotyto cunicularia*). In The Birds of North America, No. 61 (A. Poole and F. Gill, Eds.). Philadelphia: The Academy of Natural Sciences; Washington, D.C.: The American Ornithologists' Union.
- Wenger, S. 1999. A Review of the Scientific Literature on Riparian Buffer Width, Extent and Vegetation. Revised Version. March 5. Prepared for the Office of Public Service & Outreach, Institute of Ecology, University of Georgia. Athens, Georgia.
- Wildlands, Inc. 2005. *Greenbriar Project: Draft Conceptual Habitat Restoration Design*. Wildlands, Inc., Rocklin, CA.
- Wylie, G. and M. Cassaza. 2000. Investigation of Giant Garter Snakes in the Natomas Basin: 1998-1999. U.S. Geological Survey-Biological Resources Division, Dixon, CA. Cited in *Natomas Basin Habitat Conservation Plan*.

- Wylie, G. D., M. Cassaza, and J. K. Daugherty. 1997. 1996 progress report for the giant garter snake study. Preliminary report, U.S. Geological Survey, Biological Resources Division. Cited in Natomas Basin Habitat Conservation Plan.
- Yanes, Miguel, José M. Velasco, and Francisco Suárez. 1995. Permeability of Roads and Railways to Vertebrates: the Importance of Culverts. In *Biological Conservation* 71:217–222.
- Yosef, R. 1996. Loggerhead Shrike (*Lanius ludovicianus*). In The Birds of North America, No. 231 (A. Poole and F. Gill, eds.). The Academy of Natural Sciences, Philadelphia, and The American Ornithologists' Union, Washington, D.C.
- Yosef, R., T. C. Grubb. 1992. Territory size influences nutritional condition in non-breeding Loggerhead Shrikes: a ptilochronology approach. *Conservation Biology* 6: 447–449.
- ———. 1994. Resource dependence and territory size in Loggerhead Shrikes. Auk 111: 465–469.
- Zeiner, D. C., W. F. Laudenslayer, and K. E. Mayer (eds.). 1988. California's wildlife. Volume I: Amphibians and reptiles. California Statewide Wildlife Habitat Relationships System. Sacramento, CA: California Department of Fish and Game.
- Zeiner, D. C., W. F. Laudenslayer, K. E. Mayer and M. White (eds.). 1990a. California's wildlife. Volume II: Birds. California Statewide Wildlife Habitat Relationships System. Sacramento, CA: California Department of Fish and Game.
- Zeiner, D. C., W. F. Laudenslayer, Jr., K. E. Mayer, and M. White (eds.). 1990a. California's wildlife. Volume III: Mammals. California Statewide Wildlife Habitat Relationships System. Sacramento, CA: California Department of Fish and Game.

| Appendix A |
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Assessment of Avoidance and Minimization of Construction-Related Effects and Human Wildlife Conflicts

# APPENDIX A ASSESSMENT OF AVOIDANCE AND MINIMIZATION OF CONSTRUCTION-RELATED EFFECTS AND HUMAN-WILDLIFE CONFLICTS

The effects analysis evaluates the overall effect of the Greenbriar project on the viability of species covered by the NBHCP, on the effectiveness of the NBHCP conservation strategy, and on the attainment of the goals and objectives of the NBHCP. As part of that evaluation, this appendix evaluates the effectiveness and completeness of the Greenbriar project's avoidance and minimization measures.

The NBHCP includes a goal and objective that address avoidance and minimization of direct impacts and of human wildlife conflicts. These are listed below.

**Overall Goal 4.** Ensure that direct impacts of Authorized Development upon Covered Species are avoided or minimized to the maximum extent practicable. (NBHCP, page I-16)

**Overall Objective 1.** Minimize conflicts between wildlife and human activities, including conflicts resulting from airplane traffic, roads and automobile traffic, predation by domestic pets, and harassment by people. (NBHCP, page I-16).

To attain this goal and this objective, the NBHCP includes a set of avoidance and minimization measures to be implemented where applicable. For these measures, we assessed the effects of the Greenbriar Project on their effectiveness as avoidance and minimization measures for activities covered by the NBHCP. We also used this set of measures from the NBHCP to assess the effectiveness and completeness of the Greenbriar project's avoidance and minimization measures.

### EFFECTIVENESS OF NBHCP MEASURES WITH THE GREENBRIAR PROJECT

For each of the NBHCP's land use agency's conservation measures, the potential for the Greenbriar project to reduce the measure's effectiveness as a means of avoiding or minimizing construction-related effects or human-wildlife conflicts was evaluated. The Greenbriar project would not alter the effectiveness of any of these measures. Most of these NBHCP measures are seasonal avoidance or exclusion zone measures based on the ecology of the species and the nature of construction activities. Because no individual construction project alters this basis, there are few means by which one construction project could affect the effectiveness of these measures. For example, the effectiveness of pre-construction surveys for a particular species is largely unaffected by the extent or location of development. Similarly, the effectiveness of requiring that developers consult with the USFWS regarding covered species observed during preconstruction surveys also is unaffected by development on other sites. Similarly, the ability to apply these measures to a development project in general would not be altered by the effects of another development project.

It is possible, however, that by fragmenting habitat, a development project can create barriers to animal movement to and from a future development site. In this instance, the effectiveness measures that reduce construction-caused mortality by allowing animals to leave construction sites would likely be reduced because animals may no longer be able to move to habitat outside of the construction site. For example, NBHCP measures 3 and 7 are intended to increases the movement of giant garter snakes off of construction sites. If a construction site is isolated from other giant garter snake habitat, these measures would be ineffective. The Greenbriar project is not more likely to cause this set of circumstances than are projects permitted by the NBHCP. The Greenbriar site is isolated from the development authorized by the NBHCP by Interstate 5 and SR 99, and development of the Greenbriar site

therefore would not reduce the connectivity of areas authorized for development by the NBHCP to habitat in the remainder of the Natomas Basin.

The assessment of all of the land use agency's conservation measures of the NBHCP is summarized below.

#### MEASURES FOR PRE-CONSTRUCTION SURVEYS

The effectiveness of pre-construction surveys is based on each species' ecology and on the attributes of the site being surveyed and the biologist's conduct of the survey. The Greenbriar project would not affect this basis of the effectiveness of pre-construction surveys, nor would it affect the ability to implement pre-construction surveys for development authorized by the NBHCP.

#### MEASURE FOR PRESERVATION OF THE AREA ADJACENT TO FISHERMAN'S LAKE

This measure consists of the City agreeing to initiate a North Natomas Community Plan amendment to potentially widen the agricultural buffer along the City side of Fisherman's lake to 800 feet wide. The Greenbriar site is not in or adjacent to this zone. The project would, however, preserve the Natomas 130 site, which is in and adjacent to this zone. The preservation of the Natomas 130 site is unlikely to affect the City's initiation of an amendment to potentially widen an agricultural buffer along Fisherman's Lake. The project also would not otherwise affect the City's initiation of an amendment to potentially widen an agricultural buffer at this site.

#### **GENERAL MEASURES TO MINIMIZE TAKE**

The NBHCP includes four general measures to minimize take. These measures are to 1) protect large trees, 2) incorporate native plants into buffers, developed areas and parks, 3) schedule construction activities to avoid the raptor nesting season, and 4) conduct pre-construction surveys at an appropriate time of year. The Greenbriar project would not affect the ability to implement these measures. But, development at the Greenbriar site might affect the habitat value of protected trees or native vegetation incorporated into landscaping.

In general, additional development could affect the value for wildlife of preserved trees and natural vegetation incorporated into landscaping by increasing the isolation of these features from natural or agricultural vegetation that provides habitat. To do so, additional development would have to reduce connectivity between the preserved tree or native vegetation inside a developed area and habitat outside of the developed area. Because Interstate 5 and SR 99 already separate the Greenbriar site from the City of Sacramento, this potential effect would be limited to possible consequences for Swainson's hawks nesting in a preserved tree within the City of Sacramento adjacent to the Greenbriar site. While this effect is conceivable, no Swainson's hawk nests are known within 1 mile to the east of the Greenbriar site, and a future nest in this portion of the City of Sacramento, while possible is unlikely and would not have limited access to foraging habitat even if the Greenbriar site remained undeveloped.

Conversely, the Greenbriar project's preservation, enhancement, and restoration of the Natomas 130 and Spangler sites, which are adjacent to areas authorized for development under the NBHCP, could increase the effectiveness of the measures to preserve large trees in developed areas and to incorporate native vegetation into buffers and landscaping. Because trees may not be preserved and native species may not be planted in the vicinity of these sites, this effect may not occur.

#### MEASURES TO MINIMIZE TAKE OF VERNAL POOL SPECIES

The Greenbriar project would not affect vernal pool habitat, is not near vernal pool habitat, and would not affect the ability to implement the measures in the NBHCP. Therefore, the Greenbriar project would not alter the effectiveness of measures for minimizing the take of vernal pool-associated species or alter the effectiveness of these measures.

#### MEASURES TO REDUCE TAKE FOR INDIVIDUAL SPECIES

#### MEASURES TO REDUCE TAKE OF GIANT GARTER SNAKE

The NBHCP includes twelve measures to reduce take of giant garter snake by construction activities. Construction of the Greenbriar project will not reduce the effectiveness of these measures at sites authorized for development by the NBHCP. These measures include a seasonal restriction on site preparation and grading, preconstruction surveys, dewatering of canals prior to excavation, minimization of grading, construction monitoring, a restriction on the use of materials that could entangle giant garter snakes, and measures for fences and barriers along the North Drainage Canal and the East Drainage Canal to restrict the movement of giant garter snake into adjacent development.

The effectiveness of seasonal restrictions, preconstruction surveys and of restrictions on materials that could entangle snakes are based on the ecology of giant garter snakes, site attributes, how the conduct of the survey is conducted, and the nature of construction activities. Individual construction projects, including the Greenbriar project, would not alter this basis, or otherwise affect the effectiveness of these measures.

Measures for dewatering of canals or to cease development if a construction monitor locates a giant garter snake on-site also, in general would not be affected by other development projects. But, if another development project were to fragment habitat and thus reduce the ability of a snake to move from a construction site to suitable habitat off-site, then the effectiveness of these measures would be reduced. The Greenbriar project is not likely to cause this situation for development projects authorized by the NBHCP. The Greenbriar site is isolated from the development authorized by the NBHCP by I-5 and SR 99, and development of the Greenbriar site therefore would not reduce the connectivity of areas authorized for development by the NBHCP to habitat in the remainder of the Natomas Basin. Thus, the effectiveness of these measures would not be reduced.

The Greenbriar site is not adjacent to the North Drainage Canal or the East Drainage Canal. Therefore, it is unlikely to affect the effectiveness of measures for fences and barriers along these waterways.

#### MEASURES TO REDUCE TAKE OF SWAINSON'S HAWK

The NBHCP includes a measure to reduce cumulative effects on Swainson's hawk foraging habitat, five measures to reduce disturbance of nest trees, and seven measures to prevent or mitigate the loss of nest trees.

The measure to reduce cumulative effects established a 1 mile-wide Swainson's hawk zone along the Sacramento River along within which there would be no development. This zone was established because Swainson hawk nests are concentrated along the Sacramento River. The Greenbriar project is not in or adjacent to this zone, and thus it would not alter its effectiveness.

The measures to reduce disturbance of nest trees are based on the ecology of Swainson's hawk and the nature of construction activities; this basis would not be altered by the Greenbriar project. The Greenbriar project also would not affect the ability to implement these measures.

#### MEASURES TO REDUCE TAKE TO VALLEY ELDERBERRY LONGHORN BEETLE (VELB)

These measures include the avoidance of VELB habitat, and measures for the transplanting of elderberry bushes and for the planting and monitoring of elderberry bushes. The Greenbriar project would not affect the ability to avoid, transplant, plant, or monitor elderberry bushes, nor would it affect the effectiveness of those measures for reducing the take of VELB. (The project does not affect VELB habitat except for preserving a small area of land [at the Natomas 130 site] at which planting or natural establishment of elderberry could provide suitable habitat for VELB at a desirable location.)

#### MEASURES TO REDUCE TAKE ON TRICOLORED BLACKBIRD

Measures for pre-construction surveys and exclusion zones around nesting colonies are included in the NBHCP as measures to reduce the take of tricolored blackbird. The Greenbriar project would not affect the ability to conduct pre-construction surveys or establish exclusion zones at construction sites in areas that were authorized for development by the NBHCP.

#### MEASURES TO REDUCE TAKE ON ALEUTIAN CANADA GOOSE

Measures for pre-construction surveys and consultation with USFWS and CDFG (if Aleutian Canada goose is present) are included in the NBHCP as measures to reduce the take of Aleutian Canada goose. The Greenbriar project would not affect the ability to conduct pre-construction surveys at construction sites in areas that were authorized for development by the NBHCP or to consult with USFWS or CDFG if Aleutian Canada goose is present.

#### MEASURES TO REDUCE TAKE ON WHITE-FACED IBIS

Measures for pre-construction surveys and a seasonal restriction on construction activities within a ¼ mile of active nests were included in the NBHCP. The Greenbriar project would not affect the ability to conduct pre-construction surveys at construction sites in areas that were authorized for development by the NBHCP or to seasonally restrict construction at sites authorized for development by the NBHCP.

#### MEASURES TO REDUCE TAKE ON LOGGERHEAD SHRIKE

Measures for pre-construction surveys and exclusion zones around active nests are included in the NBHCP as measures to reduce the take of loggerhead shrike. The Greenbriar project would not affect the ability to conduct pre-construction surveys or establish exclusion zones at construction sites in areas that were authorized for development by the NBHCP.

#### MEASURES TO REDUCE TAKE OF BURROWING OWL

Several measures to reduce the take of burrowing owls are included in the NBHCP. These measures include, preconstruction surveys, establishment of exclusion zones, seasonal restrictions on the disturbance of occupied nests, relocation of owls, and mitigation for disturbed nests. The Greenbriar project would not affect the ability to conduct preconstruction surveys, restrict activities, or establish exclusion zones at construction sites in areas that were authorized for development by the NBHCP. The Greenbriar project also would not affect the feasibility or potential benefits of relocating owls or of mitigating effects on burrowing owls. Therefore, the Greenbriar project would not affect the effectiveness of measures for reducing the take of burrowing owl.

#### MEASURES TO REDUCE TAKE ON BANK SWALLOW

Pre-construction surveys and establishment of an exclusion zone (if a bank swallow colony is present) are included in the NBHCP as measures to reduce the take of bank swallow. The Greenbriar project would not affect the ability to conduct pre-construction surveys or establish exclusion zones at construction sites in areas that were authorized for development by the NBHCP.

#### MEASURES TO REDUCE TAKE ON NORTHWESTERN POND TURTLE

The only measure included in the NBHCP to reduce take of northwestern pond turtle is the canal dewatering requirement that was included for giant garter snake. The Greenbriar project would not affect the dewatering of canals in areas authorized for development by the NBHCP, or the ability of animals to move from dewatered canals to suitable habitat off-site. (The Greenbriar site is only directly connected to areas authorized for

development through the Lone Tree Canal crossing of I-5, and the ability of turtles to use this crossing and to move up Lone Tree Canal would not be reduced by the Greenbriar project.)

#### MEASURES TO REDUCE TAKE ON CALIFORNIA TIGER SALAMANDER

The Greenbriar project would not affect California tiger salamander habitat, is not near California tiger salamander habitat, and would not affect the ability to implement the measures in the NBHCP. Therefore, the Greenbriar project would not alter the effectiveness of measures for minimizing the take of California tiger salamander.

#### MEASURES TO REDUCE TAKE ON WESTERN SPADEFOOT TOAD

The Greenbriar project would not affect western spadefoot toad habitat, is not near western spadefoot toad habitat, and would not affect the ability to implement the measures in the NBHCP. Therefore, the Greenbriar project would not alter the ability to implement measures for minimizing the take of western spadefoot toad.

### MEASURES TO REDUCE TAKE OF VERNAL POOL FAIRY SHRIMP, VERNAL POOL TADPOLE SHRIMP, AND MIDVALLEY FAIRY SHRIMP

The Greenbriar project would not affect habitat for these branchiopod species, is not near habitat for these branchiopod species, and would not affect the ability to implement the measures in the NBHCP. Therefore, the Greenbriar project would not alter the effectiveness of measures for minimizing the take of vernal pool fairy shrimp, vernal pool tadpole shrimp, and midvalley fairy shrimp.

#### MEASURES TO REDUCE TAKE OF DELTA TULE PEA

The NBHCP includes a pre-construction survey and the opportunity to transplant any Delta tule pea located during the survey as measures to reduce take of Delta tule pea. The Greenbriar project would not affect the ability to conduct pre-construction surveys of sites authorized for development by the NBHCP, or to transplant Delta tule pea to suitable habitat elsewhere. Therefore, the Greenbriar project would not affect the effectiveness of these measures at reducing take of Delta tule pea.

#### MEASURES TO REDUCE TAKE ON SANFORD'S ARROWHEAD

The NBHCP includes a pre-construction survey and the opportunity to transplant any Delta tule pea located during the survey as measures to reduce take of Sanford's arrowhead. The Greenbriar project would not affect the ability to conduct pre-construction surveys of sites authorized for development by the NBHCP, or to transplant Sanford's arrowhead to suitable habitat elsewhere. Therefore, the Greenbriar project would not affect the effectiveness of these measures at reducing take of Sanford's arrowhead.

### MEASURES TO REDUCE TAKE ON BOGGS LAKE HEDGE-HYSSOP, SACRAMENTO ORCUTT GRASS, SLENDER ORCUTT GRASS, COLUSA GRASS, AND LEGENERE

The Greenbriar project would not affect habitat for these vernal pool-associated plant species, is not near vernal pool habitat, and would not affect the ability to implement the measures in the NBHCP for minimizing the take of these species. Therefore, the Greenbriar project would not alter the effectiveness of these measures.

## ASSESSMENT OF AVOIDANCE AND MINIMIZATION BY THE GREENBRIAR PROJECT

For this assessment, the avoidance and minimization measures in the NBHCP were considered a comprehensive set of effective measures to avoid and minimize the construction-related effects and human-wildlife conflicts potentially resulting from the NBHCP.

Development at the Greenbriar site is comparable to the development permitted by the NBHCP, and the construction-related effects and human-wildlife conflicts potentially caused by the Greenbriar are the same as those potentially caused by the development permitted by the NBHCP.

Therefore, for comparable effects potentially caused by the Greenbriar project, incorporation of the applicable measures from the NBHCP was considered to be avoidance and minimization to the maximum extent practicable. The NBHCP's avoidance and minimization measures related to development were reviewed to determine the measures that were applicable to the Greenbriar project, and if the measure or a comparable (but more specific or stringent) measure was incorporated into the Draft Environmental Impact Report (DEIR). All applicable measures (or comparable but more stringent measures) were incorporated into the DEIR. The results of this assessment are summarized in Table A-1.

In addition, the Greenbriar project could cause other effects that differ from those addressed by the avoidance and minimization measures of the NBHCP. These effects are the construction and human-wildlife conflict-related effects on giant garter snakes and giant garter snake habitat along Lone Tree Canal. Avoiding and minimizing these effects to the maximum extent practicable requires measures in addition to the applicable measures from the NBHCP. The DEIR mitigation for the Greenbriar project contains a comprehensive set of such measures to avoid, minimize, and mitigate human disturbance and other related effects on giant garter snake use of Lone Tree Canal. These measures include:

- a. To ensure that the project does not diminish habitat connectivity for giant garter snake between the southwest and northwest zones identified in the NBHCP, approximately 30.6 acres along Lone Tree Canal shall be protected and managed as giant garter snake habitat. This on-site habitat preservation shall protect an approximately 250-foot wide corridor of giant garter snake habitat that includes the canal and approximately 200 feet of adjacent uplands. Uplands within the linear open space/buffer area shall be managed as perennial grassland as described below. Additional aquatic habitat for giant garter snake shall be created along the east bank of Lone Tree Canal by construction and maintenance of a 2.7 acre tule bench. The habitat shall be managed in perpetuity as high-quality habitat for giant garter snake. Compliance and biological effectiveness monitoring shall be performed and annual monitoring reports prepared within six months of completion of monitoring for any given year. This monitoring, reporting, and adaptive management shall be performed as described in Section IV of the NBHCP.
- b. To ensure that the project does not diminish giant garter snake movement along Lone Tree Canal, all new road crossings of Lone Tree Canal shall be designed to minimize obstacles to giant garter snake movement. The use of culverts under new road crossings on Lone Tree Canal shall be prohibited unless it can be demonstrated that the culverts will not diminish the potential for giant garter snake movement through the section of Lone Tree Canal protected by the setback fence and conservation easement.
- c. Upland giant garter snake habitat within the Lone Tree Canal linear open space/buffer area shall be created and managed to provide cover, basking areas, and refugia during the winter dormant period. Hibernaculae would be constructed at regular intervals by embedding concrete or coarse rock in the bank or in a berm along the Lone Tree Canal corridor to provide additional winter refugia. Upland habitat with the linear open space/buffer areas shall be converted to native perennial grassland and managed, in perpetuity, as perennial grassland habitat.
- d. Aquatic habitat shall be maintained throughout the giant garter snake active season in Lone Tree Canal, in perpetuity. This is the legal responsibility and obligation of Metro Air Park property owners (MAP). The MAP HCP includes provisions for maintaining water in the canal such that the basic habitat requirements of the giant garter snake are met. The MAP HCP also provides a road map, through "Changed Circumstances", to address procedures to follow if water is not being maintained in the canal to meet these requirements. As described in the MAP HCP, the MAP is legally obligated to assure these requirements are met, and financial and procedural mechanisms are included in the MAP HCP to enforce this. It is, therefore, assumed that MAP

will provide water to Lone Tree Canal, as required by the MAP HCP and ITP, in perpetuity. It is also assumed that USFWS will use all reasonable means available to it, to enforce this MAP HCP requirement. If water is not provided to Lone Tree Canal by the MAP to meet the habitat requirements of giant garter snake, as required by the MAP HCP, and USFWS exhausts its enforcement responsibilities, the project applicant shall assume the responsibility of providing suitable giant garter snake aquatic habitat throughout the section of Lone Tree Canal protected by the fence and conservation easement. However, as stated herein, the project applicant shall only assume this responsibility if it has been sufficiently demonstrated to the City that USFWS has exhausted all reasonable means to compel MAP to comply with the relevant conditions of the MAP ITP. Specific requirements related to ensuring suitable aquatic habitat in Lone Tree Canal is present, in perpetuity, throughout the giant garter snake active season shall be developed through consultation with DFG and USFWS, and included in the new or amended HCP for Greenbriar, and may include mechanisms, such as installation of a well, to assure water is provided in the canal to meet habitat requirements.

- e. A barrier shall be installed between the giant garter snake habitat linear open space/buffer area and the adjacent Greenbriar development to ensure that giant garter snakes do not enter the development area, and to prohibit humans and pets from entering the giant garter snake habitat. The design of this barrier shall be subject to USFWS and CDFG review and approval. The entire length of the barrier, which shall be bordered by yards rather than roadways, shall be maintained on the preserve side by a nonprofit land trust to ensure that vegetation or debris does not accumulate near the barrier and provide opportunities for wildlife and pets to climb over the barrier. On the development side, Covenants, Codes and Restrictions (CCRs) shall prohibit accumulation of vegetation or debris adjacent to the barrier. Chain link fencing shall be placed at both ends of the corridor, with locked gates permitting entry only by RD 1000 and NMWD for channel maintenance, and by the preserve manager for habitat monitoring and maintenance purposes.
- f. Specific requirements associated with the barrier shall be developed through consultation with USFWS and DFG, and may include the following and/or other specifications that DFG and USFWS consider to be equally or more effective:
  - Adequate height and below-ground depth to prevent snakes or burrowing mammals from providing a through-route for snakes by establishing burrows from one side to the other crossing;
  - ► Constructed using extruded concrete or block construction extending a minimum of 36-inches above ground level;
  - Maintenance to repair the barrier and to prevent the establishment of vegetation or collection of debris that could provide snakes with a climbing surface allowing them to breech the barrier;
  - A cap or lip extending at least two-inches beyond the barrier's vertical edge to prevent snakes from gaining access along the barrier's top edge; and
  - ▶ Signage to discourage humans and their pets from entering the area.
- g. The Lone Tree Canal linear open space/buffer area shall be protected in perpetuity under a conservation easement and managed to sustain the value of this area for giant garter snake habitat connectivity. Compliance and biological effectiveness monitoring shall be performed and annual monitoring reports prepared. This monitoring, reporting, and adaptive management shall be performed as described in Section IV of the NBHCP or following procedures developed in formal consultation with USFWS and DFG and contained in an ESA Incidental Take Permit for the Greenbriar project.

The need for, and purpose and effectiveness of, these additional measures are described in Section 3.5 *Connectivity of Habitat in the Natomas Basin* and in Section 4.1 *Giant Garter Snake*.

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|    |            | Mitigation for   | the Project   |           |  |
|----|------------|--|---------------|-----------|--|
|    |            | Natomas Basin HCP Measure  | Applicability | Inclusion | Rationale  |
| 1. | or into o  | e-construction Surveys (p V-1) shall be conducted not less than 30 days more than 6 months prior to commencement of construction activities, determine the status and presence of, and likely impacts to, all Covered ecies on the site. Pre-construction surveys for an individual species may completed up to one year in advance if the sole period for reliable ection of that species is between May 1 and December 31. | Applicable    | Included  | Comparable and more stringent measures have been included in the mitigation proposed in the project's DEIR for each species with potential to occur on-site. |
| 2. | to t<br>Na | servation of the Area Adjacent to Fisherman's Lake (p V-2): Pursuant the Settlement Agreement, the City has agreed to initiate a North tomas Community Plan amendment to potentially widen the icultural buffer along the City side of Fisherman's lake to 800 feet the.   | N/A           |           | This measure is specific to locations outside the project area.  |
| 3. | Ge         | neral Measures to Minimize Take (p V-3)  |               |           |  |
|    | a.         | Tree Preservation: Valley oaks and other large trees should be preserved whenever possible. Preserve and restore stands of riparian trees used by Swainson's hawks and other animals for nesting, particularly adjacent to Fisherman's Lake.   | N/A           | Included  | The Greenbriar site currently has not large trees.   |
|    | b.         | Native Plants: Improve the wildlife value of landscaped parks, buffers, and developed areas by planting trees and shrubs which are native to the Natomas Basin and therefore are used by native animals.   | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.  |
|    | c.         | Protect Raptor Nests: Avoid the raptor nesting season when scheduling construction near nests. Specific avoidance criteria are set forth in the species specific measures later in this chapter.   | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.  |
|    | d.         | Protected Plant/Animal Species, also referred to as "Special Status Species": Search for protected plant species during flowering season prior to construction and protected animal species during the appropriate season.   | Applicable    | Included  | Comparable and more specific measures have been included in the mitigation proposed in the project's DEIR for each species with potential to occur on-site.  |
| 4. | Me         | easures to Minimize Take of Vernal Pool Species (p V-3)  | N/A           |           | No vernal pool habitat exists on site.   |
|    | a.         | General Biological Survey and Information Required (p V-4): In the event a biological reconnaissance survey or the pre-construction survey identifies that vernal pool resources are on-site, a vernal pool species specific biological assessment must be provided during the appropriate season (as established by USFWS) to determine the type  | N/A           |           | No vernal pool habitat exists on site.   |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|    | witigation for the Project |   |               |           |  |  |  |
|----|----------------------------|---|---------------|-----------|--|--|--|
|    |                            | Natomas Basin HCP Measure   | Applicability | Inclusion | Rationale                              |  |  |
|    | and                        | d abundance of species present.   |               |           |  |  |  |
|    | 1.                         | Where site investigations indicate vernal pool species may occur, the developer shall notify the Land Use Agency regarding the potential for impacts to vernal pool species.  | N/A           |           | No vernal pool habitat exists on site. |  |  |
|    | 2.                         | USFWS and CDFG shall identify specific measures required to avoid, minimize and mitigate impacts to vernal pool species to be implemented prior to disturbance and in accordance with adopted standards or established guidelines.  | N/A           |           | No vernal pool habitat exists on site. |  |  |
|    | 3.                         | The requirement by USFWS to preserve a vernal pool within development would be based on identification of an intact vernal pool with minimal disturbance where the presence of one or more of the following species is recorded: slender orcutt grass, Sacramento orcutt grass, Colusa grass, or vernal pool tadpole shrimp. No such preservation requirement shall be made unless the vernal pool is a suitable site for TNBC Mitigation Lands.  | N/A           |           | No vernal pool habitat exists on site. |  |  |
|    | 4.                         | Such vernal pool areas, including any required buffer land dedication, shall apply toward the Land Acquisition Fee component of the development project's NBHCP mitigation obligation.  | N/A           |           | No vernal pool habitat exists on site. |  |  |
| b. | Mi                         | tigation Strategies (p. V-5)  | N/A           |           | No vernal pool habitat exists on site. |  |  |
|    | 1.                         | Avoidance and Preservation On-Site to Minimize Impacts: In the event USFWS requires on-site preservation in accordance with Section a.3 above, on-site mitigation shall be required. In the event USFWS does not require on-site mitigation, a developer or private land owner may still propose to dedicate fee title or conservation easement for that portion of the property with vernal pool resources and an associated 250-foot buffer surrounding the vernal pool resource to the TNBC. If the dedication is accepted, a reduction in the Land Acquisition Fee portion of the habitat Mitigation Fee shall be granted the developer for the portion (calculated on an acreage basis) of the site permanently preserved by easement or dedication. However, habitat Mitigation Fees, in full, must be paid on the remaining developable acreage on the site, and all fees other than Land Acquisition Fees shall be paid | N/A           |           | No vernal pool habitat exists on site. |  |  |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|           | Mitigation for   | the Project   |           |  |
|-----------|--|---------------|-----------|--|
|           | Natomas Basin HCP Measure  | Applicability | Inclusion | Rationale  |
|           | for all acres on the site. Additional conditions to preserve the biological integrity of the site (such as reasonable drainage conditions) may be imposed by the Land Use Agency in consultation with TNBC and the TAC.  |               |           |  |
| 2.        | Construction Period Avoidance and Relocation of Vernal Pool Resources (p. V-6).  | N/A           |           | No vernal pool habitat exists on site.   |
|           | a. No grading, development or modification of the vernal pool<br>site or the buffer area extending 250 feet around the<br>perimeter of the vernal pool site may occur during the vernal<br>pool "wet" season as identified by USFWS. Protective<br>fencing shall be established around the perimeter of the<br>vernal pool site and the buffer area during the vernal pool<br>wet season.  | N/A           |           | No vernal pool habitat exists on site.   |
|           | b. In consultation with TNBC and the TAC, soils and cysts from the vernal pool may be relocated as soon as practicable during the dry season to a suitable TNBC or other reserve site provided the relocation/recreation site is approved by TNBC, and the USFWS.  | N/A           |           | No vernal pool habitat exists on site.   |
| 3.        | Payment Into a USFWS Approved Conservation Bank (p. V-6). In the event all of the above approaches are not appropriate for the site, the Land Use Agency shall require the developer to purchase credits from a USFWS-approved mitigation bank in accordance with the following mitigation ratios: 2:1 for preservation in mitigation banks, 1:1 for creation in mitigation banks, 3:1 for preservation in acres outside of mitigation banks, 2:1 for creation in acres outside of mitigation banks. | N/A           |           | No vernal pool habitat exists on site.   |
| 5. Measur | res to Reduce Take for Individual Species (p. V-7)   |               |           |  |
| a. Me     | easures to Reduce Take of Giant Garter Snake (p. V-7)  |               |           |  |
| 1.        | Within the Natomas Basin, all construction activity involving disturbance of habitat, such as site preparation and initial grading, is restricted to the period between May 1 and September 30. This is the active period for the giant garter snake and direct mortality is lessened, because snakes are expected to actively move and avoid danger.  | Applicable    | Included  | A comparable and more detailed measure has been included in the mitigation proposed in the project's DEIR. |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|    | Natomas Basin HCP Measure  | Applicability | Inclusion | Rationale  |
|----|--|---------------|-----------|--|
| 2. | Pre-construction surveys for giant garter snake, as well as other NBHCP Covered Species, must be completed for all development projects by a qualified biologist approved by USFWS. If any giant garter snake habitat is found within a specific site, the following additional measures shall be implemented to minimize disturbance of habitat and harassment of giant garter snake, unless such project is specifically exempted by USFWS.  | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR, combined with measure 4 below. |
| 3. | Between April 15 and September 30, all irrigation ditches, canals, or other aquatic habitat should be completely dewatered, with no puddled water remaining, for at least 15 consecutive days prior to the excavation or filling in of the dewatered habitat. Make sure dewatered habitat does not continue to support giant garter snake prey, which could detain or attract snakes into the area. If a site cannot be completely dewatered, netting and salvage of prey items may be necessary. This measure removes aquatic habitat component and allows giant garter snakes to leave on their own. | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                                |
| 4. | For sites that contain giant garter snake habitat, no more than 24-hours prior to start of construction activities (site preparation and/or grading), the project area shall be surveyed for the presence of giant garter snake. If construction activities stop on the project site for a period of two weeks or more, a new giant garter snake survey shall be completed no more than 24-hours prior to the re-start of construction activities.   | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                                |
| 5. | Confine clearing to the minimal area necessary to facilitate construction activities. Flag and designate avoided giant garter snake habitat within or adjacent to the project as Environmentally Sensitive Areas. This area shall be avoided by all construction personnel.  | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                                |
| 6. | Construction personnel completing site preparation and grading operations shall receive USFWS approved environmental awareness training. This training instructs workers on how to identify giant garter snakes and their habitats, and what to do if a giant garter snake is encountered during construction activities. During this training an on-site biological monitor shall be  | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                                |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|    | Natomas Basin HCP Measure   | Applicability | Inclusion | Rationale   |  |
|----|---|---------------|-----------|---|--|
|    | designated.   |               |           | _   |  |
| 7. | If a live giant garter snake is found during construction activities, immediately notify the USFWS and the project's biological monitor. The biological monitor, or his/her assignee, shall do the following:   | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                       |  |
|    | a. Stop construction in the vicinity of the snake. Monitor the snake and allow the snake to leave on its own. The monitor shall remain in the area for the remainder of the work day to make sure the snake is not harmed or if it leaves the site, does not return. Escape routes for giant garter snake should be determined in advance of construction and snakes should always be allowed to leave on their own. If a giant garter snake does not leave on its own within one working day, further consultation with USFWS is required. | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                       |  |
| 8. | Upon locating dead, injured or sick threatened or endangered wildlife species, the Permittees or their designated agents must notify within one working day the Service's Division of Law Enforcement and Sacramento Fish and Wildlife Office. Written notification to both offices must be made within 3 calendar days and must include the date, time, and location of the finding of a specimen and any other pertinent information.   | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                       |  |
| 9. | Fill or construction debris may be used by giant garter snake as an over-wintering site. Therefore, upon completion of construction activities remove any temporary fill and/or construction debris from the site. If this material is situated near undisturbed giant garter snake habitat and it is to be removed between October 1 and April 30, it shall be inspected by a qualified biologist to assure that giant garter snake are not using it as hibernaculae.  | Applicable    | Included  | A comparable and more stringent measure has been included in the mitigation proposed in the project's DEIR. |  |
| 10 | No plastic, monofilament, jute, or similar erosion control matting that could entangle snakes will be placed on a project site when working within 200 feet of snake aquatic or rice habitat. Possible substitutions include coconut coir matting, tactified hydroseeding compounds, or other material approved by the Wildlife Agencies.   | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                       |  |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|      | Natomas Basin HCP Measure  | Applicability | Inclusion | Rationale  |
|------|--|---------------|-----------|--|
| 11   | I. Fences will be constructed along the shared boundary of urban development and the North Drainage Canal and the East Drainage Canal within Sutter County's Permit Area.  | N/A           |           | This measure is specific to locations outside the project area.                    |
|      | <ul> <li>A minimum of 100 feet will be provided from fence-to-fence<br/>and access to the canals shall be limited by gates.</li> </ul>   | N/A           |           | This measure is specific to locations outside the project area.                    |
|      | b. A snake deterrent will be placed along the fences on the North Drainage Canal and the East Drainage Canal (i.e., fence construction that restricts snake movement or an appropriate vegetative barrier either inside or outside of the boundary fence). The design of the deterrent shall be subject to approval by the Wildlife Agencies.  | N/A           |           | This measure is specific to locations outside the project area.                    |
|      | c. The specific fence/snake barrier design adjacent to a given<br>development will be determined within Sutter County's<br>review of the proposed development and the fence/barrier<br>shall be installed immediately after site grading is completed.   | N/A           |           | This measure is specific to locations outside the project area.                    |
| 12   | 2. At the time of urban development along the North and East Drainage Canals, Sutter County shall consult with the Wildlife Agencies to determine design strategies that would enhance conditions for giant garter snake movement through the North and East Drainage Canals. Possible strategies may include expanded buffer areas and modified canal cross sections if such measures are, in the determination of Sutter and the Water Agencies, found to be feasible. | N/A           |           | This measure is specific to locations outside the project area.                    |
| b. M | leasures to Reduce Take of Swainson's Hawk (V-9)   |               |           |  |
| 1.   | Measures to Reduce Cumulative Impacts to Foraging Habitat (V-9): Sutter County and the City of Sacramento will not will not grant development approvals within the one-mile wide Swainson's Hawk Zone adjacent to the Sacramento River.  | N/A           |           | This measure is specific to locations outside the project area.                    |
| 2.   | Measures to Reduce Nest Disturbance (V-10)   |               |           |  |
|      | 1. Pre-construction surveys shall be completed by the respective developer to determine whether any Swainson's hawk nest trees will be removed on-site, or active Swainson's hawk nest sites occur on or within ½ mile of the  | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed the project's DEIR. |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|    | Natomas Basin HCP Measure   | Applicability   | Inclusion | Rationale   |
|----|---|-----------------|-----------|---|
|    | development site.   |                 |           |   |
|    | 2. If breeding Swainson's hawks (i.e. exhibiting nest building or nesting behavior) are identified, no new disturbances (e.g., heavy equipment operation associated with construction) will occur within ½ mile of an active nest between March 15 and September 15, or until a qualified biologist, with concurrence by CDFG, has determined that young have fledged or that the nest is no longer occupied. Routine disturbances such as agricultural activities, commuter traffic, and routine facility maintenance activities within ½ mile of an active nest are not restricted. | Applicable      | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR. |
|    | 3. Where disturbance of a Swainson's hawk nest cannot be avoided, the nest tree may be destroyed during the nonnesting season. For purposes of this provision the Swainson's hawk nesting season is defined as March 15 to September 15. If a nest tree (any tree that has an active nest in the year the impact is to occur) must be removed, tree removal shall only occur between September 15 and February 1.   | Applicable      | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR. |
|    | 4. If a Swainson's hawk nest tree is to be removed and fledglings are present, the tree may not be removed until September 15 or until the California Department of Fish and Game has determined that the young have fledged and are no longer dependent upon the nest tree.  | Applicable      | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR. |
|    | 5. If construction or other project related activities which may cause nest abandonment or forced fledgling are proposed within the 1/4 mile buffer zone, intensive monitoring (funded by the project sponsor) by a Department of Fish and Game approved raptor biologist will be required. Exact implementation of this measure will be based on specific information at the project site.   | Applicable      | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR. |
| 3. | Measures to Prevent the Loss of Nest Trees  | Section heading |           |   |
|    | <ol> <li>Valley oaks, tree groves, riparian habitat and other large<br/>trees will be preserved wherever possible, particularly near<br/>Fisherman's Lake and elsewhere where large oak groves,</li> </ol>  | N/A             |           | There are currently no large trees at the Greenbriar site.                            |

Table A-1
Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR
Mitigation for the Project

|    |    | Natomas Basin HCP Measure   | Applicability | Inclusion | Rationale   |
|----|----|---|---------------|-----------|---|
|    |    | tree groves and riparian habitat have been identified.  |               |           |   |
|    | 2. | The raptor nesting season shall be avoided when scheduling construction near nests in accordance with applicable guidelines published by the Wildlife Agencies or through consultation with the Wildlife Agencies.  | Applicable    | Included  | A comparable and more detailed measure has been included in the mitigation proposed in the project's DEIR, combined with measure 2.2 above. |
| 4. | Me | easures to Mitigate the Loss of Nest Trees (V-11)   |               |           |   |
|    | 1. | Fifteen trees (five gallon container size) must be planted, maintained and monitored within the habitat reserves for every Swainson's hawk nesting tree anticipated to be impacted by Authorized Development.   | N/A           |           | No Swainson's hawk nesting trees exist on site.   |
|    | 2. | The Land Use Agency Permittee approving a project that impacts an existing Swainson's hawk nest tree shall provide funding sufficient for monitoring survival success of trees for a period of 5 years. For every tree lost during this time period, a replacement tree must be planted immediately upon the detection of failure. Trees planted to replace trees lost shall be monitored for an additional 5-year period to ensure survival until the end of the monitoring period. A 100% success rate shall be achieved. All necessary planting requirements and maintenance (i.e., fertilizing, irrigation) to ensure success shall be provided. Trees must be irrigated for a minimum of the first 5 years after planting, and then gradually weaned off the irrigation in an approximate 2-year period. If larger stock is planted, the number of years of irrigation must be increased accordingly. In addition, 10 years after planting, a survey of the trees shall be completed to assure 100% establishment success. Remediation of any dead trees shall include completion of the survival and establishment process described. | N/A           |           | No Swainson's hawk nesting trees exist on site.   |
|    | 3. | Of the replacement trees planted, a variety of native tree species will be planted to provide trees with differing growth rates, maturation, and life span. This will ensure that nesting habitat will be available quickly (5-10 years in the case of cottonwoods and willows), and in the long term (i.e., valley   | N/A           |           | No Swainson's hawk nesting trees exis on site.  |

Table A-1
Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR
Mitigation for the Project

| Mitigation for the Project  |                      |           |   |  |  |  |
|---|----------------------|-----------|---|--|--|--|
| Natomas Basin HCP Measure   | <b>Applicability</b> | Inclusion | Rationale                                       |  |  |  |
| oaks, black walnut and sycamores). Trees shall be sited on reserves in proximity to hawk foraging areas. Trees planted shall be planted in clumps of 3 trees each. Planting stock shall be a minimum of 5-gallon container stock for oak and walnut species.  |                      |           |   |  |  |  |
| 4. In order to reduce temporal impacts resulting from the loss of mature nest trees, the City of Sacramento will fund mitigation planting within 14 months of permit of the NBHCP and ITP's, to be reimbursed by private developers at the time of approval of their development projects that impact mature nest trees.  | N/A                  |           | No Swainson's hawk nesting trees exist on site. |  |  |  |
| 5. For each additional nesting tree removed by Land Use Agencies' Covered Activities, the Land Use Agency shall fund and provide for the planting of 15 native sapling trees of suitable species with differing growth rates at suitable locations on TNBC preserves. Funding for such plantings shall be provided by the applicable Permittee within 30 days of approving a Covered Activity that will impact a Swainson's hawk nesting tree.  | N/A                  |           | No Swainson's hawk nesting trees exist on site. |  |  |  |
| c. Measures to Reduce Take to Valley Elderberry Longhorn Beetle (VELB) (p. V-13): developers must comply with conservation practices for VELB set forth in the conditions of the "USFWS Compensation Guidelines for the Valley Elderberry Longhorn Beetle," dated 1999. This policy assumes that any elderberry bushes found within the range of the species are likely to provide beetle habitat, and any destruction or loss of such elderberry shrub habitat must be mitigated according to the Guidelines. The principle conditions of the Guidelines are summarized below. | N/A                  |           | No elderberry shrubs exist on site.             |  |  |  |
| 1. Any direct or indirect impacts to VELB habitat will be avoided whenever possible. To the maximum extent practicable, projects will be designed to avoid stands of elderberry bushes and to avoid isolation of the plants from other nearby populations. Preconstruction surveys at the construction impact site will be conducted to assess the appropriate amount of mitigation.  | N/A                  |           | No elderberry shrubs exist on site.             |  |  |  |
| 2. If elderberry plants cannot be avoided, they shall be transplanted   | N/A                  |           | No elderberry shrubs exist on site.             |  |  |  |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|    | Mitigation for the Project |   |                 |           |   |  |  |  |
|----|----------------------------|---|-----------------|-----------|---|--|--|--|
|    |                            | Natomas Basin HCP Measure   | Applicability   | Inclusion | Rationale   |  |  |  |
|    |                            | during the dormant season (November 1 to February 15) to an area protected in perpetuity and approved by the USFWS.   |                 |           |   |  |  |  |
|    | 3.                         | Replacement seedling plants will be provided at a ratio between 2:1 and 5:1 depending on the extent of beetle utilization of the plants moved or lost. A 1,800-square-foot area will be provided for each transplanted elderberry shrub or every five elderberry seedling plants.   | N/A             |           | No elderberry shrubs exist on site.                                   |  |  |  |
|    | 4.                         | Annual monitoring of VELB habitat will be provided in the planted mitigation sites for a ten year period.   | N/A             |           | No elderberry shrubs exist on site.                                   |  |  |  |
|    | 5.                         | Replacement elderberry shrubs will meet a 60% survival rate by the end of the ten year period and the 60% survival rate shall be required for the term of the applicable permit.  | N/A             |           | No elderberry shrubs exist on site.                                   |  |  |  |
| d. | Me                         | easures to Reduce Take on Tricolored Blackbird (V-13)   | Section heading |           |   |  |  |  |
|    | 1.                         | A pre-construction survey is required for potential nesting habitat and presence of nesting tricolored blackbirds.  | Applicable      |           | Suitable tricolored blackbird nesting habitat does not exist on site. |  |  |  |
|    | 2.                         | If surveys determine tricolored blackbirds are present, the following measures shall be implemented in accordance with the Migratory Bird Treaty Act, to avoid disturbance to occupied nesting colonies during the nesting season. A boundary shall be marked by brightly colored construction fencing that establishes a boundary 500 feet from the active colony. No disturbance associated with Authorized Development shall occur within the 500 foot fenced area during the nesting season to July 1, or while birds are present. A qualified biologist, with concurrence of USFWS, must determine young have fledged and nest sites are no longer active before the nest site may be disturbed. | Applicable      |           | Suitable tricolored blackbird nesting habitat does not exist on site. |  |  |  |
| e. | Me                         | easures to Reduce Take on Aleutian Canada Goose (V-14)  |                 |           |   |  |  |  |
|    | 1.                         | A pre-construction survey for Aleutian Canada geese will be required. If geese are present, the developer must consult with USFWS and CDFG to determine appropriate measures to avoid and minimize take of individuals. Such measures shall be appropriate for the use (e.g., foraging, roosting, etc.) and activity of the species, since this species is a seasonal visitor to the Basin.   | Applicable      |           | This subspecies is not expected to occur on site.                     |  |  |  |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

| Miligation for the Project |  |            |          |   |  |  |  |  |  |
|----------------------------|--|------------|----------|---|--|--|--|--|--|
|                            | Natomas Basin HCP Measure Applicability Inclusion Rationale  |            |          |   |  |  |  |  |  |
| f.                         | Measures to Reduce Take on White-faced Ibis (V-14)   |            |          |   |  |  |  |  |  |
|                            | <ol> <li>Prior to approval of an Urban Development Permit, a pre-<br/>construction survey will be required.</li> </ol>   | N/A        |          | Suitable white-faced ibis nesting habitat does not exist on site.   |  |  |  |  |  |
|                            | 2. If surveys determine the presence of active nest sites of White-faced ibis, disturbance by Authorized Development within 1/4 mile of nests will be avoided within the nesting season of May 15 through August 31 or until a qualified biologist, with concurrence of Wildlife Agencies, has determined that young have fledged or that the nest is no longer occupied.  | N/A        |          | Suitable white-faced ibis nesting habitat does not exist on site.   |  |  |  |  |  |
| g.                         | Measures to Reduce Take on Loggerhead Shrike (V-14)  |            |          |   |  |  |  |  |  |
|                            | 1. Prior to approval of an Urban Development Permit, a preconstruction survey will be required.  | Applicable | Included | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                       |  |  |  |  |  |
|                            | 2. If surveys identify an active loggerhead shrike nest that will be impacted by Authorized Development, the developer shall install brightly colored construction fencing that establishes a boundary 100 feet from the active nest. No disturbance associated with Authorized Development shall occur within the 100 foot fenced area during the nesting season of March 1 through July 31. A qualified biologist, with concurrence of USFWS must determine young have fledged or that the nest is no longer occupied prior to disturbance of the nest site.   | Applicable | Included | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                       |  |  |  |  |  |
| h.                         | Measures to Reduce Take of Burrowing Owl (V-15)  |            |          |   |  |  |  |  |  |
|                            | 1. Prior to the initiation of grading or earth disturbing activities, the applicant/developer shall hire a CDFG approved qualified biologist to perform a pre-construction survey of the site to determine if any burrowing owls are using the site for foraging or nesting. The preconstruction survey shall be submitted to the Land Use Agency with jurisdiction over the site prior to the developer's commencement of construction activities and a mitigation program shall be developed and agreed to by the Land Use Agency and developer prior to initiation of any physical disturbance on the site. | Applicable | Included | A comparable and more stringent measure has been included in the mitigation proposed in the project's DEIR. |  |  |  |  |  |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

| whitigation for the Project |   |               |           |   |  |  |  |  |
|-----------------------------|---|---------------|-----------|---|--|--|--|--|
|                             | Natomas Basin HCP Measure   | Applicability | Inclusion | Rationale   |  |  |  |  |
| 2.                          | Occupied burrows shall not be disturbed during nesting season (February 1 through August 31) unless a qualified biologist approved by the CDFG verifies through noninvasive measures that either: 1) the birds have not begun egg-laying and incubation; or 2) that juveniles from the occupied burrows are foraging independently and are capable of independent survival.   | Applicable    | Included  | A comparable and more stringent measure has been included in the mitigation proposed in the project's DEIR. |  |  |  |  |
| 3.                          | If nest sites are found, the USFWS and CDFG shall be contacted regarding suitable mitigation measures, which may include a 300 foot buffer from the nest site during the breeding season (February 1 - August 31), or a relocation effort for the burrowing owls if the birds have not begun egg-laying and incubation or the juveniles from the occupied burrows are foraging independently and are capable of independent survival. If on-site avoidance is required, the location of the buffer zone will be determined by a qualified biologist. The developer shall mark the limit of the buffer zone with yellow caution tape, stakes, or temporary fencing. The buffer will be maintained throughout the construction period.  | Applicable    | Included  | A comparable and more stringent measure has been included in the mitigation proposed in the project's DEIR. |  |  |  |  |
| 4.                          | If relocation of the owls is approved for the site by USFWS and CDFG, the developer shall hire a qualified biologist to prepare a plan for relocating the owls to a suitable site. The relocation plan must include: (a) the location of the nest and owls proposed for relocation; (b) the location of the proposed relocation site; (c) the number of owls involved and the time of year when the relocation is proposed to take place; (d) the name and credentials of the biologist who will be retained to supervise the relocation; (e) the proposed method of capture and transport for the owls to the new site; (f) a description of the site preparations at the relocation site (e.g., enhancement of existing burrows, creation of artificial burrows, one-time or long-term vegetation control, etc.); and (g) a description of efforts and funding support proposed to monitor the relocation. Relocation options may include passive relocation to another area of the site not subject to disturbance through one way doors on burrow openings, or construction of artificial burrows in accordance with the CDFG's October 17, 1995, Staff Report on Burrowing Owls Mitigation (see Appendix | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                       |  |  |  |  |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

| Mitigation for the Project |   |  |            |          |   |  |  |  |
|----------------------------|---|--|------------|----------|---|--|--|--|
|                            | Natomas Basin HCP Measure Applicability Inclusion Rationale |  |            |          |   |  |  |  |
|                            |   | D).  |            |          |   |  |  |  |
|                            | 5.  | Where on-site avoidance is not possible, disturbance and/or destruction of burrows shall be offset through development of suitable habitat on TNBC upland reserves. Such habitat shall include creation of new burrows with adequate foraging area (a minimum of 6.5 acres) or 300 feet radii around the newly created burrows. Additional habitat design and mitigation measures are described in the CDFG's October 17, 1995, Staff Report on Burrowing Owl Mitigation (see Appendix D).   | Applicable | Included | A comparable and more stringent measure has been included in the mitigation proposed in the project's DEIR. |  |  |  |
| i.                         | Me  | easures to Reduce Take on Bank Swallow (V-16)  |            |          |   |  |  |  |
|                            | 1.  | Disturbance to bank swallows nesting colonies will be avoided within the nesting season of May 1 through August 31 (or until a qualified biologist, with concurrence of USFWS and CDFG, has determined that young have fledged or that the nest is no longer occupied) during all Authorized Development activities conducted in the Permit Areas.   | N/A        |          | Suitable bank swallow nesting habitat does not exist on site.   |  |  |  |
|                            | 2.  | If surveys identify an active bank swallow nesting colony that will be impacted by Authorized Development, the developer shall install brightly colored construction fencing that establishes a boundary 250 feet from the active nesting colony. No disturbance associated with Authorized Development shall occur within the 250 foot fenced area during the nesting season of May 1 through August 31. Additionally, disturbance within ½ mile upstream or downstream of the colony will be avoided if the colony is located upon a natural waterway. | N/A        |          | Suitable bank swallow nesting habitat does not exist on site.   |  |  |  |
| j.                         | Me  | easures to Reduce Take on Northwestern Pond Turtle (V-16)  |            |          |   |  |  |  |
|                            | 1.  | Take of the northwestern pond turtle as a result of habitat destruction during construction activities, including the removal of irrigation ditches and drains, and during ditch and drain maintenance, will be minimized by the dewatering requirement described above for giant garter snake (see Section 5.a.(3)).  | Applicable |          | The NBHCP measure has been included in the mitigation proposed in the project's DEIR.                       |  |  |  |
| k.                         | Me  | easures to Reduce Take on California Tiger Salamander (V-16)   |            |          |   |  |  |  |
|                            | 1.  | Prior to approval of an Urban Development Permit, the involved   | N/A        |          | Suitable California tiger salamander  |  |  |  |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|    |   | witigation for the Project |           |   |  |  |  |  |  |
|----|---|----------------------------|-----------|---|--|--|--|--|--|
|    | Natomas Basin HCP Measure   | Applicability              | Inclusion | Rationale   |  |  |  |  |  |
|    | Land Use Agency shall require a pre-construction survey. If a future survey determines the presence of California tiger salamander, the Land Use Agency shall require the developer to consult with USFWS and CDFG to determine appropriate measures to avoid and minimize take of individuals.   |                            |           | habitat does not exist on site.   |  |  |  |  |  |
| 1. | Measures to Reduce Take on Western Spadefoot Toad (V-16)  |                            |           |   |  |  |  |  |  |
|    | 1. Prior to approval of an Urban Development Permit, the involved Land Use Agency shall require a pre-construction survey. If such survey determines western spadefoot toad are present, the Land Use Agency shall require the developer to consult with CDFG and USFWS to determine appropriate measures to avoid and minimize take of individuals.  | N/A                        |           | Suitable western spadefoot toad habitat does not exist on site.                       |  |  |  |  |  |
| m. | Measures to Reduce Take of Vernal Pool Fairy Shrimp, Vernal Pool Tadpole Shrimp, and Midvalley Fairy Shrimp (V-17)  |                            |           |   |  |  |  |  |  |
|    | 1. Prior to approval of an Urban Development Permit, the involved Land Use Agency shall require a pre-construction survey. If such survey determines vernal pool fairy shrimp, vernal pool tadpole shrimp, and midvalley fairy shrimp are present, the Land Use Agency shall require the developer to consult with USFWS to determine appropriate measures to avoid and minimize take of individuals. Procedures for reviewing projects that could affect vernal pools and vernal pool species are discussed under Section V.A.4 above. | N/A                        |           | No vernal pool habitat exists on site.  |  |  |  |  |  |
| n. | Measures to Reduce Take of Delta Tule Pea (V-17)  |                            |           |   |  |  |  |  |  |
|    | 1. If Delta tule pea plants are identified through a pre-construction survey, the involved Land Use Agency shall provide notice to USFWS, CDFG and the California Native Plant Society. Under such circumstances, the development proponent shall allow the transplantation of plants prior to site disturbance.  | Applicable                 | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR. |  |  |  |  |  |
| 0. | Measures to Reduce Take on Sanford's Arrowhead (V-17)   |                            |           |   |  |  |  |  |  |

Table A-1 Inclusion of NBHCP Measures to Reduce Construction-related Effects and Human-Wildlife Conflicts in the Greenbriar Project or the DEIR Mitigation for the Project

|                                   | Natomas Basin HCP Measure  | Applicability | Inclusion | Rationale   |
|-----------------------------------|--|---------------|-----------|---|
| c<br>n<br>S                       | f Sanford's arrowhead plants are identified through a pre-<br>construction survey, the involved Land Use Agency shall provide<br>notice to USFWS, CDFG and the California Native Plant<br>Society. Under such circumstances, the development proponent<br>hall allow the transplantation of plants prior to site disturbance.  | Applicable    | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR. |
|                                   | ures to Reduce Take on Boggs Lake Hedge-Hyssop, Sacramento tt Grass, Slender Orcutt Grass, Colusa Grass, and Legenere (V-  |               |           |   |
| L<br>si<br>g<br>tl<br>U<br>n<br>p | Prior to approval of an Urban Development Permit, the involved Land Use Agency shall require a pre-construction survey. If such urvey determines Boggs Lake hedge-hyssop, Sacramento orcutt grass, Slender orcutt grass, Colusa grass, or legenere are present, the Land Use Agency shall require the developer to consult with USFWS to determine appropriate measures to avoid and minimize loss of individuals. If Authorized Development is proposed for areas containing vernal pools, the applicant will be equired to complete additional review, permitting and mitigation is described under Section V.A.4. | N/A           | Included  | The NBHCP measure has been included in the mitigation proposed in the project's DEIR. |



Change in Natomas Basin Land Cover in 2001–2004

# APPENDIX B CHANGE IN NATOMAS BASIN LAND COVER IN 2001–2004

#### INTRODUCTION

EDAW analyzed 2001 and 2004 land cover of the Natomas Basin to describe changing conditions in the Natomas Basin and their bearing on analyses of the Natomas Basin Habitat Conservation Plan (NBHCP) and on analyses of the Greenbriar project.

The NBHCP used 2001 land cover as a primary data source in analyses of the anticipated future condition. For example, change in habitat availability for covered species was analyzed by evaluating the change in land cover types providing suitable habitat. This was done by subtracting 2001 acreages in areas permitted for development from total 2001 acreages.

In 2004, land cover in the Natomas Basin was mapped by Jones & Stokes for TNBC (Jones & Stokes 2005). This land cover data provides useful information about more recent conditions.

A comparison of 2001 and 2004 land cover could provide useful information regarding on-going changes. Unfortunately, the mapping of 2001 land cover by CH2M Hill (CH2M Hill 2002) and the mapping of 2004 land cover by Jones & Stokes (Jones & Stokes 2005) used different land cover classifications and different mapping methods. Consequently, changes in land use and habitat availability cannot be interpreted by directly comparing them. For example, more intensively developed land was mapped as airport, highway, other, rural residential, and other in 2001; but as developed in 2004. Also, many areas mapped as urban in 2001 were mapped as natural or urban vegetation in 2004, apparently because the 2004 mapping was done with much more conservative boundaries around structures and pavement.

Therefore, EDAW processed each data set to increase their compatibility, and then evaluated changes in land cover during 2001–2004 in: 1) areas permitted for development, 2) The Natomas Basin Conservancy (TNBC) reserve system, and 3) in the remainder of the Natomas Basin.

#### **METHODS**

Data layers for the 2001 and 2004 land cover mapping were provided by CH2M Hill and Jones & Stokes, respectively. Analyses of these data layers were performed using ArcInfo 9.1.

Several steps were taken to make these two maps more comparable and to facilitate an informative comparison of land cover change from 2001 to 2004. First, we developed a cross-walk between the 2001 and 2004 land cover classifications and a derived classification. Table B-1 presents this crosswalk and the derived classification. Second, land mapped in developed land cover types in 2001 was considered to still be developed. Thus, the 2001 land cover classification of these areas was retained for 2004. Third, land cover acreages were adjusted to incorporate habitat along canals and drains as a distinct type (i.e., canal in Table B-1). This was done by transferring acreage from each land cover category to a canal category based on the acreages intersecting buffers placed around canals in a GIS analysis. (Buffer widths were based on the widths used in Table 4-3 of CH2M Hill [2002].) Canals passing through developed land cover types, however, were included in the developed category.

#### **RESULTS AND DISCUSSION**

Table B-2 provides a comparison of 2001 and 2004 land cover overall, and within development areas, TNBC reserves, and the rest of the Natomas Basin. (Development areas include the Sutter County, City of Sacramento, and MAP permit areas.) This subdivision of the Natomas Basin allows changes due to management of TNBC

reserves and changing land use in areas authorized for development to be distinguished from changes in the remainder of the Natomas Basin.

Changes in land cover from 2001 to 2004 were most substantial on TNBC reserves. In areas incorporated into the TNBC reserve system, the creation of managed marshes increased the acreage of ponds, marsh, and seasonally wet areas by over 500 acres, while the acreage of rice decreased by less than 100 acres. This indicates that most managed marsh has been created from land mapped as non-rice cropland or idle in 2001. If this pattern continues more total habitat for species using marshes and wetlands will exist in the future condition than estimated because more conversion of rice to marsh was anticipated (CH2M Hill 2002). Grassland and pasture has also increased on reserve lands, while non-flooded cropland decreased by approximately 900 acres during 2001–2004 within the current TNBC reserve system. Interestingly, there has been no increase in alfalfa on reserve lands. Overall, the proportions of marsh, rice and upland land cover types are consistent with those specified by the NBHCP.

Within areas permitted for development by the NBHCP, developed land cover has increased and so has the acreage of grassland, while disturbed areas and non-flooded crops have decreased in extent. Interestingly, the acreage of rice within developed areas did not decrease during 2001–2004. This rice is primarily in the Sutter County's permit area, and to a lesser extent in the Metro Air Park. Almost no rice was present in the City of Sacramento's permit area in either 2001 or 2004. Thus, as of 2004, there is no evidence that rice has been fallowed in anticipation of development. Non-flooded cropland has been fallowed or abandoned, however. Non-flooded cropland decreased in acreage, and the corresponding increase in grassland acreage is likely due to the increase in idle cropland.

Outside of TNBC reserves and areas authorized for development, the primary change in land cover has been a 42% decrease in the acreage of non-flooded cropland, and a concurrent increase in the acreage of grassland and rice. Because both grassland and rice have increased, there has not been a substantial change in the acreage of habitat for either upland-associated or wetland-associated species covered by the NBHCP. This change in the proportions of the different agricultural land cover types outside of reserves and areas undergoing development does illustrate the dynamic nature of agricultural landscapes over short periods of time, in this case just three years. Recent concerns over water prices and the viability of rice cultivation in the Natomas Basin also indicate this dynamism.

# Table B-1 Crosswalk between CH2M Hill and Jones & Stokes Land Cover Classifications and a Combined Classification

| Combined Classification               | CH2M Hill  | Jones & Stokes   |  |  |  |
|---------------------------------------|--|--|--|--|--|
| Alfalfa                               | Alfalfa  | Alfalfa  |  |  |  |
| Canal                                 | Canal, small portions of other land cover<br>types that canals passed through (except<br>for developed land cover) | Open Water [in part], Riparian Scrub [in part], Grassland [in part], Rice [in part], Row Crops [in part] and small amounts of other land cover types |  |  |  |
| Developed                             | Airport, Highway or Major Road, Other,<br>Urban  | Developed [in part], and small portions of other land cover types  |  |  |  |
| Grassland                             | Grassland  | Grassland [in part]  |  |  |  |
| Orchard                               | Orchard  | Orchard  |  |  |  |
| Pasture                               | Pasture  | Irrigated Grassland, Grass Hay   |  |  |  |
| Ponds, Marsh and Seasonally wet areas | Ponds and Seasonally Wet Areas   | Fresh Emergent Marsh, Managed Marsh, Open Water [in part], Seasonal Wetland  |  |  |  |
| Rice                                  | Rice   | Rice [in part]   |  |  |  |
| Riparian                              | Riparian   | Riparian Scrub [in part], Riparian Woodland  |  |  |  |
| Non-rice Crops                        | Non-rice Crops, idle   | Row Crops [in part]  |  |  |  |
| Ruderal                               | Ruderal  | Disturbed / Bare   |  |  |  |
| Rural Residential                     | Rural Residential  | Developed [in part], and small portions of other land cover types  |  |  |  |
| Tree Grove                            | Tree Grove   | Non-riparian Woodland  |  |  |  |
| Valley Oak Woodland                   | Oak Grove  | Valley Oak Woodland  |  |  |  |

Note: CH2M Hill classification used in mapping 2001 land cover as described in CH2M Hill 2002; Jones & Stokes classification used in mapping 2004 land cover as described in Jones & Stokes 2005.

| Table B-2<br>Land Cover Change in the Natomas Basin 2001–2004 |                                |       |                            |       |               |        |        |        |
|---|--------------------------------|-------|----------------------------|-------|---------------|--------|--------|--------|
| Land Cover Type   | Development Areas <sup>1</sup> |       | TNBC Reserves <sup>2</sup> |       | Rest of Basin |        | Total  |        |
| Land Gover Type   | 2001                           | 2004  | 2001                       | 2004  | 2001          | 2004   | 2001   | 2004   |
| Alfalfa   | 0                              | 0     | 64                         | 67    | 305           | 529    | 369    | 596    |
| Canal   | 508                            | 436   | 113                        | 111   | 830           | 833    | 1,451  | 1,380  |
| Developed   | 8,353                          | 9,766 | 26                         | 42    | 2,931         | 3,173  | 11,311 | 12,980 |
| Grassland   | 564                            | 2,328 | 13                         | 349   | 225           | 2,179  | 802    | 4,856  |
| Orchard   | 0                              | 0     | 0                          | 0     | 165           | 145    | 165    | 145    |
| Pasture   | 165                            | 255   | 80                         | 164   | 423           | 315    | 668    | 734    |
| Ponds, Marsh and Seasonally Wet Areas                         | 21                             | 60    | 0                          | 514   | 73            | 106    | 94     | 680    |
| Rice  | 7,562                          | 8,363 | 2,499                      | 2,414 | 11,360        | 13,308 | 21,421 | 24,085 |
| Riparian  | 23                             | 24    | 4                          | 12    | 87            | 86     | 114    | 122    |
| Non-flooded Cropland  | 3,214                          | 939   | 1,096                      | 291   | 9,374         | 5,427  | 13,683 | 6,657  |
| Ruderal   | 2,825                          | 1,111 | 66                         | 0     | 378           | 28     | 3,269  | 1,139  |
| Tree Grove  | 56                             | 8     | 7                          | 1     | 37            | 48     | 100    | 56     |
| Valley Oak Woodland   | 13                             | 14    | 0                          | 3     | 77            | 89     | 90     | 106    |

23,303

23,303

3,968

3,968

26,266

26,266

53,537

53,536

Notes: All values are in acres.

Total

<sup>1 –</sup> Areas authorized for development by the NBHCP.

<sup>2 –</sup> Areas in TNBC reserve system in 2005.